

2.4.4 RFT Measurements

Formation pressures were measured in the Cretaceous using the Schlumberger RFT tool. The data is listed in Table 2.7. In figure 2.3 the pressures are plotted versus depth. As the data show, some points were tight and could not be used.

The upper zone between 3445 and 3471m RKB has a gas gradient of 0.4 psi/m. In the deeper zone between 3525 and 3541m RKB a water gradient of 1.54 psi/m is indicated. This gradient is less reliable due to few points of measurement and some spreading in the values.

The two zones mentioned seem to belong to different pressure systems.

In Table 2.8, the RFT pressure readings in the Jurassic Sandstones are listed.

Table 2.7 : RFT Pressure Measurements, Lower Cretaceous.
WELL 35/3 - 4

DEPTH	NUMBER	HYDROSTATIC	DRAWDOWN	FORMATION	REMARKS
3446	2	7187	4792	5093	
3449.5	3	7193	4938	5090	
3451.5	4	7198	5040	5091	
3456.5	5	7210	5025	5092	
3465	6	7228	5063	5095	
3467.5	23	7210 ⁺	5005	5097	+ Test made coming up, may affect repeatability still building when retract
3469.8	22	7215 ⁺	0	5125	
3483.8	12	7263 ⁺	5311	7088	
3484.2	13	7265 ⁺	4800	7092	
3486.3	14	7268 ⁺	0	5231	
3489	7	7280	83	5390	
3491	8	7279	10	26	Tight
3491.3	9	7280	0	0	Tight
3492.5	11	7283	0	0	Tight
3493	10	7283	0	0	Tight
3501	15	7300	0	0	Tight
3506	16	7312	0	0	Tight
3527	17	7356	2860	5291	
3531.5	18	7364	1459	5299	
3535.5	21	7362 ⁺	0	5315	
3538.5	19	7380	681	5719	Still building when retract
3548.7	20	7401	0	0	Tight

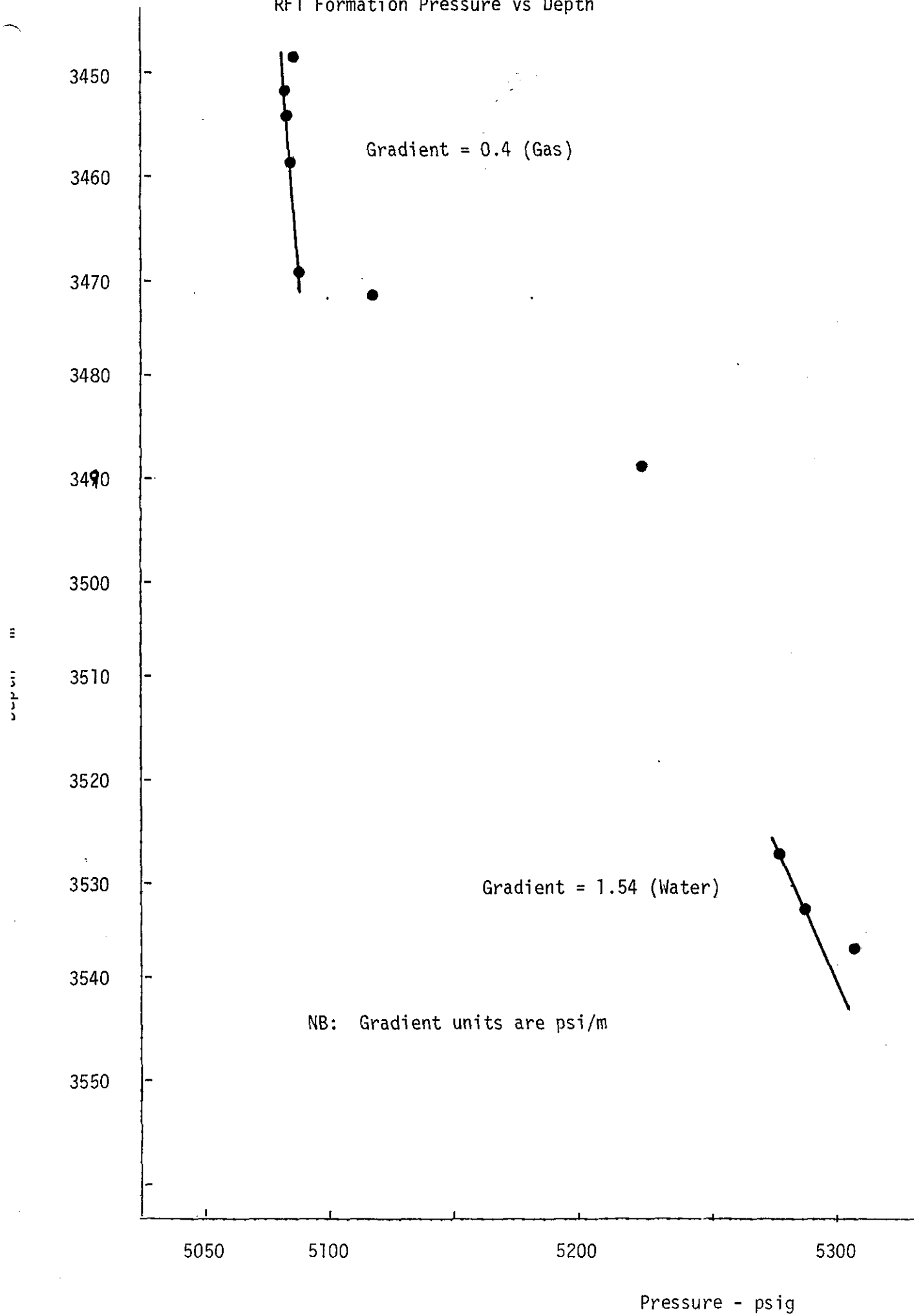
+ The Formation Pressure is Temperature Compensated.

