

DRILL STEM TESTING SUMMARY

WELL 6507/7-6

The Drill Stem Test (DST) program commenced with the setting of a full string of 9 5/8" casing at 2510m. After setting the seal assembly and testing the BOPE, a gyro survey was run to total depth. A spaceout run was made with the sub surface test tree (SSTT) to the wellhead, followed by a bit and scraper run to 2481m while picking up 6 1/2" drill collars and 3 1/2" tubing. With the bit on bottom, the mud was circulated and conditioned, and the mud weight was reduced from 10.6 to 10.0 ppg. The bit and scraper were then pulled and a cement bond log was run. The CBL indicated adequate cement bonding across the proposed test interval. The CBL was followed by a velocity survey (VSP) from 2475m to 1800m and a gauge ring / junk basket run to 2475m. The DST No 1 interval was then perforated from 2411.5 to 2415.5m and from 2421-2424m in two runs with 5" casing guns. The downhole test tools were picked up and pressure tested with water before running in on tubing. Another pressure test was performed on the string after picking up the SSTT (tubing filled with diesel). The landing string was run with a lubricator valve positioned one stand below the surface test tree. The surface lines were then connected, the packer set, and all final pressure tests were performed.

A safety meeting was held with all crew members before beginning the test. The well was opened for a 40 minute initial flow period at 2036 hours on 23 August, and then shut in for 7 hours. During the 21 hour second flow period, 6 downhole fluid samples were taken on 3 wireline runs. A 6 hour second shut-in preceded a 19 hour final flow period which yielded 4911 BOPD of 23° API oil and 1.628 MMCFPD of gas through a 90.5/64" choke. The final flowing wellhead pressure was 531 psig. The well was shut in for a final build up period of 8 hours after which the well was killed, circulated out, and the test string pulled.

Following DST No 1, a CCL was run on wireline to check for sand buildup in the rathole. No buildup was detected and a cement retainer was set with the wireline at 2402m. The perforations below the retainer were then squeezed with cement, and the BOP equipment was tested before commencing with DST No 2.

The DST No 2 interval from 2348 to 2365m was perforated using 5" casing guns on 3 separate wireline runs. The test tools were then run, and the surface equipment was hooked up and tested. The well was opened at 2014 hours on 27 August for a 12 minute initial flow and then shut-in for 93 minutes. The well was opened and allowed to "clean up" for 10 1/2 hours through a 12/64" choke before wireline sampling on the second flow period. Four wireline sample runs were made with inconclusive results.

After completing the recombination sampling at the separator, the choke size was increased to 16/64" to clean up the well for additional wireline samples. The sample chamber and gauge would not go to bottom at the higher flow rate, so the choke was reduced back to 12/64". Once the downhole pressure was verified from the gauge run, the choke was reduced to 8/64" and three additional wireline sample runs were made. The choke was slowly opened to 132/64" upon completion of the downhole sampling. The well produced 3950 BOPD of 27° API oil and 2.170 MMCFPD of gas at a FFHP of 331 psig. The well was also producing large amounts of sand at this rate which eventually brought the flow period to a premature end. The second flow period lasted 55 hours, of which 3 1/2 hours were at the maximum choke size while bypassing the heater. The final shut in period was 9 hours. The well was then killed and the test tools recovered. A CCL/gauge ring run tagged the sand fill at 2361m, which was 41m above the top of the plugged back depth.

A cement retainer was set on wireline above the test zone at 2340m. The test tubing and drill collars were then laid down before final plugging and abandoning the well. Total testing time was 14 days.

3.5 MUD DATA

- 3.5.1 Discussions, Conclusions,
and Recommendations by Intervals.
- 3.5.2 Material Consumption and Cost.
- 3.5.3 Mud Properties Recap.
- 3.5.4 Graphs.



CONOCO NORWAY INC
Nortrym
6507/7-6

INTERVAL DISCUSSION

36" Hole 375 to 473 meters
30" Casing at 473 meters

The Nortrym was moved to its new location, 6507/7-6. This well was spudded on the 23rd July 1986. The seabed was tagged at 375 meters RKB (Rotary Kelly Bushing).

