RFT RESULTS
WELL: 30/9-6

| Run/ <br> Test no. | Depth <br> (m RKB) | IHP <br> (bar) | FP <br> (bar) | FHP <br> (bar) | Permeability/ <br> Remarks |
| :---: | :---: | :---: | :---: | :---: | :--- |
| 2A/1 | 2591.80 | 310.816 | -9999.000 | -9999.000 | Seal failure |
| 2A/2 | 2592.50 | 310.885 | 281.435 | 310.885 | V good perm |
| $2 A / 3$ | 2595.50 | 311.229 | -9999.000 | 311.229 | Tight |
| 2A/4 | 2611.50 | 313.160 | 282.424 | 313.181 | Fair-poor perm |
| $2 A / 5$ | 2615.50 | 313.608 | -9999.000 | 313.608 | Seal failure |
| $2 A / 6$ | 2616.00 | 313.642 | 283.649 | 313.677 | V good perm |
| $2 A / 7$ | 2619.00 | 313.987 | 283.832 | 313.987 | V good perm |
| $2 A / 9$ | 2640.00 | 316.538 | 285.963 | 316.538 | Good perm |
| $2 A / 10$ | 2643.00 | 316.780 | 286.146 | 316.849 | V good perm |
| $2 A / 11$ | 2662.50 | 319.193 | 287.133 | 319.193 | V good perm |
| $2 A / 12$ | 2678.00 | 321.041 | 288.548 | 321.020 | V good perm |
| $2 A / 13$ | 2687.00 | 321.944 | 289.359 | 321.951 | Excellent perm |
| $2 A / 14$ | 2694.00 | 322.813 | 290.058 | 322.806 | V gd-exc.perm |
| $2 A / 15$ | 2986.00 | 356.776 | 346.173 | 356.824 | Fair-good |
| $2 A / 16$ | 2996.00 | 357.927 | 347.122 | 357.962 | Fair perm |
| $2 A / 17$ | 3002.50 | 358.734 | 347.954 | 358.803 | V gd-exc.perm |

All pressures from HP-gauge, units bar.
Value -9999.000 indicates missing data.

## $\xlongequal[(!)]{(I)}$ HYDRO

|  | RFT RESULTS |  |  | WELL: 30/9-6 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Run/ Test no. | $\begin{aligned} & \text { Depth } \\ & \text { (m RKB) } \end{aligned}$ | $\begin{aligned} & \text { IHP } \\ & \text { (bar) } \end{aligned}$ | $\begin{aligned} & \text { FP } \\ & \text { (bar) } \end{aligned}$ | $\begin{aligned} & \text { FHP } \\ & \text { (bar) } \end{aligned}$ | Permeability/ Remarks |
| 2B/1 | 2592.50 | 311.009 | 282.471 | 310.967 | $V$ good perm |
| 2B/2 | 2611.50 | 313.256 | 283.395 | 313.208 | Good perm |
| 2B/3 | 2616.00 | 313.691 | 283.657 | 313.691 | Fair-good perm |
| 2B/4 | 2619.00 | 314.091 | 283.871 | 314.049 | $V$ good-exc. perm |
| 2B/5 | 2640.00 | 316.552 | -9999.000 | -9999.000 | Tight |
| 2B/6 | 2640.50 | 316.593 | 285.981 | 316.566 | $V$ good perm |
| 2B/7 | 2643.00 | 316.849 | 286.167 | 316.849 | $\checkmark$ good perm |

All pressures from HP-gauge, units bar.
Value -9999.000 indicates missing data.
! ! IINHYRO


DST RESULTS
WELL: 30/9-6

DST \# 2
Main Flow period
Interval:
2591.5-2596.5 mRKB (2590.9-2595.9 mTVD)

Choke Size, mm(inch)
7.94 (20/64")