TABLE 2.8 RFT PRESSURE MEASUREMENTS, JURASSIC
WELL 35 / 3 - 4

Depth	Formation (psi)	Remarks
3859.5		No seal
3859.0		Tight
3859.3	6148	No seal
3860.0		Sampling point
3862.0		No seal
3861.8		No seal
3869.5		No seal
3872.5		No seal
3872.5		Tight
3874.0	6941	No permeability, super charge
3873.0		Tight
3875.5	6395	
3877.0		Tight
3877.0		Tight
3876.5		Tight
3877.5	6410	
3874.5		Tight

+ The Formation Pressure is Temperature Compensated.

RFT Formation Pressure vs Depth



2.4.5 . DST MEASUREMENTS

35/3-4 DST-1 SUMMARY AND DISCUSSION OF RESULTS

1. Test interval

The lower Cretaceous sandstone was perforated with 4" csg. guns (4SPF) over the following interval:

3488,50 - 3495,00

3498,25 - 3503,25

3504,50 - 3507,75

Depths are in mBRT ref. ISF/SONIC Run 3B.

2. Flow and Shut-in periods

The well was opened for appx. 10 minutes for initial flow followed by initial p.b.u of 134 minutes.

Due to no indications of flow during first period it was decided to attempt injection into the formation. After bullheading into formation the N₂ backpressure was bled off to start the main flow period. The wellhead pressure was decreased to atmospheric pressure with no indications of flow. While observing the well, the APR-M valve inadvertently sheared. Mud from annulus U-tubed into D.P. and pushed cushion and a small amount of h.c. gas to surface. This concluded the flow test and the final p.b.u. of 197 minutes was recorded during reversing out.

3. Fluid production

No rates were measured since production was not established.

4. Fluid sampling

Four one litre water samples were taken as the well was reversed out.

On site analysis as follows:

<u>Sample</u>	<u>Cl⁻</u>	<u>Ca⁺⁺</u>	<u>Mg⁺⁺</u>
1	19000	400	543
2	19000	240	243
3	8000	280	437
4	15000	240	583
Mud filtrate	9000	280	0
Sea water	18500	240	720
Fresh water	500	40	50

Gas samples were taken for on site analysis only. Exlog's chromatograph gave the following composition:

C ₁	90,5%
C ₂	5,4%
C ₃	2,6%
iC ₄	0,5%
nC ₄	0,8%
C ₅	0,2%

There was no trace of H₂S.