The 36" hole was drilled with seawater and high viscosity pills. Returns were to the sea bed. 450 barrels of 9.5ppg (pounds per gallon) kill mud was built in accordance with CONOCO NORWAY INC's contingency plan for shallow gas. While drilling in formations containing boulders, the drill pipe backed off at a TD (Total Depth) of approximately 420 meters. Because of the ensuing problems of fishing out the drill string, it was decided to respudd the well 10 meters from the first location. No significant problems were encountered drilling the hole at its new location. TD was reached at 472 meters.

Approximately 25 barrels of 100 seconds/quart viscosity mud was circulated at each connection. At TD, the hole was circulated with 100 barrels of high viscosity mud and 400 barrels of seawater prior to a wiper trip to 400 meters. After running back to bottom, 400 barrels of 9.5 ppg kill mud was spotted in the hole. The drill string was pulled out of the hole. The 30" casing was run and cemented with no problems.

2450 barrels of mud were built in this interval, of which, 1345 barrels were transferred to the next interval. The 1105 barrels used on this interval was 25% lower than the programmed 1475 barrels. The mud program displacements were calculated to displace the open hole twice at 150% of the calculated hole volume. In actual practice the hole was swept with a 100 barrel high viscosity pill and displaced with 100% calculated hole volume. The unprogrammed barite was \$0.80 per barrel. When this is taken into consideration, the actual per barrel mud cost was \$0.09 lower than programmed.



CONOCO NORWAY INC
Nortrym
65077-6

INTERVAL DISCUSSION

26" Hole 473 to 1030 meters
20" Casing at 1024 meters

This section was drilled without a riser using seawater and high viscosity pills. 630 barrels of 10 ppg kill mud was built in accordance with CONOCO NORWAY INC's contingency plan for shallow gas.

A 17 1/2" pilot hole was drilled to 1030 meters without any problems. At TD, 100 barrels of high viscosity mud were pumped and was followed by 400 barrels of seawater. 500 barrels of 10 ppg kill mud were spotted in the open hole prior to tripping for the 26" bit.

The hole was opened to 26" without any significant problems. Reaming was necessary on only the last few joints. 1000 barrels of 10 ppg kill mud was built in accordance with CONOCO NORWAY INC's contingency plan for shallow gas.

When the hole had been opened to 26", 100 barrels of high viscosity mud were pumped and was followed by 400 barrels of seawater. After a wiper trip to the 30" casing shoe, another 100 barrel high viscosity sweep was done. The hole was displaced to 10 ppg kill mud in preparation to run the 20" casing. The 20" casing was run and cemented.

The programmed per barrel cost of \$2.14 was based on a closed system for the pilot hole. The increased bentonite concentration, required for the high viscosity cost \$1.76 per barrel and the increased barite concentration for the kill muds cost \$0.93 per barrel. This resulted in a mud cost of \$322.70 over the programmed cost.

CONOCO NORWAY INC
Nortrym
6507/7-6



INTERVAL DISCUSSION

17 1/2" Hole 1030 to 2087 meters
13 3/8" Casing at 2080 meters

The pits were cleaned out after cementing the 20" casing. A KCl/Polymer system was mixed up for the 17 1/2" hole interval. Displaced to the KCl/Polymer system after running the leak-off-test to 12.7 ppg equivalent mud weight.

The mud weight was raised in increments from 9.5 to 12.0 ppg during the course of this interval. Throughout this interval KCl/Polymer premixes were added to the system to maintain volume and the required mud properties. Prior to drilling the soft clay at approximately 1500 meters, the KCl content was increased to 37 ppb (pounds per barrel) and the polymer concentration was doubled to maintain hole stability and encapsulate the drill cuttings.

While coming out of the hole at 1778 meters for a bit change, a great deal of overpull was experienced and several joints had to be pumped out. Only three slightly tight spots were encountered on the trip back in the hole. This would indicate stress relief of the well bore in the soft clay section.

Drilling continued to TD. Prior to reaching TD, gas shows of up to 11% were recorded. The mud weight was raised from 11.5 to 11.8 ppg. While making a wiper trip at TD, swabbing occurred and the well flowed at approximately 6 barrels per hour. The mud weight was raised to 12.0 ppg. The well was static, and the drill string was pulled with no further problems.

The 13 3/8" casing was run and landed with no problems. 30 barrels of mud were lost to the formation while circulating the casing prior to cementing. A further 102 barrels were lost while displacing the cement.

The KCl/Polymer system was maintained to meet CONOCO NORWAY INC's specifications. At one point the MBT was 16 ppb which was slightly higher than +/- 15 ppb called for in the program. No problems occurred, and the mud was returned to the required specification. The calcium content did rise above the recommended maximum level of 200 mg/l level and was treated with soda ash.