Oil flowrate $\mathrm{Sm}^{3} / \mathrm{D},(B / D)$ 166 (1044)
Gas flowrate $\mathrm{Sm}^{3} / \mathrm{D}$, (Scf/D) 16980 (599649)
Gas oil ratio $\mathrm{Sm}^{3} / \mathrm{Sm}^{3}$ 102.3

Oil density $\mathrm{g} / \mathrm{cc}\left({ }^{\circ} \mathrm{API}\right)$ 0.856 (33.8)

Gas density (air=1) 0.698
WHP, bar (psia)
91.4 (1326)

Flowing BH Pressure,bar (psia) 254.64 (3693)

Initial BH Pressure,bar (psia) 276.7 (4013)
WHT, ${ }^{\circ} \mathrm{C}\left({ }^{\circ} \mathrm{F}\right)$
18.1 (65)
$\mathrm{BHT},{ }^{\circ} \mathrm{C}$ ( $\left.{ }^{\circ} \mathrm{F}\right) \quad 100 \quad$ (212)
$\mathrm{CO}_{2} \%$ : 1.0
$\mathrm{H}_{2} \mathrm{~S}$, ppm
0
B S \& W (\%) 0

Separator $P$ (bar) 35
Separator $T\left({ }^{\circ} \mathrm{C}\right) \quad 55$
Flowing time:
22 hours 16 minutes
Build up time: 20 hours 45 minutes

### 6.5 Mud report

36" hole

Drilled to $213,5 \mathrm{~m}$ with high viscous pills pumped on each connection. At $T D$, a $10 \mathrm{~m}^{3} \mathrm{high}$ viscous pill was circulated around prior to make a wiper trip. Back on bottom another 10 $m^{3}$ pill was pumped around before the hole was displaced with $65 \mathrm{~m}^{3}$ high viscous mud. The $30^{\prime \prime}$ casing was then run and cemented.

17 1/2" hole

The cement, shoe $+5,5 \mathrm{~m}$ new formation was drilled with a 17 1/2" bit + 26" holeopener. Tripping in with a new bit, drilling continued to 597 m with high viscous pills on every second connection. At this stage the hole was displaced with $60 \mathrm{~m}^{3}$ of 1.20 rd mud. A wiper trip to the $30^{\prime \prime}$ shoe proved a slick hole. Drilling continued to $T D$ of the section at 970 m with high viscous pills on every connection. The hole was displaced with $120 \mathrm{~m}^{3} 1,20$ rd mud before making a wiper trip to the shoe. During this trip, no hole problems were experienced. The hole was then displaced with $150 \mathrm{~m}^{3}$ of 1,20 rd before pulling out. Casing was then run and cemented.

## 12 1/4" hole

Cement and shoe was drilled using seawater. While drilling new formation, the hole was displaced to $1,34 \mathrm{rd} \mathrm{KCl} / \mathrm{polymer}$ mud. Drilling continued to 1345 m where the bit was pulled. Maximum overpull of 131 kN was recorded at 1223 m .3 m fill was recorded when running back in. Drilling continued then to 1512 m where the bit was pulled.

No hole problems were encountered during the trip out. When running back in, the hole was washed and reamed from 1480 m to 1512 m . After having drilled through extremely hard silicious sandstone, the bit was pulled at $1516,5 \mathrm{~m}$. No hole problems during the trip. The next bit drilled to 1902 m and no hole problems was observed during the trip. Drilling continued to 2181 m where the ROP dropped. The bit proved to be balled up with claystone. At this stage all the processing equipment were running at their optimum to control the increasing build up of fine solids. Tight spots at $2027 \mathrm{~m}-2064 \mathrm{~m}$ and $2146 \mathrm{~m}-2181 \mathrm{~m}$ were washed and reamed through when running back in. The new bit drilled to 2400 m with occasional bit balling which was cured with a $25 \mathrm{~kg} / \mathrm{m}^{3}$ Wallnut pill. The round trip indicated no hole problems and the next two bits drilled to $T D$ at 2587 m . A wiper trip and trip out of hole at TD indicated no hole problems and the hole was logged and cased off.

