

# TABLES

## a) CASING RECORD

Table 1 *Esso well 9/8-1*

Diameter	Depth below KB	
	m	ft
36"	138	451
20"	360	1180
13 3/8"	1265	4148

## b) DEVIATION

Table 1 *Esso well 9/8-1*

Depth below KB		Degrees
m	ft	
1265	4150	0.3
1309	4295	0.1
1330	4363	0.3
1429	4688	0.8
1507	4944	1.3
1539	5049	1.3
1599	5246	1.9
1726	5663	3.3
1770	5807	3.1
1909	6263	4.0
2113	6932	2.2

Table 2a *Esso well 9/8-1*

## MUD PROGRAM

Depth below KB		Mud base	Additives	Problems	Remarks
m	ft				
Sea fl.—410	Sea fl. - 1350	Sea water	Salt gel, bentonite	Bridging, tight hole	Returns to sea fl.
360 —1280	1180—4198		XP-20, Spersene, Salinex, bentonite, barite, diesel oil		
1280	4198		Barite	2000 units of gas detected	Raised mud wt. to 10.4 ppg.
1265—2176	4148—7138		XP-20, Spersene, Salinex, diesel oil		Chloride content reduced to 11000 ppm.
1554	5100				

Table 2b *Esso well 9/8-1*

Depth below KB		Weight, ppg	Funnel visc., sec	Filt. loss, cm <sup>3</sup>	% oil
m	ft				
360	1180	9.8	54	4.0	4
1128	3700	9.8	54	4.0	4
1280	4198	10.4	42	4.3	1
1295	4250	10.5	38	3.6	2
1369	4490	10.6	36	3.6	8
1439	4720	10.5	46	3.7	6
1524	5000	10.6	46	3.8	7
1686	5530	10.6	46	2.5	10
1734	5690	10.6	48	2.4	10
1895	6218	10.5	48	2.4	10
1974	6478	10.5	43	2.0	10
2024	6639	10.5	43	2.8	10
2085	6842	10.5	41	2.2	8
2176	6990	10.6	42	3.0	9
2131	7138	10.5	48	3.3	6

H. Testing: The Schlumberger wireline formation tester (FIT)

was used with the following results:

	Test No. 1 6762'	Test No. 2 6764'	Test No. 3 6535'	Test No. 4 6320'
<u>Pressure Data -</u>				
Initial shut in	-	-	-	-
Shut in time	-	-	-	-
Sampling	-	-	0 psi.	1000 psi.
Sampling time	-	-	15 min.	20 min.
Final shut in	-	-	0	3590 psi.
Shut in time	-	-	15 min.	15 min.
Hydrostatic	-	-	3680 psi.	3660 psi.
Surface chamber	-	-	0 psi.	0 psi.
<u>Recovery Data</u>				
Gas (Total	-	-	-	-
Condensate	-	-	-	-
Cil	-	-	-	-
Water	-	-	-	14,550 cc
Mud	15,400 cc	12,200 cc	200 cc	200 cc
Sand	Traces	Traces	-	Traces
<u>Remarks</u>	Immediate seal failure	Immediate seal failure	Tight formation	Resistivity of water 0.12 at 59° F Rmf was 0.24 at 64° F.

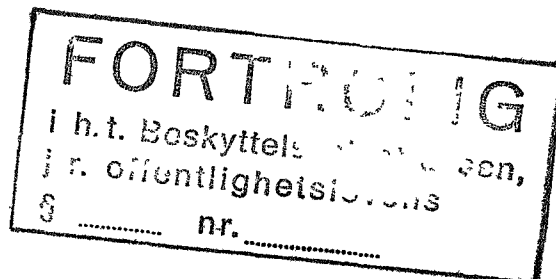
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KEROGEN AND SOURCE ANALYSES OF CANNED CUTTINGS  
FROM THE ESSO 9/8-1 AND ESSO 16/9-1 WELLS, NORWAY

by

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SUMMARY

Canned cuttings samples from 1400-7100 feet in the Esso 9/8-1 well and 1350-11,985 feet in the Esso 16/9-1 well were analyzed for their hydrocarbon gases. Chips of uniform lithologies were picked from selected cuttings samples and analyzed for total organic matter, gasoline (C<sub>4</sub>-C<sub>7</sub>) yields, and visual kerogen characteristics.

In the 9/8-1 well the intervals 1350-2400 feet and 3000-4000 feet are interpreted to be immature oil source intervals, based on data from the combined visual kerogen and chemical analyses. Under present subsurface conditions these zones might be associated with accumulations of methane gas, and possibly with heavy asphaltic oils in adjacent reservoir beds. The zone from 6250 to 6450 feet is quite rich in organic matter and is tentatively rated as an immature oil source. The cyclohexane/methylcyclopentane ratios suggest it is more likely to be a gas source, but the other criteria suggest it is an oil source interval. Possibly this contradiction is a function of the early stage of maturation of the section.

In the 16/9-1 well the interval 1350-4250 feet, particularly below 3750 feet, is interpreted to be an immature oil prone section. The interval 7650-8250 feet is rich in organic matter and is rated as a source section. Low cyclohexane/methylcyclopentane ratios suggest it is a gas source, but other criteria suggest an oil source interval. Again, this might be attributable to the maturation state of the organic matter, and this section is therefore interpreted to be an immature oil source interval. A group of samples from the 11,150-11,350 feet section appear to be cavings, for they are nearly identical in all respects to shales from about 7650-8250 feet.

Tentative zonations of organic facies are suggested from the types of kerogen materials and from the gasoline data. However, the exploration significance of these zonations should be determined by someone familiar with the geology of the area.

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Kerogen alteration data indicate that high subsurface temperatures have not been a problem in the two sampled sections. Alterations are rated at a maximum of 2+ on the 1-5 alteration scale.

### INTRODUCTION

Canned cuttings samples from the intervals 1400-7100 feet in the Esso 9/8-1 well and 1350-11,985 feet in the Esso 16/9-1 well were analyzed for their yields of hydrocarbon gases. Chips of uniform lithologies were hand picked from selected samples and analyzed further for characteristics of visual kerogen, total organic matter concentrations and light gasoline (C<sub>4</sub>-C<sub>7</sub>) yields.

The purpose of these analyses was to provide means for estimating the source character and the degree of diagenetic maturity of the organic matter in the sections penetrated by the two wells.

Results of cuttings gas analyses were plotted on 1:2000 vertical scale strip logs and transmitted to the North Sea Study Group with our letter of November 25, 1968. Samples that were selected for further analyses were chosen on the basis of results of the cuttings gas data, and they also included cuttings from specific zones of interest that were listed in the October 24, 1968 letter NSG-1047 by A. J. Caan of the North Sea Study Group.

This report includes complete tabulations of results of the cuttings gas, visual kerogen, total organic matter and gasoline analyses that were run, plus graphic plots of the various types of data. Explanations of our criteria for interpreting these types of data plus brief discussions of the results of the analyses are included.

Charges for this service work have been billed to the North Sea Study Group through our Job No. 9488 for samples from the 16/9-1 well and Job No. 9489 for samples from the 9/8-1 well.

### PROCEDURE

Compositions and concentrations of hydrocarbon gases in the air spaces above the cuttings in the sample cans were determined by gas chromatography. Similar data were obtained on the gases released from a standard mixture of cuttings plus tap water after agitation for 2 minutes in a Waring blender. Combined results on air space gas plus cuttings gas were calculated for each sample. The data from the combined results were plotted graphically to show the vertical variations in total gas (C<sub>1</sub>-C<sub>4</sub>) and wet gas (C<sub>2</sub>-C<sub>4</sub>) and graphical plots were also made of the percent wet gas in total gas (Figs. 1 and 2).

Cuttings gas yields showed several vertical zonations which roughly correspond to different organic facies in the stratigraphic sections represented by the samples. Representative cuttings samples from the different distinctive zones defined by the cuttings gas were selected for further analyses. Sample intervals cited by the North Sea Group as of particular interest were also considered in choosing the samples for further analysis. The selected samples were then picked by hand to provide materials of uniform lithologies for the additional work.

Some of the sample intervals that were chosen contained soft argillaceous cuttings dispersed in drilling mud, and they completely disaggregated when we attempted to wash the mud away. As a result, we were not able to obtain cuttings chips from all of the intervals of interest.

The "picked" cuttings were analyzed for light gasoline ( $C_4-C_7$ ) compounds, total organic matter and visual kerogen characteristics.

Results of the cuttings gas analyses are given in Tables I and II; results of the additional chemical and visual kerogen analyses are given in Tables III and IV for well 9/8-1 and Tables V and VI for well 16/9-1.

#### BASES FOR INTERPRETING DATA

##### Cuttings Gas

Cuttings gas data give indications of the vertical variability in the source character of a section of interest. The ratio of wet gas ( $C_2-C_4$ ) to total gas ( $C_1-C_4$ ) may distinguish methane-prone from oil- and "wet" gas-prone sections. The critical value of this ratio varies from basin to basin. In Western Canada wet gas concentrations of about 45% or greater are considered to be indicative of sections that are likely to produce oil or gas with significant amounts of hydrocarbon liquids. In the Permian section of West Texas the significant ratio appears to be closer to 20% or greater of wet gas in total gas.

The significant values for total amounts of hydrocarbon gas yielded by the cuttings also appear to vary from basin to basin, and possibly must be established separately for each area of interest. Zones with the greatest yields of gas are considered to be of most interest as sources.

Oil in the drilling mud makes it nearly impossible to establish practical quantitative criteria that can be used in comparing different wells. The oil will tend to reduce the amount of cuttings gas released during agitation in the blender, and it will affect the composition of the hydrocarbon gas that is obtained for analysis. However, even with oil in the mud, significant vertical patterns in hydrocarbon gas concentrations and compositions can be established in each well. The patterns from different wells can be compared to establish regional trends or areal configurations of different organic facies within a section of interest.

## Visual Kerogen

Kerogen data give two types of information. The color alteration (carbonization) provides a gross indication of the amount of thermal diagenesis that the organic matter has undergone. The types of materials comprising the kerogen help define different organic facies that are present in the sampled sections and they may indicate the source character of some of these facies.

Kerogen color alterations are rated on a 1 to 5 scale, from unaltered to almost completely carbonized, respectively. Ratings of 4 or 5 suggest that subsurface temperatures have been high enough to destroy most of the producible liquid hydrocarbons. Sections in which kerogen alteration is rated 4 and 5 are more likely to be characterized by dry gas production, if producible hydrocarbons are found in the associated reservoirs. Immobile pyrobitumens may also be found in these reservoir beds. Alteration ratings of 1 to 2 suggest that thermal diagenesis of the kerogen has barely begun, and reservoir hydrocarbons, if present, are likely to be gases, possibly associated with heavy, asphaltic oils. Ratings of 2+ to 3 suggest that maturation of the material has progressed to the point that gas, liquid hydrocarbons, or mixed oil and gas may be produced, depending on the nature of the original source materials. A rating of 2 may be associated with either immature or moderately mature sediments, based on other chemical evidence, and hence is not diagnostic. The interpretation of the significance of alteration ratings of 4 or 5 is the most reliable of the above tentative rules of thumb.