Dilution rates were not as high as estimated and the per barrel cost was \$0.80 lower resulting in a cost savings of \$8,549.53 or 13% on the estimated cost of the interval.

CONOCO NORWAY INC
Nortrym
6507/7-6



INTERVAL DISCUSSION

12 1/4" Hole 2087 to 2087 meters
9 5/8" Casing at 2510 meters

The mud from the previous interval was diluted to 10.5 ppg and the KCl content was allowed to deplete while drilling this interval. Seawater was used for dilution for the PAC/DEXTRID mud system recommended for this interval.

10 cores (213 meters) were cut in the interval from 2129 meters. The average core recovery was 90.2%.

No difficulties were experienced with drilling or hole stability. The caliper log showed the hole was close to gauge throughout the interval. There was some overpull on the wiper trip at TD, but the hole cleaned up hole after the wiper trip. The wireline logging, final wiper trip and 9 5/8" casing operations all went smoothly.

The increased barite concentration over the estimated barite concentration and higher than estimated dilution requirements in a higher than estimated mud cost for the interval of \$11,397.05.

CONOCO NORWAY INC
Nortrym
6507/7-6



INTERVAL DISCUSSION

Testing
9 5/8" Casing at 2510 meters

Testing was done using the PAC/DEXTRID mud from the 12 1/4" hole interval. SURFLO B-21 was added to the mud system to prevent any boildgradation of the polymers while the mud was static in the hole.

Two drill stem tests were run. The perforations were cemented off after the testing program was completed. A cement plug was set in the casing at 600 to 400 meters. The casing was cut and the well was abandoned.



CONOCO NORWAY INC
Nortrym
6507/7-6

CONCLUSIONS AND RECOMMENDATIONS

*pounds
per
gallon*

The CONOCO NORWAY INC well 6507/7-6 was drilled to TD at 2525 meters in 28 days. The total rotating hours was 202.3, of which 52.5 hours were spent coring in the 12 1/4" hole interval. The well went extremely smoothly and no major problems were encountered. The mud material cost was 8% higher than estimated. This was due to the kill mud requirements in the first two hole intervals, which was not included in the estimate, and a higher dilution requirement than estimated in the final drilling interval.

In the Heidrun field in Haltenbanken, reactive gumbo clays can be expected in the 17 1/2" hole interval at approximately 1500 meters. Prior to drilling these clays, it is of paramount importance to increase the potassium content to 35 to 40 ppb KCl for inhibition of these clays and to ensure that there is sufficient polymer in the mud system for encapsulation of the drill cuttings to prevent solids build-up in the mud system. This was done in this well and the dilution requirements was approximately 350 barrels less than estimated.

The mud weight should be increased, in increments, to a maximum of 12.0 ppg, as hole conditions dictate, in these reactive gumbo clays in the 17 1/2" section. 11.8 ppg was sufficient to drill this interval, but 12.0 ppg was required at TD in order to trip out of the hole to run casing.

Control of the calcium content to as low as possible, but less than 200 mg/l, is recommended for the 17 1/2" interval for efficient use of the polyacrylamide (Alcomer 110L in this well) which is calcium sensitive. The use of potassium carbonate is recommended instead of soda ash. The potassium carbonate will reduce the calcium level and will add potassium ions to the mud system to increase inhibition. The soda ash, sodium carbonate, will reduce the calcium content, but the sodium ions will compete with the potassium ions in the mud system and does not provide the inhibition that the potassium ion does.

N Baroid

OPERATING AREA

CONOCO NORWAY INC.

6507/7-6



INTERVAL SUMMARY

SECTION

| | |
|---------------------------------|---------------------|
| Hole Size: | 36 " |
| Casing Size: | 30 " |
| Casing Set At: | 472 m |
| Interval Length: | 97 m |
| Mud Type: | Spud |
| Spud Depth: | 375 m |
| Spud Date: | 23.07.86 |
| TD Depth: | 472 m |
| TD Date: | 26.07.86 |
| Maximum Hole Deviation: | 0 |
| Drilling Days: | 2.3 |
| Total Days on Interval: | 4 |
| Interval Mud Cost: | \$ 7,614.00 |
| Volume Built: | 2450 bbl |
| Volume Transferred to Interval: | 0 |
| Volume Salvaged: | 1345 bbl |
| Volume Left Behind Casing: | 0 |
| Volume Lost To Formation: | 0 |
| Volume Dumped: | 1105 bbl |
| Volume Lost Over Solids Equip.: | 0 |
| Total Volume To Sea: | 1105 bbl |
| Volume Cuttings Drilled: | 63.3 m ³ |
| Cost per Barrel | \$ 3.11 |
| Cost per ft. m ...X....: | \$ 78.49 |
| Cost per Day: | \$ 1,903.50 |
| Cost Of Mud Used On Interval: | \$ 3,436.55 |



