## III 10. DRILLING FLUID SUMMERY



		CASING IN	TERVAL		
Well: Casing: Bit:	6507/3-1 20" 26"	Operator: From/to: From/to:	Statoil 392,0 m 456,0 m	881,0 m - 900,0 m	·
Quantity:	Material:	· · · · · · · · · · · ·	Units:	Unit Price:	Total Cost NOK:
87 387	Barite CMC HV		ton 25 kg	700,00 290,00	60 900,00 112 230,00
	VOLUME	m3			1 010,00
		Total Cost f	or Interval:		173 130,00
		Cost per me	eter	A <b>R</b> 11 4 .	389,93
Days:	4	Cost per m	3:		171.42

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				CASING INT	ERVAL		
Well: Casing: Bit:		65) 13 17	07/3-1 3/8" 1/2"	Operator: From/to: From/to:	Statoil 392,0 m 900,0 m	1846,0 m 1860,0 m	
Quantity:			Material:	······	Units:	Unit Price:	Total Cost NOK:
	199 224 84 148 19 14		Barite Propol SL Propol Reg Gypsum Caustic Soda Probio II	a m3	ton 25 kg 25 kg 40 kg 25 kg 25 l	700,00 506,00 55,00 85,00 485,00	139 300,00 113 344,00 42 504,00 8 140,00 1 615,00 6 790,00
				Total Cost fo	r Interval:		311 693,00
				Cost per me	ter	<del>.</del>	324,68
Days:	·	7	, -	Cost per m3	• • . • • • • • • • • • • • • • • • • •		429,92



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CASING INTERVAL						
Well: Casing: Bit:	650 9 5 12	07/3-1 /8" 1/4"	Operator: From/to: From/to:	Statoil 392,0 m 1860,0 m	a 3168,0 m a 3183,0 m	
Quantity:		Material:		Units:	Unit Price:	Total Cost NOK:
1146 516 255 51 24 57 33 40 46		Barite Propol SL Gypsum Caustic Sod Probio II Sodium Bica Lime Propol reg. Wyoming Be	a arbonate entonite m3	ton 25 kg 40 kg 25 kg 25 l 25 kg 25 kg 25 kg 25 kg	700,00 506,00 55,00 85,00 485,00 485,00 43,75 506,00 76,00	802 200,00 261 096,00 14 025,00 4 335,00 11 640,00 4 560,00 1 443,75 20 240,00 3 496,00
			Total Cost fo	r Interval:	<u>.</u>	1 123 035,75
			Cost per me	ter		848,86
Days:	19	-	Cost per m3		<u> </u>	965,64

CASING INTERVAL							
Well: Casing: Bit:	6507/3-1 7" Liner 8 1/2"	Operator: From/to: From/to:	Statoil 392,0 m 3183,0 m	3953,0 m 3974,0 m			
Quantity:	Material:		Units:	Unit Price:	Total Cost NOK:		
1136 289 286 218 633 213 43 34 5 1 230 197 8 230 197 8 237 8 237 8 237 8 237 5 9	Barite Lignite Caus Prothin Caustic Sod Proseal Miltemp Bentonite W Prodefoam Proplug F Soda Ash Gypsum Prothin C Imcospot Pipelax Propol SL Propol SL Propol reg Probio II Kemseal Sodium Bica Lime	atic yom.	ton 25 kg 25 kg 25 kg 25 kg 50 lb ton 25 l 25 kg 25 kg	700,00 100,00 90,00 85,00 2 360,00 2 360,00 2 000,00 768,00 120,00 55,00 90,00 580,00 8 250,00 506,00 506,00 485,00 2 400,00 80,00 43,75	$\begin{array}{c} 795\ 200,00\\ 28\ 900,00\\ 25\ 740,00\\ 18\ 530,00\\ 262\ 695,00\\ 502\ 680,00\\ 86\ 000,00\\ 26\ 112,00\\ 600,00\\ 120,00\\ 110,00\\ 20\ 700,00\\ 114\ 260,00\\ 66\ 000,00\\ 119\ 922,00\\ 4\ 048,00\\ 16\ 490,00\\ 621\ 600,00\\ 10\ 320,00\\ 218,75\end{array}$		
6 17	Diaseal M Bentonite	•	40 lb 25 kg	448,64 60,00	2 691,84 1 020,00		
	VOLUME	m3 Total Cost f	or Interval:		1 646,00 <u>2 723 9</u> 57,59		
		Cost per me	eter	····	3 443,69		
Days: 52 Cost per m3: 1 654							