Types of kerogen materials that are recognized include amorphous, finely disseminated, algal, herbaceous, woody and coaly. The source significance of these types is not established, but there have been suggestions in some areas, such as the offshore of southern Australia, that gas production is possibly associated with woody and coaly kerogen, whereas beds rated as oil sources may include rocks containing amorphous, finely disseminated and algal materials. These observations are speculative.

## Total Organic Matter

The total organic matter concentration gives a rough indication of the richness of a rock in materials that can produce hydrocarbons. However, this measure alone does not indicate whether the organic material is oil-prone, gas-prone or mixed oil and gas prone. Rocks containing less than about 0.5% total organic matter are generally rated as poor sources, but this is modified by lithology. Carbonate sequences possibly include source rocks with still lower concentrations of total organic matter than 0.5%.

Sections that are notable for their production of dry gas (mainly methane) have commonly been found to be characterized by source rocks containing greater than about 1.1% total organic matter. However, a measure of the liquid hydrocarbons in these richer rocks is also necessary to determine whether they should be rated as oil prone or gas prone.

## Light Gasoline (C<sub>1</sub>-C<sub>7</sub>) Hydrocarbons

Light gasolines apparently do not appear in source beds in concentrations above one or two parts per million until a fair degree of maturation occurs. Therefore, gasoline concentrations give one criterion of the degree of thermal maturation that the organic matter has attained.

In addition, ratios of specific gasoline compounds may indicate the possible source character of the rocks. In particular, the ratio of cyclohexane to methylcyclopentane (CH/MCP) has been found to be useful in the U. S. Gulf Coast and the Alaskan areas for distinguishing "non oily" from "oily" facies. To date commercial oil has not been found associated with strata having a CH/MCP ratio of less than 0.25. However, dry gas has been found in strata characterized by lower ratio values as well as in sections with ratios greater than 0.25.

The CH/MCP ratio is also useful in helping distinguish different organic facies that may be present within an oil-like section. Ratios all above 0.25 in value may show groupings in vertical patterns that correlate with stratigraphic zones that have distinctive source characteristics. Definition of such zones may be quite useful for correlating reservoir oils with specific source intervals.

### DISCUSSION AND INTERPRETATION OF RESULTS

#### A. Esso 9/8-1 Well

The analytical results are summarized graphically in Fig. 1 and are tabulated in Tables I, III, and IV.

The cuttings gas plot (Fig. 1) shows zones of high methane yields from samples from the gross intervals 1350-2400 feet and 3000-4000 feet. Total organic matter in picked samples from these zones ranges from about 1 to 2.3 percent. These two observations both suggest that the two intervals cited are potential hydrocarbon source intervals, and that methane gas could be found in associated reservoir beds. These data do not determine whether the two sections contain potentially oil prone organic matter that is still immature diagenetically or whether the material is basically gas prone, regardless of maturation state. Kerogen in the picked samples is predominantly amorphous, which suggests that the former is the case. That is, these two zones possibly represent immature oil-prone organic facies, and under present subsurface conditions they would be associated mainly with methane and possibly heavy asphaltic oils. With deeper burial and elevated temperatures the gas would probably become wetter and the oils would become medium gravity or distillates.

Another zone of higher gas yields is the interval 6250-6450 feet. The cuttings gas here is wetter (Fig. 1) and suggests an oil prone zone. Total organic matter in picked cuttings in this interval is quite high,

approximately 7%; these samples are quite rich in potential source material. Kerogen alteration ratings are 1+ and 2, suggesting an immature diagenetic stage, although gasoline yields of 5 to 21 ppm indicate that at least moderate maturation has occurred. Kerogen is predominantly amorphous.

The cyclohexane/methylcyclopentane (CH/MCP) ratios are low, ranging from .15 to .37, suggesting that significant oil-like hydrocarbons have not been generated by this section. These combined criteria suggest a relatively immature but rich oil-prone organic facies which at present subsurface conditions would likely be characterized by gas and possibly distillate accumulations in associated reservoir beds.

Tentative zonations of the section suggested by the types of kerogen and by the CH/MCP ratios are suggested by dashed lines in Fig. 1. These could be more effectively placed by combining geochemical with other geological information.

Comments on samples from specific zones cited by the North Sea Study Group are included below:

1. 1900-2000 feet

Limestone chips from the 1950 feet sample contain enough organic matter (1%) to be rated as potential sources of hydrocarbons. Small amounts of amorphous kerogen present suggest a potential oil prone facies, but the data do not adequately distinguish whether the matter is potentially oil prone or gas prone. At present depths it would have generated mainly methane gas.

2. 3000 feet

Limestone chips from the 3050 feet sample contained above average total organic matter (1.9%). The same comments made above for the 1900-2000 feet sample are applicable.

3. 3400 feet

Limestone chips from the 3400 feet sample contained above average total organic matter and kerogen material is predominantly amorphous and herbaceous. This is interpreted as an immature oil prone source facies. Predominantly methane gas from the cuttings supports this interpretation.

4. 5500 feet

Shale chips from 5700 feet samples contained mainly coaly and woody kerogen, suggesting gas prone organic matter. Total organic matter is low (0.76%) for a significant gas source facies, and low yields of cuttings gas from these samples suggest that this is not a notable source interval.

5. 5800-6000 feet

Silty shale cuttings from the 5950 and 6000 feet samples contained nearly 2% total organic matter, suggesting a source facies. Kerogen was mainly amorphous, suggesting an oil-prone source, and this is supported by the sharp increase of wetness of the cuttings gas from this interval. Relatively low gasoline yields suggest the material is still relatively immature so that significant hydrocarbon liquids generation has not yet occurred.

6. 6200-6400 feet

Shale cuttings that were picked from samples in this interval were rich in organic matter (6-8%), suggesting a good source interval. This interval was discussed in the general introductory remarks above in regard to the 6250-6450 ft. section, where it is suggested that this is an immature oil-prone zone.

B. Esso 16/9-1 Well

The analytical results are summarized graphically in Fig. 2 and tabulated in Tables II, V, and VI.

The cuttings gas plot (Fig. 2) shows above normal yields of methane in the general interval from 1350-4250 feet with higher yields below 3750 feet. Total organic matter of picked cuttings is mainly about 0.9%, and visual kerogen is predominantly amorphous material in this interval. This is interpreted to be an immature oil-prone zone which under present conditions might be characterized with methane gas and possibly heavy asphaltic oils in associated porous zones. With deeper burial or elevated subsurface temperatures, wet gas and medium to high gravity oils might be generated.

A cuttings gas anomaly in the interval 7650-8250 feet indicates a hydrocarbon source interval. The high content of wet gas (over 50% C<sub>2</sub>-C<sub>4</sub>), high gasoline yields, and predominantly amorphous kerogen in the picked samples suggest an oil-prone source interval. Unusually high total organic content (up to 13%) of many of the picked samples suggests a rich source interval that might tend to be more associated with gas production. Low CH/MCP ratios (.12 to .17) suggest a "non-oily" section and are more indicative of a methane-prone interval. Possibly this is a feature of an immature oily section that has not yet released significant amounts of liquid hydrocarbons to the reservoir beds.

*← only one sample high*

The cuttings gas anomaly at 11,150-11,350 feet may be due to cavings. Shale chips analyzed from this interval show organic compositions very similar to shales from about 7700-8250 feet, and the comments made in the paragraph above are applicable for the samples from this lower interval.

Possible zonations of organic facies based on kerogen type and on the CH/MCP ratios are indicated in Fig. 2. These could be placed more reliably by using other geologic information in addition to the geochemical data.

Comments on samples from specific zones cited by the North Sea Study Group are given below:

1. 2800-2950 feet

Samples were lost during washing, and no analyses were obtained. The soft clay chips disaggregated.

2. 3400-3800 feet

Sample were lost during washing.

3. 3950-4200 feet

Argillaceous cuttings chips from the 4150 and 4200 ft. samples and limestone chips from the 3950 ft. sample contained about 0.9% total organic matter. Their gasoline yields were fairly low and the cuttings gas from gross samples in this interval was predominantly methane. Visual kerogen was mainly amorphous material. These data suggest an immature oil source interval characterized at present conditions by dry gas plus possible heavy asphaltic oils in porous zones.

4. 6100-6300 feet

The chalky limestone analyzed from the 6100 ft sample is rated as a poor source.

5. <sup>4072</sup>6800-7000 feet

Shale picked from the 6950 ft. sample is rated as a gas source on the basis of relatively high total organic matter (1.9%) and predominantly woody and coaly visual kerogen. Kerogen alteration of 2+ suggests a moderately matured diagenetic stage.

6. 7600-7700 feet

Wetness of the cuttings gas increases abruptly to over 50% at 7600 feet, as was mentioned above in the general remarks on the 16/9-1 well. Also, the kerogen changes to predominantly amorphous material. The CH/MCP ratios become quite low. This is a source section, but it is not clear whether it is an immature oil-prone interval or a gas-prone interval, as was discussed above. The CH/MCP ratio suggests it is limited to a gas-prone character, but the other data suggest oil-prone material.

7. 7750-7900 feet

This zone is quite rich in total organic matter, but the organic material appears to be generally of the same type found in the 7600-7700 ft.

zone, and the same remarks are applicable.

8. 11,100-11,400 feet

As was mentioned in the general discussion above on the 16/9-1 samples, the cuttings picked from 11,200, 11,250, 11,300, 11,350, and 11,400 feet samples resemble those from the 7750-7900 feet interval. They are probably cavings, but whether they are or not, the same remarks made regarding samples from 7750-11,400 feet are applicable.

9. 11,955-T.D.

A limestone sample from the 11,985 feet cuttings is rated as a poor to fair source. This lithology may not be the cause of the increased cuttings gas yield at this depth. The organic material in the limestone is possibly mixed oil and gas source material based on kerogen type and gasoline yield.

C. Kerogen Alteration, Both Wells

None of the kerogen observed from samples in either of the wells was strongly altered, with 2+ being the maximum alteration rating. Excessive subsurface temperatures do not appear to have been experienced by any of the samples from these wells. The sections appear to be diagenetically immature or only moderately matured, and harmful destruction of hydrocarbon liquids by thermal alteration has not been a problem.