OPERATING AREA

CONOCO NORWAY INC.

6507/7-6



INTERVAL SUMMARY

SECTION

| | |
|--|----------------------|
| Hole Size: | 26 " |
| Casing Size: | 20 " |
| Casing Set At: | 1024 m |
| Interval Length: | 558 m |
| Mud Type: | Spud |
| Spud Depth: | 472 m |
| Spud Date: | 27.07.86 |
| TD Depth: | 1030 m |
| TD Date: | 29.07.86 |
| Maximum Hole Deviation: | 0 |
| Drilling Days: | 1.2 |
| Total Days on Interval: | 3 |
| Interval Mud Cost: | \$ 8,356.20 |
| Volume Built: | 1529 bbl |
| Volume Transferred to Interval: | 1345 bbl |
| Volume Salvaged: | 0 |
| Volume Left Behind Casing: | 0 |
| Volume Lost To Formation: | 0 |
| Volume Dumped: | 2874 bbl |
| Volume Lost Over Solids Equip.: | 0 |
| Total Volume To Sea: | 2874 bbl |
| Volume Cuttings Drilled: | 183.5 m ³ |
| Cost per Barrel | \$ 5,47 |
| Cost per ft. m ^X : | \$ 14.98 |
| Cost per Day: | \$ 2,785.40 |
| Cost Of Mud Used On Interval: | \$ 12,533.65 |



OPERATING AREA

CONOCO NORWAY INC.

6507/7-6



INTERVAL SUMMARY

SECTION

| | |
|---------------------------------|--------------------|
| Hole Size: | 17 1/2 " |
| Casing Size: | 13 3/8 " |
| Casing Set At: | 2080 m |
| Interval Length: | 1057 m |
| Mud Type: | KCl/Polymer |
| Spud Depth: | 1030 m |
| Spud Date: | 01.08.86 |
| TD Depth: | 2087 m |
| TD Date: | 05.08.86 |
| Maximum Hole Deviation: | 0.4 ^o |
| Drilling Days: | 3 |
| Total Days on Interval: | 8 |
| Interval Mud Cost: | \$ 59,236.97 |
| Volume Built: | 4054 bbl |
| Volume Transferred to Interval: | 0 |
| Volume Salvaged: | 2770 bbl |
| Volume Left Behind Casing: | 118 bbl |
| Volume Lost To Formation: | 230 bbl |
| Volume Dumped: | 715 bbl |
| Volume Lost Over Solids Equip.: | 221 bbl |
| Total Volume To Sea: | 936 bbl |
| Volume Cuttings Drilled: | 165 m ³ |
| Cost per Barrel | \$ 14.61 |
| Cost per ft. m ...X....: | \$ 56.04 |
| Cost per Day: | \$ 7,404.62 |
| Cost Of Mud Used On Interval: | \$ 18,759.24 |



OPERATING AREA

CONOCO NORWAY INC.

6507/7-6

INTERVAL SUMMARY

SECTION

| | |
|---------------------------------|---------------------|
| Hole Size: | 12 1/4" |
| Casing Size: | 9 5/8" |
| Casing Set At: | 2510 m |
| Interval Length: | 438 m |
| Mud Type: | PAC/DEXTRID |
| Spud Depth: | 2087 m |
| Spud Date: | 08.08.86 |
| TD Depth: | 2525 m |
| TD Date: | 16.08.86 |
| Maximum Hole Deviation: | |
| Drilling Days: | 2.9 |
| Total Days on Interval: | 13 |
| Interval Mud Cost: | \$ 21,788.40 |
| Volume Built: | 2178 bbl |
| Volume Transferred to Interval: | 2770 bbl |
| Volume Salvaged: | 1862 bbl |
| Volume Left Behind Casing: | 180 bbl |
| Volume Lost To Formation: | 188 bbl |
| Volume Dumped: | 2456 bbl |
| Volume Lost Over Solids Equip.: | 262 bbl |
| Total Volume To Sea: | 2718 bbl |
| Volume Cuttings Drilled: | 33.3 m ³ |
| Cost per Barrel | \$ 10.00 |
| Cost per ft. mX...: | \$ 49.75 |
| Cost per Day: | \$ 1,676.03 |
| Cost Of Mud Used On Interval: | \$ 43,629.70 |



OPERATING AREA

CONOCO NORWAY INC.

