

RFT PRESSURE POINTS RUN NO. 1

| NO | DEPTH M RKB | HYDROSTAT BEF.PSIA | FORMATION (PSIA) | G/CC | HYDROSTAT AFT.PSIA | REMARKS PERMEABILITY |
|----|----------------|-----------------------|---------------------|-------|-----------------------|-------------------------|
| 1 | 2250 | 3895.4 | 3544.1 | 1.108 | 3895.4 | EXCELLENT |
| 2 | 2317 | 4012.0 | 3566.9 | 1.083 | 4012.0 | VERY GOOD TO EXC. |

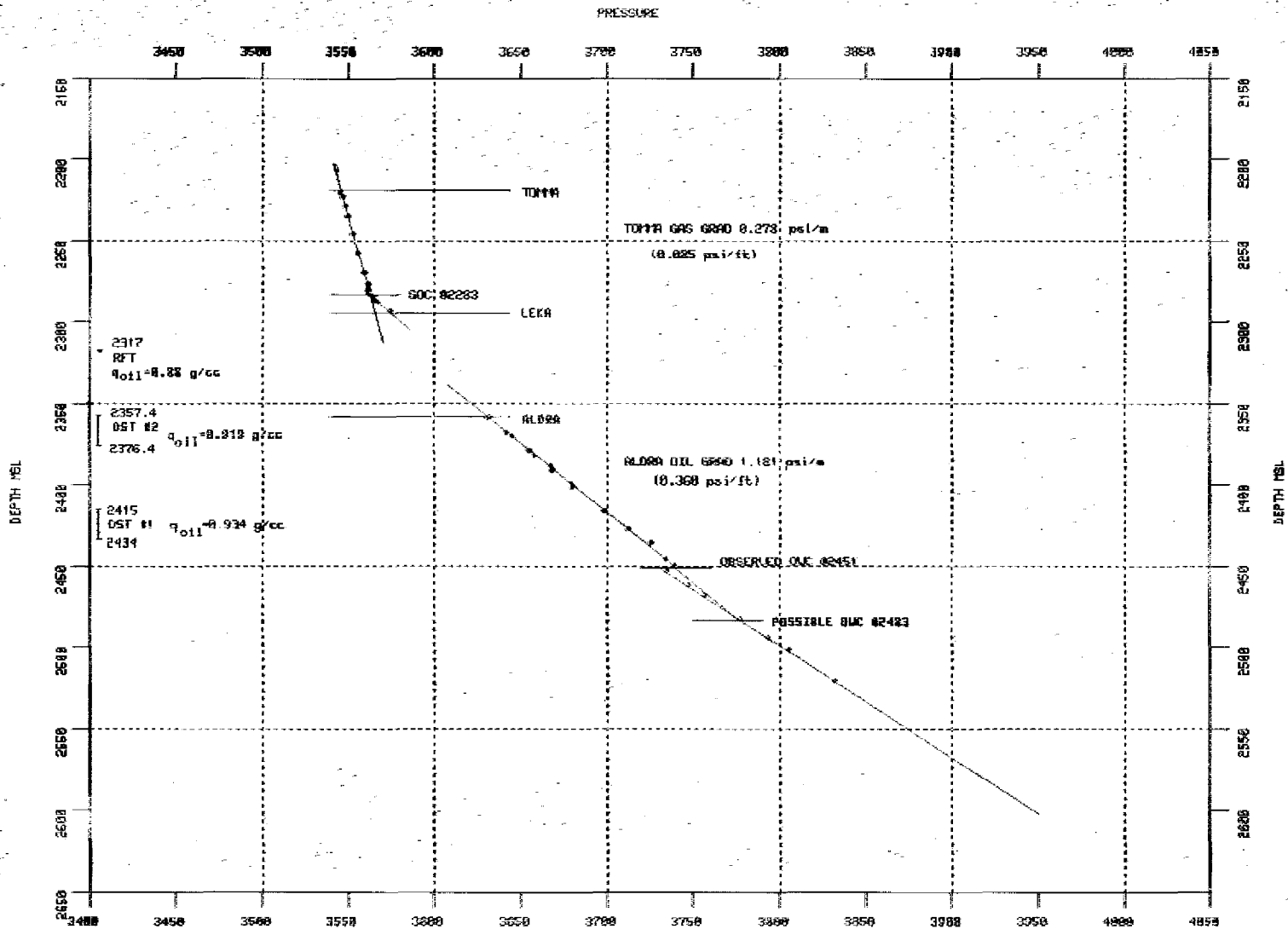
LETK87202034R

RFT PRESSURE POINTS RUN NO. 2

| NO | DEPTH M RKB | HYDROSTAT BEF.PSIA | FORMATION (PSIA) | HYDROSTAT AFT.PSIA | REMARKS PERMEABILITY |
|----|----------------|-----------------------|---------------------|-----------------------|-------------------------|
| 1 | 2252.5 | 3903.1 | 3546.5 | 3903.8 | EXCELLENT |
| 2 | 2258 | 3913.4 | 3547.8 | 3913.7 | EXCELLENT |
| 3 | 2264 | 3924.4 | 3549.8 | 3924.4 | VERY GOOD TO EXC. |
| 4 | 2275 | 3942.6 | 3552.5 | 3942.9 | EXCELLENT |
| 5 | 2287 | 3963.2 | 3555.5 | 3963.4 | EXCELLENT |
| 6 | 2299 | 3984.5 | 3559.2 | 3984.5 | EXCELLENT |
| 7 | 2306 | 3995.7 | 3561.2 | 3996.4 | FAIR |
| 8 | 2309.4 | 4001.8 | 3561.5 | 4002.1 | EXCELLENT |
| 9 | 2312 | 4006.4 | 3562.3 | 4006.6 | EXCELLENT |
| 10 | 2315 | 4012.1 | | | SUPERCHARGE |
| 11 | 2314 | 4010.6 | 3564.7 | 4010.7 | VERY GOOD |
| 12 | 2316 | 4013.7 | 3565.2 | 4015.2 | EXCELLENT |
| 13 | 2319 | 4020.2 | | | TIGHT |
| 14 | 2318 | 4016.5 | | | TIGHT |
| 15 | 2322 | 4022.7 | 3573.7 | 4023.1 | EXCELLENT |
| 16 | 2330 | 4036.4 | 3592.6 | 4037.7 | SUPERCHARGE |
| 17 | 2388 | 4136.3 | 3630.6 | 4136.2 | GOOD |
| 18 | 2397.5 | 4152.0 | 3641.2 | 4151.6 | EXCELLENT |
| 19 | 2408.7 | 4170.7 | 3654.4 | 4170.5 | EXCELLENT |
| 20 | 2420.2 | 4189.3 | 3667.7 | 4189.7 | EXCELLENT |
| 21 | 2431 | 4208.9 | | | SEAL FAILURE |
| 22 | 2430 | 4208.1 | 3679.7 | 4208.8 | EXCELLENT |
| 23 | 2445.3 | 4234.9 | 3697.9 | 4234.9 | EXCELLENT |
| 24 | 2457.5 | 4255.6 | | | SEAL FAILURE |
| 25 | 2456.5 | 4253.6 | 3712.0 | 4253.9 | FAIR/GOOD |
| 26 | 2465.0 | 4267.4 | 3725.0 | 4267.5 | TIGHT |

RFT PRESSURE POINTS RUN NO. 3

