



Continental Shelf Institute

**Institutt for  
kontinentalsokkelundersøkelser**

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| Source rock analyses of well 31/4-2 |           |
| CONTRACTOR                          |           |
| Norsk Hydro                         |           |
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| SCIENTIST<br>M. Bjørøy, T.M. Rønningsland, J.O. Vigran | DATE               | PROJECT NO.<br>0-233                   |
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|  |                    | RESPONSIBLE SCIENTIST<br>Malvin Bjørøy |

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## KEY WORDS

Source rock

## SUMMARY

Based on the various analyses the analysed sequence is given the following rating.

- A: 1400 - 1810 m: Immature, poor potential as a source rock for oil and gas.
- B: 1810 - 1975 m: Immature, poor potential as a source rock for gas.
- C: 1975 - 2125 m: As zone B.
- D: 2125 - 2325 m: Immature, good potential as a source rock for oil and gas. Probably migrated HC in lower part of the zone.
- E: 2325 - 2475 m: Immature, good potential as a source rock for oil and gas.
- F: 2475 - 2625 m: Moderate mature, good potential as a source rock for oil and gas.
- G: 2675 - 2685 m: Moderate mature. Claystone has a good potential as a source rock for gas.
- H: 2685 - 2770 m: Moderate mature. Upper part as zone G, lower part has a good potential as a source rock for oil and gas.
- I: 2770 - 2900 m: Moderate mature. Claystone has a poor potential as a source rock for gas.

## EXPERIMENTAL

One ml. of the headspace gas from each of the cans was analysed gas chromatographically for light hydrocarbons. The results are shown in Table Ia. The canned samples were washed with tempered water on a 0.125 mm sieve to remove drilling mud and thereafter dried at 35<sup>0</sup>C.

### Total Organic Carbon (TOC)

The various selected samples were crushed on a centrifugal mill and sieved. The portions with a particle size between 0.125 mm and 0.063 mm were used in the further work. Aliquotes of the samples were treated with hot 6N HCl to remove carbonate and washed twice with distilled water to remove traces of HCl, then placed in a vacuum oven at 50<sup>0</sup>C, evacuated to 20 mm Hg for 12 hrs. The samples were then analysed on a Leco E C 12 carbon determinator, to determine the total organic carbon (TOC).

### Extractable Organic Matter (EOM)

From the TOC results samples were selected for extraction. Of the selected samples, approximately 100 gm of each was extracted on soxhlet apparatus for 48 hrs using dichloromethane (DCM) as solvent. The DCM used as solvent was distilled in an all glass apparatus to remove contaminants. The paper thimbles used in the soxhlet apparatus were previously washed with DCM on a large soxhlet apparatus for 48 hrs. to remove any soluble components.

Activated copper foil was used in the flasks to remove any free sulphur from the samples.

After extraction, the solvent was removed on a Buchi Rotavapor and transferred to a 50 ml flask. The rest of the solvent was then removed and the amount of extractable organic matter (EOM) determined.

#### Chromatographic Separation

The extractable organic matter (EOM) was separated on chromatographic columns, packed with silica, Riedel & Hähn, 0.063 mm, using the slurry method with hexane as solvent. On top of the silica, small amounts of alumina, approximately 2 cm, was added. The EOM, after it was "taken up" on alumina, was transferred to the top of the columns, which were then eluted with predistilled hexane, benzene and methanol using a ratio of 200 ml of each solvent pr. gm of EOM.

The various eluants were removed on a Buchi Rotavapor and the samples transferred to vials and dried at 40<sup>0</sup>C in a stream of dry nitrogen, and the amount of the various fractions, saturated, aromatic and NSO fraction (Nitrogen, Sulphur, Oxygen), determined. The saturated fractions were analysed gas chromatographically on a 25 m OV 101 glass capillary column with He as carrier gas (0.7 ml/min.) using the splitless injection technique. The glass capillary column was mounted in a Carlo Erba F V 2150 gas chromatograph.

#### Vitrinite Reflectance

Samples, taken at various intervals, were sent for vitrinite reflectance measurements at Geoconsultants, Newcastle-upon-Tyne. The samples were mounted in Bakelite resin blocks; care being taken during the setting of the plastic to avoid temperatures in excess of 100<sup>0</sup>C. The samples were then ground, initially on a diamond lap followed by two grades of corundum paper. All grinding and subsequent polishing stages in the preparation were carried out using isopropyl alcohol as lubricant, since water leads to the swelling and disintegration of the clay fraction of the samples.

Polishing of the samples was performed on Selvyt cloths using three grades of alumina, 5/20, 3/50 and Gamma, followed by careful cleaning of the surface.

Reflectance determinations were carried out on a Leitz M.P.V. microphotometer under oil immersion, R.I. 1.516 at a wavelength of 546 nm. The field measured was varied to suit the size of the organic particle, but was usually of the order of 2 micron diameter.

The surface of the polished block was searched by the operator for suitable areas of vitrinitic material in the sediment. The reflectance of the organic particle was determined relative to optical glass standards of known reflectance. Where possible, a minimum of twenty individual particles of vitrinite was measured, although in many cases this number could not be achieved.

#### Processing of Samples for Evaluation of Visual Kerogen

The rock samples were crushed and afterwards treated with hydrochloric and hydrofluoric acids to remove the minerals. A series of microscopic slides was mounted in glycerine jelly:

T-slide represents the total acid insoluble residue.

O-slide represents the residue screened through 15 sieves.

N-1,2,3 slides contain palynodebris remaining after flotation ( $Zn Br_2$ ) to remove disturbing heavy minerals.

X-1,2,3 slides contain oxidized residues, when oxidizing is required due to high coalification or much sapropel.

T & O slides are necessary to evaluate kerogen composition/palynofacies which is closely related to sample lithology.

Screened slides are normally required to concentrate the larger fragments, and to study palynomorphs (pollen, spores and dinoflagellates) for paleo-dating and colour evaluation.

So far visual evaluations of kerogen have been undertaken from residues mounted in glycerine jelly, and studied by Leitz Dialux in normal light (halogene) using x10 and x40 objectives.

Rock-Eval Pyrolyses

100 mg crushed sample was put into a boat whose bottom and cover are made of sintered steel and analysed on a Rock-Eval pyrolyser.

## RESULTS AND DISCUSSION

### Light hydrocarbons

On the basis of the light hydrocarbon results, the analysed sequence of the well will be divided into nine zones:

|                   |                               |
|-------------------|-------------------------------|
| A: 1400 - 1810 m  | <i>Coal. 2073-2146</i>        |
| B: 1810 - 1975 m  | <i>Kim. Cl. Fin 2146-2171</i> |
| C: 1975 - 2125 m  | <i>Heather Fin 2171-2325</i>  |
| D: 2125 - 2350 m  | <i>Bout Fin 2325-2353</i>     |
| E: 2350 - 2475 m  | <i>Dun. Fin 2353-2632</i>     |
| F: 2475 - 2625 m  | <i>Stafj. Fin 2632-2786</i>   |
| G: 2625 - 2685 m  | <i>Conn. Fin 2786-2900</i>    |
| H: 2685 - 2760 m  |                               |
| I: 2760 - 2900 m. |                               |

The analysis shows a large variation in abundance of light hydrocarbons, wetness of the gas and in the  $iC_4/n-C_4$  ratio throughout the analysed sequence.

A: 1400 - 1810 m: This zone shows a fair and good abundance of  $C_1 - C_4$  hydrocarbons, while the abundance of  $C_5 - C_7$  hydrocarbons is poor throughout the zone. The gas is dry throughout the whole zone while the  $iC_4/n-C_4$  ratio is very high. All this indicates an immature zone.

B: 1810 - 1975 m: At 1810 m the abundance of  $C_5 - C_7$  hydrocarbons shows a sharp increase and is found to be fair to good in this zone. The abundance of  $C_1 - C_4$  hydrocarbons and the wetness of the gas are similar to the zone above, while the  $iC_4/n-C_4$  ratio drops sharply. These changes occur in the same interval as coal is found, and this might be the reason for these changes.

C: 1975 - 2125 m: At 1975 m almost all parameters change compared with higher up in the well. Both the  $C_1 - C_4$  and  $C_5 - C_7$  hydrocarbon abundance drop to fair and poor abundances respectively. The wetness of the gas increases slowly throughout the zone, while the  $iC_4/n-C_4$  ratio shows a steady decrease. The lithological examination shows this zone to contain limestone, and this might be the reason for the decrease of light hydrocarbon abundance.

D: 2125 - 2350 m: At 2125 m a very sharp increase both in the  $C_1 - C_4$  and the  $C_5 - C_7$  abundance are found at the same level as a very sharp increase in the wetness of the gas. The zone contains a fair amount of coal and this is possibly the reason for these sharp changes.

E: 2350 - 2475 m: In the same manner as a sharp increase in the various parameters were found at 2125 m a similar decrease is seen at 2350 m. The abundance of  $C_1 - C_4$  hydrocarbons is relatively steady, showing a fair/good abundance while the abundance of the  $C_5 - C_7$  hydrocarbons is very erratic varying from poor to good. This could be due to a variation in the lithology in this zone.

F: 2475 - 2625 m: The abundance of  $C_1 - C_4$  hydrocarbons in this zone is similar to the zone above, while the wetness of the gas increases sharply, and the gas is found to be wet throughout the zone. The abundance of  $C_5 - C_7$  is poor at the top of the zone, increasing to good towards the lower part. This zone is found to contain a large amount of sandstone, and the large abundance of  $C_5 - C_7$  hydrocarbons together with the gas being very wet indicate that there might be migrated hydrocarbons in this zone.

G: 2625 - 2685 m: The results are very erratic in this zone, with some sampling showing high abundance of  $C_1 - C_4$  hydrocarbons, while others only show a fair abundance. The wetness of the gas is relatively constant, approximately 50 %, while the  $iC_4/n-C_4$  ratio vary considerably. The large variation found in this zone is probably due to the large variation of the lithology.

H: 2685 - 2760 m: Most of the parameters in this zone also vary considerably. The  $iC_4/n-C_4$  ratio is, however, constant and is found to be very high. The reason for the large variation in the abundance of light hydrocarbons is probably due to the variation in lithology.

G: 2760 - 2900 m: The  $iC_4/n-C_4$  ratio drops sharply at 2760 m at the same time as the abundance of  $C_1 - C_4$  hydrocarbons is found to level out, showing a fair abundance, and the wetness of the gas increases approximately 90 %. The abundance of the  $C_5 - C_7$  hydrocarbons increases with increasing depth and is found to show a fair abundance towards the lower part of the zone.



### Total Organic Carbon (TOC)

- A: The Toc values show a steady decrease with increasing depth in this zone from 2 % at 1450 m to 0.6 % at 1800 m.
- B: The TOC values level out in this zone at approximately 0.8 %, i.e. the whole zone is found to have a fair abundance of organic carbon.
- C: The TOC values of the claystone is fairly similar in this zone to the zone above, while the limestone is found to have TOC values at approximately 0.2 %.
- D: The TOC values increase sharply at the top of this zone compared to the zones above, then to decrease with increasing depth leveling out at approximately 1.3 % at 2300 m.
- E: The TOC values are rather erratic in this zone, but all the claystone samples are found to have a good or rich abundance of organic carbon.
- F: The upper part of this zone shows a steady increase of the TOC values with increasing depth, while the lower part of the zone vary considerably. This variation could be due to contamination from other lithologies. The upper half of the zone is found to have a good abundance of organic carbon, while the lower part has a rich abundance.
- G: Again a zone with considerable variation in the TOC values, but on the whole this zone has a good abundance of organic carbon.
- H: As the zone above.
- I: The TOC values drop sharply at 2700 m, and the whole zone is found to have a fair abundance of organic carbon.

### Extraction and Chromatographic Separation

Zone A: Three samples from this zone, 1495 - 1510, 1660-75 and 1750-65 m, where extracted. Samples 1495 - 1510 m and 1660-75 m have very poor abundances

of extractable hydrocarbons, while the sample from 1750-65 m has a good abundance. The gas chromatograms of the saturated hydrocarbon fractions vary considerably on various areas for the two samples. The sample from 1495 - 1510 m has an unidentified peak between  $n\text{-C}_{19}$  and  $n\text{-C}_{20}$ . A peak in this region has been found in various samples from the North Sea earlier and is believed to be a diterpane. The pristane peak is considerably larger than both the  $n\text{-C}_{17}$  and the phytane peak giving large pristane/ $n\text{-C}_{17}$  and pristane/phytane ratios. The carbon preference index is, however, low for a tertiary sample, and the amount of heavy  $n$ -alkanes is low compared to the medium weight  $n$ -alkanes. The amount of steranes and triterpanes is also found to be relatively low. These results indicate an input of mainly marine origin under a non reducing environment condition.

The gas chromatogram of the saturated hydrocarbon fraction from sample 1660-75 m varies only slightly from the sample above. The most noticeable difference is the disappearance of the peak between  $n\text{-C}_{19}$  and  $n\text{-C}_{20}$ .

The gas chromatogram of the saturated hydrocarbon fraction of the sample from 1750-65 m does not show any sign of the peak between  $n\text{-C}_{19}$  and  $n\text{-C}_{20}$ , while  $n\text{-C}_{14}$  is very abundant compared to  $n\text{-C}_{13}$  and  $n\text{-C}_{15}$ . The pristane/ $n\text{-C}_{17}$  ratio is in the same magnitude of order as the sample above, while the pristane/phytane ratio is much larger. The CPI is much larger for this sample than for the sample above, and the sterane/triterpanes are very pronounced, indicating a larger input of terrestrial material than in the sample above, and a low maturity.

Zone B: Two samples from this zone, 1885 - 1900 m and 1945-60 m, were analysed, showing a poor and fair abundance of extractable hydrocarbons, respectively. The gas chromatogram of the saturated hydrocarbon fraction of the sample from 1885 -1900 m is very similar to the one from 1750-65 m in the zone above, except that the  $n\text{-C}_{14}$  is of a more normal abundance in this sample. The gas chromatogram of the saturated hydrocarbon fraction of the sample from 1945-60 m is very much different. The pristane/phytane ratio is almost equal to 1.0, and the steranes and triterpanes are very pronounced. The latter indicates an input of terrestrial material. The peak between  $n\text{-C}_{19}$  and  $n\text{-C}_{20}$ , seen in the sample from 1495 -1510 m is again recognized in this sample.

Zone C: One sample from this zone, 2035-50 m, was extracted, showing a poor abundance of extractable hydrocarbons. The gas chromatogram of the saturated hydrocarbon fraction shows the major peak to be the unknown peak between n-C<sub>19</sub> and n-C<sub>20</sub> found in earlier samples. The pristane/n-C<sub>17</sub> ratio has dropped slightly from the uppermost samples in this well, while the pristane/phytane ratio has dropped more. The CPI value is similar to those samples above, and the steranes/triterpanes are very pronounced.

Zone D: Four samples from this zone were extracted. The uppermost sample, 2155-70 m has a rich abundance of extractable hydrocarbons, while the three other samples have a good abundance of extractable hydrocarbons. The gas chromatograms of the saturated hydrocarbon fractions of the four samples vary slightly from sample to sample. The variation is mainly in the pristane - phytane area with a decrease in the pristane/n-C<sub>17</sub> ratio with increasing depth. One sample, 2200-75 m shows a larger variation than the others. In this sample the above mentioned peak between n-C<sub>17</sub> and n-C<sub>20</sub> is again very pronounced, and the CPI value is larger than in the other samples. The small variation seen in three samples is probably caused by a slight increase in maturation combined with small variations in the environments of deposition rather than a change in type of organic matter.

E: Two samples, 2380-95 m and 2455-70 m from this zone were extracted and are found to have a good and rich abundance of extractable hydrocarbons respectively. The gas chromatograms of the saturated hydrocarbon fractions of the two samples are very similar, with a large pristane/n-C<sub>17</sub> ratio and relatively high CPI values. They also show a large input of steranes and triterpanes, indicating terrestrial origin.

Zone F: Two samples, 2530-45 m, and 2590 - 2605 m, from this zone were extracted, both showing a good abundance of extractable hydrocarbons. The gas chromatograms of the saturated hydrocarbon fractions are very similar to those from the zone above.

Zone G: One sample, 2650-65 m, from this zone was extracted, showing a good abundance of extractable hydrocarbons. The saturated/aromatic ratio is much lower for this sample compared to those from the zone above, and the gas chromatogram of the saturated hydrocarbon fraction varies considerably. the pristane/n-C<sub>17</sub> and pristane/phytane ratios are much larger, and the

CPI value is also increased compared to those from the zone above. These changes are probably caused by a change both in the organic matter and the environment of deposition.

Zone H: No samples from this zone were extracted.

Zone I: One sample, 2860-75 m, was extracted showing a poor abundance of extractable hydrocarbons. The gas chromatogram of the saturated hydrocarbons shows a distinct maximum in the heavy n-alkane area, indicating an input of terrestrial material.

### Vitrinite Reflectance

Twenty samples were analysed for vitrinite reflectance. Together with the vitrinite reflectance data, other information is recorded. This is given for the individual samples in the following.

1450 m: Calcareous siltstone,  $R_o = 0.31(21)$ .

The sample has a low to moderate organic content. Bitumen wisps and wispy particles of vitrinite with about an equal proportion of reworked material and inertinite. UV light shows a yellow fluorescence from spores and a low exinite content.

1630 m: Calcareous shale,  $R_o = 0.37(8)$ .

The sample has a low organic content with variable bitumen staining. Very occasional particles, mostly of inertinite and reworked material. A few of poor vitrinite. UV light shows a yellow fluorescence from spores and a low exinite content.

1705 m: Calcareous shale and carbonate,  $R_o = 0.37(20)$ .

The sample has a low to moderate organic content, mostly bitumen wisps and staining. A few wisps and particles of vitrinite with subordinate inertinite and reworked material. UV light shows a yellow fluorescence from spores and a low exinite content.

1810 m: Shale and lignite,  $R_o = 0.30(23)$ .

The shale, which shows iron oxide staining, has very little bitumen, almost

wholly particles of inertinite and reworked material. The lignite contains normal vitrinite and resin globules, no inertinite. All the readings are on lignite. UV light shows a yellow/orange and light orange fluorescence from spores and a low to moderate exinite content.

1885 m: Calcareous shale and carbonate,  $R_o = 0.38$  (20).

The sample, which is rather pyritic, has a low to moderate organic content. Bitumen wisps with plentiful staining. A low content of vitrinite wispy particles and inertinite. UV light shows a yellow and light orange fluorescence from spores together with a low to moderate exinite content.

1960 m: Mixed shale lithologies,  $R_o = 0.37$ (4).

The sample has a low organic content, most cuttings are barren. A few contain bitumen wisps and particles of reworked material and inertinite. Only a trace of vitrinite wisps. UV light shows a yellow/orange fluorescence from spore specks and a trace of exinite.

2063 m: Calcareous sandstone,  $R_o = 0.40$ (3).

The organic material in this sample is restricted to occasional shaly wisps containing bitumen and iron oxide staining. A few particles of vitrinite and inertinite. UV light shows an overall carbonate fluorescence.

2126 m: Shale,  $R_o = 0.35$ (20).

The sample is moderate to rich in organic material, full of small particles of inertinite and reworked material. Only a low content of particles and wispy particles of vitrinite. Differentiation between reworked and true material is difficult, and this might have resulted in a slight elevation of values. UV light shows a light to mid-orange fluorescence from spores and a moderate exinite content.

2173 m: Shale and calcareous shale,  $R_o = 0.44$ (16).

The sample has a low to moderate organic content with variable bitumen staining. Particles of inertinite and reworked material are dominant. A few wispy particles and particles of vitrinite. UV light shows a light orange fluorescence from spores and a low exinite content.

2230 m: Siltstone,  $R_o = 0.31(20)$ .

The sample has a low organic content apart from an overall bitumen staining. a few particles of reworked material and inertinite, but mostly small particles and wisps of vitrinite. UV light shows a light and mid-orange fluorescence from spores and hydrocarbon traces together with a trace of exinite.