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			CASING IN	TERVAL		
Well: Casing: Bit:	650 Tes	7/3-1 ting	Operator: From/to: From/to:	Statoil		
Quantity:		Material:		·Units:	Unit Price:	Total Cost NOK:
375 9 5 24 33 22 29 6 95 10 16 35 3		Barite Propol reg Kemseal Prothin Bentonite Miltemp Bentonite W Prodefoam Sodium Bica Probio II Caustic Sod Nutplug C/F Zinc Carbor	yom. arbonate la ate m3	ton 25 kg 50 lb 25 kg 25 kg 50 lb ton 25 kg 25 kg 25 kg 25 kg 25 kg	700,00 506,00 2 400,00 90,00 2 360,00 2 000,00 768,00 80,00 485,00 120,00 425,00	262 500,00 4 554,00 12 000,00 2 160,00 2 508,00 51 920,00 4 608,00 7 600,00 4 850,00 1 360,00 1 275,00 149,00
· ·			<u>Total Cost f</u> Cost per me	or Interval:		417 535,00
Days:	47		Cost per ma	3:		2 802,25

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			MUD VOLUME :	SUMMARY				
WELL: RIG:	6507/3-1 Ross Rig		OPERATOR:	Statoil		<u></u>	<u> </u>	<b>.</b> .
Section:	36"	26*	17 1/2"	12 1/4"	8 1/2"	6* Tes	ling	1
Hole from (m)	392	456	900	1860	3183	3974		
Hole to [m]	456	900	1860	3183	3974	4757		
Hole length [m]	64	444	960	1323	791	783		
Mud Type	Bentonite	CMC	Gyp/polymer	Gyp/polymer	Gel/Ligno.	Kemseal/Pac/Milter	np.	
Vol buildt	48	1010	725	1163	1646	536	149	
Vol transfered from external	120	0	0	0	0	0	C	
Vol transfered to external	0	0	0	0	0	0	145	
Vol behind casing [m3]	0	0	23	107	0	0	276	Squeezed/left in hol
Vol dumped	134	970	251	798	1035	351	250	
Vol lost to formation	0	0	0	83	12	0	27	
Vol lost on solids equipment	0	0	157	249	305	121	103	
Vol transferred to next interval	34,0	74,0	368,0	294,0	588,0	652	C	)
Vol cuttings drilled (cub. m)	42,0	152,0	149,0	101,0	29,0	14,3	0	
TOTALS								, ,
mud buildt	5277,0		total buildt	5277				.
mud dumped	3789,0		total dumped	4724				
mud lost to formation	122,0	t	otal left in hole	528				4
mud lost on solids cont.	935,0							
mud behind csg	130,0							
mud left in hole	276,0							
total mud left in hole	406,0							
total vol cuttings drilled	487,3							



### 4.2 <u>Repeat Formation Testing</u>

A total of 3 RFT run were performed in the well. All RFT runs were done before the well was sidetracked.

A total of 42 pressure measurements were attempted during the RFT logging. 7 pressure points indicated good/very good permeability, 2 points demonstrated fair/low permeability and 2 points poor permeability. Seal failure/supercharge occurred in 8 attempts while 3 measurements showed a tight formation. In as many as 19 attempts the tool was not able to get any seal to the formation.

The only sampling obtained was in RFT run 3c in the Garn formation at 3610 m RKB. The 2 3/4 gallon chamber was emptied offshore, containing gas and some condensate. The 1 gallon chamber was sent onshore for laboratory analysis, but was lost during transfer in the laboratory. Data from 2 3/4 gallon chamber:

Fill up time : 18 minutes Opening pressure : 145 bar.