| NO | DEPTH M RKB | HYDROSTAT BEF.PSIA | FORMATION (PSIA) | HYDROSTAT AFT.PSIA | REMARKS PERMEABILITY |
|----|----------------|-----------------------|---------------------|-----------------------|-------------------------------|
| 1 | 2288 | 3960.3 | | | TIGHT |
| 2 | 2287 | 3958.5 | 3554.6 | 3958.6 | EXCELLENT |
| 3 | 2308 | 3994.4 | 3560.5 | 3994.4 | EXCELLENT |
| 4 | 2310 | 3996.6 | 3559.8 | 3997.5 | EXCELLENT |
| 5 | 2311.5 | 3999.9 | 3560.5 | 4000.5 | VERY GOOD |
| 6 | 2306 | 3990.5 | 3559.8 | 3991.6 | VERY GOOD |
| 7 | 2299 | 3979.2 | | | SEAL FAILURE |
| 8 | 2298.5 | 3977.5 | 3557.6 | 3977.7 | VERY GOOD |
| 9 | 2310.3 | 3998.1 | 3561.4 | 3998.4 | VERY GOOD TO EXC. |
| 10 | 2311.7 | 4000.7 | | | SEAL FAILURE |
| 11 | 2312 | 4001.3 | 3561.4 | 4001.5 | EXCELLENT |
| 12 | 2314 | 4004.6 | 3563.3 | 4004.9 | VERY GOOD TO EXC. |
| 13 | 2317 | 4009.5 | 3566.5 | 4009.2 | VERY GOOD |
| 14 | 2322 | 4018 | 3572.9 | 4018.6 | GOOD |
| 15 | 2313.5 | 4004.3 | 3562.9 | 4004.5 | VERY GOOD |
| 16 | 2399.5 | 4151.1 | 3644.0 | 4151.4 | GOOD TO VERY GOOD |
| 17 | 2411 | 4171.2 | 3656.9 | 4171.8 | EXCELLENT |
| 18 | 2418 | 4183.5 | 3666.1 | 4183.5 | VERY GOOD |
| 19 | 2429 | 4202.8 | 3678.5 | 4202.2 | EXCELLENT |
| 20 | 2440 | 4221.5 | | | SEAL FAILURE |
| 21 | 2445 | 4229.5 | 3697.0 | 4229.5 | VERY GOOD TO GOOD |
| 22 | 2482 | 4293.4 | 3734.0 | 4293.8 | POOR ? |
| 23 | 2479.5 | 4288.9 | 3738.8 | 4288.5 | FAIR/GOOD |
| 24 | 2497 | 4319.0 | | | SEAL FAILURE |
| 25 | 2497 | 4318.0 | 3755.3 | 4318.4 | VERY GOOD |
| 26 | 2491 | 4306.7 | 3746.5 | 4307.7 | VERY GOOD |
| 27 | 2475 | 4278.4 | | | FORM LEAK |
| 28 | 2475 | 4279.2 | | | SEAL FAILURE |
| 29 | 2475.5 | 4280.2 | 3733.7 | 4280.0 | VERY GOOD TO GOOD |
| 30 | 2511.5 | 4343.7 | 3776.7 | 4242.4 | EXCELLENT |
| 31 | 2531 | 4375.3 | 3804.9 | 4375.0 | FORMATION LEAK |
| 32 | 2531.5 | 4375.7 | 3804.5 | 4375.6 | GOOD |
| 33 | 2565 | 4432.3 | | | SEAL FAILURE |
| 34 | 2523.5 | 4361.2 | 3792.7 | 4361.5 | VERY GOOD |
| 35 | 2550 | 4405.7 | 3830.9 | 4405.7 | EXCELLENT |
| 36 | 2575 | 4447.1 | | | TIGHT |
| 37 | 2580 | | 3874 | | EXCELLENT HP GAUGE PLUGGED |