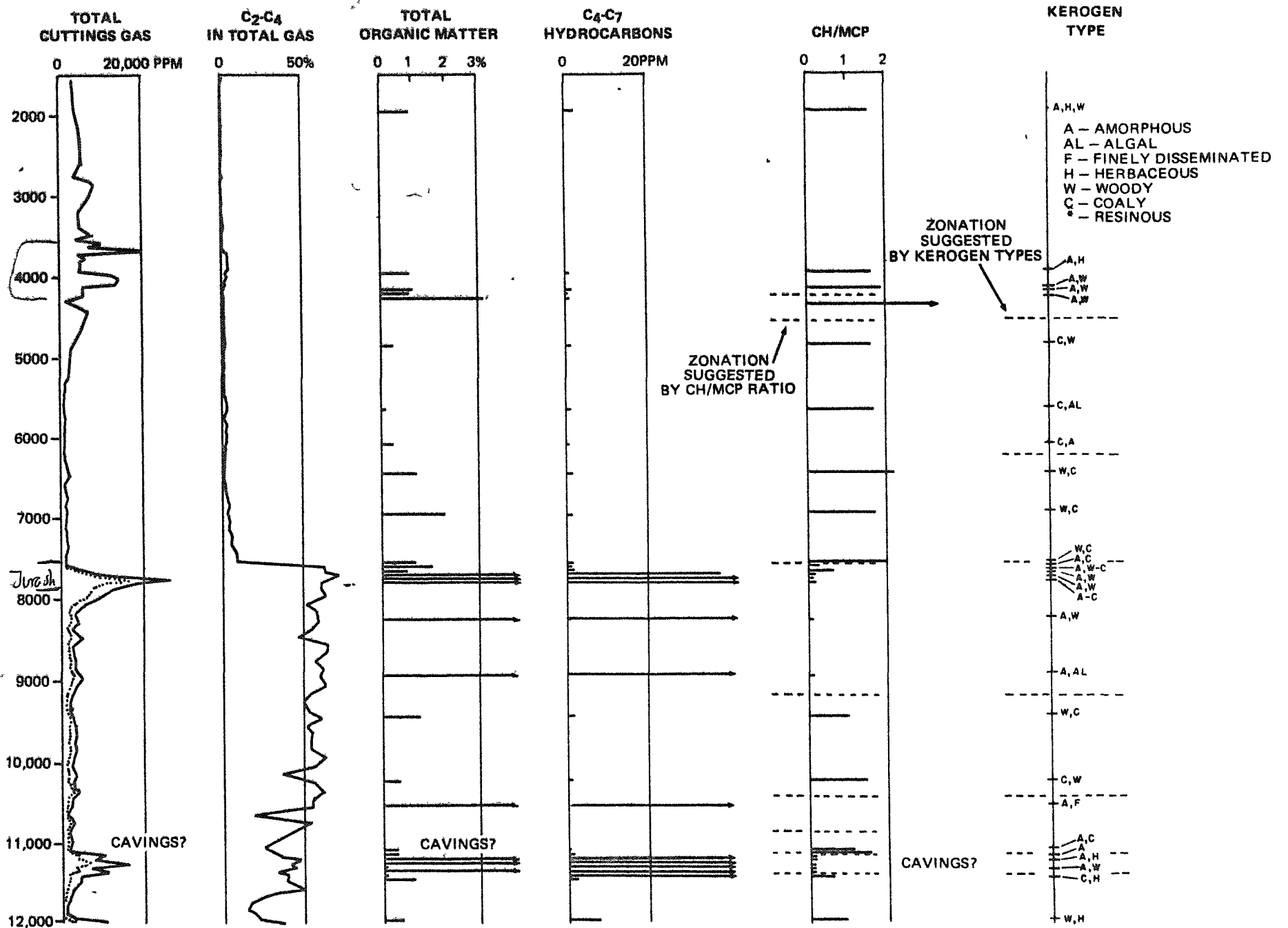


FIGURE 2. WELL 16/9-1, CHEMICAL AND VISUAL KEROGEN PATTERNS.

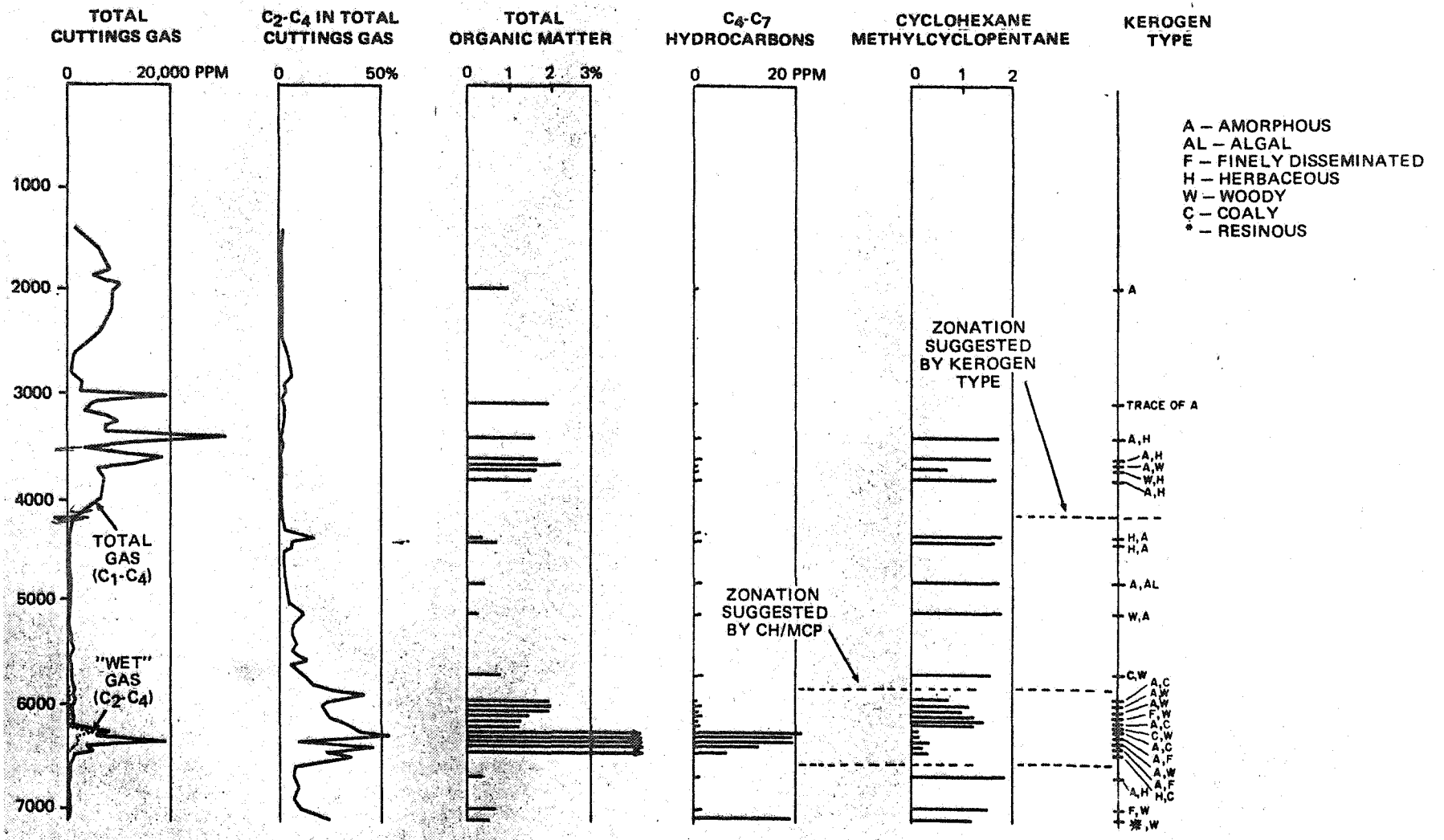


FIGURE 1. WELL 9/8-1, CHEMICAL AND VISUAL KEROGEN PATTERNS.