2290 m: Calcareous siltstone,  $R_o = 0.35(20)$ .

The sample has a low to moderate organic content with bitumen staining, good particles and wispy particles of vitrinite and only a trace of particles of inertinite. UV light shows a light orange fluorescence from spore fragments and a trace of exinite.

2348 m: Shale,  $R_o = 0.35(3)$ .

The sample is virtually barren with a few very high reflectance vitrinite, particles of inertinite and reworked material. Three particles of low reflectance vitrinite located. UV light shows a light orange fluorescence from spores and a trace of exinite.

2477 m: Calcareous, silty shale,  $R_o = 0.46(20)$ .

The sample has a low to moderate organic content with some good wisps and particles of vitrinite. About equal proportion of inertinite and low reflectance reworked material. Some bitumen wisps. UV light shows a light orange fluorescence from spores and a moderate exinite content.

2539 m: Calcareous siltstone,  $R_o = 0.37(20)$ .

The sample has a low organic content with bitumen staining. Particles of inertinite and reworked material are dominant, but good content of particles and wispy particles of vitrinite. UV light shows a mid orange fluorescence from spores and a moderate exinite content.

2598 m: Silty shale,  $R_o = 0.48(20)$ .

The sample has a moderate organic content with some good wisps and wispy particles of vitrinite, particles of inertinite and bitumen wisps. UV light shows a yellow to orange and mid-orange fluorescence from spores together with a moderate exinite content.

2686 m: Siltstone,  $R_o = 0.37(18)$ .

The sample showing an iron oxide staining, has a few vitrinite particles in occasional less-stained cuttings and very little inertinite or reworked material. UV light shows a light to mid-orange fluorescence from spores and a trace of exinite.

2743 m: Red micaceous silty shale. No determination possible since no organic material was located.

2799 m: Shale with iron oxide staining. No determination possible since no organic material was located.

2851-55 m: Calcareous siltstone,  $R_o = 0.44(9)$ .

The sample, showing a trace of iron oxides, has only a trace of organic material. A few particles of inertinite and reworked material with a similar content of vitrinite particles. Some bitumen wisps. UV light shows a light orange fluorescence from spore specks and a trace of exinite.

2884 m: Micaceous siltstone,  $R_o = 0.36(21)$ .

The sample has a moderate to rich organic content. Bitumen staining and plentiful of good particles of inertinite and reworked material. Good wisps of vitrinite and bitumen. UV light shows a mid-orange fluorescence from spores and hydrocarbon traces together with a low to moderate exinite content.

#### Visual Kerogen

Twentyfive samples were processed for analysis of kerogen in this well, the interval 1440 m down to 2884 m at approximate intervals of about 50 m.

Most residues are finely dispersed, and the general colour tone of the kerogen/exinite in frownish yellow to yellow brown down to about 2628 m swe, indicating that the deposits are immature to moderately mature.

Description of material.

1440 m: The residue consists mainly of sapropel with a minor element of terrestrial material also sapropelized and with signs of fungal activity. Colour index: -2/2 for a formation with potential for oil and gas formation.

1695 m: The residue is dominated by sapropel as above, but there are also aggregates of finely dispersed particles. Small spherical black particles adhere to palynomorphs, which are otherwise well preserved.

Colour index: -2/2 or 2 probably increased due to influence from carbonate. Potential for oil and gas formation.

1800 m: The residue consists mostly of coaly (fairly coarse) particles. Beside those a small part of finely dispersed material suggested as sapropel and some dinoflagellate cysts.

Colour index: 2 probably increased due to oxidation, and too high as a maturation index.

1880 m to 1960 m: The residues seem to consist of equal parts land derived and marine material. Acid insoluble minerals remain and the residues are fairly small indicating deposits poor in organic material deposited in a fairly high energy area with presence of carbonate.

Colour index: -2/2 or 2 potential for oil and gas.

2063 m swc: The residue consists of finely dispersed material suggested to be derived mainly from landplants. Acid insoluble minerals are present and support fairly high energy condition during the deposition.

Colour index: 2 may be too high as a maturation index, because it is controlled by lithology.

2126 m swc: Terrestrial material dominates and includes a major part of woody material/coal fragments beside indeterminate herbaceous remains. About one third is sapropel and includes well preserved dinoflagellate cysts which are fairly dark and could be reworked.

Colour index: 2/2+ probably a too high estimate based in oxidized material. Potential for gas and oil.



2173 m to 2290 m: Residues are finely disperse and consist mostly of amorphous material. Terrestrial remains are in low quantities. Cysts are fairly common.

At 2230 m increased terrestrial material, and the particles are recorded in aggregates which could indicate a carbonatic lithology.

Colour index: 2 for a formation with potential for oil and gas.

2348 m: The residue consists of dominantly terrestrial material, ?reworked coal particles and woody fragments.

Colour index: ?2 for a formation with potential mainly for gas.

2390 m swc to 2477 m swc: Sapropel dominates the interval, but there is also about 30 to 40 per cent of land derived material. The indeterminate finely disseminated terrestrial material of 2390 m swc embeds fungal hyphae. The residues of 2430 m swc and 2477 m swc contain varied assemblages of coarser terrestrial particles.

Colour index: 2 or 2/2+ for a formation with potential for oil and gas formation.

2529 m swc: The residue is dominated by a varied terrestrial assemblage, half of which is woody/coaly material. About 20 per cent is amorphous material. Otherwise this residue resembles those above.

Colour index: 2 for a formation with potential for gas and oil.

2581 m swc, 2605 m swc, and 2628 m swc: Residues composed by a major part of terrestrial material and 20 to 50 per cent of amorphous material. The residue of 2581 m swc contains undissolved minerals and aggregates which may be derived from a carbonatic lithology. The residue of 2605 m swc is heavily disturbed by undissolved minerals, and cuticular fragments are prominent. The residue of 2628 m swc resembles those above, but also includes fungal spores and hyphae suggesting fungal growth on the organic remains.

Colour index: 2/2+. There may be lithologic changes within this interval of changing water energy.

2633 m swc: Barren. Only undissolved minerals remain and were recorded as aggregates as if derived from a ?calcareous lithology.

Colour index: Indeterminate.

2676 m swc: Finely dispersed indeterminate herbaceous material dominates. Undissolved minerals are remaining as very small particles.

Colour index: 2/2+ for a formation with potential for gas and oil formation.

2743 m swc: A finely dispersed residue, suggested to consist mostly of amorphous material. Undissolved minerals are remaining and the lithology seems very poor in organic matters.

Colour index: 3- may be under lithological control, and too high as a maturation parametre.

2776 m swc, 2790.5 m swc, 2886 m: The residues are practically barren in organic matter of value for kerogen analyses.

### Rock-Eval Pyrolysis

A total of thirty samples were pyrolysed using the Rock-Eval method.

Most of the samples are found to have a  $T_{\max}$  value of less than  $430^{\circ}\text{C}$  and will therefore be classified as immature. The lowermost samples have  $T_{\max}$  values slightly above  $430^{\circ}\text{C}$ , and this indicates moderate mature samples.

The hydrogen index is low on most of the samples which indicate type III kerogen. The few exceptions are the samples from approximately 2150 - 2230 m and 2380 - 2650 m. The sample from 2725-40 m is also found to have a high hydrogen index and a low oxygen index which indicates type II kerogen.

### Conclusion

Based on the light hydrocarbon data the analysed sequence of the well was divided into nine zones, A: 1400 - 1810 m, B: 1810 - 1975 m, C: 1975 - 2125 m, D: 2125 - 2350 m, E: 2350 - 2475 m, F: 2475 - 2625 m, G: 2625 - 2685 m, H: 2685 - 2760 m, and I: 2760 - 2900 m.

In our evaluation of the well, the richness rating is based on the abundance of light hydrocarbons, total organic carbon and extractable hydrocarbons.

The maturity rating is based on the vitrinite reflectance, the colour of the kerogen and the  $T_{\max}$  from the Rock-Eval pyrolysis, while the type of source rock estimation is based on the type of kerogen found both by the visual estimation and by Rock-Eval pyrolysis.

A: 1400 - 1810 m: This zone has a good abundance of  $C_1 - C_4$  hydrocarbons and a poor abundance of  $C_5 - C_7$  hydrocarbons. The gas is very dry, and the  $iC_4/n-C_4$  ratio is low. The abundance of extractable hydrocarbons is poor for the whole zone, except sample 1750-65 m. The visual kerogen examination shows this zone to contain mainly amorphous material, while the Rock-Eval pyrolysis shows this zone to contain kerogen type III. Vitrinite reflectance measurements show, however, the samples from this zone to contain large proportions of reworked material. Reworked particles might often be completely hidden by the voluminous sapropelic material, and therefore not show up as well in the visual kerogen examination. These results fit in well with the total organic carbon (TOC) values which are rather high, and probably mainly caused by reworked particles.

Based on the various analyses, this zone is found to be immature with a poor potential as a source rock for gas and oil.

B: 1810 - 1975 m: This zone shows a large increase in the abundance of  $C_5 - C_7$  hydrocarbons, while the extractability of  $C_{15}^+$  hydrocarbons is still poor. Visual kerogen and Rock-Eval pyrolysis show this zone to contain mainly terrestrial material. Based on the various analyses, this zone is found to be immature with a poor potential as a source rock for gas.

C: 1975 - 2125 m: Same rating as the zone above.

D: 2125 - 2350 m: Both the abundance of light hydrocarbons and  $C_{15}^+$  hydrocarbons increase sharply in this zone compared to the zones above, at the same time as the visual kerogen and the Rock-Eval pyrolysis show this zone to contain mainly amorphous kerogen. Fluorescence in UV light indicates migrated hydrocarbons in parts of this zone. Based on these analyses, the zone is found to be immature with a good potential as a source rock for <sup>nch</sup> oil and gas. Probably migrated hydrocarbons at the lower part of the zone.

E: 2350 - 2475 m: Parts of this zone contain sandstone, and our analyses are undertaken only on the claystone. The abundance of  $C_1 - C_4$  hydrocarbons drops sharply in this zone compared to the zone above, while the abundance  $C_5 - C_7$  hydrocarbons is very erratic. The extractability of  $C_{15}^+$  hydrocarbons is still good. The erratic values of  $C_5^+$  hydrocarbons could indicate that parts of this zone contain migrated hydrocarbons, but our analysis does not give any direct evidence for such. This zone is found to be immature with a good potential as a source rock for oil and gas.

F: 2475 - 2628 m: The maturity increases slightly in this zone to moderate mature, while the richness and the type of kerogen is fairly similar to the zone above. The zone is rated to be moderate mature with a good potential as a source rock for oil and gas.

G: 2625 - 2685 m: The type of kerogen changes in this zone compared to the zone above, and is found to be mainly terrestrial. The claystone in this zone is found to be moderate mature with a good potential as a source rock for gas.

H: 2685 - 2770 m: The upper part of this zone is very similar to the zone above, while a small section approximately 2720 - 2750 m is found to have a good potential as a source rock for oil and gas.

I: 2770 - 2900 m: This zone is also found to be moderate mature. The vitrinite reflectance on the lowermost sample is very low. This is a sidewall core, and examination has shown this to contain Tertiary fossils. Due to this, the measurement on this sample will be excluded. The zone is found to be moderate mature, and the claystone has a poor potential as a source rock for gas. The above mentioned sidewall core shows fluorescing hydrocarbons in UV light. If this core is from the lower end of this zone, this would indicate this part of the zone to contain migrated hydrocarbons.

TABLE Ia

CONCENTRATION  $\mu\text{GAS/PR. KG ROCK (Headspace)}$ 

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5</sub> <sup>+</sup> | $\Sigma\text{C}_1\text{-C}_4$ | $\Sigma\text{C}_2\text{-C}_4$ | % wetness | $\frac{i\text{C}_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------------------|-------------------------------|-------------------------------|-----------|----------------------------|
| K1192  | 1450 - 65   | 3399           | 5              | 23             | 24              | 18              | 840                         | 3469                          | 70                            | 2,02      | 1,35                       |
| K1193  | 1465 - 80   | 8068           | 71             | 87             | 65              | 38              | 713                         | 8329                          | 261                           | 3,13      | 1,69                       |
| K1194  | 1480 - 95   | 7366           | 69             | 82             | 62              | 95              | 1061                        | 7674                          | 308                           | 4,02      | 0,65                       |
| K1195  | 1495 - 1510 | 13998          | 13             | 57             | 42              | 24              | 582                         | 14135                         | 137                           | 0,97      | 1,72                       |
| K1196  | 1510 - 25   | 11488          | 19             | 44             | 27              | 16              | 411                         | 11595                         | 106                           | 0,92      | 1,61                       |
| K1197  | 1525 - 40   | 6110           | 32             | 37             | 20              | 12              | 494                         | 6210                          | 100                           | 1,62      | 1,64                       |
| K1198  | 1540 - 55   | 8645           | 10             | 22             | 5               | 14              | 244                         | 8697                          | 52                            | 0,60      | 0,42                       |
| K1199  | 1555 - 70   | 8647           | 18             | 24             | 12              | 7               | 309                         | 8708                          | 62                            | 0,71      | 1,69                       |
| K1200  | 1570 - 85   | 2117           | 14             | 14             | 8               | 5               | 237                         | 2958                          | 42                            | 1,41      | 1,57                       |
| K1201  | 1585 - 1600 | 6150           | 7              | 15             | 9               | 5               | 163                         | 6186                          | 36                            | 0,59      | 1,84                       |
| K1202  | 1600 - 15   | 16060          | 7              | 40             | 25              | 15              | 334                         | 16148                         | 88                            | 0,55      | 1,62                       |
| K1203  | 1615 - 30   | 13796          | 9              | 31             | 8               | 20              | 528                         | 13864                         | 68                            | 0,49      | 0,40                       |
| K1204  | 1630 - 45   | 15791          | 14             | 47             | 10              | 27              | 355                         | 15890                         | 99                            | 0,62      | 0,39                       |
| K1205  | 1645 - 60   | 12867          | 6273           | 15             | 7               | 4               | 219                         | 19166                         | 6299                          | 32,87     | 1,78                       |
| K1206  | 1660 - 75   | 25370          | 4              | 36             | 15              | 9               | 295                         | 25435                         | 65                            | 0,26      | 1,61                       |
| K1207  | 1675 - 90   | 2091           | 17             | 12             | 6               | 4               | 187                         | 2129                          | 38                            | 1,81      | 1,60                       |
| K1266  | 1690 - 1705 | 7085           | 108            | 70             | 36              | 18              | 351                         | 7318                          | 233                           | 1,81      | 1,95                       |
| K1267  | 1705 - 20   | 18986          | 382            | 107            | 12              | 32              | 157                         | 19520                         | 534                           | 2,73      | 0,37                       |
| K1268  | 1720 - 35   | 18591          | 251            | 94             | 47              | 29              | 362                         | 19012                         | 421                           | 2,22      | 1,62                       |
| K1269  | 1735 - 50   | 31119          | 395            | 111            | 45              | 28              | 285                         | 31699                         | 580                           | 1,83      | 1,64                       |
| K1270  | 1750 - 65   | 34156          | 458            | 98             | 33              | 21              | 228                         | 34766                         | 610                           | 1,76      | 1,62                       |
| K1271  | 1765 - 80   | 6658           | 112            | 66             | 34              | 26              | 509                         | 6896                          | 238                           | 3,45      | 1,31                       |

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5</sub> <sup>+</sup> | ΣC <sub>1</sub> -C <sub>4</sub> | ΣC <sub>2</sub> -C <sub>4</sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------------------|---------------------------------|---------------------------------|-----------|---------------------|
| K1272  | 1780 - 95   | 17530          | 243            | 90             | 38              | 29              | 626                         | 17930                           | 400                             | 2.23      | 1.31                |
| K1273  | 1795 - 1810 | 25708          | 485            | 212            | 83              | 84              | 524                         | 26571                           | 863                             | 3.25      | 0.98                |
| K1274  | 1810 - 25   | 22891          | 605            | 315            | 117             | 130             | 734                         | 24059                           | 1168                            | 4.86      | 0.90                |
| K1275  | 1825 - 40   | 22452          | 612            | 354            | 144             | 168             | 1107                        | 23730                           | 1278                            | 5.39      | 0.86                |
| K1276  | 1840 - 55   | 15532          | 594            | 440            | 197             | 255             | 1897                        | 17019                           | 1486                            | 8.73      | 0.77                |
| K1277  | 1855 - 70   | 21615          | 647            | 350            | 113             | 140             | 827                         | 22866                           | 1250                            | 5.47      | 0.81                |
| K1278  | 1870 - 85   | 18827          | 840            | 493            | 161             | 209             | 1462                        | 20530                           | 1703                            | 8.30      | 0.77                |
| K1279  | 1885 - 1900 | 20370          | 833            | 491            | 153             | 199             | 1402                        | 22047                           | 1677                            | 7.60      | 0.77                |
| K1280  | 1900 - 15   | 9317           | 369            | 198            | 64              | 52              | 743                         | 10001                           | 683                             | 6.83      | 1.22                |
| K1281  | 1915 - 30   | 22776          | 576            | 328            | 105             | 130             | 1562                        | 23917                           | 1141                            | 4.77      | 0.81                |
| K1282  | 1930 - 45   | 11869          | 421            | 269            | 94              | 124             | 1087                        | 12778                           | 909                             | 7.12      | 0.75                |
| K1283  | 1945 - 60   | 12276          | 616            | 516            | 156             | 234             | 1475                        | 13798                           | 1523                            | 11.04     | 0.67                |
| K1284  | 1960 - 75   | 424            | 17             | 10             | 0               | 0               | 0                           | 451                             | 27                              | 6.09      | 1.00                |
| K1285  | 1975 - 90   | 7867           | 398            | 278            | 79              | 99              | 733                         | 8721                            | 854                             | 7.79      | 0.79                |
| K1286  | 1990 - 2005 | 4679           | 297            | 210            | 51              | 70              | 478                         | 5307                            | 628                             | 11.83     | 0.72                |
| K1287  | 2005 - 20   | 6249           | 702            | 699            | 150             | 204             | 647                         | 8004                            | 1755                            | 21.92     | 0.74                |
| K1288  | 2020 - 35   | 2838           | 250            | 193            | 40              | 57              | 238                         | 3378                            | 540                             | 15.98     | 0.69                |
| K1289  | 2035 - 50   | 1638           | 306            | 272            | 53              | 63              | 359                         | 2334                            | 696                             | 29.81     | 0.85                |
| K1290  | 2050 - 65   | 2658           | 311            | 245            | 52              | 85              | 357                         | 3351                            | 694                             | 20.70     | 0.62                |
| K1291  | 2065 - 80   | 3839           | 438            | 408            | 77              | 140             | 314                         | 4902                            | 1663                            | 21.68     | 0.55                |
| K1292  | 2095 - 2110 | 4590           | 752            | 850            | 153             | 337             | 500                         | 6682                            | 2092                            | 31.31     | 0.45                |
| K1293  | 2110 - 25   | 1217           | 218            | 287            | 58              | 132             | 195                         | 1913                            | 696                             | 36.36     | 0.44                |
| K1294  | 2125 - 40   | 2680           | 533            | 674            | 135             | 330             | 686                         | 4353                            | 1673                            | 38.44     | 0.41                |