5. Interpretation of Pressure data

The Horner plot from the initial build-up based on Sperry Sun gauge No. 0121 shows the extrapolated pressure $p^* = 5375$ psig and a slope of 795 psi/log cycle. The gauge was set at 3469 mBRT. The Horner plot from the second build-up period shows a continuous curvature upwards indicating that the well has not been shut-in long enough.

No value for kh has been determined since no good estimates for flow rates exist.

35/3-4 DST-2 SUMMARY AND DISCUSSION OF RESULTS

1. Test interval

The lower Cretaceous sandstone was perforated with 4" csg. guns (4SPF) over the following interval:

3445,00 - 3447,50

3449,25 - 3453,50

3454,50 - 3459,50

3464,00 - 3471,50

Depths are in mBRT ref. ISF/SONIC Run 3B.

2. Flow and Shut in Periods

Prior to opening the well, it had been established during the pressure testing of the well that the APR-N valve leaked when pressurized from above. Despite of this, it was decided to go ahead with the test. The well was flowed for a 7 minute initial flow period and the shut-in for a 84 minute initial shut-in. An increase of 25 psi was observed in 2 minutes at the well head after opening the APR-N tester valve, prior to opening the choke manifold, indicating the APR-N valve to be open.

While trying to open the APR-N tester valve for the first main flow period, the APR-M circulating valve sheared at 2000 psig, aborting the test. The APR-M valve was set to shear at 2400 psig annulus pressure.

3. Fluid Production

There was no trace of gas while reverse circulating the string.

4. Fluid Sampling

2 samples of the fluid reversed out through the drill pipe was taken. The analysis of the fluid indicates that it was water cushion.

5. Pressure data.

The APR-N valve appears to have leaked during the whole test and the pressure data does not seem to be valid. The report from Sperry Sun is not available yet, but will be distributed as soon as it is received.

5/3-4 DST-2A SUMMARY AND DISCUSSION OF RESULTS

1. Test interval

The lower Cretaceous sandstone was perforated with 4" csg. gun (4SPF) over the following interval:

3445,00 - 3447,50

3449,25 - 3453,50

3454,50 - 3459,50

3464,00 - 3471,50

Depths are in mBRT ref. ISF/SONIC Run 3B. The interval was perforated prior to DST-2.

2. Flow and Shut-in Periods

The well was flowed for 6 minutes initial flow and then shut-in for 63 minutes initial build-up. The well was then opened up for the first main flow period on a 32/64" choke for 3 hrs and 47 min before flowing through a 36/64" fixed choke for the remaining part of the first main flow period, 13 hrs 12 min.

The well was then shut-in for 16 hrs and 28 min. Wellhead pressure increased to 3840 psig during the first hour of shut-in, indicating that the downhole APR-N tester valve did not close.

When the down hole valve was "opened" for the second main flow period, no increase in wellhead pressure was observed while keeping choke manifold closed.

The choke manifold was then opened and due to hydrate problems the well was flowed at a high rate initially to warm up the well. After 3 hrs and 45 min the well was stabilized on a 24/64" fixed choke and flowed at this setting for 13 hrs and 5 minutes.

The well was then shut-in by shearing the APR-M circulating valve to

ensure proper bottom hole shut-in. The well was shut in for 16 hrs and 30 min before the packer was released.

3. Fluid production

The well flowed gas during the first main flow period at 24.30 MMSCF/D on a 36/64" choke and a flowing wellhead pressure of 3055 psig. The corresponding condensate flow rate was 528 B/D.

The last gas rate measured during the second main flow period was 12.63 MMSCF/D on a 24/64" choke and a flowing well head pressure of 3584 psig. The corresponding condensate flow rate was 326 B/D.