C<sub>1</sub>-C<sub>4</sub> HYDROCARBON ANALYSES - CUTTINGS ONLY

SAMPLE NUMBER	DEPTH	GAS CONCENTRATION (VOLUME GAS PER MILLION VOLUMES CUTTINGS)							GAS COMPOSITION (PERCENT)								NOTES		
		METHANE (C <sub>1</sub> )	ETHANE (C <sub>2</sub> )	PROPANE (C <sub>3</sub> )	ISO BUTANE (iC <sub>4</sub> )	NORMAL BUTANE (nC <sub>4</sub> )	WET (C <sub>2</sub> -C <sub>4</sub> )	TOTAL (C <sub>1</sub> -C <sub>4</sub> )	TOTAL GAS				WET GAS						
									C <sub>2</sub> -C <sub>4</sub>	C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub>	iC <sub>4</sub>	nC <sub>4</sub>	C <sub>2</sub>	C <sub>3</sub>		iC <sub>4</sub>	nC <sub>4</sub>
89137A	4	1400	627.60	4.78	4.02	0.74	1.21	10.75	638.35	1.6840	98.1	1.0	0.0	0.0	65.37	7.11			
89137E	4	1400	787.30	3.01	3.23	0.36	0.68	6.38	793.78	0.8289	100.0	0.0	0.0	0.0	44.33	8.10			
89137I	4	1800	2737.50	3.01	4.70	3.92	13.07	24.70	2762.20	0.8742	100.0	0.0	0.0	0.0	12.19	16.33			
89137J	4	1800	1276.86	0.88	3.11	3.78	8.64	16.42	1384.93	1.2729	98.0	0.0	0.0	0.0	5.18	17.88			
89137K	4	1900	1662.00	0.97	4.48	4.84	17.65	27.94	1689.94	1.4533	99.0	0.0	0.0	0.0	3.16	17.64			
89137L	4	1950	1648.50	1.35	3.39	2.94	11.65	19.83	1689.33	1.8203	99.0	0.0	0.0	0.0	10.17	16.38			
89137M	4	2000	1039.20	4.60	3.93	8.24	23.47	42.24	1081.44	3.9099	98.0	0.1	1.0	2.0	11.14	20.55			
89138A	4	2050	844.80	1.42	6.88	0.23	0.84	3.34	852.34	0.2918	100.0	0.0	0.0	0.0	42.23	7.25			CC
89138B	4	2200	975.60	3.36	2.65	1.67	4.67	12.35	987.95	1.2500	100.0	0.0	0.0	0.0	27.21	14.38			
89138C	4	2400	987.60	3.30	4.45	1.84	3.53	12.16	989.76	1.2539	100.0	0.0	0.0	0.0	18.37	18.20			
89138I	4	2600	399.60	2.72	4.04	4.84	3.66	16.26	415.86	3.9099	96.1	1.1	1.1	1.1	23.23	29.18			
89138M	4	2600	445.80	4.34	4.24	4.94	8.50	23.66	469.46	5.9098	94.1	1.1	1.1	1.1	21.26	26.23			
89138O	4	2900	374.50	1.23	3.17	6.17	4.55	17.22	391.72	2.9101	97.0	0.1	1.1	1.1	8.30	27.26			
89138R	4	2950	504.75	1.35	10.77	6.76	5.69	24.51	529.26	4.6209	96.0	0.2	1.1	1.1	8.44	27.21			
89139A	4	3000	3310.55	13.72	17.95	12.09	8.35	32.11	3362.66	1.5497	99.0	0.1	0.0	0.0	26.35	29.16			
89139B	4	3050	430.25	2.30	4.38	12.70	3.27	27.33	467.80	4.2824	98.0	0.1	1.1	1.1	6.21	14.19			
89139C	4	3100	1071.00	2.37	8.21	9.34	4.50	24.62	1095.62	2.2471	99.0	0.1	1.0	0.0	10.33	39.18			
89139D	4	3150	300.00	2.83	10.48	16.53	4.45	34.28	394.28	3.4477	97.0	0.1	2.0	0.0	4.26	49.18			
89139E	4	3200	1448.80	11.95	23.81	28.50	7.71	71.97	1517.97	4.7412	94.1	1.2	1.1	1.1	17.33	39.18			
89139F	4	3250	1101.00	3.54	10.84	16.37	4.87	33.73	1136.72	3.1423	98.0	0.1	1.0	0.0	10.31	42.14			
89139G	4	3300	839.50	3.54	6.96	10.30	3.37	24.17	863.67	2.7351	98.0	0.1	1.0	0.0	19.39	42.14			
89139M	4	3300	1512.00	3.84	8.18	14.10	4.77	31.50	1543.50	2.5853	98.0	0.1	1.0	0.0	11.33	30.18			
89139I	4	3400	3389.14	12.83	19.92	16.88	7.08	56.71	3445.85	1.6353	99.0	0.1	0.0	0.0	23.35	40.18			
89139J	4	3450	434.00	2.83	3.33	5.21	2.67	14.44	448.44	1.7281	98.0	0.0	1.0	0.0	18.27	30.18			
89139K	4	3500	730.50	2.83	3.16	4.48	1.43	11.92	742.42	1.6055	99.0	0.0	1.0	0.0	24.27	37.18			
89139L	4	3550	1638.00	3.54	5.16	4.34	3.62	17.64	1655.62	1.6798	99.0	0.0	1.0	0.0	20.29	30.18			
89139M	4	3600	9374.99	16.99	33.99	21.61	10.05	82.69	9497.62	0.6737	100.0	0.0	0.0	0.0	21.41	28.18			
89139N	4	3650	6638.82	4.34	38.72	17.22	11.13	58.62	6738.01	0.8728	100.0	0.0	0.0	0.0	8.44	28.18			
89139O	4	3700	4823.99	3.89	15.85	12.76	4.99	37.48	4861.47	0.7710	100.0	0.0	0.0	0.0	10.43	30.18			
89140A	4	3800	4148.44	10.27	18.37	13.21	3.32	47.34	4195.80	1.3288	100.0	0.0	0.0	0.0	23.28	28.18			
89140E	4	4000	1669.33	5.90	9.52	7.18	3.34	26.94	1696.47	1.8002	99.0	0.1	1.0	0.0	26.35	27.18			
89140M	4	4200	344.00	3.01	1.78	1.18	0.84	6.82	352.82	1.3330	99.1	0.0	0.0	0.0	48.38	17.18			
89140J	4	4300	330.00	1.24	0.94	0.93	4.01	7.12	342.32	1.3128	99.0	0.0	0.0	1.1	17.18	17.18			
89140K	4	4350	320.00	3.30	3.63	10.40	44.14	60.73	450.73	13.4726	86.1	1.0	1.0	1.0	4.11	27.18			
89140L	4	4400	480.00	1.24	1.71	3.33	15.26	21.74	501.74	4.3328	96.0	0.0	1.0	0.0	6.16	16.70			
89140N	4	4450	383.80	1.35	1.58	2.64	13.13	17.31	403.11	4.2240	96.0	0.0	1.0	0.0	11.18	16.70			
89140O	4	4500	507.00	1.77	1.03	0.97	2.25	8.09	515.09	1.1752	100.0	0.0	0.0	0.0	29.17	16.38			
89140P	4	4600	404.40	2.85	3.04	0.61	0.23	7.25	411.65	1.7611	98.0	1.1	0.0	0.0	37.48	9.18			
89140Q	4	4800	432.40	4.42	0.92	0.56	0.64	6.54	438.94	1.6249	99.1	0.0	0.0	0.0	67.16	9.10			
89141M	4	5000	300.00	2.30	1.04	1.82	6.32	11.68	311.68	3.7473	94.1	0.0	1.0	0.0	30.18	16.38			
89141J	4	5100	462.50	3.54	3.68	9.95	32.99	50.16	472.66	10.1814	89.1	1.0	1.0	2.0	7.18	20.60			
89141L	4	5200	378.80	2.30	1.38	3.16	12.12	19.92	399.72	4.8824	95.1	0.0	1.0	0.0	17.0	16.60			
89141N	4	5300	314.50	9.07	13.04	5.77	6.36	34.44	348.94	6.2738	94.0	2.0	1.0	1.0	20.38	17.18			
89141R	4	5400	704.40	12.74	24.76	11.80	3.76	38.10	742.80	7.7406	93.0	3.0	3.0	1.0	22.42	20.18			
89142A	4	5450	500.25	1.50	18.47	9.19	7.63	36.79	537.04	6.8303	94.0	0.3	2.0	1.0	4.50	25.21			
89142B	4	5500	338.20	8.47	20.79	11.34	8.31	48.23	408.53	8.1042	93.1	1.0	2.0	1.0	18.43	23.18			
89142C	4	5550	262.87	3.54	17.88	9.82	7.00	37.94	300.81	12.6125	88.1	0.0	3.0	2.0	9.47	26.18			
89142D	4	5600	402.48	3.84	13.88	9.60	7.63	34.74	437.16	9.4534	98.1	2.0	1.0	1.0	17.37	24.20			
89142F	4	5700	680.00	16.64	27.28	20.09	13.04	87.05	717.05	12.1399	88.0	2.0	3.0	2.0	19.45	23.18			
89142M	4	5800	382.80	20.32	34.43	33.70	19.84	129.82	721.32	17.8173	81.0	3.0	3.0	3.0	16.43	26.18			
89142I	4	5850	410.40	30.87	33.43	37.73	34.09	216.12	626.52	34.4933	66.0	3.0	3.0	3.0	16.43	27.18			
89142J	4	5900	217.20	23.32	113.02	28.68	31.71	287.73	504.93	56.8841	42.0	6.24	18.10	10.41	23.18				
89142K	4	5950	708.00	25.49	98.50	71.42	43.25	238.66	946.66	25.2107	74.0	3.10	6.0	5.0	11.41	30.18			
89143L	4	6000	632.40	28.48	71.27	41.84	33.07	181.69	814.09	22.3181	72.0	3.0	6.0	4.0	14.39	28.18			
89143M	4	6050	787.20	35.61	84.41	59.27	36.73	208.02	995.22	21.5315	77.0	4.0	6.0	4.0	17.60	26.18			CC
89143N	4	6100	481.80	25.84	88.04	59.74	42.23	212.90	904.10	23.5482	76.0	3.0	7.0	5.0	12.46	25.18			
89143O	4	6150	576.00	22.20	84.82	75.89	48.34	231.39	807.39	28.8700	71.0	3.11	6.0	4.0	10.30	23.18			
89143P	4	6200	703.20	43.06	149.64	92.24	77.89	354.55	1057.75	33.5192	66.0	4.14	6.0	7.0	12.40	26.18			
89143R	4	6250	2079.00	271.87	971.28	516.24	450.29	2209.78	4279.78	21.6330	48.0	6.23	12.11	12.63	23.20				
89143S	4	6300	2119.78	313.78	1104.24	623.38	524.44	2724.73	4843.48	26.2557	44.0	6.24	14.12	12.42	23.18				
89143T	4	6350	3468.00	77.88	322.51	225.41	214.33	843.13	4311.12	19.5969	51.0	2.0	7.0	3.0	9.39	27.18			
89143U	4	6400	1630.00	139.34	331.03	235.33	238.16	1340.44	2969.46	32.9350	44.0	6.23	13.12	10.41	27.18				
89143V	4	6450	649.00	67.26	233.24	136.24	133.86	590.30	1439.30	41.0130	39.0	3.16	11.0	9.0	11.40	26.18			
89143W	4	6500	382.40	25.32	129.86	92.24	78.00	330.04	912.64	36.1632	44.0	3.14	10.0	9.0	9.39	26.18			
89143X	4	6600	496.20	4.60	11.80	8.80	8.74	38.94	535.14	6.4020	94.1	2.0	2.0	2.0	16.34	26.18			
89143Y	4	6700	608.00	3.83	14.06	11.88	13.38	43.44	649.44	6.4088	94.0	0.0	2.0	2.0	7.33	25.18			
89143Z	4	6800	298.20	2.3															