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5+</sub> | ΣC <sub>1</sub> -C <sub>4</sub> | ΣC <sub>2</sub> -C <sub>4</sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------|---------------------------------|---------------------------------|-----------|---------------------|
| K1295  | 2140 - 55   | 5634           | 4681           | 2823           | 350             | 737             | 792             | 14225                           | 8591                            | 60.40     | 0.48                |
| K1296  | 2155 - 70   | 14576          | 12446          | 8975           | 1313            | 2983            | 3221            | 40293                           | 25717                           | 63.82     | 0.44                |
| K1297  | 2170 - 85   | 4665           | 3820           | 2054           | 257             | 560             | 721             | 11357                           | 6692                            | 58.92     | 0.46                |
| K1303  | 2185 - 2200 | 9791           | 9108           | 5752           | 765             | 1578            | 2661            | 26996                           | 17205                           | 63.75     | 0.48                |
| K1304  | 2200 - 15   | 7985           | 8162           | 5606           | 701             | 1479            | 1654            | 23933                           | 15948                           | 66.64     | 0.47                |
| K1305  | 2215 - 30   | 2489           | 2763           | 1659           | 200             | 424             | 438             | 7536                            | 5047                            | 66.97     | 0.47                |
| K1306  | 2230 - 45   | 2889           | 2487           | 1695           | 270             | 546             | 1239            | 7887                            | 4998                            | 63.37     | 0.49                |
| K1307  | 2245 - 60   | 12254          | 11497          | 8250           | 1203            | 2577            | 3319            | 35783                           | 23529                           | 65.75     | 0.47                |
| K1308  | 2260 - 75   | 15397          | 16607          | 14638          | 2710            | 6312            | 1948            | 55663                           | 40266                           | 72.34     | 0.43                |
| K1309  | 2275 - 90   | 7867           | 7760           | 6340           | 1164            | 2245            | 2715            | 25376                           | 17509                           | 69.00     | 0.52                |
| K1310  | 2290 - 2305 | 27             | 31             | 27             | 5               | 9               | 6               | 100                             | 73                              | 72.58     | 0.53                |
| K1311  | 2305 - 20   | 8315           | 11325          | 11605          | 1724            | 4383            | 6516            | 37353                           | 29038                           | 77.74     | 0.39                |
| K1312  | 2320 - 35   | 4645           | 4017           | 3475           | 710             | 1579            | 2511            | 11426                           | 9780                            | 67.80     | 0.45                |
| K1313  | 2335 - 50   | 6961           | 7465           | 4632           | 573             | 1327            | 2332            | 20958                           | 13997                           | 66.79     | 0.43                |
| K1314  | 2350 - 65   | 2949           | 3160           | 2707           | 606             | 1356            | 4004            | 10779                           | 7830                            | 72.64     | 0.45                |
| K1315  | 2365 - 80   | 5587           | 3824           | 2022           | 261             | 543             | 728             | 12236                           | 6650                            | 54.34     | 0.48                |
| K1316  | 2380 - 95   | 4763           | 4091           | 2063           | 271             | 529             | 441             | 11717                           | 6954                            | 59.35     | 0.51                |
| K1317  | 2395 - 2410 | 3103           | 1204           | 569            | 73              | 146             | 113             | 5095                            | 1992                            | 39.10     | 0.50                |
| K1318  | 2410 - 25   | 3227           | 3128           | 1856           | 265             | 619             | 569             | 9096                            | 5869                            | 64.52     | 0.43                |
| K1319  | 2425 - 40   | 6369           | 5002           | 4077           | 623             | 1294            | 1027            | 17266                           | 10997                           | 63.33     | 0.48                |
| K1320  | 2440 - 55   | 7728           | 5085           | 3579           | 532             | 1078            | 910             | 18002                           | 10274                           | 57.07     | 0.49                |
| K1321  | 2455 - 70   | 5379           | 4038           | 2705           | 370             | 754             | 747             | 13246                           | 7866                            | 59.39     | 0.49                |
| K1322  | 2470 - 85   | 3388           | 2321           | 1727           | 276             | 482             | 473             | 8193                            | 4806                            | 58.36     | 0.57                |

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5+</sub> | ΣC <sub>1</sub> -C <sub>4</sub> | ΣC <sub>2</sub> -C <sub>4</sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------|---------------------------------|---------------------------------|-----------|---------------------|
| K1323  | 2485 - 2500 | 530            | 561            | 403            | 59              | 116             | 148             | 1668                            | 1138                            | 68.24     | 0.51                |
| K1324  | 2500 - 15   | 1846           | 1458           | 1015           | 133             | 211             | 243             | 4663                            | 2817                            | 60.40     | 0.63                |
| K1325  | 2515 - 30   | 1889           | 1584           | 1177           | 150             | 255             | 268             | 5056                            | 3166                            | 62.63     | 0.59                |
| K1326  | 2530 - 45   | 2427           | 2065           | 1598           | 212             | 381             | 414             | 6684                            | 4256                            | 63.68     | 0.56                |
| K1389  | 2545 - 60   | Open lid       |                |                |                 |                 |                 |                                 |                                 |           |                     |
| K1390  | 2560 - 75   | 6098           | 1174           | 1250           | 2392            | 495             | 463             | 3769                            | 3159                            | 83.82     | 0.48                |
| K1391  | 2575 - 90   | 136            | 1958           | 2051           | 373             | 723             | 5693            | 5241                            | 5105                            | 97.40     | 0.52                |
| K1392  | 2590 - 2605 | 107            | 360            | 578            | 123             | 271             | 316             | 1440                            | 1333                            | 92.58     | 0.45                |
| K1393  | 2605 - 20   | 221            | 404            | 583            | 116             | 226             | 180             | 1550                            | 1329                            | 85.76     | 0.51                |
| K1394  | 2620 - 35   | 4706           | 1865           | 847            | 75              | 152             | 60              | 7647                            | 2941                            | 38.46     | 0.49                |
| K1395  | 2635 - 50   | 4040           | 1978           | 1395           | 214             | 526             | 351             | 8153                            | 4114                            | 50.45     | 0.41                |
| K1396  | 2650 - 65   | 24498          | 10741          | 5123           | 8347            | 4725            | 497             | 53434                           | 28936                           | 54.15     | 1.77                |
| K1397  | 2665 - 80   | 18307          | 6431           | 3323           | 2591            | 1556            | 153             | 32208                           | 13901                           | 43.16     | 1.67                |
| K1398  | 2680 - 95   | Open lid       |                |                |                 |                 |                 |                                 |                                 |           |                     |
| K1399  | 2695 - 2710 | 18318          | 1977           | 1358           | 1411            | 771             | 150             | 23836                           | 5517                            | 23.15     | 1.83                |
| K1400  | 2710 - 25   | 6800           | 2346           | 1528           | 1880            | 1027            | 217             | 13582                           | 6782                            | 49.93     | 1.83                |
| K1401  | 2725 - 40   | 10450          | 3845           | 2409           | 2928            | 1477            | 275             | 21109                           | 10659                           | 50.50     | 1.98                |
| K1402  | 2740 - 55   | 45874          | 12327          | 3596           | 2752            | 1185            | 96              | 65735                           | 19861                           | 30.21     | 2.32                |
| K1479  | 2755 - 70   | 5333           | 2599           | 1709           | 1806            | 3464            | 160             | 14921                           | 9588                            | 64.26     | 0.52                |
| K1480  | 2770 - 85   | 369            | 421            | 367            | 511             | 1059            | 106             | 2727                            | 2358                            | 86.48     | 0.48                |
| K1481  | 2785 - 2800 | 2052           | 428            | 386            | 514             | 1148            | 116             | 4628                            | 2476                            | 54.69     | 0.45                |
| K1482  | 2800 - 15   | 1514           | 945            | 943            | 1395            | 3286            | 368             | 8084                            | 6570                            | 81.27     | 0.42                |
| K1483  | 2815 - 30   | 526            | 620            | 677            | 989             | 2336            | 251             | 5147                            | 4621                            | 89.78     | 0.42                |
| K1484  | 2830 - 45   | 237            | 180            | 239            | 467             | 1066            | 133             | 2189                            | 1952                            | 89.16     | 0.44                |



| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5</sub> <sup>+</sup> | ΣC <sub>1</sub> -C <sub>4</sub> | ΣC <sub>2</sub> -C <sub>4</sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------------------|---------------------------------|---------------------------------|-----------|---------------------|
| K1485  | 2845 - 60   | 1061           | 722            | 652            | 933             | 2156            | 228                         | 5525                            | 4464                            | 80.79     | 0.43                |
| K1486  | 2860 - 75   | 922            | 997            | 512            | 731             | 1671            | 213                         | 4833                            | 3911                            | 80.91     | 0.44                |
| K1487  | 2875 - 90   | 587            | 529            | 500            | 702             | 1635            | 196                         | 3953                            | 3366                            | 85.15     | 0.43                |
| K1488  | 2890 - 2905 | 758            | 767            | 866            | 1449            | 3314            | 590                         | 7154                            | 6396                            | 89.40     | 0.44                |

Table Ib  
 CONCENTRATION  $\mu$ GAS/PR. KG ROCK (GAS IN CUTTINGS)

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5+</sub> | $\Sigma C_1-C_4$ | $\Sigma C_2-C_4$ | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------|------------------|------------------|-----------|---------------------|
| K1192  | 1450 - 65   | 49             | 18             | 3              | 4               | 11              | 344             | 85               | 36               | 42.74     | 0.34                |
| K1193  | 1465 - 80   | 45             | 17             | 4              | 3               | 4               | 194             | 75               | 29               | 39.16     | 0.84                |
| K1194  | 1480 - 95   | 151            | 78             | 36             | 34              | 33              | 4278            | 332              | 181              | 54.58     | 1.02                |
| K1195  | 1495 - 1510 |                |                |                |                 |                 |                 |                  |                  |           |                     |
| K1196  | 1510 - 25   | 13             | 3              | 2              | 2               | 2               | 148             | 22               | 9                | 40.22     | 1.00                |
| K1197  | 1525 - 40   | 32             | 12             | 5              | 2               | 2               | 223             | 54               | 21               | 39.41     | 0.99                |
| K1198  | 1540 - 55   | 42             | 15             | 7              | 5               | 5               | 267             | 74               | 32               | 42.82     | 0.99                |
| K1199  | 1555 - 70   | 32             | 10             | 5              | 2               | 3               | 192             | 54               | 21               | 39.72     | 0.83                |
| K1200  | 1570 - 85   | 39             | 12             | 5              | 2               | 2               | 216             | 59               | 21               | 35.00     | 1.06                |
| K1201  | 1585 - 1600 |                |                |                |                 |                 |                 |                  |                  |           |                     |
| K1202  | 1600 - 15   | 59             | 3              | 5              | 4               | 3               | 173             | 75               | 16               | 21.21     | 1.03                |
| K1203  | 1615 - 30   | 169            | 31             | 14             | 6               | 6               | 365             | 227              | 58               | 25.40     | 1.00                |
| K1204  | 1630 - 45   | 124            | 5              | 10             | 7               | 8               | 281             | 154              | 31               | 19.85     | 0.97                |
| K1205  | 1645 - 60   | 112            | 4              | 5              | 2               | 2               | 192             | 126              | 14               | 10.92     | 1.02                |
| K1206  | 1660 - 75   | 99             | 5              | 7              | 5               | 4               | 162             | 120              | 21               | 17.60     | 1.04                |
| K1207  | 1675 - 90   |                |                |                |                 |                 |                 |                  |                  |           |                     |
| K1266  | 1690 - 1705 | 37             | 13             | 13             | 11              | 4               | 153             | 79               | 41               | 52.44     | 2.53                |
| K1267  | 1705 - 20   | 56             | 39             | 32             | 22              | 18              | 43              | 169              | 111              | 65.80     | 1.21                |
| K1268  | 1720 - 35   | 54             | 9              | 11             | 10              | 10              | 102             | 94               | 40               | 42.90     | 1.03                |
| K1269  | 1735 - 50   | 70             | 26             | 26             | 18              | 6               | 70              | 146              | 76               | 52.27     | 2.83                |
| K1270  | 1750 - 65   | 39             | 18             | 16             | 12              | 8               | 6               | 92               | 54               | 58.13     | 1.47                |
| K1271  | 1765 - 80   |                |                |                |                 |                 |                 |                  |                  |           |                     |

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5</sub> <sup>+</sup> | ΣC <sub>1</sub> -C <sub>4</sub> | ΣC <sub>2</sub> -C <sub>4</sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------------------|---------------------------------|---------------------------------|-----------|---------------------|
| K1272  | 1780 - 95   |                |                |                |                 |                 |                             |                                 |                                 |           |                     |
| K1273  | 1795 - 1810 | 45             | 18             | 14             | 11              | 17              | 131                         | 105                             | 60                              | 57.17     | 0.68                |
| K1274  | 1810 - 25   | 54             | 16             | 21             | 18              | 34              | 239                         | 144                             | 89                              | 62.10     | 0.52                |
| K1275  | 1825 - 40   | 81             | 17             | 27             | 21              | 38              | 343                         | 183                             | 102                             | 55.95     | 0.54                |
| K1276  | 1840 - 55   | 209            | 44             | 93             | 67              | 140             | 6714                        | 553                             | 344                             | 62.28     | 0.48                |
| K1277  | 1855 - 70   | 120            | 49             | 73             | 41              | 89              | 1911                        | 373                             | 252                             | 67.67     | 0.46                |
| K1278  | 1870 - 85   | 172            | 81             | 97             | 61              | 119             | 1880                        | 530                             | 358                             | 67.51     | 0.51                |
| K1279  | 1885 - 1900 | 212            | 108            | 140            | 63              | 138             | 2377                        | 662                             | 450                             | 67.92     | 0.46                |
| K1280  | 1900 - 15   | 116            | 38             | 37             | 20              | 43              | 884                         | 254                             | 138                             | 54.43     | 0.47                |
| K1281  | 1915 - 30   |                |                |                |                 |                 |                             |                                 |                                 |           |                     |
| K1282  | 1930 - 45   | 121            | 15             | 26             | 10              | 29              | 3027                        | 201                             | 80                              | 39.80     | 0.33                |
| K1283  | 1945 - 60   |                |                |                |                 |                 |                             |                                 |                                 |           |                     |
| K1284  | 1960 - 75   |                |                |                |                 |                 |                             |                                 |                                 |           |                     |
| K1285  | 1975 - 90   |                |                |                |                 |                 |                             |                                 |                                 |           |                     |
| K1286  | 1990 - 2005 | 24             | 6              | 11             | 7               | 9               | 148                         | 57                              | 33                              | 57.24     | 0.91                |
| K1287  | 2005 - 20   | 62             | 24             | 68             | 22              | 49              | 262                         | 226                             | 164                             | 72.73     | 0.45                |
| K1288  | 2020 - 35   |                |                |                |                 |                 |                             |                                 |                                 |           |                     |
| K1289  | 2035 - 50   |                |                |                |                 |                 |                             |                                 |                                 |           |                     |
| K1290  | 2050 - 65   | 31             | 9              | 20             | 8               | 21              | 1                           | 89                              | 58                              | 65.42     | 0.38                |
| K1291  | 2065 - 80   | 82             | 32             | 60             | 28              | 82              | 170                         | 283                             | 201                             | 70.99     | 0.34                |
| K1292  | 2095 - 2110 |                |                |                |                 |                 |                             |                                 |                                 |           |                     |
| K1293  | 2110 - 25   |                |                |                |                 |                 |                             |                                 |                                 |           |                     |
| K1294  | 2125 - 40   | 122            | 36             | 56             | 16              | 63              | 40                          | 294                             | 172                             | 58.61     | 0.26                |

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5+</sub> | ΣC <sub>1-C4</sub> | ΣC <sub>2-C4</sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------|--------------------|--------------------|-----------|---------------------|
| K1295  | 2140 - 55   | 264            | 1329           | 2470           | 406             | 1438            | 1552            | 5906               | 5643               | 95.54     | 0.28                |
| K1296  | 2155 - 70   | 338            | 4798           | 11317          | 2310            | 7502            | 6653            | 26265              | 25927              | 98.71     | 0.31                |
| K1297  | 2170 - 85   | 134            | 1211           | 3230           | 739             | 2459            | 3070            | 7773               | 7639               | 98.28     | 0.30                |
| K1303  | 2185 - 2200 | 77             | 282            | 1727           | 393             | 1497            | 25262           | 3976               | 3900               | 98.06     | 0.26                |
| K1304  | 2200 - 15   | 13             | 116            | 517            | 114             | 412             | 1756            | 1174               | 1160               | 98.83     | 0.28                |
| K1305  | 2215 - 30   | 40             | 76             | 1373           | 443             | 1657            | 20076           | 3589               | 3549               | 98.89     | 0.27                |
| K1306  | 2230 - 45   | 46             | 66             | 2203           | 739             | 2800            | 55370           | 5855               | 5809               | 99.21     | 0.26                |
| K1307  | 2245 - 60   | 14             | 116            | 517            | 114             | 412             | 7113            | 1174               | 1160               | 98.83     | 0.28                |
| K1308  | 2260 - 75   | 1              | 35             | 1450           | 497             | 2270            | 57476           | 4253               | 4252               | 99.97     | 0.22                |
| K1309  | 2275 - 90   | 6              | 4              | 87             | 27              | 147             | 489             | 272                | 266                | 97.89     | 0.18                |
| K1310  | 2290 - 2305 | 68             | 4              | 97             | 20              | 133             | 336             | 322                | 254                | 78.88     | 0.15                |
| K1311  | 2305 - 20   | 3              | 114            | 1186           | 273             | 1168            | 24285           | 2744               | 2741               | 99.87     | 0.23                |
| K1312  | 2320 - 35   | 25             | 66             | 303            | 84              | 313             | 170             | 791                | 765                | 96.78     | 0.27                |
| K1313  | 2335 - 50   | 0              | 0              | 326            | 71              | 354             | 726             | 751                | 751                | 99.98     | 0.20                |
| K1314  | 2350 - 65   | 80             | 353            | 1240           | 292             | 1028            | 865             | 2994               | 2913               | 97.32     | 0.28                |
| K1315  | 2365 - 80   | 12             | 16             | 302            | 68              | 301             | 565             | 699                | 687                | 98.31     | 0.23                |
| K1316  | 2380 - 95   | 15             | 213            | 541            | 102             | 338             | 172             | 1209               | 1194               | 98.74     | 0.30                |
| K1317  | 2395 - 2410 | 30             | 584            | 1043           | 185             | 607             | 630             | 2449               | 2418               | 98.77     | 0.30                |
| K1318  | 2410 - 25   | 8              | 4              | 67             | 21              | 123             | 403             | 223                | 215                | 96.44     | 0.17                |
| K1319  | 2425 - 40   | 4              | 5              | 280            | 85              | 367             | 593             | 741                | 737                | 99.48     | 0.23                |
| K1320  | 2440 - 55   | 9              | 114            | 1013           | 254             | 869             | 10932           | 2260               | 2251               | 99.62     | 0.29                |
| K1321  | 2455 - 70   | 17             | 38             | 769            | 192             | 702             | 1002            | 1718               | 1701               | 99.03     | 0.27                |
| K1322  | 2470 - 85   | 13             | 29             | 474            | 103             | 395             | 54              | 1014               | 1001               | 98.76     | 0.26                |