6507/7-6



INTERVAL SUMMARY

SECTION

| | |
|---------------------------------|--------------|
| Hole Size: | TESTING |
| Casing Size: | 9 5/8" |
| Casing Set At: | 2510 m |
| Interval Length: | 0 |
| Mud Type: | PAC/DEXTRID |
| Spud Depth: | |
| Spud Date: | |
| TD Depth: | |
| TD Date: | |
| Maximum Hole Deviation: | |
| Drilling Days: | |
| Total Days on Interval: | 16 |
| Interval Mud Cost: | \$ 7,481.25 |
| Volume Built: | 380 bbl |
| Volume Transferred to Interval: | 1862 bbl |
| Volume Salvaged: | 0 |
| Volume Left Behind Casing: | 213 bbl |
| Volume Lost To Formation: | 488 bbl |
| Volume Dumped: | 1533 bbl |
| Volume Lost Over Solids Equip.: | 8 bbl |
| Total Volume To Sea: | 1541 bbl |
| Volume Cuttings Drilled: | 0 |
| Cost per Barrel | \$ 19.69 |
| Cost per ft. m ...X.....: | |
| Cost per Day: | \$ 467.58 |
| Cost Of Mud Used On Interval: | \$ 26,117.68 |



CONOCO NORWAY INC
 Nortrym
 6507/7-6

TOTAL MATERIAL CONSUMPTION

| MATERIAL | PACKAGING | QUANTITY |
|---------------------|-----------|----------|
| Alcomer 110L | 25kg | 54 |
| Barite | MT | 398 |
| Bentonite | MT | 54 |
| Caustic Soda | 25kg | 34 |
| Dextrid | 25kg | 518 |
| Drispac | 50lb | 40 |
| Lime | 20kg | 1 |
| PAC-L | 25kg | 95 |
| PAC-R | 25kg | 73 |
| Potassium Chloride | 50kg | 1116 |
| Potassium Hydroxide | 50kg | 12 |
| Soda Ash | 50kg | 13 |
| Sodium Bicarbonate | 50kg | 16 |
| Surflo B-21 | 25kg | 14 |
| Walnut | 25kg | 12 |
| XCD Polymer | 25kg | 67 |

Included in above totals

BROKEN SACKS

| | | |
|---------|------|---|
| Dextrid | 25kg | 5 |
| PAC-L | 25kg | 4 |

USED ON CEMENT JOBS

| | | |
|--------------|------|----|
| Barite | MT | 20 |
| Caustic Soda | 25kg | 7 |

COSTS

| INTERVAL | METERS | BARRELS | COST\$ |
|-----------------|-----------------|---------|--------------|
| 36" | 97 | 2450 | \$7,614.00 |
| 26" | 558 | 1529 | \$8,356.20 |
| 17 1/2" | 1057 | 4054 | \$59,236.97 |
| 12 1/4" | 438 | 2178 | \$21,788.40 |
| Testing | | 380 | \$7,481.25 |
| Totals | 2150 | 10591 | \$104,476.82 |
| | Drilling | | Total |
| Cost per barrel | \$9.50 | | \$9.86 |
| Cost per meter | \$45.11 | | \$48.59 |