SAMPLE NUMBER	DEPTH	GAS CONCENTRATION (VOLUME GAS PER MILLION VOLUME)					CUTTINGS		GAS COMPOSITION (PERCENT)										
		METHANE	ETHANE	PROPANE	ISOBUTANE	NORMAL BUTANE	WET	OTIA	TOTAL GAS					WET GAS					
		(C <sub>1</sub> )	(C <sub>2</sub> )	(C <sub>3</sub> )	(iC <sub>4</sub> )	(nC <sub>4</sub> )	C <sub>2</sub> C <sub>1</sub>	(C <sub>1</sub> )	C <sub>2</sub> C	C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub>	iC <sub>4</sub>	nC <sub>4</sub>	C <sub>2</sub>	C <sub>3</sub>	iC <sub>4</sub>	nC <sub>4</sub>	
99167A	4	3350	2844.46	14.26	10.70	9.88	21.74	56.38	2900.84	1.9423	99	0	0	0	1	25.19	17.39		
99167B	4	1850	3030.82	5.80	3.21	4.10	13.49	26.70	8662.83	0.9715	100	0	0	0	0	32.12	18.81		
99167C	4	1750	3763.83	8.84	3.84	3.33	9.79	22.00	1786.63	0.9468	100	0	0	0	0	30.12	15.93		
99167D	4	1800	3838.81	6.82	1.23	2.27	7.78	18.88	6874.88	0.9488	100	0	0	0	0	38.10	12.48		
99168A	4	2150	4913.66	8.93	1.70	2.12	6.04	18.87	9364.47	0.9812	100	0	0	0	0	48.9	11.32		
99168B	4	2850	5144.90	6.88	1.88	3.30	6.48	17.43	8139.88	0.9382	100	0	0	0	0	40.8	13.88		
99168C	4	2950	3332.94	9.93	8.88	9.45	18.73	37.40	1869.94	0.9605	100	0	0	0	0	25.24	15.36		
99168D	4	3750	3848.45	11.43	3.22	3.02	38.42	48.78	3914.24	1.7574	98	0	0	0	1	17.12	18.82		
99169A	4	2800	6834.07	5.88	42.63	17.02	22.83	88.36	9222.42	1.2764	99	0	1	0	0	7.48	19.26		
99169B	4	2850	3138.43	8.83	30.40	12.01	18.20	46.16	8468.87	0.9004	100	0	0	0	0	8.46	16.29		
99169C	4	2800	7738.02	13.53	28.90	12.38	20.63	75.44	7810.45	0.9638	100	0	0	0	0	18.39	16.27		
99169D	4	3250	7538.88	18.13	38.27	11.92	26.49	78.00	7614.63	1.0349	100	0	0	0	0	23.36	15.26		
99169E	4	3150	4678.23	11.36	23.62	17.55	17.56	79.89	4758.42	1.0789	99	0	1	0	0	14.42	22.22		
99169F	4	3350	4910.70	14.32	44.17	24.70	17.99	181.18	3011.87	2.0184	99	0	1	0	0	14.44	24.18		
99169G	4	3600	5910.50	11.99	38.22	20.40	15.05	85.65	1996.15	1.4284	99	0	1	0	0	16.44	24.18		
99169H	4	3450	7833.88	14.00	62.77	21.42	18.35	33.34	7386.58	1.3747	98	0	1	0	0	18.46	23.16		
99169I	4	3300	3698.35	7.64	36.55	20.99	16.81	81.79	3780.14	1.2637	98	0	1	0	0	9.88	26.20		
99169J	4	3850	3473.71	33.40	43.33	28.35	17.22	142.29	9418.00	1.4789	98	0	1	0	0	23.48	20.18		
99169K	4	3600	6684.50	8.83	50.94	23.07	16.11	100.97	6783.47	1.4924	99	0	1	0	0	9.30	25.16		
99169L	4	3850	12643.43	26.04	126.43	48.18	24.75	226.39	1868.82	1.1864	98	0	1	0	0	12.58	22.11		
99169M	4	3700	4453.85	22.51	58.61	32.19	18.93	131.24	4885.09	2.8623	98	0	1	0	0	17.44	25.14		
99169N	4	3750	3643.73	24.14	117.82	62.24	30.31	243.44	8489.37	4.1710	98	0	1	1	0	14.46	26.12		
99170A	4	3800	4172.67	25.23	73.02	48.07	23.00	189.92	4862.59	4.2534	95	1	2	1	1	19.30	25.12		
99170B	4	3850	4628.44	27.13	84.04	47.84	23.84	181.47	4878.91	3.8728	98	1	2	1	0	14.44	25.12		
99170C	4	3900	4464.00	28.03	103.29	55.84	24.42	209.40	4673.40	4.4807	95	1	2	1	1	12.44	27.12		
99170D	4	3950	12828.12	42.72	118.81	58.98	27.43	247.73	1873.85	1.9374	98	0	1	0	0	17.44	23.12		
99170E	4	4000	14092.87	63.84	166.39	64.02	28.03	321.77	14874.64	2.2895	97	0	1	0	0	20.51	20.9		
99170F	4	4050	13248.44	48.83	137.84	61.17	31.88	306.84	13448.41	2.2048	98	0	1	0	0	17.88	20.11		
99170G	4	4100	9099.00	23.84	40.93	22.37	19.99	117.32	5110.32	2.2492	97	0	1	0	0	20.44	19.17		
99170H	4	4150	5448.78	30.30	42.41	17.73	17.21	97.84	5847.38	1.7821	98	0	1	0	0	21.44	18.18		
99170I	4	4200	5999.57	25.82	33.46	17.24	25.78	102.30	5531.87	1.8593	99	0	1	0	0	23.39	17.29		
99170J	4	4250	7483.27	2.52	4.01	1.15	1.52	9.21	784.88	1.2209	99	0	1	0	0	27.44	12.17		
99170K	4	4400	6858.03	35.63	21.06	13.72	23.82	113.75	6971.78	1.6936	99	0	1	0	0	40.19	12.21		
99170L	4	4450	4704.27	27.27	18.88	10.18	18.27	72.28	4746.88	1.8132	98	1	0	0	0	28.27	12.21		
99171A	4	4850	2224.30	23.93	6.25	2.30	2.91	23.39	239.69	1.5601	99	1	0	0	0	68.16	9.8		
99171B	4	4850	1841.78	8.70	3.22	0.31	2.14	17.47	188.44	0.8017	100	0	0	0	0	84.20	7.18		
99171C	4	4950	351.27	4.67	1.70	0.71	1.73	8.83	360.10	1.3705	99	1	0	0	0	59.19	8.20		
99171D	4	4850	388.87	5.38	2.42	0.70	3.12	11.47	610.34	1.8792	98	1	0	0	0	46.22	8.27		
99171E	4	4950	327.67	3.67	2.26	1.22	1.89	9.14	337.01	2.7120	97	1	0	0	1	40.28	13.22		
99171F	4	4850	686.04	4.38	1.81	1.70	4.87	12.47	444.81	2.7803	98	1	0	0	1	38.18	13.96		
99171G	4	4950	92.68	4.31	1.97	1.05	2.10	9.43	602.11	1.5661	98	1	0	0	1	46.21	11.22		
99171H	4	4850	434.00	5.24	1.20	1.27	1.22	10.49	481.54	2.2635	99	1	0	0	0	84.18	13.15		
99171I	4	4950	471.11	5.62	2.25	1.34	1.48	9.82	433.82	2.2635	99	1	0	0	0	59.22	13.12		
99171J	4	4850	383.44	3.60	2.32	1.98	2.02	8.84	405.28	2.4278	98	1	0	0	0	36.29	20.21		
99171K	4	4850	274.40	1.28	1.35	0.88	1.28	4.79	279.19	1.7137	100	0	0	0	0	27.28	18.27		
99171L	4	4850	834.14	3.34	3.52	2.23	2.21	11.24	843.38	2.0608	98	1	1	0	0	30.21	20.19		
99171M	4	4850	391.80	1.44	2.90	1.90	2.01	8.25	600.05	1.3748	100	0	0	0	0	17.30	23.26		
99171N	4	4850	878.21	4.28	3.29	1.82	1.47	10.74	886.05	1.8326	98	1	1	0	0	29.21	14.18		
99171O	4	4900	848.44	3.75	2.33	1.15	1.06	8.20	856.73	0.9675	100	0	0	0	0	45.28	14.18		
99171P	4	4850	1156.84	4.34	3.02	1.81	1.71	10.58	1177.92	0.8944	100	0	0	0	0	41.29	14.18		
99171Q	4	4650	1468.31	7.39	5.28	3.01	2.94	16.82	1687.32	1.2653	99	1	0	0	0	40.28	16.18		
99171R	4	4850	1486.83	2.83	2.80	2.12	1.97	10.74	890.77	1.3567	99	1	0	0	0	36.26	20.18		
99171S	4	4650	921.05	6.34	4.30	3.16	2.85	17.05	938.10	1.8174	99	1	0	0	0	38.26	19.17		
99171T	4	4850	785.80	8.48	6.34	3.85	3.32	22.21	774.11	2.2616	98	1	1	0	0	39.21	17.17		
99171U	4	4850	616.32	8.31	9.34	6.28	3.24	29.17	645.49	4.3190	98	1	1	1	1	28.32	22.18		
99171V	4	4850	846.80	8.04	8.23	3.14	4.23	25.71	872.51	2.8466	97	1	1	1	0	31.39	20.18		
99171W	4	7050	385.33	7.93	7.08	4.63	4.18	23.84	589.17	4.0463	96	1	1	1	1	33.30	19.18		
99171X	4	7150	827.87	8.18	7.44	4.84	4.31	24.59	622.46	3.8903	94	1	1	1	1	30.30	19.18		
99171Y	4	7250	594.88	10.06	11.05	6.50	6.07	32.39	622.56	5.3382	94	2	2	1	1	30.30	19.18		
99171Z	4	7350	1070.00	14.68	18.88	12.80	13.52	88.00	1128.90	8.2090	98	1	2	1	1	28.31	21.23		
99172A	4	7450	669.13	9.29	18.95	14.76	16.59	39.59	738.72	8.1772	92	1	3	2	2	16.31	25.28		
99172B	4	7550	340.91	10.48	18.87	12.80	14.14	86.31	897.28	9.4285	91	2	3	2	2	18.34	23.28		
99172C	4	7600	929.28	10.73	34.93	34.93	41.77	1375.10	2505.38	62.8687	37	8	25	14	17	13.38	22.27		
99172D	4	7650	2438.27	18.06	154.44	500.20	107.70	4679.11	738.07	64.0528	34	10	27	12	18	16.42	15.28		
99172E	4	7700	3633.48	112.06	3770.21	1904.83	2434.10	8938.01	1239.49	72.1302	28	9	30	13	20	13.42	18.27		
99172F	4	7750	858.88	247.39	7450.88	2413.43	3784.88	14888.88	2603.37	63.3347	33	11	23	10	14	18.44	17.22		
99172G	4	7800	6744.94	1844.63	4482.60	1032.54	2483.59	10443.55	17187.49	40.7625	39	11	28	9	14	16.42	16.24		
99172H	4	7850	1383.72	1383.88	2417.67	1244.74	1831.20	7898.96	1030.30	80.3869	39	11	28	10	14	18.44	16.24		
99172I	4	7900	3605.82	1170.78	2853.47	927.07	1283.52	6234.82	9840.65	63.337									