Recovery : 2.05 m3 gas and 1.69 litres of condensate/ mudfiltrate. Density mudfiltrate : 1.00 g/cm3 Density condensate : 0.79 g/cm3 Amount CO2 : 0.5 % Amount H2S : none

Approximately gas composition:

C1 : 84.7 % C2 : 9.3 % C3 : 4.3 % IC4: 0.7 % NC4: 1.0 %

Opening pressure 1 gallon chamber 145 bar.

Fill up time: 32 min Recovery: Lost in laboratory.

# 4.3.4 DST No. 2

**Objectives:** 

- Confirm movable hydrocarbons.
- Receive good reservoir samples for analyses.
- Pressure and temperature measurements.
- Determine permeability and productivity of the perforated interval.

Perforation interval: 3690 - 3724 m RKB.

The test was performed by using of the following test string:

- 3.5" tubing in a 7" liner
- Downhole tester valve
- 4 pressure gauges in gauge carriers
- Tubing conveyed perforation, 12 shot/foot

### Test performance

The well was perforated underbalance using drillwater as cushion with a differential pressure of approximately 10000 kPa.

The well was perforated with the choke manifold open on a 25.4 mm choke to surge tank. There was little response of flow.

After 7 hours and 21 minutes the well was shut-in. The cumulative production was measured to approximately 550 litres. One buildup period was performed before the well was opened to run bottom hole samplers. Three bottom hole samplers were run. The bottom hole sampling was done with three PSTE sampler types at three different depths. The depths were 3636.6, 3639.1 and 3641.6 m RKB. The bottom hole pressure and temperature during sampling were 36379.4 kPa and 131.0 Deg.C. Some oil and gas was trapped between the LPR-N and the APR-M values.

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Analysis of the gas samples from Sta
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	PSTE	PSTE
Component	TS-19-12	TS-20-12
N2	0	8.41
CO2	0	4.80
C1	54.64	57.66
C2	20.42	12.01
C3	6.81	8.09
IC4	4.7	1.59
NC4	3.32	2.82
IC5	2.90	0.95
NC5	0.92	1.00
SUM C6/NC6	2.14/0.27	0.95/0.37
SUM C7/NC7	2.91/0.09	1.01/0.12
SUM C8/NC8	1.41/0.05	0.54/0.03
SUM C9/NC9	0.05	0.05/0.004
SUM CIO+		0.004
TOTAL	100.22	99.88

TS-20-12: MW = 21.182 g/mol and a density of 0.731 (Air=1.0).

Analyses of the oil and the gas trapped between the LPR-N and the APR-M valves from Schlumberger:

Component	<u>011</u>	<u>Gas</u>
N2	0	4.00
CO2	0	1.52
C1	0	75.21
C2	0.05	10.05
C3	0.63	6.00
IC4	0.0	1.68
NC4	0.33	1.93
IC5	1.73	0.00
NC5	1.43	0.00
C6	0.57	0.12
C7+	95.26	0.08
Total	100.00	100.59

The oil was heated to 50 Deg. C.

•	oil	gas
Density	0.858 g/cc at 30 Deg.C	0.740 (air=1.0)
Viscosity	795 cp at 40 Deg.C	
Avg. molar mass	278.4 g/mol	21.4 g/mol

### 4.3.5 DST No. 3

**Objectives:** 

- Receive good reservoir samples for analyses.
- Pressure and temperature measurements.
- Determine permeability and productivity of the perforated interval.

Perforation interval: 3611 - 3636 m RKB.

The test was performed by using of the following test string:

- 3.5" tubing in a 7" liner
- Downhole tester valve
- 4 pressure gauges in gauge carriers
- Tubing conveyed perforation, 12 shot/foot

#### Test performance

The well was perforated underbalance using drillwater as cushion with a differential pressure of approximately 10000 kPa.

The following flow and shut-in periods were performed:

Clean-up flow	:	378	min.
Clean-up buildup	:	575	min.
Main flow	:	816	min.
Main buildup	:	1247	min.
Multirate flow	:	364	min.
Multirate buildup	:	722	min.

Figure 4.3.1 shows the test performance. Three out of four gauges performed well during the test.