The gas gravity was 0.62 (air = 1) and condensate gravity was 50.3 °API.

4. Fluid sampling

Three sets of gas and condensate samples for recombination were taken under separator conditions during each of the two main flow periods.

Samples of water and condensate from the separator were also taken under atmospheric conditions.

5. Interpretation

The reservoir encountered in 35/3-2 is thought to be very close to its dew point. The reservoir penetrated by 35/3-4 is in a different pressure regime showing the two reservoirs to be different. From the current data it is difficult to say if the 35/3-4 reservoir is close to its dew point or not. This may be clarified by the PVT analysis. The preliminary pressure analysis presented is based on Sperry Sun gauge No. 0124 located at 3424.6 mBRT.

The extrapolated pressure, p^* , for the initial flow, from the Horner plot is 5067 psig.

The build-up period following the first main flow period was analyzed by regular Horner plot. A log-log plot of p vs t shows that the pressures after about 100 minutes are not affected by wellbore storage and can be used for traditional build-up analysis. The extrapolated pressure p^* was 5025 psig and the slope m was 118 psi/log cycle. This gives a permeability of 14.5 md and no skin using net thickness of 46 ft.

The build-up period following the second main flow period was analyzed by using the principle of superposition. Extrapolated pressure, p^* , was 5025 psig and the slope, m , was 88 psi/log cycle. This gives a permeability of 9.1 md and a skin of -2.7.

The skin was less for the lower flow rate as expected considering turbulence. The possible effect of any liquid condensation in the formation on skin and permeability will be evaluated when the PVT data are available.

3.4.4

Ta

Mud recap 35/3-3

Casing interval		Total	30"	20"			
Material	Unit Weight	Quantity	Quantity	Quantity			
Milbar	L/T	407		407			
Wyoming Bentonite	50 kg	1986	968	1018			
Milgel	50 kg	1227	120	1107			
Soda Ash	50 kg	9	2	7			
Bicarb. of Soda	50 kg	10	10				
Caustic Soda	25 kg	107	15	92			
Gypsum	50 kg	21	21				
Driscopac.Reg	50 lbs	2		2			
CMC HiVis	25 kg	8		8			
Milfree	55 gal	4		4			
Milspot	50 lbs	73		73			

Mud recap 35/3-4

Casing interval		Total	30"	20"	13 3/8"	9 5/8"	8 1/2" hole & testing
Material	Unit Weight	Quantity	Quantity	Quantity	Quantity	Quantity	Quantity
Barite	M Ton	2.447,92		466,3	1.077,2	626	278,42
Wyoming Bentonite	50 kg	1.941	345	1.095	141	360	
Milgel	50 kg	4.473	95	1.056	2.402	530	390
Caustic Soda	25 kg	706	12	60	276	338	20
Soda Ash	50 kg	12	1		7		4
Milmica fine	25 kg	158	35		123		
Milmica coarse	25 kg	153	30		123		
Unical	25 kg	2.277		11	1.365	705	196
Drispac S/L	50 lbs	394			171	117	106
Drispac Reg	50 lbs	113			33	79	1
CMC HiVis	25 kg	52			36		16
CMC LoVis	25 kg	65			24	12	29
Gypsum	50 kg	454			454		
EML	55 gal	73			73		
MD-detergent	55 gal	6			6		
Bicarbonate	50 kg	48			25	8	15
Milfibre	40 lbs	20			20		
LD-8	5 gal	14			5	9	
Lime	50 kg	12			12		
Milplug fine	25 kg	58			58		
Milplug coarse	25 kg	38			38		
Lubrisal	55 gal	24				22	2
Ammonium Nitr	25 kg	5				5	



COMPANY Saga Petroleum A/S
WELL NO. 35/ 3-4
FIELD Block 35/ 3
DATE May 5, 1981 thru May 28, 1981

JUL 1981

BAKER EASTERN, S. A.

4056 TANANGER, NORWAY
TELEX: 856-33173
PHONE: 0459664/96520



BAKER PRODUCTION SERVICES NORWAY A.S.

