

R.F.T. RESULTS					31/4 - 7
No.	Depth. (mRKB)	P.H.I. psia	P.F. psia	P.H.A. psia	Perm/remarks
<b>RUN 3 A</b>					
1/3A	2030	3834.8	3097.8	3835.2	Supercharged
2/3A	2031.5	3837.8	3092.8	3837.9	Low perm
3/3A	2033.7	3842.0	3098.2	3842.3	Low perm.
4/3A	2030	3835.4	3097.8	3835.4	Supercharged
5/3A	2035.5	3846	—	3846.2	Tight
6/3A	2035.2	3845	—	3845.3	Tight
7/3A	2036.5	3845.9	—	3846.4	Tight
8/3A	2038.7	3849.9	—	3850.5	Tight
9/3A	2045.5	3862.9	3129.5	3863	V. poor perm.
10/3A	2048.5	3868.4	—	3868.7	Tight
11/3A	2120	4001.7	3191.3	4002.4	Poor perm.
12/3A	2031.5	3837.1	3092.8	3836.1	Segr. sample
Attempted segregated sample at 2031.5 m: Lost seal after 1 minute and recovered 5.7 litre mud filtrate and thin oil film from 2 <sup>3</sup> / <sub>4</sub> gal chamber.					
<b>RUN 3 B</b>					
1/3B	2031.2	3834.0	3092.7	3834.2	Low perm/lost seal
2/3B	2030.5	3832.6	—	3832.8	Tight
3/3B	2030	3831.4	—	3831.9	Tight
4/3B	2031	3833.8	—	3833.8	Tight
5/3B	2033.7	3838.5	—	3838.5	Tight
6/3B	2031.5	3834.6	—	3834.5	Seal failure
<b>RUN 4 C</b>					
1/4C	2030	3987.2	3098.9	3988.0	Supercharged
2/4 C	2031.5	3990.9	3094.2	3991.0	Low perm.
3/4 C	2033.7	3995.4	—	3995.7	Tight
4/4 C	2035.5	3998.8	—	3999.0	Tight
5/4 C	2045.5	4017.9	3135.4	4018.5	V. poor perm
6/4 C	2120	4162.2	3198.3	4162.8	Poor perm.
7/4 C	2237	4387.6	3308.3	4387.9	Good perm.
8/4 C	2243.7	4401.2	3318.0	4401.6	V. good perm.
9/4 C	2247.8	4409.6	3324.3	4409.5	Fair perm.
10/4 C	2391.2	4685.3	3549.8	4685.0	Fair perm.
11/4 C	2393.7	4690.6	3551.8	4690.5	V. good perm.
12/4 C	2396	4695.5	3554.3	4695.8	V. good perm.
13/4 C	2397.7	4698.8	3556.0	4698.7	V. good perm.
14/4 C	2400.5	4703.6	3558.8	4703.5	V. good perm.
15/4 C	2406.5	4715.3	3564.8	4715.0	V. good perm.
16/4 C	2417	4736.0	3580.6	4736.2	V. good perm.
17/4 C	2429	4758.6	3597.5	4758.8	V. good perm.
18/4 C	2436.5	4773.3	3608.3	4773.2	V. good perm.
19/4 C	2458.2	4815.0	3639.9	4815.2	V. good perm.
20/4 C	2490.5	4877.4	3686.9	4877.8	V. good perm.
21/4 C	2031.5	3991.3	—	3991.8	Attempted sample. seal failure.
22/4 C	2031.5	3991.7	—	3991.8	Seal failure.
<b>RUN 4 D</b>					
1/4 D	2396	4697.2	3554.7	4697.6	Segr. sample - aborted.
2/4 D	2395.7	4696.7	3554.3	4696.8	
Took segregated sample at 2395.7 m and recovered 7.3 oil, 275 l gas and 1.7 l mud filtrate.					

# DST RESULTS

# 31/4 - 7

## DST 1

Perforated interval	:	2389.9 - 2397.9 m (RKB)
Choke size	:	40/64"
Oil flow rate	:	4300 BOPD
Oil gravity	:	0.83 g/cm <sup>3</sup>
Gas flow rate	:	0.88 - 10 <sup>6</sup> scf/d
Gas gravity	:	0.775 (air = 1)
GOR	:	205 scf/bbl
CO <sub>2</sub>	:	0.25%
H <sub>2</sub> S	:	0
BSW	:	0.25%
Wellhead pressure	:	725 psia

## DST 2

Perforated interval	:	2028.5 - 2039.5 m (RKB)
Choke size	:	32/64"
Gas flow rate	:	0.95 . 10 <sup>6</sup> scf/d
Gas gravity	:	0.77 (air = 1)
Condensate flow rate	:	Not measureable
Condensate gravity	:	0.75 g/cm <sup>3</sup>
CO <sub>2</sub>	:	Trace - 0.5%
H <sub>2</sub> S	:	0
BSW	:	—
Wellhead pressure	:	175 psia.

6.4 Mud report36" Hole Section:  
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This section was drilled from 161 m to 248 m using seawater and high viscosity pills pumped on each connection. Before running the 30" casing, 56 m<sup>3</sup> of high viscosity mud was circulated into the well. The casing was run and cemented without problems.