TIME	WELL	HEAD	CONDEN	NSATE	G2	AS	GOR	H2S	C02
	PRESS	TEMP	RATE	GRAV.	RATE	GRAV.	6m2 /		
hh:mm	Bar	DegC	Sm3	g/cc	1000	air=1	Sm3/ Sm3	ppm	8
Clear	up f	Low w	th 12	7 mm	(12/64	4") fi:	ked cl	<u>loke</u>	1
14:30	295.0	44.0	-	0.783	575	0.710	-		0
15:00	295.5	46.0	181.4	0.799	593	0.710	3038	-	-
16:00	296.5	49.0	196.4	0.799	591	0.710	3011	5.5	4.5
17:00	296.5	53.0	169.4	0.803	590	0.715	3483	-	-
18:00	292.4	54.0	186.7	0.806	588	0.715	3152	-	-
End c	<u>lean u</u> r	<u>flo</u>	ž i		1	I		I. 1	1
11.10	90							-	
03:30	129.5	7.0	0	-	O	-	-	-	-
Main 1	flow pe	eriod.	with :	<u>19.05 1</u>	<u>nm (48</u>	<u>3/64")</u>	choke	2	1
07:30	236.0	62.0	301.6	0.792	811	0.705	2689	-	-
09:00	240.0	67.0	282.3	0.795	864	0.720	3062	5.5	3.2
11:00	241.2	71.0	277.0	0.798	763	0.710	2752	5.0	3.0
14:00	220.5	73.0	293.2	-	913	0.715	3112	4.6	1.4
16:00	221.5	74.5	276.7	0.803	915	0.714	3309	3.8	4.0
17:00	221.0	74.5	290.0	0.802	905	0.715	3120	3.9	3.6
End ma	ain flo	<u>pw per</u>	riod			1	t i		
18:00	358.0								
23:30	352.5								
12.10	90								
13:55	349.0								
Multi	rate f	low pe	eriod v	vith 1:	2.7 mi	<u>n (32/6</u>	5 <u>4") (</u>	<u>choke</u>	
15:00	292.0	36.0	204.0	0.794	627	0.710	3060	10	2.6
15:45	298.5	51.0	193.4	0.799	613	0.715	3170	-	-
Multi	rate f	low pe	eriod v	vith 19	9.05 r	<u>nm (48</u>	(64")	chol	<u>ce</u>
17:15	218.5	69.5	281.7	0.799	962	0.723	3288	6.0	3.0
17:45	219.5	71.0	282.7	0.808	880	0.721	3112	-	-
Multi	rate f	low pe	eriod v	vith 2	5.4 mi	<u>n (64/6</u>	<u>54") (</u>	hoke	
19:00	149.5	74.0	307.8	0.799	1076	0.724	3496	-	-
19:30	150.0	75.0	308.4	0.829	1076	0.720	3489	5.0	2.3
20:15	<u>Close</u>	chole	<u>e manif</u>	<u>fold.</u>	PR-N	not cl	Losed		
13.10	90								
08:00	349.0								
End D	ST No.	3							

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### <u>Test analysis</u>

Data from the Halliburton gauge no. 10119 is used in the test analyses.

The test analyses are performed on the build up periods from the Clean-up flow, Main flow and the Multirate flow periods.

The test is evaluated as a gas test. The semilog data is reached.

Analyses	Pressure P (kPa)			Perm. k (md)	Skin S	Build-up Period
	Gauge P*	Reservo	ir P			
Horner	47024	47459	*	96.4	3.88	Clean-up
Horner	46966	47400	*	92.3	4.14	Main
Horner	46982	47417	*	90.1	2.26	Multirate

Gauge 10119 sensing depth: 3568.11 m RKB

\* Reservoir pressure P is calculated to mid perforations with a fluid density of 0.8 g/cc.

Figure 4.3.2 shows the rate history used in the analyses. Figure 4.3.3, 4.3.4 and 4.3.5 shows the Log-Log Buildup, Horner Buildup and the Horner Analysis plot.

The results from the Clean-up shut in period give the best results because the LPR-N tester valve failed during the Main and the Multirate shut in periods.