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5</sub> <sup>+</sup> | ΣC <sub>1</sub> -C <sub>4</sub> | ΣC <sub>2</sub> -C <sub>4</sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------------------|---------------------------------|---------------------------------|-----------|---------------------|
| K1323  | 2485 - 2500 | 23             | 13             | 204            | 32              | 214             | 322                         | 487                             | 464                             | 95.27     | 0.15                |
| K1324  | 2500 - 15   | 95             | 146            | 488            | 96              | 310             | 194                         | 1135                            | 1040                            | 91.63     | 0.31                |
| K1325  | 2515 - 30   | 41             | 35             | 835            | 194             | 722             | 11614                       | 1827                            | 1786                            | 97.78     | 0.27                |
| K1326  | 2530 - 45   | 96             | 318            | 784            | 144             | 458             | 265                         | 1801                            | 1704                            | 92.62     | 0.31                |
| K1389  | 2545 - 60   | 58             | 186            | 1052           | 263             | 850             | 1623                        | 2410                            | 2352                            | 97.60     | 0.31                |
| K1390  | 2560 - 75   | 81             | 142            | 784            | 223             | 782             | 1702                        | 2012                            | 1931                            | 95.99     | 0.29                |
| K1391  | 2575 - 90   | 105            | 111            | 751            | 183             | 665             | 1620                        | 1815                            | 1710                            | 94.22     | 0.28                |
| K1392  | 2590 - 2605 | 324            | 218            | 1113           | 338             | 1291            | 3179                        | 3285                            | 2961                            | 90.14     | 0.26                |
| K1393  | 2605 - 20   | 169            | 81             | 152            | 35              | 89              | 384                         | 527                             | 358                             | 67.84     | 0.40                |
| K1394  | 2602 - 35   | 1194           | 1317           | 1036           | 82              | 271             | 126                         | 3899                            | 2706                            | 69.39     | 0.30                |
| K1395  | 2635 - 50   | 26             | 40             | 105            | 18              | 55              | 116                         | 244                             | 218                             | 89.12     | 0.33                |
| K1396  | 2650 - 65   | 1269           | 1290           | 1363           | 182             | 845             | 724                         | 4949                            | 3680                            | 74.36     | 0.21                |
| K1397  | 2665 - 80   | 350            | 1111           | 1486           | 231             | 876             | 641                         | 4054                            | 3704                            | 91.36     | 0.26                |
| K1398  | 2680 - 95   | 164            | 632            | 904            | 97              | 417             | 346                         | 2215                            | 2051                            | 92.60     | 0.23                |
| K1399  | 2695 - 2710 | 109            | 236            | 468            | 67              | 263             | 392                         | 1143                            | 1034                            | 90.49     | 0.26                |
| K1400  | 2710 - 25   | 57             | 174            | 471            | 78              | 335             | 602                         | 1114                            | 1058                            | 94.92     | 0.23                |
| K1401  | 2725 - 40   | 72             | 232            | 603            | 98              | 401             | 677                         | 1408                            | 1335                            | 94.86     | 0.24                |
| K1402  | 2740 - 55   | 3565           | 3567           | 2745           | 258             | 546             | 146                         | 10682                           | 7116                            | 66.62     | 0.47                |
| K1479  | 2755 - 70   | 139            | 383            | 651            | 93              | 249             | 112                         | 1515                            | 1376                            | 90.37     | 0.37                |
| K1480  | 2770 - 85   | 136            | 145            | 187            | 28              | 117             | 157                         | 614                             | 478                             | 77.83     | 0.24                |
| K1481  | 2785 - 2800 | 21             | 37             | 69             | 14              | 54              | 81                          | 195                             | 174                             | 88.98     | 0.25                |
| K1482  | 2800 - 15   | 127            | 106            | 238            | 63              | 267             | 505                         | 801                             | 674                             | 84.09     | 0.24                |
| K1483  | 2815 - 30   | 116            | 68             | 111            | 28              | 124             | 245                         | 449                             | 332                             | 74.04     | 0.23                |
| K1484  | 2803 - 45   | 31             | 41             | 51             | 11              | 33              | 77                          | 168                             | 137                             | 81.53     | 0.32                |
| K1485  | 2845 - 60   | 71             | 52             | 122            | 45              | 191             | 594                         | 482                             | 411                             | 85.24     | 0.24                |
| K1486  | 2860 - 75   | 101            | 156            | 372            | 92              | 349             | 731                         | 1070                            | 969                             | 90.56     | 0.26                |

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5+</sub> | ΣC <sub>1</sub> -C <sub>4</sub> | ΣC <sub>2</sub> -C <sub>4</sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------|---------------------------------|---------------------------------|-----------|---------------------|
| K1487  | 2875 - 90   | 12             | 13             | 26             | 7               | 24              | 45              | 83                              | 71                              | 85.57     | 0.30                |
| K1488  | 2890 - 2900 | 408            | 256            | 574            | 205             | 620             | 1414            | 2063                            | 1656                            | 80.24     | 0.33                |

Table 1c  
 CONCENTRATION  $\mu$ LGAS/PR. KG ROCK (Ia + Ib)

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5+</sub> | $\Sigma$ C <sub>1</sub> -C <sub>4</sub> | $\Sigma$ C <sub>2</sub> -C <sub>4</sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------|---|---|-----------|---------------------|
|        | 1450 - 65   | 3448           | 23             | 26             | 28              | 29              | 1184            | 3554                                    | 106                                     | 2.98      | 0.97                |
|        | 1465 - 80   | 8113           | 88             | 91             | 68              | 42              | 907             | 8404                                    | 290                                     | 3.45      | 1.62                |
|        | 1480 - 95   | 7517           | 147            | 118            | 96              | 128             | 5339            | 8006                                    | 489                                     | 6.11      | 0.75                |
|        | 1495 - 1510 | 13998          | 13             | 57             | 42              | 24              | 582             | 14135                                   | 137                                     | 0.97      | 1.75                |
|        | 1510 - 25   | 11501          | 22             | 46             | 29              | 18              | 559             | 11617                                   | 115                                     | 0.99      | 1.61                |
|        | 1525 - 40   | 6142           | 44             | 42             | 22              | 14              | 717             | 6264                                    | 121                                     | 1.93      | 1.57                |
|        | 1540 - 55   | 8687           | 25             | 29             | 10              | 19              | 511             | 8771                                    | 74                                      | 0.84      | 0.53                |
|        | 1555 - 70   | 8679           | 28             | 29             | 14              | 10              | 501             | 8762                                    | 83                                      | 0.95      | 1.4                 |
|        | 1570 - 85   | 2156           | 26             | 19             | 10              | 7               | 453             | 3017                                    | 63                                      | 2.09      | 1.43                |
|        | 1585 - 1600 | 6150           | 7              | 15             | 9               | 5               | 163             | 6186                                    | 36                                      | 0.58      | 1.80                |
|        | 1600 - 15   | 16119          | 10             | 45             | 29              | 18              | 507             | 16223                                   | 104                                     | 0.64      | 1.61                |
|        | 1615 - 30   | 13855          | 40             | 45             | 14              | 26              | 893             | 14091                                   | 126                                     | 0.89      | 3.2                 |
|        | 1630 - 45   | 15915          | 19             | 57             | 17              | 36              | 636             | 16044                                   | 130                                     | 0.81      | 3.35                |
|        | 1645 - 60   | 12979          | 6773           | 20             | 9               | 6               | 500             | 25555                                   | 6313                                    | 24.7      | 2.22                |
|        | 1660 - 75   | 25469          | 9              | 43             | 20              | 13              | 487             | 19292                                   | 86                                      | 0.45      | 2.15                |
|        | 1675 - 90   | 2091           | 17             | 12             | 6               | 4               | 187             | 2129                                    | 38                                      | 1.78      | 2.-                 |
|        | 1690 - 1705 | 7122           | 131            | 83             | 47              | 22              | 504             | 7397                                    | 274                                     | 3.70      | 1.77                |
|        | 1705 - 20   | 19042          | 421            | 138            | 34              | 50              | 200             | 19689                                   | 644                                     | 3.27      | 4.09                |
|        | 1720 - 35   | 18645          | 260            | 105            | 57              | 39              | 464             | 19106                                   | 461                                     | 2.41      | 1.46                |
|        | 1735 - 50   | 31189          | 421            | 137            | 63              | 34              | 355             | 31845                                   | 656                                     | 2.06      | 1.85                |
|        | 1750 - 65   | 34195          | 476            | 114            | 45              | 29              | 234             | 34858                                   | 664                                     | 1.90      | 1.55                |
|        | 1765 - 80   | 6658           | 112            | 66             | 34              | 26              | 509             | 6896                                    | 238                                     | 3.45      | 1.31                |
|        | 1780 - 95   | 17530          | 243            | 90             | 38              | 29              | 626             | 17939                                   | 400                                     | 2.23      | 1.31                |
|        | 1795 - 1810 | 25753          | 503            | 2134           | 94              | 101             | 654             | 26676                                   | 923                                     | 3.46      | 0.93                |
|        | 1810 - 25   | 22945          | 621            | 336            | 135             | 164             | 973             | 24203                                   | 1257                                    | 5.19      | 1.21                |

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5+</sub> | ΣC <sub>1</sub> -C <sub>4</sub> | ΣC <sub>2</sub> -C <sub>4</sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------|---------------------------------|---------------------------------|-----------|---------------------|
|        | 1825 - 40   | 22522          | 629            | 381            | 165             | 206             | 1450            | 23913                           | 1380                            | 5.77      | 0.80                |
|        | 1840 - 55   | 15741          | 638            | 533            | 264             | 395             | 8611            | 17572                           | 1830                            | 10.41     | 0.67                |
|        | 1855 - 70   | 21735          | 696            | 423            | 154             | 229             | 2738            | 23239                           | 1502                            | 6.46      | 0.67                |
|        | 1870 - 85   | 18999          | 921            | 590            | 222             | 328             | 2342            | 21060                           | 2061                            | 9.79      | 0.68                |
|        | 1885 - 1900 | 20582          | 941            | 631            | 216             | 337             | 3779            | 22709                           | 2127                            | 9.37      | 0.64                |
|        | 1900 - 15   | 9433           | 407            | 235            | 84              | 95              | 1627            | 10255                           | 821                             | 8.01      | 0.88                |
|        | 1915 - 30   | 22776          | 576            | 328            | 105             | 130             | 1562            | 23917                           | 1141                            | 4.77      | 0.81                |
|        | 1930 - 45   | 11990          | 436            | 295            | 104             | 153             | 4114            | 12979                           | 989                             | 7.62      | 0.68                |
|        | 1945 - 60   | 12276          | 616            | 516            | 156             | 234             | 1475            | 13798                           | 1523                            | 11.04     | 0.67                |
|        | 1960 - 75   | 424            | 17             | 10             | 0               | 0               | 0               | 451                             | 27                              | 5.99      | 0                   |
|        | 1975 - 90   | 7867           | 398            | 278            | 79              | 99              | 733             | 8721                            | 854                             | 9.79      | 0.80                |
|        | 1990 - 2005 | 4699           | 303            | 222            | 58              | 78              | 626             | 5364                            | 661                             | 12.32     | 0.74                |
|        | 2005 - 20   | 6311           | 726            | 767            | 72              | 253             | 909             | 8230                            | 1919                            | 23.32     | 0.28                |
|        | 2020 - 35   | 2838           | 250            | 193            | 40              | 57              | 238             | 3378                            | 540                             | 1.60      | 0.70                |
|        | 2035 - 50   | 1638           | 306            | 272            | 53              | 63              | 359             | 2334                            | 696                             | 29.82     | 0.84                |
|        | 2050 - 65   | 2689           | 320            | 265            | 60              | 106             | 358             | 3440                            | 752                             | 21.86     | 0.57                |
|        | 2065 - 80   | 3921           | 470            | 468            | 106             | 222             | 484             | 5185                            | 1264                            | 24.38     | 0.48                |
|        | 2095 - 2110 | 4590           | 752            | 850            | 153             | 337             | 500             | 6682                            | 2092                            | 31.31     | 0.45                |
|        | 2110 - 25   | 1217           | 218            | 287            | 58              | 132             | 195             | 1913                            | 696                             | 36.38     | 0.44                |
|        | 2125 - 40   | 2802           | 569            | 730            | 151             | 393             | 726             | 4647                            | 1845                            | 39.70     | 0.38                |
|        | 2140 - 55   | 5898           | 6010           | 5293           | 756             | 2175            | 2344            | 20131                           | 14234                           | 70.71     | 0.35                |
|        | 2155 - 70   | 14914          | 17244          | 20292          | 3623            | 10485           | 9874            | 66558                           | 51644                           | 77.59     | 0.35                |
|        | 2170 - 85   | 4799           | 5031           | 5284           | 996             | 3019            | 3791            | 19130                           | 14331                           | 74.91     | 0.33                |
|        | 2185 - 2200 | 9868           | 9390           | 7479           | 1158            | 3075            | 27923           | 30972                           | 21105                           | 0.68      | 0.38                |



| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5+</sub> | ΣC <sub>1-C<sub>4</sub></sub> | ΣC <sub>2-C<sub>4</sub></sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------|-------------------------------|-------------------------------|-----------|---------------------|
|        | 2200 - 15   | 7998           | 8278           | 6123           | 815             | 1891            | 3410            | 25107                         | 117108                        | 68.14     | 0.43                |
|        | 2215 - 30   | 2529           | 2839           | 3032           | 643             | 2081            | 20514           | 11125                         | 8596                          | 77.27     | 0.31                |
|        | 2230 - 45   | 2935           | 2553           | 3898           | 1009            | 3346            | 56609           | 13742                         | 10897                         | 78.64     | 0.30                |
|        | 2245 - 60   | 12268          | 11613          | 8767           | 1317            | 2989            | 10432           | 36957                         | 24689                         | 66.80     | 0.44                |
|        | 2260 - 75   | 15398          | 16642          | 16088          | 3207            | 8582            | 69424           | 59916                         | 44518                         | 74.30     | 0.37                |
|        | 2275 - 90   | 7872           | 7764           | 6427           | 1191            | 2392            | 3204            | 25648                         | 17775                         | 69.30     | 0.50                |
|        | 2290 - 2305 | 95             | 35             | 124            | 25              | 142             | 495             | 422                           | 327                           | 77.49     | 0.18                |
|        | 2305 - 20   | 8318           | 11439          | 12791          | 2892            | 7684            | 30801           | 40097                         | 31779                         | 79.26     | 0.38                |
|        | 2320 - 35   | 4670           | 4083           | 4778           | 794             | 1892            | 2681            | 12217                         | 10545                         | 86.31     | 0.42                |
|        | 2335 - 50   | 6961           | 7465           | 4958           | 644             | 1681            | 3058            | 21709                         | 14748                         | 67.93     | 0.38                |
|        | 2350 - 65   | 3029           | 3513           | 3947           | 898             | 2384            | 4869            | 13773                         | 10743                         | 78.00     | 0.38                |
|        | 2365 - 80   | 5599           | 3840           | 2324           | 329             | 844             | 1293            | 12935                         | 7337                          | 56.72     | 0.39                |
|        | 2380 - 95   | 4778           | 4304           | 2604           | 373             | 867             | 613             | 12926                         | 8148                          | 63.04     | 0.43                |
|        | 2395 - 2410 | 3133           | 1788           | 1612           | 258             | 753             | 743             | 7533                          | 4410                          | 58.46     | 0.34                |
|        | 2410 - 25   | 3235           | 3132           | 1923           | 286             | 742             | 972             | 9319                          | 6084                          | 65.29     | 0.39                |
|        | 2425 - 40   | 6373           | 5007           | 4357           | 708             | 1661            | 620             | 18107                         | 11734                         | 64.80     | 0.43                |
|        | 2440 - 55   | 7737           | 5199           | 4592           | 786             | 1947            | 11842           | 20262                         | 12525                         | 61.82     | 0.40                |
|        | 2455 - 70   | 5396           | 4076           | 3474           | 562             | 1456            | 1749            | 14964                         | 9567                          | 63.93     | 0.39                |
|        | 2470 - 85   | 3401           | 2350           | 2201           | 379             | 877             | 527             | 9207                          | 5807                          | 63.07     | 0.43                |
|        | 2485 - 2500 | 553            | 574            | 607            | 91              | 330             | 470             | 2155                          | 1602                          | 74.34     | 0.28                |
|        | 2500 - 15   | 1941           | 1604           | 1503           | 229             | 521             | 437             | 5798                          | 3857                          | 66.52     | 0.44                |
|        | 2515 - 30   | 1930           | 1619           | 2012           | 344             | 977             | 11882           | 6883                          | 4952                          | 71.95     | 0.35                |
|        | 2530 - 45   | 2523           | 2383           | 2382           | 356             | 839             | 679             | 8485                          | 5960                          | 70.24     | 0.42                |
|        | 2545 - 60   | 58             | 186            | 1052           | 263             | 850             | 1623            | 2410                          | 2352                          | 97.60     | 0.31                |

| Sample | Depth (m)   | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | iC <sub>4</sub> | nC <sub>4</sub> | C <sub>5+</sub> | ΣC <sub>1</sub> -C <sub>4</sub> | ΣC <sub>2</sub> -C <sub>4</sub> | % wetness | $\frac{iC_4}{nC_4}$ |
|--------|-------------|----------------|----------------|----------------|-----------------|-----------------|-----------------|---------------------------------|---------------------------------|-----------|---------------------|
|        | 2560 - 75   | 6179           | 1316           | 2034           | 2615            | 1277            | 2165            | 5781                            | 5090                            | 88.05     | 2.05                |
|        | 2575 - 90   | 241            | 2069           | 2802           | 556             | 1388            | 7313            | 7056                            | 6815                            | 96.58     | 0.40                |
|        | 2590 - 2605 | 431            | 578            | 1691           | 461             | 1562            | 3495            | 4725                            | 4294                            | 90.88     | 0.30                |
|        | 2605 - 20   | 390            | 485            | 735            | 151             | 315             | 564             | 2077                            | 1687                            | 81.22     | 0.48                |
|        | 2620 - 35   | 5900           | 3182           | 1883           | 157             | 423             | 186             | 11546                           | 5647                            | 48.91     | 0.37                |
|        | 2625 - 50   | 4066           | 2018           | 1500           | 232             | 581             | 467             | 8397                            | 4332                            | 51.59     | 0.40                |
|        | 2650 - 65   | 25767          | 12031          | 6486           | 8529            | 5570            | 1221            | 58383                           | 32616                           | 55.87     | 1.53                |
|        | 2665 - 80   | 18657          | 7542           | 4809           | 2822            | 2432            | 794             | 36262                           | 17605                           | 48.55     | 1.16                |
|        | 2680 - 95   | 164            | 632            | 904            | 97              | 417             | 346             | 2215                            | 2051                            | 92.60     | 0.23                |
|        | 2695 - 2710 | 18427          | 2213           | 1826           | 1478            | 1034            | 542             | 24979                           | 6551                            | 26.23     | 1.43                |
|        | 2710 - 25   | 6857           | 2520           | 1999           | 1958            | 1362            | 819             | 14696                           | 7840                            | 53.35     | 1.44                |
|        | 2725 - 40   | 10522          | 4077           | 3012           | 3026            | 1878            | 952             | 22517                           | 11994                           | 53.27     | 1.61                |
|        | 2740 - 55   | 49439          | 15894          | 6341           | 3010            | 1731            | 242             | 76417                           | 26977                           | 35.30     | 1.74                |
|        | 2755 - 70   | 5472           | 2982           | 2360           | 1899            | 3713            | 272             | 16436                           | 10964                           | 66.71     | 0.51                |
|        | 2770 - 85   | 505            | 566            | 554            | 539             | 1176            | 263             | 3341                            | 2836                            | 84.88     | 0.46                |
|        | 2785 - 2800 | 2073           | 465            | 455            | 528             | 1202            | 197             | 4723                            | 2650                            | 56.11     | 0.44                |
|        | 2800 - 15   | 1641           | 1051           | 1181           | 1458            | 3553            | 873             | 8885                            | 7244                            | 81.53     | 0.41                |
|        | 2815 - 30   | 642            | 688            | 788            | 1017            | 2460            | 496             | 5596                            | 4953                            | 88.51     | 0.41                |
|        | 2830 - 45   | 268            | 221            | 290            | 478             | 1099            | 210             | 2357                            | 2089                            | 88.63     | 0.43                |
|        | 2845 - 60   | 1132           | 774            | 774            | 978             | 2347            | 822             | 6007                            | 4875                            | 81.16     | 0.42                |
|        | 2860 - 75   | 1023           | 1153           | 884            | 823             | 2020            | 944             | 5903                            | 4880                            | 82.67     | 0.41                |
|        | 2875 - 90   | 599            | 542            | 526            | 709             | 1659            | 241             | 4036                            | 3437                            | 85.16     | 0.43                |
|        | 2890 - 2900 | 1166           | 1023           | 1440           | 1654            | 3934            | 2004            | 9217                            | 8052                            | 87.36     | 0.42                |