SAMPLE NUMBER	R	DEPTH	GAS CONCENTRATION (VOLUME GAS PER MILLION VOLUMES CUTTINGS)							GAS COMPOSITION (PERCENT)															
			METHANE		ETHANE		PROPANE		ISO-BUTANE	NORMAL BUTANE	WET		TOTAL	TOTAL GAS					WET GAS						
			(C <sub>1</sub> )	(C <sub>2</sub> )	(C <sub>3</sub> )	(C <sub>4</sub> )	(C <sub>5</sub> )	(C <sub>6</sub> )	(C <sub>7</sub> )	(C <sub>1</sub> -C <sub>7</sub> )	(C <sub>1</sub> -C <sub>7</sub> )	C <sub>1</sub> -C <sub>7</sub>	C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub>	C <sub>4</sub>	C <sub>5</sub>	C <sub>6</sub>	C <sub>7</sub>	C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub>	C <sub>4</sub>	C <sub>5</sub>	C <sub>6</sub>
391674	4	1350	2203.66	7.18	4.37	3.22	12.45	29.22	2232.48	1.3786	99.0	0	0	0	0	0	0	23.19	19.62						
391675	4	1350	2415.23	3.32	1.44	1.76	3.09	11.58	2426.81	0.4771	100.0	0	0	0	0	0	0	28.18	17.54						
391676	4	1750	3189.03	3.83	1.37	1.55	4.81	11.81	3200.84	0.3089	100.0	0	0	0	0	0	0	32.12	12.41						
391677	4	1850	2144.61	0.32	0.32	0.32	2.48	8.88	2173.50	0.7501	100.0	0	0	0	0	0	0	42.10	11.20						
391678	4	2150	3943.68	0.65	0.67	0.84	1.91	10.07	3953.73	0.2547	100.0	0	0	0	0	0	0	66.7	8.19						
391679	4	2350	4488.70	0.33	0.47	0.61	2.08	8.38	4414.28	0.1844	100.0	0	0	0	0	0	0	87.4	11.23						
391680	4	2550	4206.34	0.87	4.84	2.10	4.03	17.83	4222.37	0.4229	100.0	0	0	0	0	0	0	38.27	12.23						
391681	4	2750	3218.08	0.13	4.85	6.05	14.81	34.64	3223.49	1.3644	100.0	0	0	0	0	0	0	26.16	17.43						
391682	4	2800	3428.97	3.93	28.61	7.33	7.43	47.52	3476.08	0.8679	99.0	1	0	0	0	0	0	2.40	10.16						
391683	4	2850	3171.42	0.86	15.95	3.55	2.36	22.60	3187.09	0.3661	100.0	0	0	0	0	0	0	4.70	10.10						
391684	4	2900	3473.32	10.70	19.47	4.90	6.70	40.77	3514.29	0.8239	100.0	0	0	0	0	0	0	20.49	12.16						
391685	4	2950	3433.83	13.33	13.20	3.36	6.49	36.73	3472.44	0.8687	100.0	0	0	0	0	0	0	36.33	3.13						
391686	4	3150	1837.91	7.47	8.33	2.37	1.83	30.04	1837.93	1.0786	100.0	0	0	0	0	0	0	37.48	12.9						
391687	4	3350	2139.33	0.18	3.40	3.60	1.43	18.63	2144.94	0.8688	100.0	0	0	0	0	0	0	33.42	12.8						
391688	4	3400	3120.00	9.91	22.71	7.94	4.36	43.11	3163.11	0.8733	100.0	0	0	0	0	0	0	22.30	18.10						
391689	4	3450	3587.28	11.88	27.82	8.42	3.48	34.83	3622.06	0.8237	100.0	0	0	0	0	0	0	21.50	18.10						
391690	4	3500	1562.33	3.75	0.97	2.39	1.09	14.20	1576.33	0.9007	100.0	0	0	0	0	0	0	26.49	17.8						
391691	4	3550	2985.21	23.13	28.75	8.01	6.46	46.54	3101.78	0.9370	100.0	0	0	0	0	0	0	33.44	13.3						
391692	4	3600	3838.50	7.3	14.21	4.39	2.12	26.03	3844.53	0.8733	100.0	0	0	0	0	0	0	20.33	17.8						
391693	4	3650	1591.43	20.31	8.01	2.43	10.23	141.44	1704.41	0.8294	98.0	1	0	0	0	0	0	14.41	13.7						
391694	4	3700	3977.83	18.97	31.99	11.24	4.49	66.99	3644.34	1.0299	98.0	1	1	0	0	0	0	23.48	17.7						
391695	4	3750	4623.33	21.13	28.11	23.46	13.68	183.33	4834.72	3.2443	96.0	1	2	1	0	0	0	13.38	20.8						
391696	4	3800	3682.87	23.11	67.51	24.61	10.24	125.49	3788.15	3.3127	98.0	1	2	1	0	0	0	13.38	20.8						
391697	4	3850	3744.44	24.43	74.99	30.33	13.48	142.83	3907.06	3.6810	98.0	1	2	1	0	0	0	17.33	21.9						
391698	4	3900	3264.00	22.66	68.33	33.36	9.88	124.43	3688.43	3.3735	98.0	1	2	1	0	0	0	13.38	21.9						
391699	4	3950	3740.00	23.60	29.22	7.34	2.44	63.44	3823.41	1.0888	98.0	1	1	0	0	0	0	27.46	13.4						
391700	4	4000	1148.87	53.74	93.25	26.67	8.93	189.61	11638.47	1.6291	98.0	1	1	0	0	0	0	31.30	13.4						
391701	4	4050	1148.87	44.21	85.34	13.38	3.27	118.34	11638.47	1.6291	98.0	1	1	0	0	0	0	37.44	13.4						
391702	4	4100	4088.00	10.88	33.01	9.92	6.23	83.05	4186.05	1.6375	98.0	1	1	0	0	0	0	28.48	13.4						
391703	4	4150	4073.23	18.13	23.40	7.65	4.08	83.49	4186.41	1.2984	99.0	0	1	0	0	0	0	30.48	14.1						
391704	4	4200	2279.57	3.12	3.93	1.80	0.21	17.82	2297.14	0.7670	100.0	0	0	0	0	0	0	46.34	10.10						
391705	4	4250	139.13	0.33	0.78	0.30	0.30	2.23	137.33	1.4172	98.0	1	1	0	0	0	0	42.33	13.4						
391706	4	4300	3839.28	22.37	3.40	2.37	2.97	33.11	3872.39	0.8350	99.0	1	0	0	0	0	0	68.18	7.9						
391707	4	4350	3921.74	13.13	3.80	2.32	4.30	38.21	3960.38	1.0448	98.0	1	0	0	0	0	0	84.28	3.12						
391708	4	4400	1834.70	21.98	3.74	2.00	2.31	32.23	1896.93	1.7081	99.0	1	0	0	0	0	0	68.18	6.8						
391709	4	4450	1378.33	3.88	1.40	0.43	1.07	8.80	1387.63	0.6412	100.0	0	0	0	0	0	0	67.17	3.12						
391710	4	4500	172.47	2.02	0.79	0.21	0.33	3.33	174.02	1.8110	99.0	1	0	0	0	0	0	37.22	5.13						
391711	4	4550	1323.27	3.33	1.27	0.24	0.97	3.41	1324.88	3.8010	94.0	2	1	0	0	0	0	88.23	4.13						
391712	4	4600	231.37	2.17	1.49	0.48	0.72	4.86	236.23	1.8968	98.0	1	1	0	0	0	0	44.33	10.13						
391713	4	4650	84.44	1.74	1.07	0.70	1.48	3.20	88.44	3.8088	94.0	2	1	1	0	0	0	23.12	13.33						
391714	4	4700	230.28	2.36	1.23	0.39	1.02	3.20	241.48	2.1334	98.0	1	1	0	0	0	0	43.24	11.20						
391715	4	4750	146.50	2.14	1.13	0.67	0.70	3.64	132.14	3.7198	97.0	2	1	0	0	0	0	86.20	13.12						
391716	4	4800	179.91	4.03	1.65	0.88	0.79	7.33	183.20	4.0107	97.0	2	1	0	0	0	0	33.22	12.11						
391717	4	4850	38.44	2.26	1.22	0.74	0.67	3.01	103.43	4.8429	98.0	2	1	1	0	0	0	48.30	13.11						
391718	4	4900	23.13	0.80	0.41	0.14	0.17	1.32	24.67	5.1912	93.0	3	2	1	1	0	0	39.27	3.11						
391719	4	4950	188.74	1.04	1.47	0.38	0.48	3.60	182.34	2.2040	98.0	1	1	0	0	0	0	29.44	13.11						
391720	4	5000	343.03	0.82	1.38	0.78	0.71	3.89	348.94	1.1146	100.0	0	0	0	0	0	0	21.41	20.13						
391721	4	5050	178.71	2.64	1.30	0.79	0.73	6.50	188.21	3.5033	98.0	1	1	0	0	0	0	41.38	13.11						
391722	4	5100	261.44	3.04	1.30	0.41	0.40	3.15	264.59	1.9172	99.0	1	0	0	0	0	0	38.23	8.8						
391723	4	5150	718.84	1.84	1.44	0.39	0.44	4.17	718.11	5.8986	100.0	0	0	0	0	0	0	43.23	4.13						
391724	4	5200	220.51	2.99	4.39	1.89	1.47	10.94	231.45	4.7257	93.0	1	2	1	1	0	0	27.44	17.11						
391725	4	5250	248.03	1.20	1.00	0.44	0.40	3.08	248.03	1.2334	100.0	0	0	0	0	0	0	86.23	13.11						
391726	4	5300	303.03	1.78	1.42	0.61	0.43	4.22	307.27	1.3732	99.0	1	0	0	0	0	0	41.34	13.10						
391727	4	5350	327.80	0.27	3.63	1.20	0.28	12.23	349.72	3.3024	97.0	2	1	0	0	0	0	81.30	13.11						
391728	4	5400	220.32	3.30	3.34	2.11	1.50	14.25	234.37	5.0749	94.0	2	2	1	1	0	0	37.37	13.11						
391729	4	5450	330.40	3.61	3.34	2.11	1.61	14.74	349.14	4.2217	94.0	2	2	1	1	0	0	38.23	13.11						
391730	4	5500	218.33	4.39	3.90	1.82	1.82	11.43	229.86	4.8704	94.0	2	2	1	1	0	0	40.34	13.11						
391731	4	5550	291.87	3.74	4.40	1.87	1.81	11.33	213.41	3.4074	94.0	2	2	1	1	0	0	33.23	13.11						
391732	4	5600	198.88	4.93	6.40	2.32	1.94	13.39	214.47	7.2691	93.0	2	2	1	1	0	0	32.41	13.11						