REPLY TO:
4056 Tananger, Norway
Telephone: (04) 696790-696836
Warehouse: (04) 696628-696822
Telex : 40360 BPS N

Saga Petroleum A/S
Postbox 5021

4001 STAVANGER

June 19, 1981
kh/117/RT

Dear Sirs,

Attached are the results of your drillstem tests. 1, 2, 2A conducted on your well 35/3-4 from May 5 - to May 28, 1981.

Arrived on board Byford Dolphin May 5, 1981. Set up equipment pressure test all surface equipment and wait on completion of well.

On May 18, 1981 drillstring was run in with test tools to test interval 3488.5 - 3495, 3498.25 - 3503.25, 3504.5 - 3507.75 for D.S.T. No. 1. All surface equipment and down hole test string was pressure test to 5000 psi with nitrogen, at which time APR-N valve was open and well would not flow.

On May 21, 1981 drillstring was again run in with test tool to conduct a test on interval 3445 - 3453, 3454.5 - 3459.5, 3464 - 3471.5 metres for D.S.T. No. 2. Due to failure of down hole tools this test was concluded on May 23, 1981 with no flow being registred.

On May 24, 1981 drillingstring and test tools were run in to test interval 3445 - 3453, 3454.50 - 3459.5, 3464 - 3471.5 metres for D.S.T. No. 2A. A.P.R.N. valve was open at 21:12 May 24, 1981 for initial flow period. Shutting for one hour and then reopened for a clean up rate of 5 $\frac{1}{2}$ hours, at which time a twelve hour rate was conducted, and well was shut in for 16 hours and 18 minutes. Valve was open for flow period No.2. Because of low well head temperatures well was flowed for 3 $\frac{1}{2}$ hours at a approx. rate of 25 - 30 mmcf/d to raise wellhead temperature. Flow was then cut back to 12.5 mmcf/d.

May 26, 1981 at 10.33. Flow was switched through separator for 12 $\frac{1}{2}$ hours and then shut in for 15 $\frac{1}{2}$ hours for buildups.

The gas flow rates was calculated in accordance with AGA Method No.3 using a pressure and temperature base of 14.73 psi. and 60 degrees F respectfully.

If there are any queries regarding this report, please do not hesitate to contact us.

Very Truly yours,


R. Tiessen

Baker Production Services Norway A/S



COMPANY Saga Petroleum A/S
WELL NAME 35/3-4
FIELD Block 35/3 TEST INTERVAL _____
COUNTRY Norway
BAKER TECHNICIAN Richard Tiessen

*Report
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**NOTE: THE SECTIONS APPEARING IN THIS REPORT
ARE INDICATED BY A CROSS**

*Operations
Log*

2





COMPANY Saga Petroleum
 WELL NAME 35/3 - 4
 FIELD Block 35/3 TEST INTERVAL 3488.5-3495
3498.25-3503.25
3504.5-3507.75
 COUNTRY Norway
 BAKER TECHNICIAN Richard Tiesson

*Operations
Log*

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DATE & TIME	OPERATIONS LOG
17/5/81 22:00	Schlumberger R.I.H. to perforate
23:51	" perforate 3497 Metres to 3507 metres at 4 shots per foot
18/5/71 01:30	Schlumberger R.I.H. to perforate
03:05	" perforate 3488 metres to 3497 metres
07:19	R.T. 7. Temperature recorder, recording section no 8731,66° - 388°, inner housing no 30337, 120 hour clock no F2171, clock wound and stylus on, recorder at 3476.02 m.
07:23	R.P.G.3. Pressure recorder, recording section no 35020,0 - 10000 P.S.I., inner housing no 32273, 180 hour clock no H 12059 with double pitch lead screw, clock wound and stylus on recorder at 3476.02m
07:28	R.P.G. Pressure Recorder, recording section no 36671, 0 - 10000 psi, inner housing no 35272, 120 hour clock no F 2159 with double pitch lead screw, clock wound and stylus on at 3476,02 M
07:41	Gauges R.I.H. with Sperrysun Hanger
23:30	Rig Up Choke Manifolds
19/5/81 00:20	Flush surface lines, heater choke pressure tested to 5000 Psi
00:49	Pressure test O.K.
01:10	Pressure test surface equipment
03:55	Pressure Test O.K.
09:20	Well Opened on 28/64 adjustable choke
09:25	Well S.I. for 1 Hour build up
10:37	Commence series of pumping Nø2 - to establish infection rate into formation
15:00	Open well on 52/64 adjustable choke