TABLE II

## Lithology and Total Organic Carbon (TOC)

| IKU No. | Depth       | TOC  | Lithology  |
|---------|-------------|------|--|
| K 1192  | 1450 - 65   | 1,96 | 100 % claystone, grey, some slightly brownish; Sm.am. limestone, brown; Claystone, brownish light grey, slightly calcareous; |
| 1193    | 1465 - 80   | 1,84 | 100 % claystone, grey; Sm. am. Marl., brownish light grey;   |
| 1194    | 1480 - 95   | 1,71 | 100 % claystone, grey; Obs. ?Dolomite, brown; Sand, grain, rounded, coarse; Pyrite;  |
| 1195    | 1495 - 1510 | 1,72 | 100 % claystone, partly sandy, grey, light brown   |
| 1196    | 1510 - 25   | 1,50 | 100 % claystone, partly sandy, grey, some slightly green;  |
| 1197    | 1525 - 40   | 1,44 | 100 % claystone, partly sandy, grey, slightly greenish; light brownish;  |
| 1198    | 1540 - 55   | 1,07 | 100 % claystone, partly sandy, grey; Sm. am. Marl., brownish, light grey;  |
| 1199    | 1555 - 70   | 0,87 | 100 % claystone, partly sandy, light grey, slightly greenish;  |
| 1200    | 1570 - 85   | 0,84 | 100 % claystone, partly sandy, grey, brownish, light green;  |
| 1201    | 1585 - 1600 | 0,68 | 100 % claystone, grey, light green;  |
| 1202    | 1600 - 15   | 0,92 | 100 % claystone, grey, slightly brownish and greenish; Sm. am. Marl., brownish, light grey;                                  |
| 1203    | 1615 - 30   | 0,81 | 100 % claystone, partly sandy, grey, slightly brownish; Sm. am. Marl., brownish, light grey;                                 |
| 1204    | 1630 - 45   | 1,03 | 100 % claystone, partly sandy, grey, slightly brownish and greenish; Obs.: Dolomite, brown;                                  |
| 1205    | 1645 - 60   | 0,68 | 100 % claystone, partly sandy, grey and greenish. Sm. am. Dolomite, brown, light grey;                                       |
| 1206    | 1660 - 75   | 0,78 | 100 % claystone, partly sandy, grey, slightly green;   |
| 1207    | 1675 - 90   | 0,80 | 100 % claystone, partly sandy, grey, light brown slightly green;   |
| 1266    | 1690 - 1705 | 1,01 | 100 % claystone, grey, slightly green; Sm. am. Marl., brown, light grey;   |
| 1267    | 1705 - 20   | 1,28 | 100 % claystone, grey, slightly green; Sm. am. Marl., brown, light grey; Sandstone, grey, light, brownish;                   |

contd .....

| IKU No. | Depth       | TOC  | Lithology   |
|---------|-------------|------|---|
| K 1268  | 1720 - 35   | 0,89 | 100 % claystone, grey, slightly green; Sm. am. Marl., red-brown; Limestone, grey;   |
| 1269    | 1735 - 50   | 1,22 | 100 % claystone, grey, some brown, light green, dark grey; Sm. am. Marl., brown, light grey;  |
| 1270    | 1750 - 65   | 0,68 | 100 % claystone, grey to brown, red brown, dark grey; Sm. am. Marl., red-brown, light grey;   |
| 1271    | 1765 - 80   | 0,58 | 100 % claystone, grey to light brown, greenish, red-brown; Sm. am. coal;  |
| 1272    | 1780 - 95   | 0,60 | 95 % claystone, grey to brown; greenish, red-brown;<br>5 % coal; Sm. am. claystone, brownish light, grey, some calcareous; Quartz, white slightly brownish; |
| 1273    | 1795 - 1810 | 0,79 | 95 % claystone, grey to brownish, greenish, red brown;<br>5 % coal; Sm. am. claystone, light grey, some calcareous;   |
| 1274    | 1810 - 25   | 0,78 | 90 % claystone, grey, light brown, green, red brown;<br>10 % coal;<br>Sm. am. Marl., red brown; claystone, light grey, some calcareous;                     |
| 1275    | 1825 - 40   | 0,80 | 90 % claystone, grey, light brown, green;<br>10 % coal;<br>Sm. am. Quartz, white, slightly brownish;  |
| 1276    | 1840 - 55   | 0,89 | 95 % claystone, grey, light brown, green, red - brown;<br>5 % coal;<br>Sm. am. Quartz, white, slightly brownish, Marl. brown;                               |
| 1277    | 1855 - 70   | 0,82 | 100 % claystone, grey, light green; red-brown; Sm. am. Marl., red brown; Claystone, light grey, some calcareous; Coal;                                      |
| 1278    | 1870 - 85   | 0,92 | 100 % claystone, grey, light green; Sm. am. Marl., brown;   |
| 1279    | 1885 - 1900 | 1,36 | 100 % claystone, grey, light green, slightly brownish; Sm. am. Marl., light grey, red-brown;  |

| IKU No. | Depth       | TOC   | Lithology  |
|---------|-------------|---|--|
| K 1280  | 1900 - 1915 | 0,71  | 100 % claystone, grey, light green, slightly brownish, red-brown; Sm. am. Marl., light grey;   |
| 1281    | 1915 - 30   | 0,69  | 100 % claystone, grey, light green, slightly brownish, red-brown; Sm. am. Marl., as above.   |
| 1282    | 1930 - 45   | 0,70  | 100 % claystone, grey, light green; Sm. am red brown, limestone/Marl., white, light grey; Marl., red-brown; Coal.                                  |
| 1283    | 1945 - 60   | 0,74  | 100 % claystone/Marl., grey, light green; Sm. am. limestone, white, light grey;  |
| 1284    | 1960 - 75   | 0,61  | 100 % claystone, grey, light green; red-brown, brown; Sm. am. limestone, white, light grey, slightly brownish;                                     |
| 1285    | 1975 - 90   | 0,80  | 100 % claystone, grey, light green; Sm. am. limestone/Marl., white, light grey, slightly brownish; Coal;   |
| 1286    | 1990 - 2005 | 0,73  | 100 % claystone, grey, light green; Sm. am. limestone/Marl., white, light grey; Coal;  |
| 1287    | 2005 - 20   | 0,92  | 95 % claystone, grey, light green;<br>5 % coal;<br>Sm. am. limestone/Marl., white, light grey, slightly brownish;                                  |
| 1288    | 2020 - 35   | 0,83  | 85 % claystone, grey, light green;<br>15 % limestone/Marl., white, light grey;<br>Sm. am. coal;  |
| 1289    | 2035 - 50   | clayst.<br>0,89<br>lime<br>0,53<br>1,12<br>clayst.<br>0,80<br>limest.<br>0,22 | Claystone, red-brown, some calcareous;<br><br>85 % claystone, grey, light green; brown;<br>15 % limestone, white, light grey;<br><br>Sm. am. coal; |

| IKU No. | Depth       | TOC  | Lithology  |
|---------|-------------|--|--|
| K 1290  | 2050 - 65   | 0,96<br>clayst.<br>0,79<br>limest.<br>0,12 | 85 % claystone, grey, light green, brown;<br>15 % limestone, white, light grey;<br><br>Sm. am. coal; claystone, light grey, some calcareous;                             |
| 1291    | 2065 - 80   | 1,07                                       | 95 % claystone, grey, light green, some brown;<br>5 % limestone, white, grey;<br>Sm. am. Marl., red-brown;   |
| 1292    | 2095 - 2010 | 0,85<br>clayst.<br>0,82<br>limest.<br>0,21 | 90 % claystone, grey, light green;<br>10 % limestone, white, light grey;<br>Sm. am. Quartz, white;   |
| 1293    | 2010 - 2125 | 1,33<br>clayst.<br>0,77<br>limest.<br>0,25 | 40 % claystone, grey, light green;<br>60 % limestone, white, light grey;<br>Sm. am coal;   |
| 1294    | 2125 - 2140 | 1,75<br>clayst.<br>0,72<br>limest.<br>0,17 | 85 % claystone, grey, light green, some brown;<br>15 % limestone, white, light grey;<br>Sm. am. Marl., red-brown;  |
| 1295    | 2140 - 2155 | 0,89<br>clayst.<br>1,06<br>limest.<br>0,11 | 90 % claystone, grey, light green, some brown;<br>10 % limestone, white, light grey;<br>Sm. am. coal; Marl., red-brown;  |
| 1296    | 2155 - 70   | 3,43                                       | 90 % claystone, grey, dark grey-black, light green, some brown, red-brown;<br>5 % limestone, white, light grey;<br>5 % coal;<br>Sm. am. Marl., red-brown; Quarts, white; |
| 1297    | 2170 - 85   | 2,72                                       | 80 % claystone, grey, dark grey-to black, light green;<br>5 % limestone, white, light grey;<br>15 % coal;<br>Sm. am. Marl., red-brown;                                   |

| IKU No. | Depth      | TOC  | Lithology   |
|---------|------------|------|---|
| K 1397  | 2185 - 200 | 1,43 | 85% Claystone, grey, dark-black, light green;<br>redbrown<br>15% Coal;<br>sm.am. Limestone, white, light grey;<br>Marl, redbrown; |
| 1304    | 2200 - 15  | 2.26 | 90% Claystone, grey, dark, light green, redbrown,<br>10% Coal;<br>sm.am. Marl, redbrown   |
| 1305    | 2215 - 30  | 2,55 | 95% Claystone, grey, dark, light grey, redbrown;<br>5% Coal;<br>sm.am. Marl, redbrown; Quartz, white;                             |
| 1306    | 2230 - 45  | 1,62 | 90% Claystone, grey, dark, light green, redbrown;<br>10% Coal;<br>sm.am. Marl, redbrown;<br>Limestone, white light grey;          |
| 1307    | 2245 - 60  | 1,44 | 90% Claystone, grey, dark, light green, redbrown;<br>10% Coal;<br>sm.am. Limestone, white, light grey;<br>Marl, redbrown;         |
| 1308    | 2260 - 75  | 1,25 | 100% Claystone, grey, dark, light green; red-<br>brown;<br>sm.am. Coal;<br>Marl, redbrown;  |
| 1309    | 2275 - 90  | 1,11 | 95% Claystone, grey, light green;<br>5% Coal;<br>sm.am. Marl, redbrown;<br>Limestone, white, light grey;                          |
| 1310    | 2290 - 305 | 1,36 | 90% Claystone, grey, dark, light green, redbrown;<br>10% Coal;<br>sm.am. Limestone, white, light grey; Marl,<br>redbrown;         |
| 1311    | 2305 - 20  | 1,30 | 95% Claystone, grey, light green;<br>5% Coal;<br>sm.am. Limestone, white, light grey; Marl, red-<br>brown;                        |
| 1312    | 2320 - 35  | 1,28 | 100% Claystone, grey, light green;<br>sm.am. Limestone, white,<br>Coal; Quartz, white;  |
| 1313    | 2335 - 50  | 1,21 | 100% Claystone, grey, light green; redbrown;<br>sm.am. Limestone, white;<br>Quartz, white; Coal;                                  |

| IKU No. | Depth      | TOC  | Lithology  |
|---------|------------|------|--|
| K 1314  | 2350 - 65  | 0,59 | 30% Claystone, grey, light green; redbrown;<br>70% Sandstone, white, subangular, coarse - fine;<br>sm.am. Coal; Marl, redbrown;  |
| 1315    | 2365 - 80  | 1,79 | 100% Claystone, grey, dark-black, light green;<br>sm.am. Coal; Marl, grey; Quartz;   |
| 1316    | 2380 - 95  | 2,07 | 100% Claystone, grey, light green;<br>sm.am. Coal; Marl, redbrown;<br>Quartz, white;   |
| 1317    | 2395 - 410 | 2.22 | 90% Claystone, grey, dark, light green, redbrown;<br>10% Sandstone, white, angular coarse;<br>sm.am. Coal; Marl, redbrown;<br>Limestone, white;  |
| 1318    | 2410 - 25  | 1,37 | 90% Claystone, grey, light green;<br>10% Sandstone, white, rounded, coarse;<br>sm.am. Coal; Limestone, white, light grey;<br>Marl, redbrown;   |
| 1319    | 2425 - 40  | 1,22 | 100% Claystone, grey, dark, light green;<br>sm.am. Limestone, white;<br>Marl, redbrown; Coal; sand grains rounded,<br>coarse;  |
| 1320    | 2440 - 55  | 2,19 | 100% Claystone, partly sandy, grey, dark, light<br>green, redbrown;<br>sma.am. Marl, redbrown Limestone, white;  |
| 1321    | 2455 - 70  | 2,96 | 100% Claystone, partly sandy, grey, dark, light<br>green;<br>sm.am. Marl, redbrown; Quartz, white;   |
| 1322    | 2470 - 85  | 2,65 | 90% Claystone, grey, dark, light green, redbrown;<br>10% Sandstone, white, subangular, very fine -<br>coarse;<br>sm.am. Marl, redbrown; Coal; Limestone, white;                        |
| 1323    | 2485 - 500 | 1,18 | 95% Claystone, grey, dark, green; redbrown;<br>5% Sandstone, white, rounded, very fine,<br>some calcareous;<br>sm.am. Marl, redbrown; Coal; sand grain, light<br>grey, rounded coarse; |
| 1324    | 2500 - 15  | 1,50 | 60% Claystone, as above;<br>40% Sandstone; white light grey, rounded, very<br>fine - fine;<br>sm.am. Marl, redbrown; Limestone, white;   |



| IKU No. | Depth      | TOC  | Lithology   |
|---------|------------|------|---|
| K 1325  | 2515 - 30  | 1,67 | 50% Claystone, grey, dark, light green;<br>50% Sandstone, redbrown; white, subangular,<br>very fine - fine;<br>sm.am. Marl, redbrown; Sand grain, grey,<br>rounded, coarse; Limestone, white; |
| 1326    | 2530 - 45  | 2,04 | 50% Claystone, as above<br>50% Sandstone, white, rounded, very fine;<br>sm.am. Marl, silty, light browngrey; Sand<br>grains, light grey, subangular, coarse;                                  |
| 1389    | 2545 - 60  | 2,38 | 60% Claystone, grey, light green, redbrown;<br>40% Sandstone, white, rounded, very fine;<br>sm.am. Marl, silty, light browngrey; Quartz,<br>white; Limestone, light grey;                     |
| 1390    | 2560 - 75  | 2,02 | 70% Claystone, grey, dark, light green, redbrown;<br>30% Sandstone, white, rounded, very fine -<br>fine;<br>sm.am. Marl, redbrown;  |
| 1391    | 2575 - 90  | 1,79 | 50% Claystone, grey, dark, light green, red-<br>brown;<br>50% Sandstone, white, rounded, very fine - fine;<br>sm.am. Marl, redbrown; Mica, white;   |
| 1392    | 2590 - 605 | 2,09 | 50% Claystone, grey, dark, light green, red-<br>brown;<br>50% Sandstone, light, grey, rounded, very fine -<br>fine;<br>sm.am. Marl, redbrown; Coal; Mica, white;                              |
| 1393    | 2605 - 20  | 2,22 | 70% Claystone, grey, light green; redbrown,<br>dark grey;<br>30% Sandstone, light grey, angular - subangular,<br>very fine - fine;<br>sm.am. Marl, redbrown; Mica, white;                     |
| 1394    | 2620 - 35  | 1,26 | 50% Claystone, grey, light green; redbrown;<br>43% Carb. shale, dark grey to black;<br>7% Coal<br>sm.am. Limestone, white; Marl, redbrown;<br>Sand grain, white, rounded, coarse;             |
| 1395    | 2635 - 50  | 1,49 | 90% Claystone, grey, light green; redbrown;<br>10% Sand/sandstone, white, angular/subangular,<br>very fine,<br>sm.am. Quartz, white; Coal; Marl, redbrown;                                    |

| IKU No. | Depth       | TOC          | Lithology  |
|---------|-------------|--------------|--|
| K 1396  | 2650 - 65   | 2,79         | 100% Claystone, grey, light green; redbrown; sm.am. Coal; Marl, redbrown; Sand grain, white subangular, coarse, Limestone, white to light grey;  |
| 1397    | 2665 - 80   | 1,77         | 30% Claystone, light grey to green; redbrown; 65% Sand/Sandstone, white to light grey; subangular/angular, coarse-medium; 5% Coal; sm.am. Marl, redbrown; Limestone, white; Mica, white; |
| 1398    | 2680 - 95   | 1,30         | 70% Claystone, grey, light grey to green, redbrown; 25% Sand/Sandstone, as above; 5% Coal; sm.am. Marl, redbrown; Limestone, white;  |
| 1399    | 2695 - 710  | 1,37         | 85% Claystone, grey to light green; 10% Sand/Sandstone, as above; 5% Coal; sm.am. Marl, redbrown;  |
| 1400    | 2710 - 725  | 1,35<br>0,23 | 60% Claystone, grey, dark, light grey; redbrown; 10% Limestone, white; 30% Sand/Sandstone, as above; sm.am. Marl, redbrown;  |
| 1401    | 2725 - 40   | 1,82<br>0,23 | 60% Claystone, light grey to green, 30% Sandstone, white, subangular, angular, very fine - fine - coarse; 10% Limestone, white; sm.am. Coal; Marl, red-brown;                            |
| 1402    | 2740 - 55   | 1,63         | 20% Claystone, silty, grey, light, dark, redbrown, green; 60% Sand/Sandstone, white, rounded, very fine; 20% Coal; sm.am. Limestone, white; Marl, redbrown;                              |
| 1479    | 2755 - 70   | 0,99         | 60% Claystone, silty, medium grey, redbrown, green; 10% Sandstone, white, subangular, fine to coarse; sm.am. Coal;   |
| 1480    | 2770 - 85   | 0,93         | 60% Claystone, silty, light to dark grey, green, redbrown; 40% Sand/Sandstone, white, subangular/angular, fine - very coarse; sm.am. Marl; redbrown; Coal;                               |
| 1481    | 2785 - 2800 | 0,92         | 40% Claystone, silty, light to dark grey, green; redbrown; 55% Sand/sandstone, as above 5% Limestone, white; sm.am. Coal; Marl, redbrown;  |

| IKU No. | Depth       | TOC  | Lithology  |
|---------|-------------|------|--|
| K 1482  | 2800 - 15   | 0,95 | 50% Claystone, redbrown, medium grey, green;<br>50% Sandstone, white, angular/subangular, very fine.<br>sm.am. Limestone, white; Coal                  |
| 1483    | 2815 - 30   | 0,75 | 60% Claystone, silty, redbrown, light grey, green;<br>40% Sand/Sandstone, white, very fine, to fine medium, coarse;<br>sm.am. Coal; fine stane, white; |
| 1484    | 2830 - 45   | 0,43 | 95% Claystone, silty, redbrown, light grey, green;<br>5% Sandstone, white rounded, coarse<br>sm.am. Limestone, white, Coal;                            |
| 1485    | 2845 - 60   | 0,79 | 85% Claystone, silty, redbrown, medium grey, green;<br>15% Sand/Sandstone, white, angular/subangular, fine to coarse<br>sm.am. Limestone, light grey;  |
| 1486    | 2860 - 75   | 0,99 | 15% Claystone, redbrown, light grey, green;<br>85% Sand/Sandstone, white; angular/subangular, fine to coarse;<br>sm.am. Limestone, white; Coal;        |
| 1487    | 2875 - 90   | 0,68 | 15% Claystone, redbrown, medium grey, green,<br>85% Sand/Sandstone, white, very fine to coarse<br>sm.am. Limestone, white; Coal!                       |
| 1488    | 2890 - 2905 | 0,87 | 50% Claystone, redbrown, grey, green<br>50% Sandstone, white, very fine to coarse;<br>sm.am. Limestone, white; Coal;                                   |