NUMBER		METHANE			ETHANE			PROPANE			NORMAL BUTANE			ISOBUTANE			TOTAL GAS			WET GAS		
		(C <sub>1</sub> )	(C <sub>2</sub> )	(C <sub>3</sub> )	(C <sub>4</sub> )	(C <sub>5</sub> )	(C <sub>6</sub> )	(C <sub>7</sub> )	(C <sub>8</sub> )	(C <sub>9</sub> )	(C <sub>10</sub> )	(C <sub>11</sub> )	(C <sub>12</sub> )	(C <sub>13</sub> )	(C <sub>14</sub> )	(C <sub>15</sub> )	(C <sub>16</sub> )	(C <sub>17</sub> )	(C <sub>18</sub> )	(C <sub>19</sub> )	(C <sub>20</sub> )	
39167A	4	1350	640.80	7.08	6.33	4.46	9.29	27.16	467.96	4.0600	98	1	1	1	1	20.28	19.31					
39167B	4	1350	421.00	3.48	1.80	2.34	4.40	15.12	388.72	2.3744	99	0	0	0	0	19.18	13.54					
39167C	4	1750	374.80	3.01	1.27	1.53	4.98	10.79	533.59	1.8425	98	1	0	0	1	28.12	16.41					
39167D	4	1850	481.20	2.30	1.03	1.41	5.00	9.40	501.00	1.3979	99	0	0	0	1	23.12	16.91					
39168A	4	2150	972.00	2.30	1.03	1.28	4.13	8.74	980.74	0.8911	100	0	0	0	0	26.12	15.41					
39168B	4	2350	736.40	1.88	0.82	1.39	4.61	8.87	743.47	1.1893	99	0	0	0	1	22.10	16.91					
39168C	4	2550	1128.00	2.40	4.04	3.35	9.70	19.37	1147.37	1.7033	99	0	0	0	1	13.21	17.41					
39168D	4	2750	626.40	2.30	3.87	6.97	21.31	34.13	666.55	1.1899	99	0	1	1	3	7.10	20.41					
39168E	4	2800	1405.50	1.93	14.02	9.49	15.38	40.84	1446.34	2.8237	97	0	1	1	1	5.34	23.31					
39168F	4	2850	2028.00	4.68	14.47	8.48	13.84	43.44	2071.48	2.9900	97	0	1	1	1	11.39	20.31					
39168G	4	2900	1261.50	2.83	10.43	7.48	13.93	34.67	1296.17	2.6748	97	0	1	1	1	8.10	22.41					
39168H	4	2950	2100.00	4.78	13.07	8.36	13.80	42.21	2142.21	1.9704	98	0	1	1	1	11.36	20.31					
39168I	4	3150	2840.62	3.89	25.07	13.16	13.71	39.85	2900.47	2.0634	97	0	1	1	1	6.43	23.24					
39168J	4	3350	2784.37	4.14	38.77	22.10	14.84	32.55	2864.92	2.8794	97	0	1	1	1	10.48	23.24					
39168K	4	3400	790.50	2.00	15.51	12.46	10.49	40.54	831.04	4.8782	96	0	2	1	1	3.78	31.24					
39168L	4	3450	1375.50	2.18	14.88	11.76	9.86	38.60	1418.18	2.7388	97	0	1	1	1	4.40	30.24					
39168M	4	3500	2136.00	3.89	29.58	18.60	13.52	67.39	2203.39	1.0672	97	0	1	1	1	9.40	28.24					
39168N	4	3550	2427.50	10.22	33.58	19.34	12.56	75.75	2913.25	3.0140	98	0	1	1	0	14.43	28.19					
39168O	4	3600	2820.00	3.54	30.73	20.68	13.99	74.94	2900.94	2.5833	98	0	1	1	0	5.48	28.19					
39168P	4	3650	2730.00	5.60	40.42	24.23	14.50	84.91	2811.91	3.0164	97	0	1	1	1	7.47	28.19					
39168Q	4	3700	780.00	3.54	24.62	21.93	14.44	64.55	940.55	6.8630	97	0	3	2	2	3.39	30.22					
39168R	4	3750	950.40	3.01	31.81	30.40	14.43	82.25	1822.45	7.8448	98	0	3	2	2	4.30	37.22					
39170A	4	3800	510.00	2.12	23.31	28.40	13.36	64.43	874.43	11.2162	90	0	4	4	2	3.40	36.21					
39170B	4	3850	864.00	3.48	19.08	17.11	10.18	48.82	912.82	3.3482	98	0	2	3	1	5.28	35.21					
39170C	4	3900	900.00	3.19	36.94	30.28	14.56	84.97	986.97	6.8266	98	0	4	3	1	4.48	36.17					
39170D	4	3950	6778.12	1.12	20.29	20.15	24.77	184.32	4862.44	2.8474	98	0	1	1	0	10.50	28.19					
39170E	4	4000	2804.00	4.80	71.14	37.33	17.08	122.17	2730.17	4.8903	98	0	3	1	1	3.58	28.19					
39170F	4	4050	6147.93	9.80	102.60	47.82	20.71	182.98	6380.27	2.8120	97	0	2	1	1	3.58	28.19					
39170G	4	4100	1011.00	4.96	17.92	12.63	13.74	44.27	1080.27	4.6469	97	0	2	1	1	10.58	26.22					
39170H	4	4150	1326.87	4.97	18.81	10.04	11.13	44.03	1640.98	3.9870	97	0	1	1	1	3.48	23.22					
39170I	4	4200	3120.00	17.70	27.59	13.44	24.01	34.68	3204.68	2.8424	97	1	1	0	0	21.93	18.22					
39170J	4	4250	330.25	1.59	3.22	0.84	1.33	6.98	1.1846	99	0	1	0	0	1	23.40	13.19					
39170K	4	4400	301.75	33.28	15.66	11.33	20.35	80.64	1099.39	2.8018	97	1	1	0	1	42.19	14.22					
39170L	4	4450	1319.52	8.14	10.83	4.83	10.87	30.47	1356.00	2.6835	94	1	1	1	1	32.28	13.20					
39171A	4	4850	369.60	1.95	0.51	0.30	0.40	3.16	372.76	0.8476	99	1	0	0	0	62.10	9.13					
39171B	4	4850	562.80	3.72	2.12	0.86	2.07	8.77	371.57	1.3243	98	1	0	0	0	42.24	16.24					
39171C	4	4850	338.80	2.63	0.91	0.50	1.22	5.28	364.08	1.4302	99	1	0	0	0	51.17	9.23					
39171D	4	4850	448.40	2.20	1.15	0.46	2.15	4.06	471.64	1.2847	100	0	0	0	0	28.19	9.23					
39171E	4	4950	76.30	1.50	0.77	0.74	1.27	4.28	80.78	1.2983	94	2	1	1	2	33.10	17.30					
39171F	4	4950	381.60	2.68	0.74	1.00	2.28	7.27	388.87	2.0227	98	1	0	0	1	36.10	14.40					
39171G	4	4950	336.40	1.95	0.74	0.46	1.08	4.23	360.63	1.1729	99	1	0	0	1	46.17	11.20					
39171H	4	4950	277.30	3.12	0.45	0.40	0.79	4.16	281.66	1.6768	99	1	0	0	0	51.10	13.18					
39171I	4	4950	293.20	1.59	0.60	0.46	0.43	3.08	298.25	1.0325	99	1	0	0	0	52.10	15.18					
39171J	4	6050	227.00	1.24	1.01	1.23	1.35	4.83	301.83	1.6001	100	0	0	0	0	26.21	23.33					
39171K	4	6100	251.25	0.48	0.94	0.74	1.11	3.27	1.2848	1.2848	100	0	0	0	0	13.29	23.33					
39171L	4	6150	374.40	3.20	3.05	1.47	1.43	7.64	383.04	1.3886	98	1	1	0	0	30.27	23.21					
39171M	4	6200	246.75	0.62	1.32	1.12	1.30	4.36	251.11	1.7363	98	0	1	0	1	14.30	20.30					
39171N	4	6250	324.40	1.55	0.95	0.74	0.92	4.24	400.84	1.0377	100	0	0	0	0	34.28	17.22					
39171O	4	6300	585.00	0.71	1.03	0.74	0.66	3.14	582.14	0.3338	100	0	0	0	0	23.38	23.21					
39171P	4	6350	439.60	2.48	1.34	1.12	1.27	4.41	439.41	1.3991	99	1	0	0	0	30.28	17.20					
39171Q	4	6450	1240.00	4.60	0.89	1.12	1.27	7.88	1233.88	0.6274	100	0	0	0	0	39.11	14.16					
39171R	4	6450	439.60	2.48	1.34	1.12	1.27	4.41	439.41	1.3991	99	1	0	0	0	30.28	17.20					
39171S	4	6550	618.00	4.78	3.08	2.35	2.42	12.83	630.83	2.0337	99	1	0	0	0	37.26	20.19					
39171T	4	6750	416.40	2.12	2.21	2.55	2.84	8.96	484.34	2.3350	97	0	1	1	1	21.28	26.24					
39171U	4	6850	396.00	3.01	4.00	4.17	3.74	14.92	410.92	3.6308	96	1	1	1	1	20.27	28.23					
39171V	4	6950	518.40	2.48	2.89	2.98	2.62	10.97	528.37	2.0760	97	0	1	1	1	23.26	27.24					
39171W	4	7050	346.80	3.36	3.10	3.01	2.86	12.41	339.21	3.4346	96	1	1	1	1	27.26	26.24					
39171X	4	7150	384.00	4.42	3.04	2.79	2.80	13.09	409.05	3.1902	96	1	1	1	1	35.23	21.21					
39171Y	4	7250	396.00	3.13	4.43	4.18	4.13	13.09	414.09	4.3683	96	1	1	1	1	28.28	23.23					
39171Z	4	7350	428.40	4.18	9.28	9.11	10.20	34.49	464.43	7.0334	93	1	2	2	2	18.27	20.23					
39172A	4	7450	403.00	3.72	8.74	10.14	12.00	34.68	438.68	7.9091	93	1	2	2	3	11.23	20.23					
39172B	4	7550	271.80	2.68	4.33	5.26	6.40	18.84	280.04	4.9984	94	1	1	2	2	14.23	20.23					
39172C	4	7600	393.25	36.99	334.13	236.68	330.72	978.52	1331.77	9.4751	27	4	23	6	25	6.36	24.24					
39172D	4	7650	866.40	182.93	864.89	531.02	720.47	2293.01	2890.71	80.1938	20	3	31	10	20	7.38	24.24					
39172E	4	7700	873.00	323.68	1997.28	1083.26	1780.80	3187.02	6060.02	16.3941	16	3	34	18	20	6.39	21.34					
39172F	4	7750	2820.00	1783.84	3734.41	2112.36	3018.00	12787.88	13467.88	81.8923	18	11	27	14	20	14.44	17.22					
39172G	4	7800	1821.00	770.30	2911.10	1220.11	2104.44	6922.33	8743.33													