COMPANY _____
 WELL NAME _____
 FIELD _____ TEST INTERVAL _____
 COUNTRY _____
 BAKER TECHNICIAN _____

*Operations
Log*

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**DATE
&
TIME**

OPERATIONS LOG

19/5/81 15:15	Switch to 3" bypass (192/64)
15:16	Sheared APR - M Circulating valve
15:20	Reduce choke to 24/64
15:33	Gas to surface
15:38	Flare ignited
15:50	Well shut in at choke manifold
16:00	Well opened 24/64 adjustable choke
16:02	Choke increased to 64/64
16:04	Flow through 3" bypass (192/64)
16:26	S.I.W. at choke manifold
16:36	Open 3" bypass to overboard (192/64)
16:42	S.I.W. at choke manifold, end of test no 1, commence reverse circulation and pulling out of hole
20/5/81	
04:55	Records out of well. Removed & Read charts
	Completion of DST no 1. Commencement of DST no. 2
21/5/81 19:00	Schlumberger commence perforation programme
01:08	Schlumberger complete perforation programme
06:11	Amerada's run in hole for DST no. 2



COMPANY _____
 WELL NAME _____
 FIELD _____ TEST INTERVAL _____
 COUNTRY _____
 BAKER TECHNICIAN _____

*Operations
 Log*
 continuation form

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DATE & TIME	OPERATIONS LOG
22/5/81 22:15	Rig up surface lines
22:35	Preasure test surface lines
23:10	Preasure test OK
23/5/81 02:27	Halliburton A.P.R.N. tool opened for initial flow period
02:28	Open adjustable choke to 20/64
02:33	Close adjustable choke, and Halliburton A.P.R.N. tool, finishing 5 minutes initial flow.
03:58	Re - open A.P.R.N. tool
04:01	Open adjustable choke to 32/64.
04:33	Fluid to surface, Halliburton A.P.R.N. tool sheared off.
04:37	Commence reversing out of hole.
04:45	Switch flow to 3" bypass.
05:00	Well shut in at surface, surface equipment rigged down, commence circulating
13:37	Amerada's out of hole
13:43	Stylus of Element no. 32347
13:49	Stylus of Element no. 9080
13:52	Stylus of Element no. 36670
24/5/81 00:15	Amerada's run in hole for DST no. 2A
03:32	Commence monitoring preasure testing of A.P.R.N. tool
03:50	Preasure testing of A.P.R.N. completed
14:25	Rig up surface lines for DST no. 2A
14:50	Commence preasure testing surface lines and equipment to 5000 P.S.I.
15:36	Preasure testing programme completed



COMPANY _____
 WELL NAME _____
 FIELD _____ TEST INTERVAL _____
 COUNTRY _____
 BAKER TECHNICIAN _____

**Operations
Log**

continuation form

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DATE & TIME	OPERATIONS LOG
24/5/81 15:47	Dowell commence preassure testing string to 5000 PST with N2
17:15	Dowell stop pumping
18:43	Dowell start pumping again
20:38	Dowell complete pumping to 5000 PST
20:58	Commence bleeding off preassure overboard after preassure test, through variable choke
21:19	Preassure bled off
21:12	Open A.P.R.N. tool
21:13	Open choke to 20/64 adjustable
21:18	Shut in choke and A.P.R.N. tool
22:20	Preassure up to open A.P.R.N. tool
22:23	Well open on 32/64 adjustable choke
23:03	Switch flow through heater
25/5/81 00:35	Switch flow through 32/64 fixed bean choke
02:00	Switch flow through 32/64 adjustable choke
02:01	Switch flow through 36/64 fixed bean choke
02:46	Switch flow through separator
07:15	Switch flare to opposite boom
15:22	Shut in A.P.R.N. valve
15:25	Shut in A.P.R.N. choke manifold, commence monitoring surface build up
26/5/81 07:40	Open well on 20/64 fixed bean choke for rate no. 2
07:42	Shut in to repair leaking chicksan
07:50	Open well for 20/64 fixed bean choke
08:30	Switch flow to 36/64 adjustable choke