Weight (mg) of EOM and chromatographic fractions

| Sample | Depth(m)  | Rock extracted (g) | EOM   | Sat. | Aro. | HC    | Non HC | TOC  |
|--------|-----------|--------------------|-------|------|------|-------|--------|------|
| K1195  | 1495-1510 | 95.2               | 16.9  | 0.9  | 1.4  | 2.3   | 3.6    | 1.72 |
| K1206  | 1660-1675 | 71.9               | 9.3   | 0.7  | 1.6  | 2.3   | 2.6    | 0.78 |
| K1270  | 1750-1765 | 42.8               | 28.3  | 4.9  | 8.6  | 13.5  | 11.1   | 0.68 |
| K1279  | 1885-1900 | 76.3               | 7.5   | 0.6  | 1.7  | 2.3   | 2.2    | 1.36 |
| K1283  | 1945-1960 | 79.8               | 28.2  | 3.4  | 7.0  | 10.4  | 9.7    | 0.74 |
| K1289  | 2036-2050 | 86.9               | 14.2  | 0.8  | 2.2  | 3.0   | 0.5    | 1.12 |
| K1296  | 2155-2170 | 98.3               | 276.7 | 50.0 | 59.3 | 109.3 | 82.3   | 3.43 |
| K1303  | 2185-2200 | 41.5               | 32.2  | 3.7  | 7.6  | 11.3  | 6.4    | 1.43 |
| K1308  | 2260-2275 | 32.7               | 55.0  | 5.6  | 7.2  | 12.8  | 17.6   | 1.25 |
| K1311  | 2305-2320 | 40.1               | 32.4  | 6.9  | 6.0  | 12.9  | 5.9    | 1.30 |
| K1316  | 2380-2395 | 36.7               | 38.7  | 7.2  | 7.7  | 14.9  | 12.8   | 2.07 |
| K1321  | 2455-2470 | 45.9               | 70.1  | 16.3 | 15.3 | 31.6  | 18.4   | 2.96 |
| K1326  | 2530-2545 | 49.9               | 46.0  | 8.7  | 11.1 | 19.8  | 11.2   | 2.04 |
| K1392  | 2590-2605 | 36.1               | 41.7  | 7.2  | 9.3  | 16.5  | 12.2   | 2.09 |
| K1396  | 2650-2565 | 101.4              | 114.9 | 8.3  | 29.0 | 37.3  | 41.4   | 2.79 |
| K1484  | 2830-2845 | 63.8               | 10.0  | 0.4  | 1.4  | 1.8   | 2.7    | 0.43 |

Table IV

Concentration of EOM and chromatographic fractions (Weight ppm of rock)

| IKU No. | Depth (m) | EOM    | SAT   | Aro   | Total hydrocarb. | Non hydrocarb. |
|---------|-----------|--------|-------|-------|------------------|----------------|
| K1195   | 1495-1510 | 178.-  | 9.-   | 15.-  | 24.-             | 38.-           |
| K1206   | 1660-1675 | 129.-  | 10.-  | 22.-  | 32.-             | 36.-           |
| K1270   | 1750-1765 | 661.-  | 114.- | 201.- | 315.-            | 259.-          |
| K1279   | 1885-1900 | 98.-   | 8.-   | 22.-  | 30.-             | 29.-           |
| K1283   | 1945-1960 | 353.-  | 43.-  | 88.-  | 130.-            | 122.-          |
| K1289   | 2035-2050 | 163.-  | 9.-   | 25.-  | 34.-             | 6.-            |
| K1296   | 2155-2170 | 2815.- | 509.- | 603.- | 1112.-           | 837.-          |
| K1303   | 2185-2200 | 776.-  | 89.-  | 183.- | 272.-            | 154.-          |
| K1308   | 2260-2275 | 1682.- | 171.- | 220.- | 391.-            | 538.-          |
| K1311   | 2305-2320 | 808.-  | 172.- | 150.- | 322.-            | 147.-          |
| K1316   | 2380-2395 | 1055.- | 196.- | 210.- | 406.-            | 349.-          |
| K1321   | 2455-2470 | 1527.- | 355.- | 333.- | 688.-            | 401.-          |
| K1326   | 2530-2545 | 922.-  | 174.- | 222.- | 397.-            | 224.-          |
| K1392   | 2590-2605 | 1155.- | 199.- | 258.- | 338.-            | 338.-          |
| K1396   | 2650-2665 | 1133.- | 82.-  | 286.- | 368.-            | 408.-          |
| K1484   | 2830-2845 | 157.-  | 6.-   | 22.-  | 28.-             | 42.-           |

Table V

Concentration of EOM and chromatographic fractions (mg/g TOC)

| IKU No. | Depth (m) | EOM   | SAT  | Aro  | Total hydrocarb. | Non hydrocarb. |
|---------|-----------|-------|------|------|------------------|----------------|
| K1195   | 1495-1510 | 10.-  | 1.-  | 1.-  | 2.-              | 2.-            |
| K1206   | 1660-1675 | 17.-  | 1.-  | 3.-  | 4.-              | 5.-            |
| K1270   | 1750-1765 | 97.-  | 17.- | 30.- | 46.-             | 38.-           |
| K1279   | 1885-1900 | 7.-   | 1.-  | 2.-  | 3.-              | 2.-            |
| K1283   | 1945-1960 | 48.-  | 6.-  | 12.- | 18.-             | 16.-           |
| K1289   | 2035-2050 | 15.-  | 1.-  | 2.-  | 3.-              | 1.-            |
| K1296   | 2155-2170 | 82.-  | 15.- | 18.- | 33.-             | 24.-           |
| K1303   | 2085-2200 | 54.-  | 6.-  | 13.- | 19.-             | 11.-           |
| K1308   | 2260-2275 | 135.- | 14.- | 18.- | 31.-             | 43.-           |
| K1311   | 2305-2320 | 62.-  | 13.- | 12.- | 25.-             | 11.-           |
| K1316   | 2380-2395 | 51.-  | 9.-  | 10.- | 20.-             | 17.-           |
| K1321   | 2455-2460 | 52.-  | 12.- | 11.- | 23.-             | 14.-           |
| K1326   | 2530-2545 | 45.-  | 9.-  | 11.- | 19.-             | 11.-           |
| K1392   | 2590-2605 | 55.-  | 10.- | 12.- | 16.-             | 16.-           |
| K1396   | 2650-2665 | 41.-  | 3.-  | 10.- | 13.-             | 15.-           |
| K1484   | 2830-2845 | 36.-  | 1.-  | 5.-  | 7.-              | 10.-           |

Table VI

COMPOSITION IN % OF THE MATERIAL EXTRACTED FROM THE ROCK

| IKU No. | Depth (m) | $\frac{\text{Sat}}{\text{EOM}}$ | $\frac{\text{Aro}}{\text{EOM}}$ | $\frac{\text{HC}}{\text{EOM}}$ | $\frac{\text{Sat}}{\text{Aro}}$ | $\frac{\text{Non HC}}{\text{EOM}}$ | $\frac{\text{HC}}{\text{Non HC}}$ |
|---------|-----------|---------------------------------|---------------------------------|--------------------------------|---------------------------------|------------------------------------|-----------------------------------|
| K 1195  | 1495-1510 | 5.3                             | 8.3                             | 13.6                           | 64.3                            | 21.3                               | 63.9                              |
| K 1206  | 1660-1675 | 8.2                             | 17.1                            | 25.3                           | 44.2                            | 28.3                               | 88.2                              |
| K 1270  | 1750-1765 | 17.3                            | 30.4                            | 47.7                           | 57.0                            | 39.2                               | 121.6                             |
| K 1279  | 1885-1900 | 8.0                             | 22.7                            | 30.7                           | 35.3                            | 29.3                               | 104.6                             |
| K 1283  | 1945-1960 | 12.1                            | 24.8                            | 36.9                           | 48.6                            | 34.4                               | 107.2                             |
| K 1289  | 2035-2050 | 5.5                             | 15.3                            | 20.8                           | 36.0                            | 3.4                                | 17.6                              |
| K 1296  | 2155-2170 | 18.1                            | 21.4                            | 39.5                           | 84.3                            | 29.7                               | 132.8                             |
| K 1303  | 2185-2200 | 11.5                            | 23.6                            | 35.1                           | 48.7                            | 19.9                               | 176.6                             |
| K 1308  | 2260-2275 | 10.2                            | 13.1                            | 23.3                           | 77.8                            | 32.0                               | 72.7                              |
| K 1311  | 2305-2320 | 21.3                            | 18.5                            | 39.8                           | 115.0                           | 18.2                               | 218.6                             |
| K 1316  | 2380-2395 | 19.0                            | 20.0                            | 39.0                           | 94.0                            | 33.0                               | 116.0                             |
| K 1321  | 2455-2470 | 23.0                            | 22.0                            | 45.0                           | 107.0                           | 26.0                               | 172.0                             |
| K 1326  | 2530-2545 | 19.0                            | 24.0                            | 43.0                           | 78.0                            | 24.0                               | 177.0                             |
| K 1392  | 2590-2605 | 17.0                            | 22.0                            | 29.0                           | 77.0                            | 29.0                               | 100.0                             |
| K 1396  | 2650-2665 | 7.0                             | 25.0                            | 32.0                           | 29.0                            | 36.0                               | 90.0                              |
| K 1484  | 2830-2845 | 4.0                             | 14.0                            | 18.0                           | 29.0                            | 27.0                               | 67.0                              |

Table VII

Tabulation of data from the gas chromatograms

| IKU Sample No | Depth     | Pristane/nC <sub>17</sub> | <u>Pristane</u><br><u>Phytane</u> | CPI  |
|---------------|-----------|---------------------------|-----------------------------------|------|
| K1195         | 1495-1510 | 1.50                      | 3.41                              | 1.20 |
| K1206         | 1660-1675 | 0.84                      | 2.10                              | 1.83 |
| K1270         | 1750-1765 | 1.40                      | 2.73                              | 2.42 |
| K1279         | 1855-1900 | 1.42                      | 2.57                              | 1.25 |
| K1283         | 1945-1960 | 1.46                      | 0.96                              | 1.26 |
| K1289         | 2035-2050 | 1.30                      | 1.49                              | 1.26 |
| K1296         | 2155-2170 | 1.45                      | 1.51                              | 1.20 |
| K1303         | 2185-2200 | 1.49                      | 1.67                              | 1.14 |
| K1308         | 2260-2275 | 1.11                      | 1.69                              | 1.47 |
| K1311         | 2305-2320 | 0.93                      | 1.82                              | 1.11 |
| K1316         | 2380-2395 | 1.71                      | 1.66                              | 1.33 |
| K1321         | 2455-2470 | 1.62                      | 1.62                              | 1.25 |
| K1326         | 2530-2545 | 1.63                      | 1.64                              | 1.25 |
| K1392         | 2590-2605 | 1.73                      | 1.90                              | 1.25 |
| K1396         | 2650-2665 | 3.06                      | 4.42                              | 1.39 |
| K1486         | 2860-2875 | 1.73                      | 2.90                              | 1.04 |

*Dublin*



Table VIII

## VITRINITE REFLECTANCE AND VISUAL KEROGEN MEASUREMENTS

| Depth (m) | Vitrinite reflectance | Color index | Type of organic matter            |
|-----------|-----------------------|-------------|-----------------------------------|
| 1440      | 0.31(21)              | -2/2        | Am/He, W, Cysts                   |
| 1630      | 0.37( 8)              |             |                                   |
| 1695      |                       | -2/2        | Am/Cut, W, Poll-spor, Cysts       |
| 1705      | 0.37(20)              |             |                                   |
| 1800      |                       | -2/2        | W/He, Am                          |
| 1810      | 0.30(23)              |             |                                   |
| 1880      |                       |             |                                   |
| 1885      | 0.38(20)              | -2/2        | Am, Cysts/W, He, Pollen           |
| 1960      | 0.37( 4)              | 2           | Am, Cysts/He, Pollen              |
| 2063      | 0.40( 3)              | 2           | He/Am, Poll-spor, Cysts           |
| 2126      | 0.35(20)              | 2-/2+       | W, He/Am                          |
| 2173      | 0.41(16)              | 2           | Am/Cysts, Poll-spor, He, Coal R!  |
| 2230      | 0.31(20)              | 2           | Am/He, W, Poll-spor               |
| 2290      | 0.35(20)              |             | Am/Cysts, He, W                   |
| 2348      | 0.35( 3)              |             | W, Coal R!                        |
| 2390      |                       | 2           | Am/He, Poll-spor                  |
| 2430      |                       | 2           | Am/He, Cut, Poll-spor, W          |
| 2477      | 0.46(20)              | 2/2+ (ox)   | Am/He, Cut, Poll-spor, W          |
| 2529      |                       | 2           | W, He, Cut, Poll-spor/Am Cysts    |
| 2539      | 0.37(20)              |             |                                   |
| 2581      |                       | 2/2+        | He/Am, W, Cut, Poll-spor, Coal R! |
| 2598      | 0.48(20)              |             |                                   |
| 2605      |                       | 2/2+        | Am, He, Cut, W                    |
| 2628      |                       | 2/2+        | Am, Cut, W, He, Poll-spor, Cysts  |
| 2633      |                       |             | (Barren)                          |
| 2676      |                       | 2/2+        | He, Poll-spor/Am, Cysts           |

VITRINITE REFLECTANCE AND VISUAL KEROGEN MEASUREMENTS

| Depth (m) | Vitrinite reflectance          | Color index | Type of organic matter |
|-----------|--------------------------------|-------------|------------------------|
| 2686      | 0.37(18)                       |             |                        |
| 2743      | NDP                            | -3 (ox)     | Am/He                  |
| 2790,5    |                                | -3 (ox)     | Almost barren          |
| 2799      | NDP                            |             |                        |
| 2851,5    | 0.44(9)                        |             |                        |
| 2864      |                                |             | (Barren)               |
| 2884      | 0.36(21)                       | 2           | Am/He, Coal R!         |
|           | NDP: No determination possible |             |                        |

TABLE IX

## ROCK EVAL PYROLYSIS

| Sample | Depth     | S <sub>1</sub> | S <sub>2</sub> | S <sub>3</sub> | C <sub>org</sub> | Hydrogen Index | Oxygen Index | Oil or gas content (S <sub>1</sub> + S <sub>2</sub> ) | Production Index $\frac{S_1}{S_1 + S_2}$ | Tmax °C |
|--------|-----------|----------------|----------------|----------------|------------------|----------------|--------------|---|--|---------|
| K1195  | 1495-1510 | 0.64           | 2.48           | 1.84           | 1.72             | 143.90         | 106.40       | 3.12  | 0.21                                     | 429     |
| K1202  | 1600- 15  | 0.16           | 0.37           | 2.04           | 0.92             | 40.11          | 221.74       | 0.53  | 0.30                                     | 426     |
| K1206  | 1660- 75  | 0.12           | 0.35           | 1.60           | 0.78             | 45.39          | 205.39       | 0.47  | 0.25                                     | 432     |
| K1269  | 1735- 50  | 0.27           | 0.79           | 2.71           | 1.22             | 64.92          | 222.20       | 1.06  | 0.25                                     | 429     |
| K1270  | 1750- 65  | 0.14           | 0.66           | 0.73           | 0.68             | 97.50          | 107.65       | 0.80  | 0.17                                     | 434     |
| K1275  | 1825- 40  | 0.14           | 0.90           | 1.51           | 0.80             | 112.5          | 188.75       | 1.04  | 0.14                                     | 432     |
| K1279  | 1885-1900 | 0.32           | 1.23           | 2.18           | 1.36             | 90.44          | 160.29       | 1.55  | 0.21                                     | 435     |
| K1283  | 1945- 60  | 0.20           | 0.53           | 2.17           | 0.74             | 71.62          | 293.24       | 0.74  | 0.27                                     | 434     |
| K1287  | 2005- 20  | 0.52           | 1.38           | 1.47           | 0.92             | 150.00         | 159.78       | 1.90  | 0.26                                     | 433     |
| K1289  | 2035- 50  | 0.28           | 0.67           | 1.44           | 1.12             | 59.82          | 128.57       | 0.95  | 0.30                                     | 438     |
| K1294  | 2125- 40  | 0.29           | 0.53           | 0.88           | 1.75             | 30.29          | 50.29        | 0.82  | 0.35                                     | 439     |
| K1296  | 2155- 70  | 0.74           | 14.74          | 0.78           | 3.43             | 429.74         | 22.74        | 15.48   | 0.05                                     | 425     |
| K1297  | 2170- 85  | 0.43           | 6.34           | 0.89           | 2.72             | 233.09         | 32.72        | 6.77  | 0.06                                     | 426     |
| K1304  | 2200- 15  | 0.21           | 2.41           | 0.93           | 2.26             | 106.64         | 41.15        | 2.62  | 0.08                                     | 434     |
| K1305  | 2215- 30  | 0.58           | 7.59           | 0.78           | 2.55             | 297.65         | 30.59        | 8.17  | 0.07                                     | 426     |
| K1306  | 2230- 45  | 0.30           | 1.35           | 0.90           | 1.62             | 83.33          | 55.56        | 1.65  | 0.18                                     | 437     |
| K1308  | 2260- 75  | 0.30           | 1.58           | 0.81           | 1.25             | 126.4          | 64.80        | 1.88  | 0.16                                     | 436     |
| K1311  | 2305- 20  | 0.28           | 1.64           | 0.76           | 1.30             | 126.15         | 58.46        | 1.92  | 0.15                                     | 428     |
| K1316  | 2380- 95  | 0.24           | 5.54           | 0.68           | 2.07             | 267,63         | 32.85        | 5.78  | 0.04                                     | 429     |