TABLE III

WELL 9/8-1 - SAMPLE DESCRIPTIONS OF "PICKED" CUTTINGS AND RESULTS OF GASOLINE AND TOTAL ORGANIC MATTER ANALYSES\*

Sample Depth (feet)	EPR Sample No.	Lithology of Analyzed Chips	GSA Color Code	Total Organic Matter (%)	C4-C7 Hydrocarbons (ppm)	Cyclohexane/Methylcyclopentane
1950	55157-L	Limestone; glauconitic, trace of pyrite	5YR 2/1	0.99	Trace	-
3050	55159-B	Limestone; pyritic and glauconitic	5YR 2/1	1.92	Trace	-
3400	-I	Limestone; argillaceous, glauconitic	5Y 2/1	1.60	0.97	1.74
3600	-M	Limestone; argillaceous, glauconitic, pyritic	5YR 2/1	1.67	1.16	1.56
3650	-N	Shale; silty, sandy, micaceous, pyritic	5Y 3/1	2.26	Trace	-
3700	-O1	Limestone; pyritic, glauconitic, argillaceous	N2	1.71	0.08	0.62
3700	-O2	Shale; calcareous, silty, pyritic, glauconitic, fossiliferous	5Y 6/1	1.60	0.13	0.76
3800	55160-A	Shale; silty, pyritic, slightly fossiliferous	5Y 2/1	1.54	1.14	1.66
4350	-K	Limestone; chalky, fossiliferous, slightly silty	5Y 3/1	0.35	0.99	1.78
4400	-L	Siltstone; pyritic, slightly fossiliferous	5YR 4/1	0.66	1.06	1.65
4800	55161-D	Limestone; fossiliferous	5YR 8/1	0.33	1.13	1.72
5100	-J	Limestone; fossiliferous	5Y 5/1	0.23	1.05	1.78
5700	55162-F	Shale; silty, pyritic	5Y 4/1	0.76	1.83	1.56
5950	-K	Shale; silty, glauconitic	5Y 3/1	1.92	0.19	0.70
6000	-L	Shale; silty, micaceous, slightly pyritic	5Y 2/1	1.96	1.57	1.10
6050	-M	Shale; silty, pyritic	5Y 3/1	1.92	0.62	1.00

\*Note: Lithologic descriptions by R. E. Hukill  
 Gasoline analyses by H. M. Fry  
 Total organic matter by T. D. Coleman

TABLE III (CONTINUED)

WELL 9/8-1 - SAMPLE DESCRIPTIONS OF "PICKED" CUTTINGS AND RESULTS OF GASOLINE AND TOTAL ORGANIC MATTER ANALYSES\*

Sample Depth (feet)	EPR Sample No.	Lithology of Analyzed Chips	GSA Color Code	Total Organic Matter (%)	Cl <sub>4</sub> -C <sub>7</sub> Hydrocarbons (ppm)	Cyclohexane/Methylcyclopentane
6100	55162-N	Shale; silty, slightly pyritic	5Y 3/1	1.46	1.59	1.21
6150	-O	Shale; silty, micaceous, pyritic, glauconitic	5GY 3/1	1.27	0.14	1.40
6200	-P	Shale; silty, slightly pyritic	5Y 3/1	1.22	1.08	1.23
6250	55163-A	Shale; silty, calcareous, micaceous, pyritic, glauconitic	5Y 2/1	7.28	21.0	0.15
6300	-B	Shale; slightly silty and pyritic	5YR 2/1	6.73	19.1	0.16
6350	-C	Shale; silty, calcareous, micaceous, pyritic, glauconitic	5Y 2/1	7.44	19.3	0.37
6400	-D	Shale; slightly silty and pyritic	5YR 2/1	6.25	12.4	0.25
6450	-E	Shale; silty, calcareous, micaceous, pyritic, glauconitic, coal laminae	5Y 4/1	5.72	5.51	0.33
6700	-J	Shale; silty, sandy, slightly micaceous (red beds)	10R 2/4	0.33	0.96	1.84
7000	-O	Shale, silty	5Y 2/1-6/1	0.63	1.33	1.48
7100	-Q	Mudstone; silty, calcareous, slightly pyritic	10YR 4/2	0.47	18.9	1.14

\*Note: Lithologic descriptions by R. E. Hukill  
 Gasoline analyses by H. M. Fry  
 Total organic matter by T. D. Coleman

TABLE IV

VISUAL KEROGEN CHARACTERISTICS OF 9/8-1 SAMPLES  
(DESCRIBED BY J. L. MORCAN)

Sample Depth, feet	EPR Sample No.	Alteration	Types of Material*		
			Predominant	Secondary	Other
1950	55157-L	2	-	A	H
3050	55159-B	2	-	-	A
3400	-I	2	A	H	
3600	-M	2	A	H	
3650	-N	2	A	W	
3700	-O1	2	W	H	
3700	-O2	2	A	C	W
3800	55160-A	2	A	H	F
4350	-K	2	H	A	
4400	-L	2	H	A	
4800	55161-D	2	A	Al	
5100	-J	2	W	A	C
5700	55162-F	2	C	W	H, true A
5950	-K	2	A	C	
6000	-L	2	A	W	C
6050	-M	2	A	W	C
6100	-N	1+	F	W	C
6150	-O	1	A	C	
6200	-P	1	C	W	H, true A
6250	55163-A	1	A	C	
6300	-B	1+	A	F	W
6350	-C	2	A	W	
6400	-D	2	A	F	C
6450	-E	2	H	C	W
6700	-J	2	A	H	
7000	-O	2	F	W	A,C
7100	-Q	2+	Resin-like substance	W	A,C

- \*A - Amorphous  
 Al - Algal Debris  
 F - Finely Disseminated Debris  
 H - Herbaceous  
 W - Woody  
 C - Coaly

TABLE V

WELL 16/9-1 - SAMPLE DESCRIPTIONS OF "PICKED" CUTTINGS AND RESULTS OF GASOLINE AND TOTAL ORGANIC MATTER ANALYSES\*

Sample Depth (feet)	EPR Sample No.	Lithology of Analyzed Chips	GSA Color Code	Total Organic Matter (%)	C4-C7 Hydrocarbons (ppm)	Cyclohexane/Methylcyclopentane
1950	55167-M	Claystone; silty, slightly calcareous	5GY 5/1	0.87	2.07	1.56
3950	55170-D	Limestone; argillaceous	5Y 3/1	0.87	0.91	1.61
4150	55170-H	Shale; silty, slightly pyritic and glauconitic	5Y 5/1	0.92	1.26	1.84
4200	-I	Claystone; calcareous (marl)	5Y 6/1	0.87	Trace (< 0.1)	-
4250	-J	Claystone; finely micaceous	5Y 5/1-6/1	3.17	0.52	5.45
4850	55171-D	Shale; glauconitic, fossiliferous, slightly calcareous and pyritic	5Y 3/1	0.26	0.95	1.59
5650	-O	Limestone; chalky, slightly fossiliferous	10YR 8/2	0.09	1.22	1.64
6100	55172-H	Chalk and chalky pellet limestone	N9	0.34	Trace (< 0.1)	-
6450	-N	Shale; silty, micaceous	5Y 3/1	1.04	1.59	2.17
6950	55173-H	Shale; slightly silty and pyritic	5Y 2/1	1.88	1.14	1.61
7550	55174-D	Shale; slightly calcareous, silty, and pyritic	5Y 2/1	1.04	1.07	1.90
7600	-E	Claystone; moderately calcareous	N4	1.56	0.40	0.26
7650	-F	Shale; slightly silty, calcareous, and pyritic	5Y 2/1	0.78	1.51	0.77
7700	-G	Shale	N3	6.28	38.0	0.13
7700	-W	Shale; calcareous (marl)	N5	1.43	2.04	0.17
7750	-H	Shale; slightly silty	5YR 3/1	9.99	314.0	0.12
7800	-I	Shale; very calcareous (marl)	N4	0.95	1.59	0.17
7800	-X	Shale	N2	13.13	195.0	0.12

\*Note: Lithologic descriptions by R. E. Hukill  
 Gasoline analyses by H. M. Fry  
 Total organic matter by T. D. Coleman

TABLE V (CONTINUED)

WELL 16/9-1 - SAMPLE DESCRIPTIONS OF "PICKED" CUTTINGS AND RESULTS OF GASOLINE AND TOTAL ORGANIC MATTER ANALYSES\*

Sample Depth (feet)	EPR Sample No.	Lithology of Analyzed Chips	GSA Color Code	Total Organic Matter (%)	C4-C7 Hydrocarbons (ppm)	Cyclohexane/Methylcyclopentane
8250	55175-B	Shale, trace of pyrite	5YR 2/1	7.87	99.6	0.12
8950	-P	Shale, as above	5YR 2/1	8.04	121.0	0.12
9450	55176-J	Shale, slightly calcareous and silty; pyritic	5Y 3/1	1.14	1.16	1.00
10,250	55177-J	Shale, slightly calcareous and silty; pyritic	5Y 4/1	.48	0.92	1.43
10,550	-P	Shale; silty, pyritic	5Y 2/1	7.80	113.0	0.10
11,100	55178-K	Claystone, siltstone, sandstone (red beds)	10YR 4/2 5YR 4/1	0.40	0.08	1.11
11,150	-L	Shale; silty (red beds)	5R 3/2	0.43	0.88	1.50
11,200	-M	Claystone	N4	5.31	109.0	0.12
11,250	-N	Shale	5Y 2/1	6.34	92.5	0.16
11,300	55178-O	Shale	N3-N4	-	107.0	0.10
11,350	-P	Shale	5Y 2/1	6.70	111.0	0.12
11,400	55179-A	Shale	5YR 2/1-3/1	-	112.0	0.10
11,450	-B	Shale; calcareous, slightly silty, pyritic, trace of glauconite	5Y 4/1	0.92	1.51	0.59
11,985	-M	Limestone; slightly silty, trace of pyrite	5Y 2/1	0.54	7.52	0.84

\*Note: Lithologic descriptions by R. E. Hukill  
 Gasoline analyses by H. M. Fry  
 Total organic matter by T. D. Coleman

TABLE VI

VISUAL KEROGEN CHARACTERISTICS OF 16/9-1 SAMPLES  
(DESCRIBED BY J. L. MORGAN)

Sample Depth, feet	EPR Sample No.	Alteration	Types of Material*		
			Predominant	Secondary	Other
1950	55167-M	1	A	H	W
3950	55170-D	2	A	H	
4150	-H	2	A	W	
4200	-I	2	A	W	
4250	-J	2	A	W	
4850	55171-D	2	C	W	H
5650	-O	1	C	Al	
6100	55172-H	2	C	A	
6450	-N	2	W	C	
6950	55173-H	2+	W	C	
7550	55174-D	2+	W	C	H
7600	-E	2	A	C	
7650	-F	2	A	W,C	
7700	-G	2	A	W	C
7700	-W	2	A	C	W
7750	-H	2	A	W	C,Al
7800	-I	2	A,C	W	
7800	-X	2	A	C	
8250	55175-B	2	A	W	C,Al
8950	-P	2	A	Al	W
9450	55176-J	2+	W	C	A,Al
10,250	55177-J	2	C	W	H
10,550	-P	2	A	F	W,C,Al
11,100	55178-K	2	A	C	
11,150	-L	2	-	A,C	
11,200	-M	2	A	-	W,C
11,250	-N	2	A	H	Al
11,350	55178-P	2	A	W	Al
11,450	-B	2	C	H	A,W
11,985	-M	2	W	H	

\*A - Amorphous  
F - Finely Disseminated  
Al - Algal  
H - Herbaceous  
W - Woody  
C - Coaly