COMPANY _____
WELL NAME _____
FIELD _____ TEST INTERVAL _____
COUNTRY _____
BAKER TECHNICIAN _____

*Operations
Log*
completion form
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DATE & TIME	OPERATIONS LOG
26/5/81 09:15	Reduce choke to 32/64
09:31	Reduce choke to 28/64
09:45	Reduce choke to 24/64
10:00	Reduce choke to 20/64
10:15	Switch flow to 20/64 fixed bean choke
10:33	Switch flow through separator
11:07	Switch flow through 20/64 adjustable
11:15	Switch flow through 24/64 fixed bean choke
16:44	Switch flare to opposite boom
27/5/81 00:20	Well shut in at choke manifold, end of DST no. 2A
00:21	shear - A.P.R. - M valve and reverse circulate
00:49	Mud to surface
00:49 to 04:00	Rig out surface equipment

*Well
Test
Report*

3



Well Test Report Continuation Form

TIME DATA		CHOKE SIZE 64THS. INCH	SUBSURFACE		WELLHEAD DATA			AMBI- ENT TEMP. °F	SEPARATOR		SAMPLES			GAS FLOW RATE MMSCFD	OIL FLOW RATE BBL/DAY	WATER FLOW RATE BBL/DAY	GAS OIL RATIO CF/BBL	CHLORIDE PPM
DATE & TIME HOURS	ELAPSED TIME		PRESSURE PSI	TEMP. °F	TUBING PRESS. PSI	TEMP. °F	CASING PRESS. PSI		PRESSURE PSI	TEMP. °F	GRAVITY		BS&W %					
										OIL °API	GAS SP. GR.							
19/5	81																	
1342		S.I.			5575													
1344		"			5565													
1346		"			5560													
1348		"			5561													
1350		"			5555													
1354		"			5640													
1358		"			5840													
1402		"			6030													
1405		"			6270													
1409		"			6330													
1409		"			6435													
1415		"			6395													
1420		"			6385													
1425		"			6373													
1427																		
1500		52			0													
1515		192			0													
1518		"			900													

Re - commence pumping N2

Stop pumping N2

Commence bleeding pressure down to zero overboard through variable choke.

Flowing well 53/64 adjustable choke, small blow at surface

Flow well through 3" bypass, annulus pressure zero.

Fluid to surface, sample taken

Well Test Report Continuation Form

TIME DATA		CHOKES SIZE 64THS. INCH	SUBSURFACE		WELLHEAD DATA			AMBI- ENT TEMP. °F	SEPARATOR		SAMPLES			GAS FLOW RATE MMSCFD	OIL FLOW RATE BBL/DAY	WATER FLOW RATE BBL/DAY	GAS OIL RATIO CF/BBL	CHLORIDE PPM
DATE & TIME HOURS	ELAPSED TIME		PRESSURE PSI	TEMP. °F	TUBING PRESS. PSI	TEMP. °F	CASING PRESS. PSI		PRESS./RE PSI	TEMP. °F	GRAVITY		BS&W %					
											OIL °API	GAS SP. GR.						
1975.81																		
1610		192						*	indicating communication between the two.									
1615		"			190													
1626		S.I.			0				Shut in well at choke manifold.									
1630		"							pressure up to 2500 P.S.I. with rig pumps (prior to reverse circulation)									
1636		192							Open on bypass to overboard.									
1642		S.I.							Shut in well at choke manifold, rig down									
									surface equipment									
									END OF TEST No. 1									