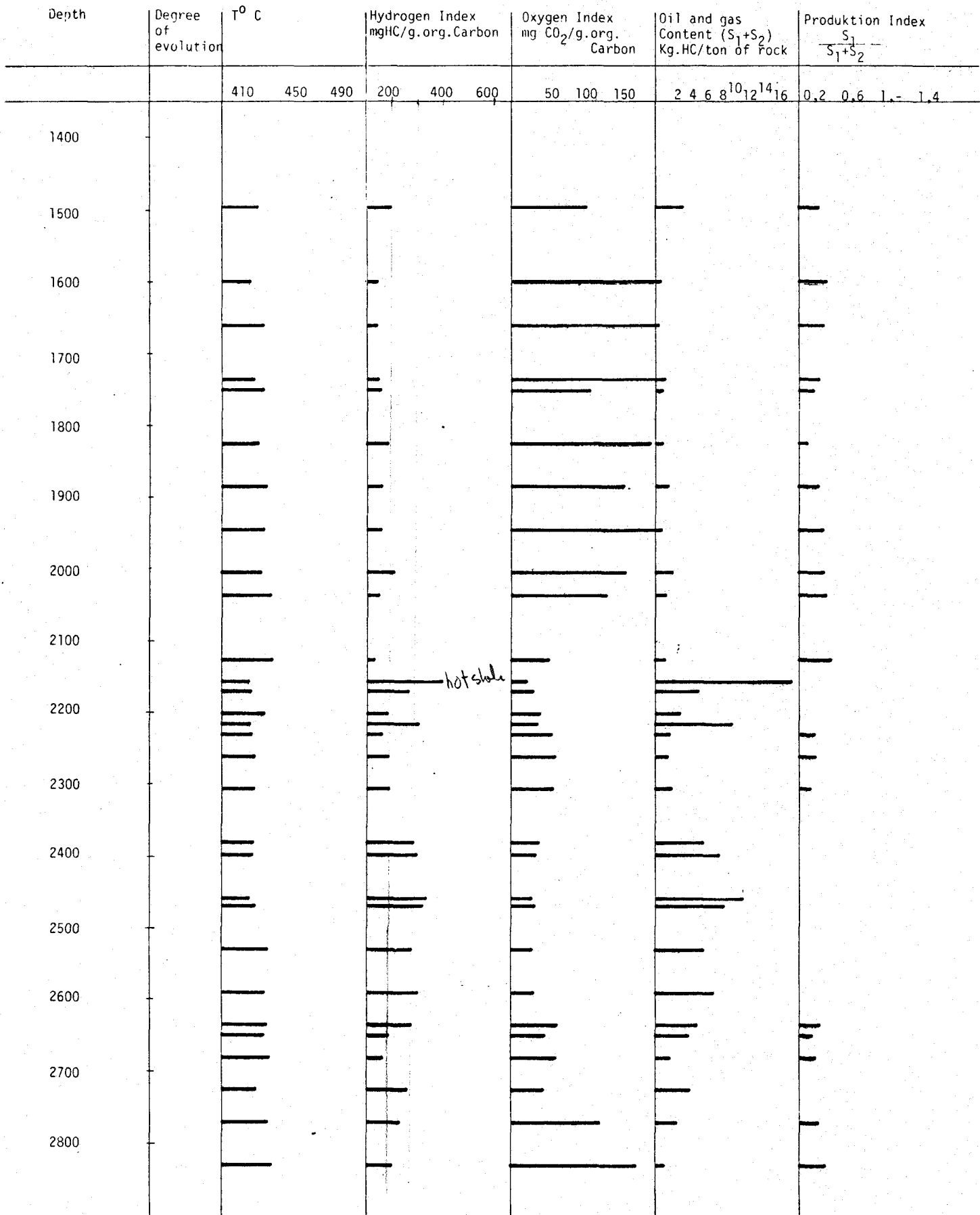
TABLE IX  
Rock Eval Pyrolysis

| Sample | Depth     | S <sub>1</sub> | S <sub>2</sub> | S <sub>3</sub> | C <sub>org</sub> | Hydrogen Index | Oxygen Index | Oil or gas content (S <sub>1</sub> + S <sub>2</sub> ) | Production Index $\frac{S_1}{S_1 + S_2}$ | Tmax °C |
|--------|-----------|----------------|----------------|----------------|------------------|----------------|--------------|---|--|---------|
| K1317  | 2395-2410 | 0.50           | 6.44           | 0.71           | 2.22             | 290.09         | 31.98        | 6.94  | 0.07                                     | 427     |
| K1321  | 2455- 70  | 0.66           | 9.16           | 0.76           | 2.96             | 309.46         | 25.68        | 9.82  | 0.07                                     | 424     |
| K1322  | 2470- 85  | 0.53           | 7.26           | 0.81           | 2.65             | 273.96         | 30.57        | 7.79  | 0.07                                     | 429     |
| K1326  | 2530- 45  | 0.30           | 4.90           | 0.60           | 2.04             | 240.20         | 29.41        | 5.20  | 0.06                                     | 435     |
| K1392  | 2590-2605 | 0.54           | 5.66           | 0.63           | 2.09             | 270.81         | 30.14        | 6.20  | 0.09                                     | 433     |
| K1395  | 2635- 50  | 0.97           | 3.39           | 0.97           | 1.49             | 227.52         | 65.10        | 4.36  | 0.22                                     | 435     |
| K1396  | 2650- 65  | 0.50           | 3.09           | 1.25           | 2.79             | 110-75         | 44.80        | 3.59  | 0.14                                     | 434     |
| K1398  | 2680- 95  | 0.27           | 1.13           | 0.85           | 1.30             | 86.92          | 65.39        | 1.40  | 0.19                                     | 437     |
| K1401  | 2725- 40  | 0.27           | 3.71           | 0.80           | 1.82             | 203.85         | 43.96        | 3.98  | 0.07                                     | 428     |
| K1480  | 2770- 85  | 0.45           | 1.68           | 1.15           | 0.93             | 180.65         | 123.66       | 2.13  | 0.21                                     | 435     |
| K1484  | 2830- 45  | 0.29           | 0.57           | 0.74           | 0.43             | 132.56         | 172.09       | 0.86  | 0.34                                     | 437     |

105

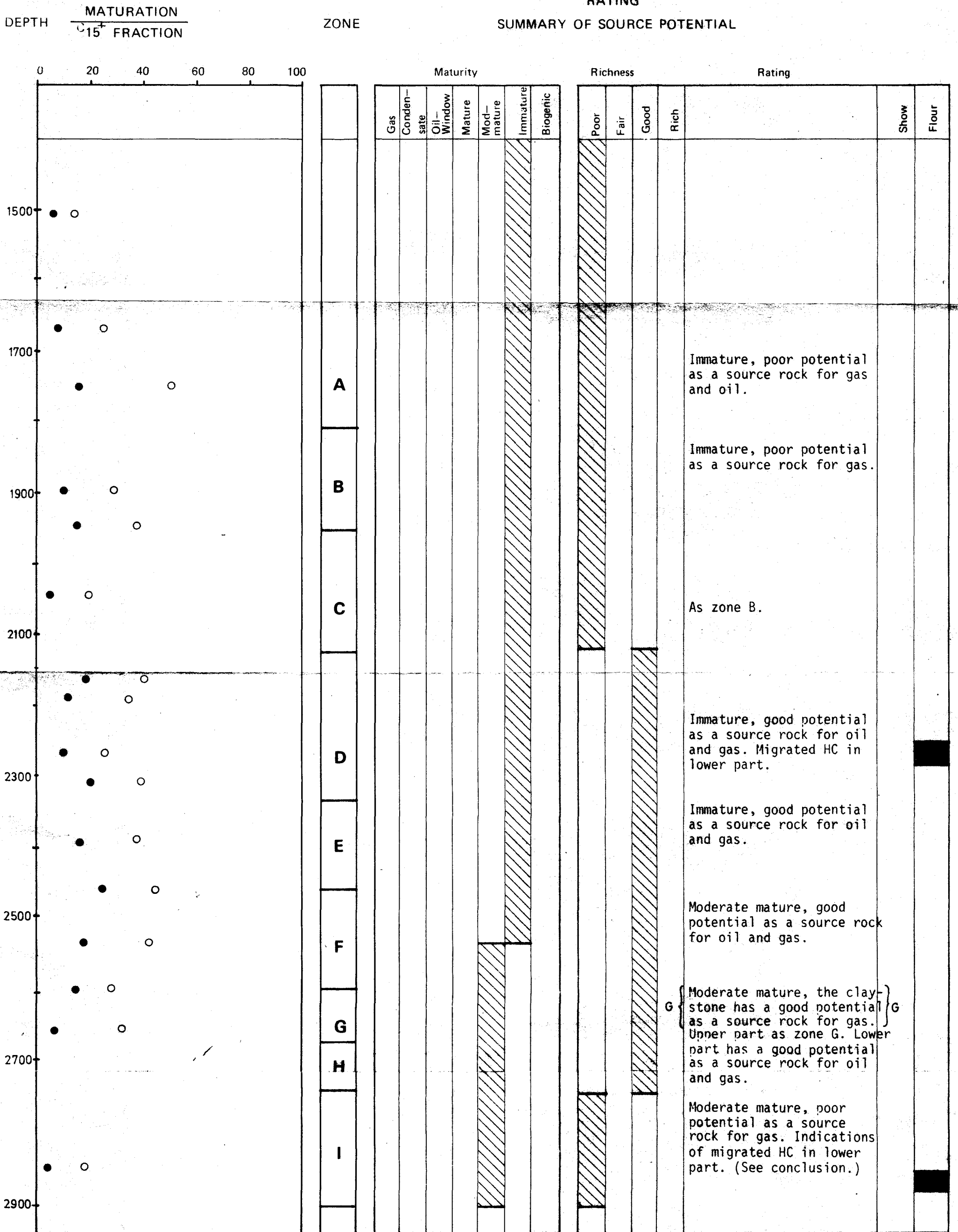
Prøver fra 'hot sh' (2746-2777) er ikke med for Ro og Visual Kerogen (omfatter både 'type kerogen' og 'spore coloration'). Vi bør søge kartlegge modningsgraden for hot sh. området for å forstå dannelse/migrasjon av HC. Ro og vis. kerogen burde supplere de andre metadene i intervallet 2746-2777, særlig siden resultatene er litt anvendbare. Ro er den mest pålitelige modningsindeks. *Ng*

Rock - Eval Pyrolysis



INTERPRETATION DIAGRAM

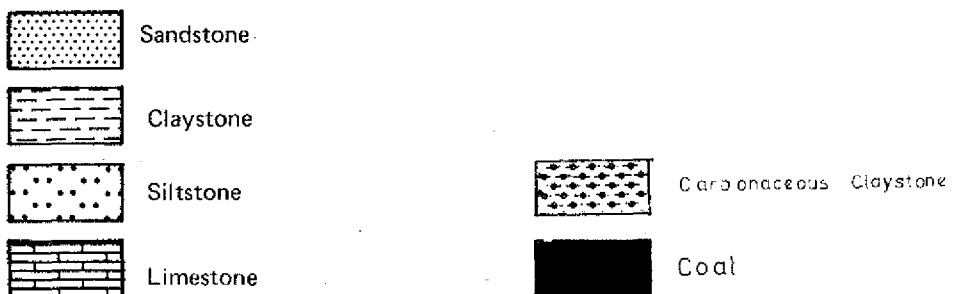
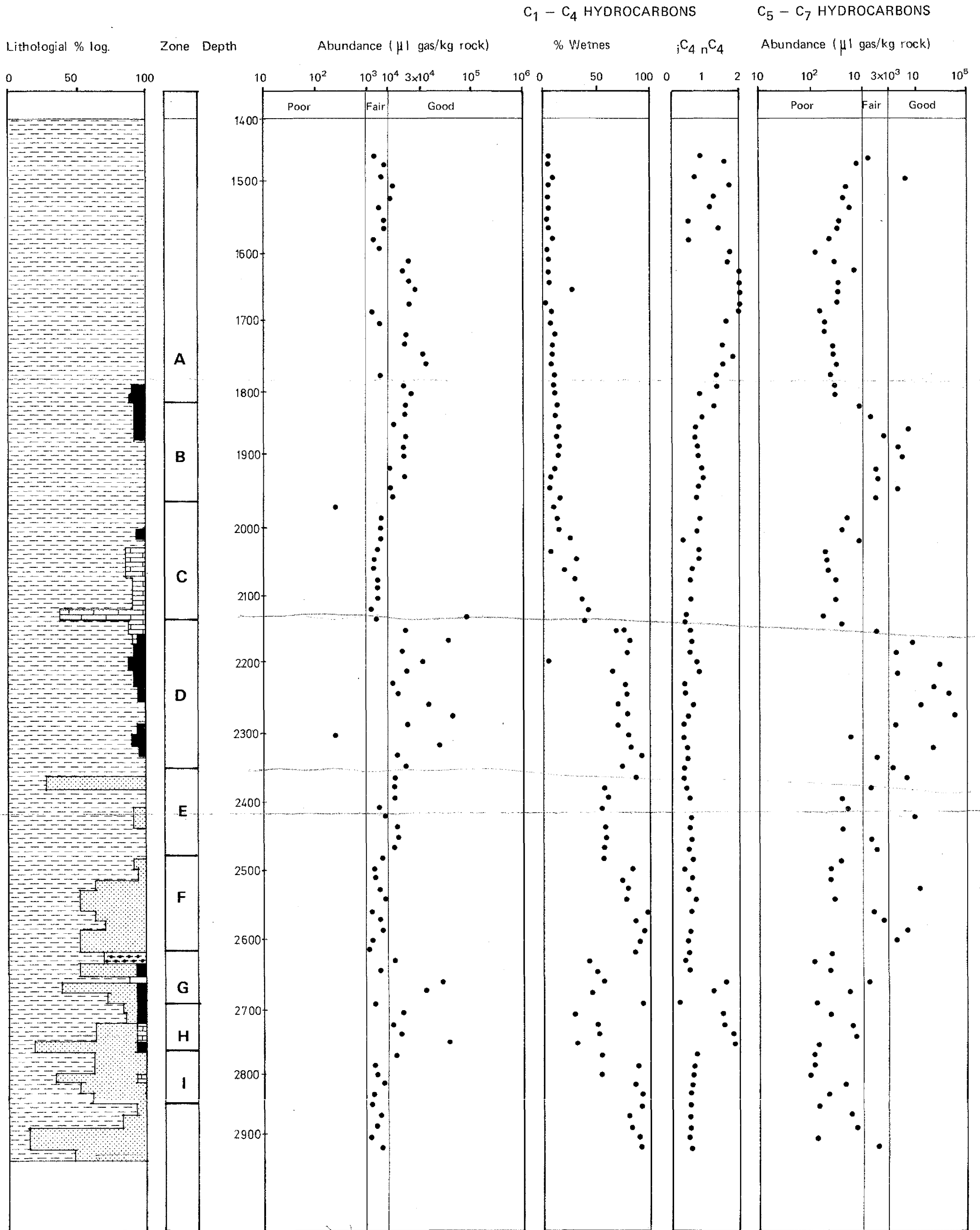
31/4-2



● %  $\frac{\text{Sat}}{\text{EOM}}$       ○ %  $\frac{\text{HC}}{\text{EOM}}$

Sat: Saturated Hydrocarbons  
 HC: Hydrocarbons  
 EOM: Extractable Organic Matter

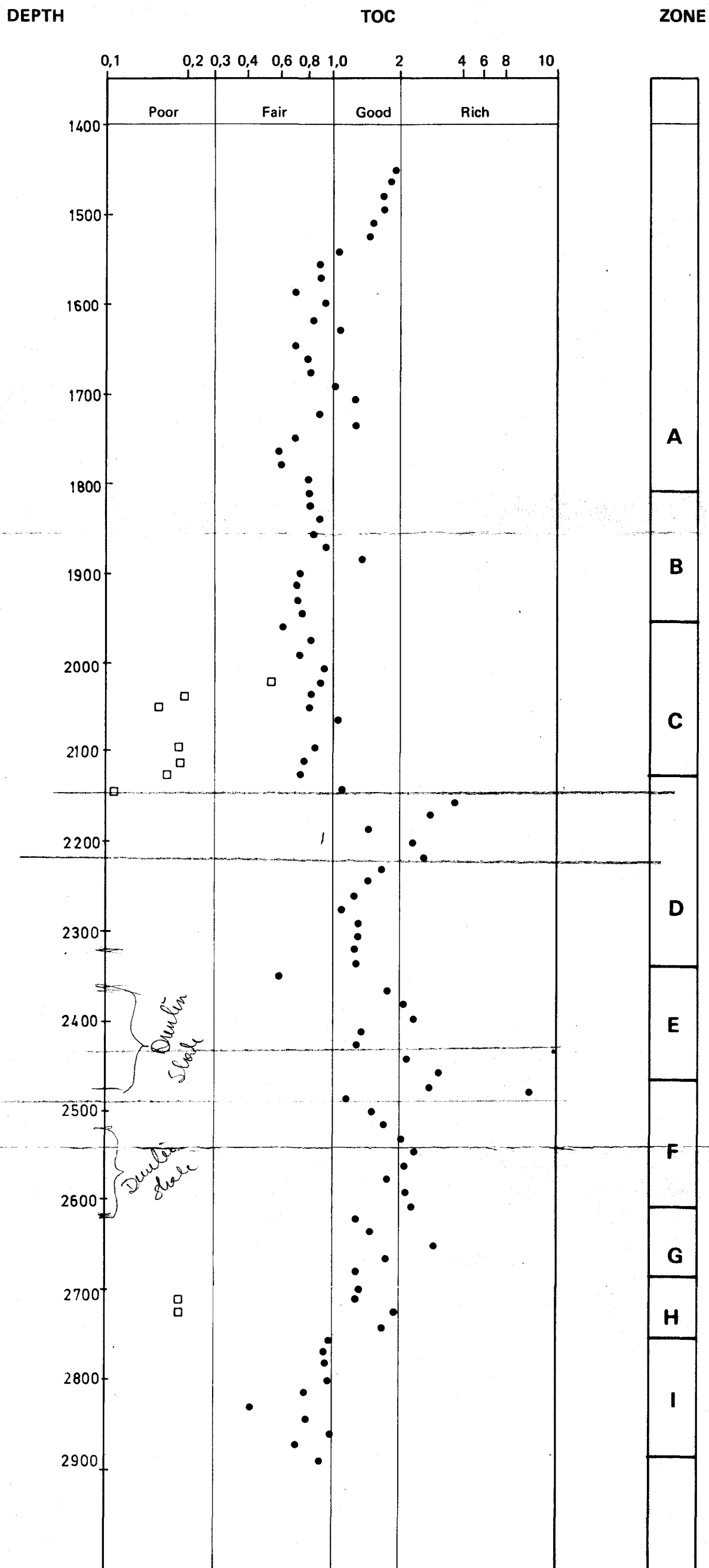
**C<sub>1</sub> - C<sub>7</sub> HYDROCARBONS**  
Presentation of Analytical Data