WELL NAME: CONOCO 6507/7-6



MUD PROPERTY RECAP

| DATE | DEPTH | DENSITY | VISC-OSITY | FILTRATE | | HY/HP filt | | pH | RHEOLOGY | | | | FILTRATE ANALYSIS | | | | | RETORT ANALYSIS | | | CEC | OTHER | | | | |
|--------|-------|---------|------------|----------|-------|------------|-------|------|----------|------------------------|------------------------|----------|-------------------|-----|-----|-----|------|-----------------|-------|--------------|------|-------|------|--|--|--|
| | | PPG/ | | | Cake | °500psi | | | PV | YP | 10" | 10' | Cl | Ca | PI | Mf | Pm | Oil | Water | Corr. Solids | PPB | KCl | | | | |
| | | metres | secs | ccs | 32/mm | ccs | 32/mm | | cp | lbs/100ft ³ | gms/100cm ³ | mg/litre | ppm | | | | % | % | % | Bent. Eq. | PPB | ASG | | | | |
| 1986 | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 08.08. | 2142 | 10.5 | 53 | 2.8 | 1 | - | - | 10.2 | 20 | 20 | 3 | 6 | 19 K | 200 | .3 | .65 | 1.1 | 0 | 89 | 8.5 | 12.5 | 20 | 3.6 | | | |
| 09.08. | PIT | 10.5+ | 48 | 2.6 | 1 | - | - | 10.2 | 21 | 16 | 3 | 4 | 17 K | 160 | .25 | .7 | 1.1 | 0 | 89 | 9.16 | 12.5 | 15 | 3.6 | | | |
| 09.08. | 2185 | 10.5+ | 53 | 2.8 | 1 | - | - | 10.2 | 21 | 20 | 3 | 5 | 16 K | 160 | .35 | .65 | 1.0 | 0 | 89 | 9.16 | 12.5 | 15 | 3.6 | | | |
| 10.08. | 2237 | 10.6 | 57 | 2.6 | 1 | - | - | 10.3 | 23 | 19 | 3 | 5 | 16 K | 140 | .2 | .65 | 1.0 | 0 | 88 | 10.5 | 12.5 | 12 | 3.4 | | | |
| 10.08. | 2305 | 10.6 | 55 | 2.8 | 1 | - | - | 10.0 | 22 | 23 | 4 | 6 | 15 K | 240 | .15 | .4 | 0.8 | 0 | 89 | 9.5 | 12.5 | 12 | 3.6 | | | |
| 11.08. | PIT | 10.5 | 50 | 2.4 | 1 | - | - | 10.1 | 22 | 17 | 2 | 3 | 14 K | 160 | .1 | .45 | 0.8 | 0 | 90 | 9 | 12.5 | 8 | 3.75 | | | |
| 11.08. | 2344 | 10.5 | 55 | 2.4 | 1 | - | - | 10.1 | 22 | 22 | 4 | 5 | 15 K | 160 | .2 | .5 | 0.75 | 0 | 90 | 9 | 12.5 | 8 | 3.75 | | | |
| 12.08. | 2365 | 10.6 | 58 | 2.1 | 1 | - | - | 10.0 | 23 | 18 | 2 | 4 | 14 K | 160 | .15 | .45 | 0.75 | 0 | 89 | 10.2 | 12.5 | 6 | 3.6 | | | |
| 12.08. | 2385 | 10.6 | 57 | 2.6 | 1 | - | - | 9.9 | 22 | 21 | 3 | 4 | 14 K | 180 | .2 | .5 | 0.65 | 0 | 89 | 10.2 | 12.5 | 6 | 3.6 | | | |
| 13.08. | PIT | 10.6 | 51 | 2.2 | 1 | - | - | 10.0 | 22 | 17 | 3 | 4 | 13 K | 200 | .1 | .3 | 0.4 | 0 | 89 | 11.0 | 11.5 | | 3.5 | | | |
| 13.08. | PIT | 10.5+ | 53 | 2.4 | 1 | - | - | 9.9 | 20 | 18 | 3 | 4 | 13 K | 180 | .2 | .5 | .6 | 0 | 89.5 | 10.5 | 11.5 | | 3.55 | | | |
| 14.08. | 2424 | 10.6+ | 59 | 3.0 | 1 | - | - | 10.0 | 24 | 22 | 4 | 5 | 12 K | 120 | .25 | .65 | .6 | 0 | 89 | 11 | 11.5 | | 3.5 | | | |
| 14.08. | 2440 | 10.5 | 54 | 2.4 | 1 | - | - | 9.8 | 22 | 23 | 5 | 6 | 13 K | 140 | .2 | .5 | .5 | 0 | 89 | 11 | 11.5 | | 3.5 | | | |
| 15.08. | 2462 | 10.7 | 59 | 2.4 | 1 | - | - | 9.5 | 24 | 22 | 3 | 4 | 12 K | 200 | .1 | .35 | .5 | 0 | 89 | 11 | 11.0 | | 3.6 | | | |
| 16.08. | 2525 | 10.5+ | 57 | 3.2 | 1 | - | - | 9.1 | 22 | 22 | 3 | 6 | 11 K | 160 | .2 | .5 | .5 | 0 | 89 | 11 | 11.0 | TR | 3.4 | | | |
| 16.08. | PIT | 10.6 | 53 | 2.7 | 1 | - | - | 9.1 | 23 | 22 | 4 | 5 | 11 K | 200 | .1 | .5 | .5 | 0 | 89 | 11 | 11 | TR | 3.5 | | | |
| 17.08. | PIT | 10.7 | 57 | 3.0 | 1 | - | - | 9.0 | 24 | 22 | 4 | 6 | 11 K | 200 | .1 | .5 | .5 | 0 | 88 | 12 | 11 | TR | 3.5 | | | |
| 18.08. | 2525 | 10.5+ | 55 | 2.8 | 1 | - | - | 8.9 | 20 | 19 | 4 | 5 | 11 K | 200 | .1 | .5 | .5 | 0 | 89 | 11 | 11 | TR | 3.44 | | | |
| 18.08. | PIT | 10.6+ | 55 | 2.4 | 1 | - | - | 9.0 | 23 | 20 | 3 | 4 | 11 K | 240 | .1 | .45 | .5 | 0 | 89 | 11 | 11 | TR | 3.49 | | | |