26" Holesection:  
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This section was drilled using the same technique as for the 36" hole section. At TD of the 17 1/2" pilot hole, 15.9 m<sup>3</sup> of high viscosity mud was circulated through the hole before a wipertrip was made. Before logging, the 17 1/2" hole was displaced with totally 111m<sup>3</sup> of the same high viscosity mud.

The 17 1/2" hole was then underreamed to 26" using seawater and high viscosity pills pumped whenever necessary. At TD, 15,9 m<sup>3</sup> of high viscosity mud was circulated through the well before the hole was displaced with 159 m<sup>3</sup> of the same mud.

Before running casing a 26" bit was run in hole. Tight spots were seen at 525 m and 581 m.

Before pulling out of the hole 95.4 m<sup>3</sup> of high viscosity mud was circulated into the hole. The casing was run and cemented without problems.

## 17 1/2" Hole Section

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This section was drilled using a KCL-polymer drilling fluid which was displaced into the hole before the cement was drilled out. A leakoff test was performed to 1.80 SG. During drilling to 1367m the mudweight was gradually increased to 1.20 SG. A survey was dropped and the bit pulled. Tight hole with max. overpull of 700 KN was seen from 1367m to 1000m.

When running back in hole the sections from 1120 m to 1135m, 1228m to 1243m and 1367m to 1490m were reamed and washed.

During drilling to 1496m the mudweight was increased to 1.29 SG.

When reaching 1528 m a 8 m<sup>3</sup> high viscosity pill was circulated around before a 10 stands wiper trip was made.

Tight hole was seen from 1446m to 1371m.

During drilling to 1671m the mudweight was increased to 1.34 SG.

Another wipertrips was made to 1471m. Tight hole were seen from 1598m to 1570m, 1551m to 1522m with max. overpull of 266 KN.

New hole was drilled down to 1816m. At this depth 8 m<sup>3</sup> of high viscosity mud was circulated around before a multishot survey was dropped and the bit pulled out to the 20" shoe. Tight hole was seen from 1800 m to 1656 m with max. overpull of 625 KN.

When running back in hole, the hole was reamed from 1675 m to 1720 m and from 1800m to 1816 m.

At this depth 8 m<sup>3</sup> of high viscosity mud was pumped around. During this circulation the mudweight was increased to 1.40 SG. Cavings were seen.

The hole was logged without problems.

Before running casing a wipertrip was made.

The casing was run and cemented without problem.

Interval discussion, conclusion and recommendation:  
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The problems seen when drilling the 17 1/2" hole section is believed to be caused by plastic flow of the claystone into the well. The tight hole seen was cured by reaming and increased the mudweight. At TD the mudweight was increased to 1.40 SG. This seemed to be enough to allow the hole to be logged and the casing run without problem.

12 1/4" Hole section  
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The 12 1/4" section was drilled using a special designed drilling fluid to prevent formation damage and ensure good log quality.

It contained:

NaCl Salt (60 000 mg/L),

Polyanionic Cellulose,

Starch.

XC- Polymer.

During the first days of drilling, only minor problems were seen. These problems were mainly reaming and washing and fill on the bottom.

After increasing the YP up to 10 to 15 Pa the problems disappeared. Except for these, few or none other problems were seen during drilling, logging or running casing.



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			Date.850201													
((				Daily mud properties												
(oo)																
-----	Well.....: 31/4-7															
Norsk	Mud Contractor...: Int. Dr. Fluid															
Hydro																3!
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Date	Mid.	Mud	PV	YP	GEL	GEL	Ph	100psi	HP/HT	Cl-	Alkalinity	Ca++	Oil	Sol	H2O	V.G. meter at 115AF						MUD
depth	dens.				0	10					Pf	Pb	Mf			1600	300	200	100	6	3	TYPE
(m)	(r.d)	cps	m	Palm	Palm	Pa	(cc)	(cc)	mg/l		mg/l	%	%	%	%	rpm	rpm	rpm	rpm	rpm	rpm	
840907	12385	11.16	15	15	6	11	9.516		150000	.20			12	18	90							NaCl/POLYMER
840908	12024	11.15	9	11	8	11	9.818.5		150000	.25	1.32		12	10	88							SALT+POLYMER
840909	12024	11.15	10	10	7	10	1019.2		146000	.15			11	10	89							SALT+POLYMER
840910	1205	11.15	15	15	11	14	1019.8		146000	.20			11	10	89							SALT+POLYMER
840911	1205	11.17													100							SALT+POLYMER

TABLE B-5

## MUD MATERIAL CONSUMPTION

<u>Material</u>	<u>Quantity</u>	<u>Unit/Weight</u>
Barite	415	M/t
Bentonite	97	M/t
Caustic Soda	27	25 kg/sx
Soda Ash	46	50 kg/sx
NaCl	1033	50 kg/sx
KCl	1858	50 kg/sx
Lime	7	40 kg/sx
SM (x)	13	25 kg/sx
Idbond	60	25 kg/sx
FLR-100	242	25 kg/sx
Idvis	138	25 kg/sx
Idflo	151	25 kg/sx
Idcide L	38	25 kg/sx
CMC	40	25 kg/sx
Drispac R	4	25 kg/sx
Defoamer	2	Drums