TOTAL ORGANIC CARBON (TOC)  
Presentation of Analytical Data

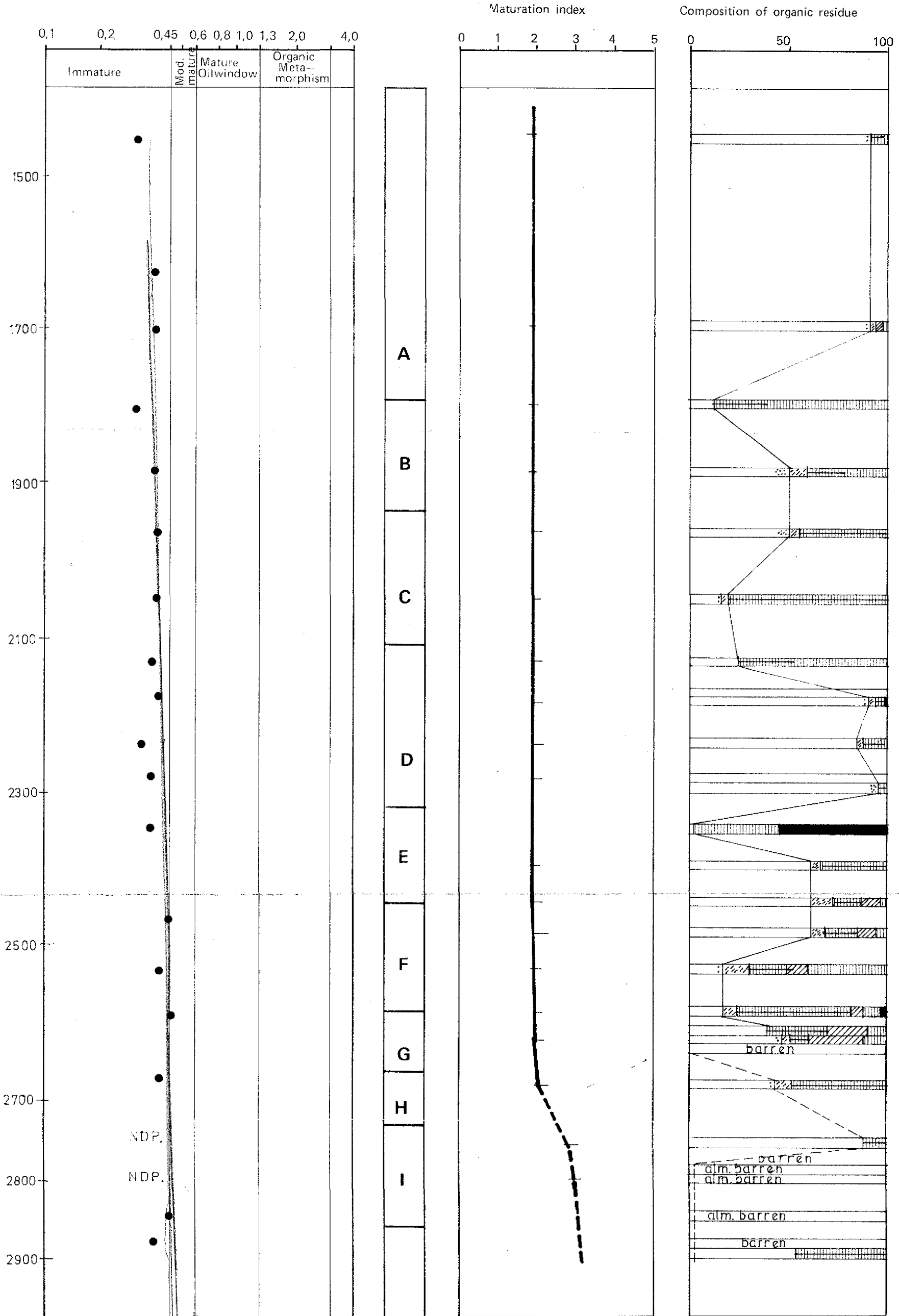
Norsk Hydro 31/4-2



● Claystone  
□ Limestone

MATURATION

DEPTH VITRINITE REFLECTANCE ZONE VISUAL KEROGEN COLORATION AND COMPOSITION OF ORGANIC RESIDUE

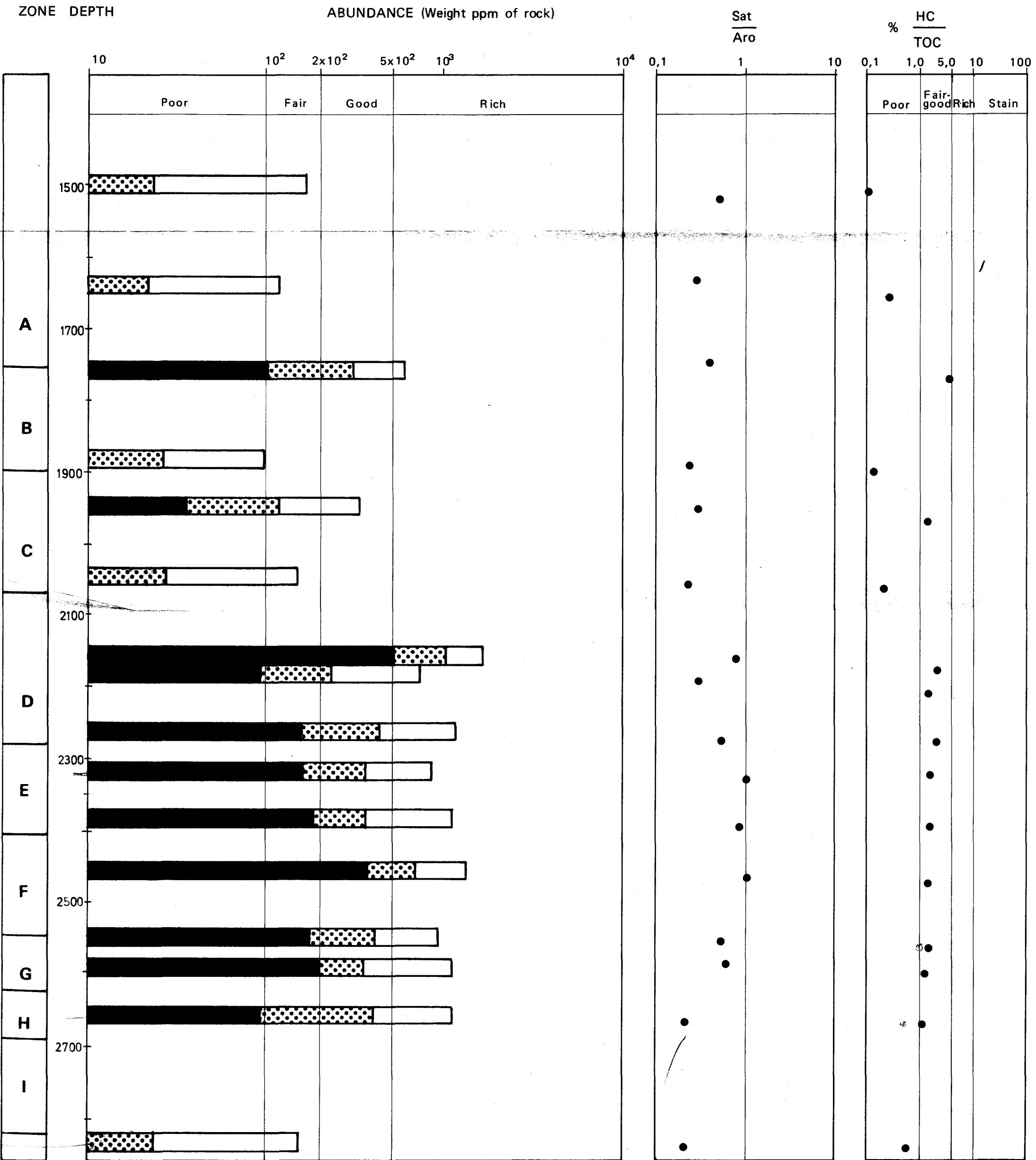


NDP. No determination possible.

- Amorphous material, Sapropel
- Algal
- Spores and pollen
- Cuticles
- Wood remains
- Undifferentiated disperse herbaceous material
- Black coal fragments
-

C<sub>15</sub><sup>+</sup> HYDROCARBONS

Presentation of Analytical Data

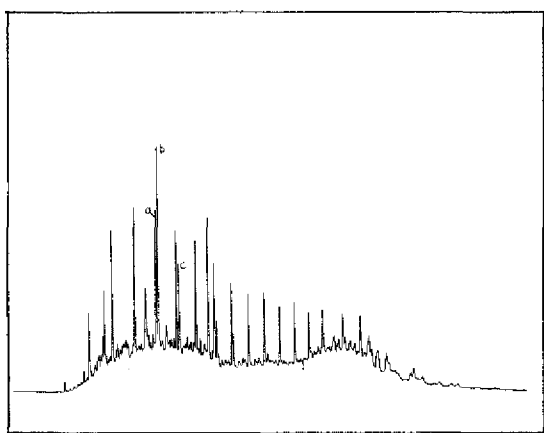
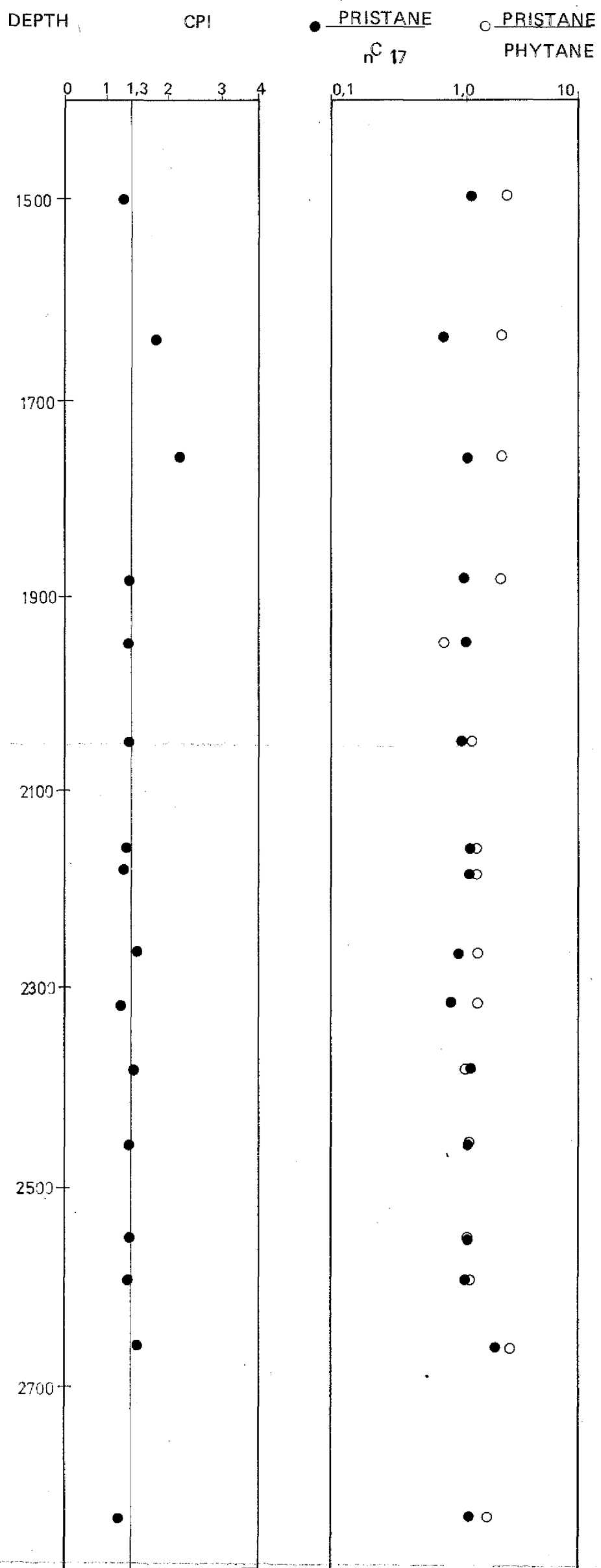


Sat.  
 Aro.  
 NSO Asp

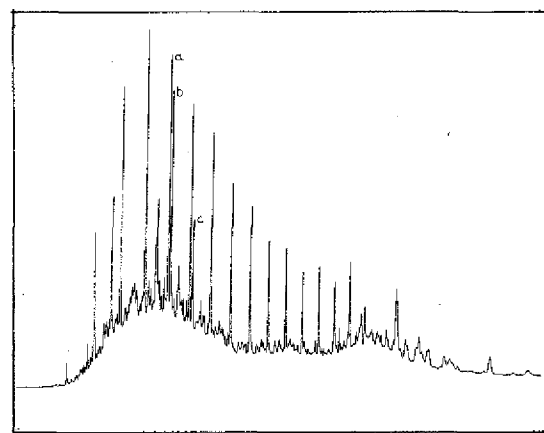
Sat: Saturated Hydrocarbons  
 Aro: Aromatic Hydrocarbons  
 NSO: Nitrogen, Sulphur and Oxygen containing compounds

Asp: Asphaltenes  
 HC: C<sub>15</sub> Hydrocarbons  
 TOC: Total Organic Carbon

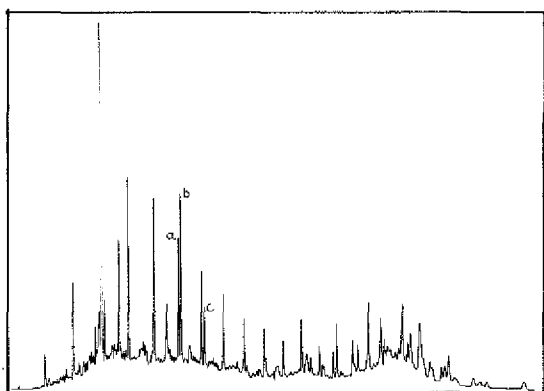
C<sub>15</sub><sup>+</sup> SATURATED HYDROCARBONS



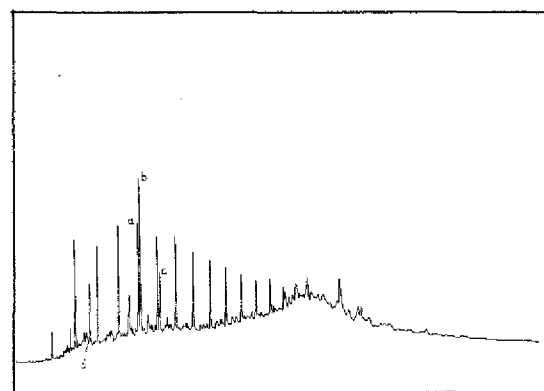
1495 - 1510



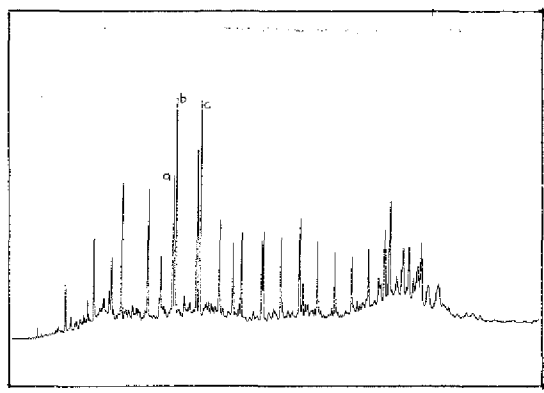
1660 - 75



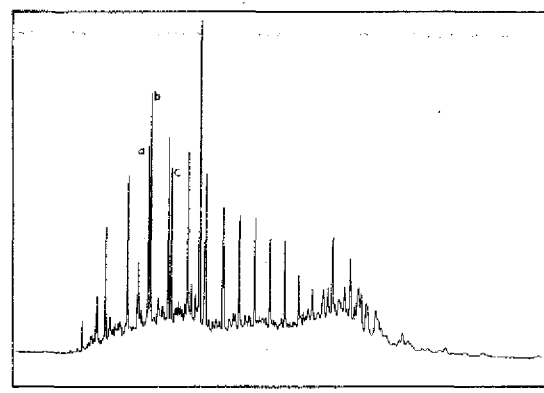
1750 - 65



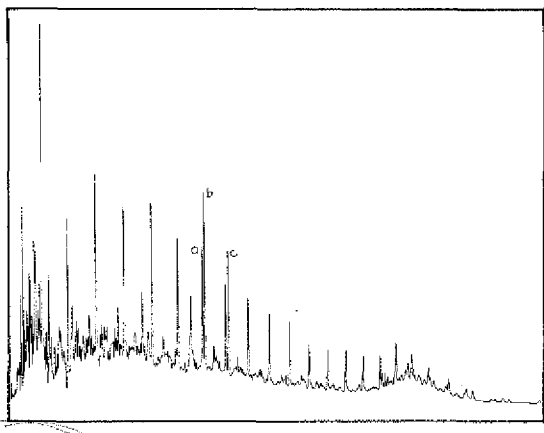
1883 - 1900



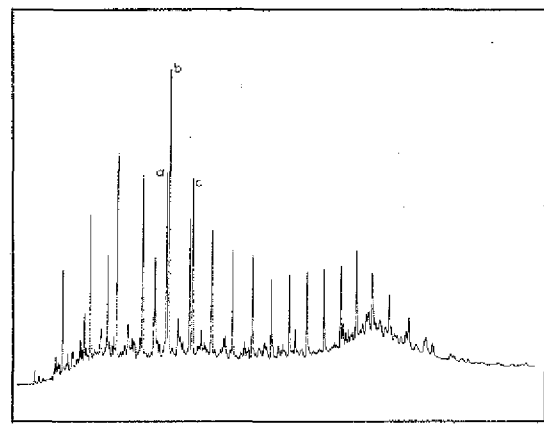
1945 - 60



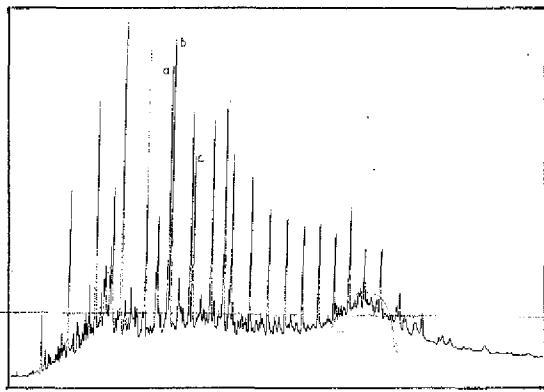
2035 - 50



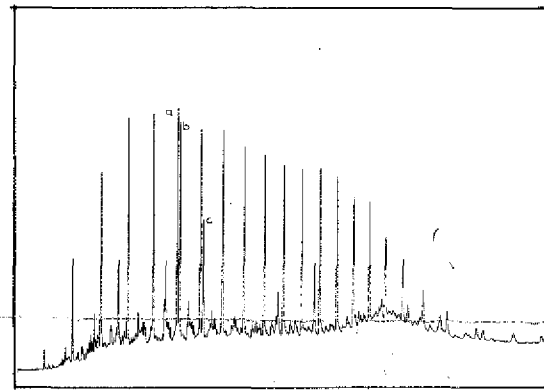
2155



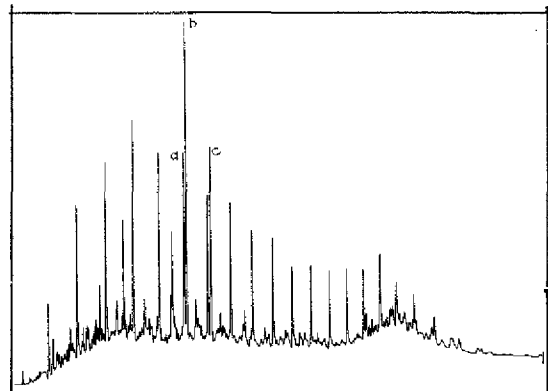
2185



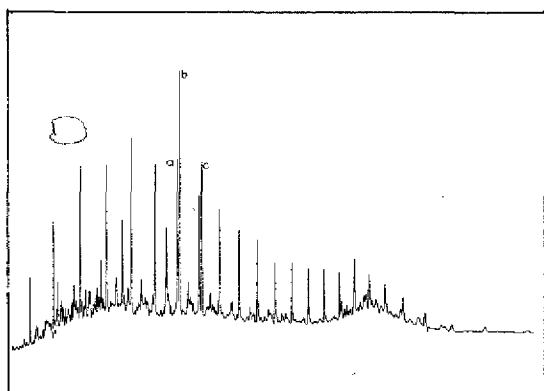
2260 - 75



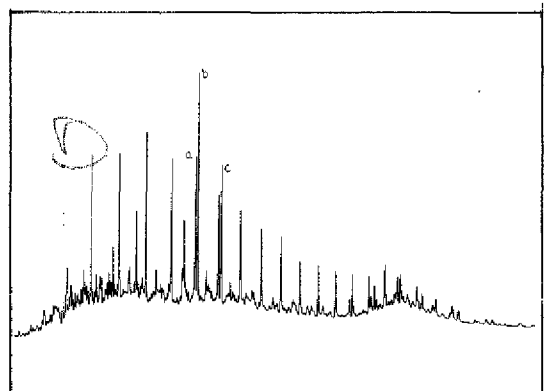
2305 - 20



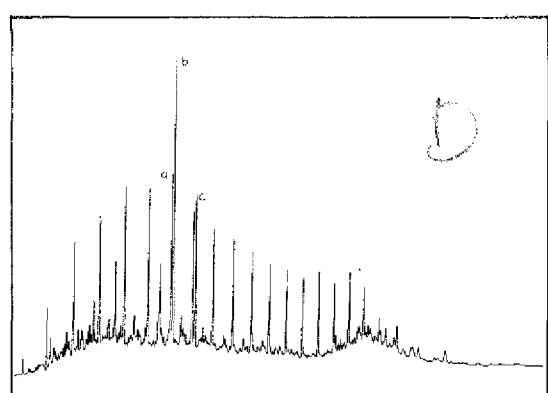
2380 - 95



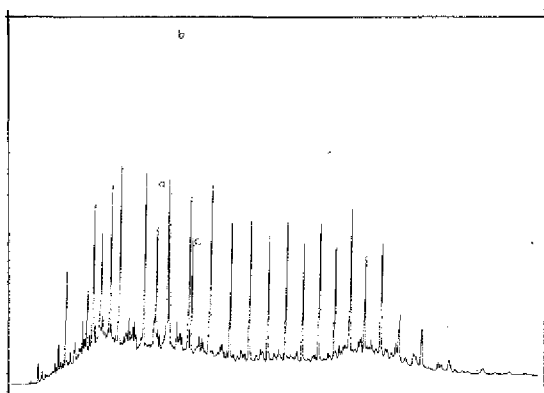
2455 - 70



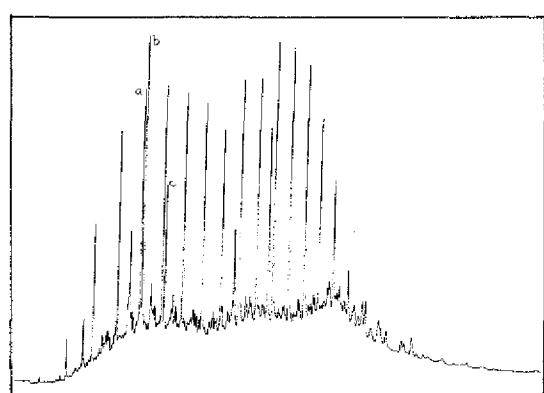
2530 - 45



2590 - 2605



2550 - 45



2860 - 75

a = nC<sub>17</sub>  
 b = Pristane  
 c = Phytane