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WELL NAME: CONOCO 6507/7-6



MUD PROPERTY RECAP

| DATE | DEPTH metres | DENSITY PPG/ sec.s | VISC- OSITY secs | FILTRATE | | | pH | RHEOLOGY | | | | FILTRATE ANALYSIS | | | | | RETORT ANALYSIS | | | CEC PPB | OTHER | | | | |
|--------|-----------------|--------------------------|------------------------|----------|-------------|----------------|----|----------|--|----------|-----|-------------------|--------|-----|-----|-----|-----------------|------------|----------------------|------------|--------------|------|--|--|--|
| | | | | ccs | Cake | °500psi ccs | | PV | YP | 10" | 10' | Cl | Ca | PI | MI | Pm | Oil % | Water % | Corr. Solids % | | Bent. Eq. | ASG | | | |
| | | | | | 1" 32/mm | | | cp | lbs/100ft ² -gms/100 cm ² | mg/litre | ppm | | | | | | | | | | | | | | |
| 19.08. | PIT | 10.0 | 45 | 2.6 | 1 | - | - | 8.3 | 15 | 13 | 3 | 4 | 10.500 | 240 | .05 | .35 | 0.1 | 0 | 92 | 8 | 8.5 | 3.53 | | | |
| 20.08. | PIT | 10.0 | 55 | 2.6 | 1 | - | - | 9.3 | 24 | 19 | 8 | 14 | 10.500 | 240 | .15 | .5 | 0.5 | 0 | 92 | 8 | 10.0 | 3.53 | | | |
| 21.08. | PIT | 10.0 | 53 | 4.3 | 1 | - | - | 10.0 | 20 | 20 | 5 | 7 | 8.000 | 100 | .1 | .25 | 0.8 | 0 | 92 | 8 | 11.5 | 3.52 | | | |
| 22.08. | PIT | 10.0 | 54 | 4.6 | 1 | - | - | 9.9 | 22 | 20 | 4 | 8 | 8.000 | 100 | .1 | .3 | 0.8 | 0 | 92 | 8 | 12 | 3.5 | | | |
| 23.08. | PIT | 10.0 | 52 | 4.4 | 1 | - | - | 9.9 | 20 | 18 | 4 | 6 | 8.000 | 100 | .1 | .3 | 0.8 | 0 | 92 | 8 | 12 | 3.5 | | | |
| 24.08. | PIT | 10.0 | 53 | 4.6 | 1 | - | - | 9.8 | 20 | 18 | 4 | 5 | 8.000 | 100 | .1 | .3 | 0.8 | 0 | 92 | 8 | 12 | 3.5 | | | |
| 25.08. | 2360 | 10.0 | 48 | 4.2 | 1 | - | - | 9.6 | 22 | 22 | 5 | 8 | 8.000 | 160 | .1 | .6 | 0.8 | 0 | 92 | 8 | 12 | 3.5 | | | |
| 26.08. | PIT | 10.0 | 47 | 4.4 | 1 | - | - | 9.3 | 21 | 21 | 5 | 7 | 8.000 | 180 | .1 | .5 | 0.7 | 0 | 92 | 8 | 12 | 3.5 | | | |
| 27.08. | PIT | 10.0 | 44 | 4.8 | 1 | - | - | 10.0 | 17 | 17 | 3 | 6 | 8.000 | 120 | .2 | .6 | 0.4 | 0 | 92 | 8 | 12 | 3.5 | | | |
| 28.08. | PIT | 10.0 | 48 | 5.2 | 1 | - | - | 10.2 | 18 | 17 | 3 | 5 | 8.000 | 160 | .1 | .8 | 0.8 | 0 | 92 | 8 | 12 | 3.5 | | | |
| 29.08. | PIT | 10.0 | 49 | 5.0 | 1 | - | - | 10.1 | 17 | 17 | 3 | 5 | 8.000 | 160 | .15 | .6 | .75 | 0 | 92 | 8 | 12 | 3.5 | | | |
| 30.08. | PIT | 10.0 | 46 | 5.4 | 1 | - | - | 10.0 | 19 | 17 | 3 | 5 | 8.000 | 140 | .2 | .6 | .6 | 0 | 92 | 8 | 12 | 3.5 | | | |
| 31.08. | PIT | 10.0 | 48 | 5.2 | 1 | - | - | 10.2 | 18 | 17 | 3 | 5 | 8.000 | 160 | .2 | .65 | .75 | 0 | 92 | 8 | 12 | 3.5 | | | |
| 01.09. | PIT | 10.0 | 48 | 5.2 | 1 | - | - | 10.2 | 18 | 17 | 3 | 5 | 8.000 | 160 | .2 | .65 | .75 | 0 | 92 | 8 | 12 | 3.5 | | | |
| 02.09. | PIT | 10.0 | 48 | 5.2 | 1 | - | - | 10.2 | 18 | 17 | 3 | 5 | 8.000 | 160 | .2 | .65 | .75 | 0 | 92 | 8 | 12 | 3.5 | | | |
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Table 5.4