## 8 1/2" hole

The first bit drilling the shoe, was pulled after only one metre of new hole to 2588 m . The next bit hit sand at 2593,5 m and was pulled for coring. The mud weight in this section was cut back from 1,40 to 1,21 using unweighted premix to reduce the gradual increase of solids being built up in the previous section. Coring was performed from 2604 m to 2686 m in four runs. Minor problems on trips were experienced. The hole was reamed through the coring section when running in with the next bit and then drilled to 2721 m . POOH caused no problems. Another two bit runs were necessary to reach $T D$ which was 3034 m . No problems were seen when $P O O H$. The hole was then logged and $7^{\prime \prime}$ liner was successfully run and cemented. The well was then plugged back and tested.





| $\begin{aligned} & (() \\ & \text { (000) } \end{aligned}$ | $\begin{gathered} \text { Mud consumption } \\ \text { System : Boredata Sandnes } \end{gathered}$ | Date $14 / 10-1987$ |
| :---: | :---: | :---: |
| Norsk <br> Hydro | System : Boredata Sandnes <br> Well: 30/9-6 <br> Mud company: Dresser Magcobar | 13 |

Hole size: 36

| BENTONITE | (Mt) | 18 |
| :--- | :--- | ---: |
| CAUSTIC SODA | (Kg) | 110 |
| SODA ASH | (Kg) | 100 |

Hole size: 17.5

|  |  |  |
| :--- | ---: | ---: |
| BARITE | (Mt) | 55 |
| BENTONITE | (Mt) | 25 |
| CAUSTIC SODA | (Kg) | 410 |
| LIME | (Kg) | 504 |
| SODA ASH | (Kg) | 80 |

Hole size: 12.25

| BARITE |  | (Mt) | 95 |
| :---: | :---: | :---: | :---: |
| CAUSTIC SODA |  | ( Kg ) | 2710 |
| POTASSIUM CL. (KCl) |  | (Kg) | 38984 |
| POTASSIUM CL. (KCl) | Brine | (m3) | 212 |
| SODA ASH |  | ( Kg ) | 720 |
| SODIUM BICARBONATE |  | ( Kg ) | 860 |
| PAC POLYMER REG |  | ( Kg ) | 3613 |
| PAC POLYMER SUPER |  | ( Kg ) | 3643 |
| XANTAN POLYMER |  | ( Kg ) | 538 |

Hole size: 8.5
BARITE
CAUSTIC SODA
GYPSUM

| $(\mathrm{Mt})$ | 24 |
| ---: | ---: |
| $(\mathrm{Kg})$ | 40 |
| $(\mathrm{Kg})$ | 1605 |
| $(\mathrm{Kg})$ | 222 |
| $(\mathrm{Kg})$ | 3152 |
| $(\mathrm{~m} 3)$ | 65 |
| $(\mathrm{Kg})$ | 2476 |
| $(\mathrm{Kg})$ | 1975 |
| $(\mathrm{Kg})$ | 932 |
| $(\mathrm{Kg})$ | 278 |

Hole size: 1
BARITE
GYPSUM
SODIUM BICARBONATE
(Mt) 3
SODIUM BICARBONATE
$(\mathrm{Kg})$ 409

PAC POLYMER SUPER
( Kg )452

LIME
$(\mathrm{Kg})$
$(\mathrm{Kg})$222

POTASSIUM CL. (KCl)

Brine
(Kg)
65
SODIUM BICARBONATE
(Kg) 1975
PAC POLYMER SUPER
XANTAN POLYMER
(Kg)
278
BARITE
GYPSUM
SODIUM BICARBONATE
PAC POLYMER SUPER
(Kg) 358

Hole size: 2

| POTASSIUM CL. (KCl) | $(\mathrm{Kg})$ | 3132 |
| :--- | :--- | ---: |
| POTASSIUM CL. (KCl) | (Krine | $(\mathrm{m} 3)$ |
| PAC POLYMER SUPER | $(\mathrm{Kg})$ | 558 |