RFT Pressure Results

| Depth (m RKB) (log depth) | Mud Hydrostatic (psia) | Formation (psia) | Permeability | Remarks |
|---------------------------------|------------------------------|---------------------|--------------|---|
| 2149 | 3911 | 3518 | V. Good | |
| 2169 | 3960 | 3540 | | gas in flow Line or poor permeability |
| 2192 | 4002 | 3530.7 | V. Good | |
| 2204 | 4023 | 3533.7 | V. Good | |
| 2221 | 4055 | 3538.8 | V. Good | |
| 2235 | 4080.1 | 3542.5 | V. Good | |
| 2263.5 | 4132.6 | 3550.6 | V. Good | |
| 2277.5 | 4157 | - | | Tight formation |
| 2302.5 | 4202.8 | 3560.2 | V. Good | |
| 2320.5 | 4235.1 | 3565.3 | V. Good | |
| 2332.5 | 4556.9 | 3567.5 | V. Good | |
| 2337.5 | 4266.5 | 3569.3 | V. Good | |
| 2346 | 4282.2 | 3604.2 | Fair | Possibly partial probe plugging |
| 2351.5 | 4292 | 3585.6 | Good | Possible partial probe plugging |
| 2356 | 4300.1 | 3604.7 | Fair | Possible partial probe plugging |
| 2360 | 4308.2 | - | | Tight formation |
| 2370.5 | 4326 | 3601 | V. Good | |
| 2380 | 4343.8 | 3615.4 | V. Good | |
| 2385 | 4352.4 | 3621 | V. Good | |
| 2405 | 4389.8 | 3638.1 | Good | |
| 2414.5 | 4406.3 | 3649.1 | Good | |
| 2424 | 4424.3 | 3660.3 | Fair | |
| 2436 | 4445.8 | 3674.7 | Good | |
| 2447 | 4466.1 | 3689.7 | Good | 2446.5 tried, not stabilised |
| 2452 | 4475.3 | 3696.6 | Good | |
| 2457 | 4484.4 | 3703.8 | Good | |
| 2472.5 | 4512 | 3726.2 | Good | |
| 2487 | 4539.6 | 3746.9 | Good | |
| 2504 | 4571.6 | 3771.5 | V. Good | |

The RFT pressure results are also presented on figure 5.4