DST SUMMARY

Two tests were performed in the Aldra Formation:

Test No. 1 : 2444 - 2463 mRKB

Test No. 2 : 2386.4 - 2405.4 mRKB

Test No. 1 (2444 - 2463 mRKB)

Objectives:

The main objectives of this test were determination of reservoir properties and estimation of sand production tendencies.

Test Performance:

The test was performed using a standard testing string and 5 inch modified drill pipe, the 7 inch liner being perforated with tubing conveyed guns at a shot density of 39 shots/meter.

After perforating against closed choke the well was opened and flowed to clean up before shutting in downhole for the initial build up.

The well was flowed at a rate of 270 M3/day for 9 hours during which time PVT samples were obtained, and the well was then again shut in to record the build up.

Bottom hole samplers were run in the hole and the well flowed at a low rate to ensure representative samples.

The final flow period was performed on a series of increasing chokes, the flow rate at each setting being recorded before proceeding to the next. No sand production was noted up to the maximum obtainable rate and the test was concluded.

LETK87202034R

Test No 2 (2386.4 - 2405.4 mRKB)

Objectives:

The objectives for this test were the same as for test no.1.

Test Performance:

Test string and perforation method were the same as for test no.1.

Test procedure was similar to test no.1 with clean up flow, build up, sampling flow, bottom hole sampling and main flow periods.

After changing choke to 1.91 cm (48/62) sand production was noted and the flow was choked back to try to regain sand free production. The well was finally shut in and killed to avoid plugging the tool string with sand. Sand had also been observed in the choke box after the bottom hole sampling flow.

TEST RESULTS

The following flowing data was obtained:

Test No. 1:

| <u>Choke</u> <u>CM</u> | <u>WHP</u> <u>KPA</u> | <u>BHP</u> <u>KPA</u> | <u>Qoil</u> <u>M³/D</u> | <u>GOR</u> <u>M³/m³</u> |
|---------------------------|--------------------------|--------------------------|---------------------------------------|--------------------------------------------------|
| 1.11 | 3860 | 22571 | 268 | 51 |
| 1.43 | 3330 | 20460 | 381 | 50 |
| 1.91 | 2720 | 18843 | 555 | 47 |
| 2.54 | 2160 | 17869 | 627 | 48 |
| 3.81 | 1800 | 17129 | 715 | 44 |

Gravity of stock tank oil 933 kg/m³

Gas gravity (Air = 1) 0.600

Test No. 2

| <u>Choke</u> <u>CM</u> | <u>WHP</u> <u>KPA</u> | <u>BHP</u> <u>KPA</u> | <u>Qoil</u> <u>M³/D</u> | <u>GOR</u> <u>M³/m³</u> |
|---------------------------|--------------------------|--------------------------|---------------------------------------|--------------------------------------------------|
| 0.79 | 6200 | 23997 | 205 | 58 |
| 1.27 | 5840 | 23268 | 508 | 57 |
| 1.91 | 5090 | 22428 | 906 | 55 |

Gravity of stock tank oil 918 kg/m³

Gas Gravity (Air = 1) 0.615

TEST ANALYSIS

Results of the test analysis will be published in a separate report when available.

LETK87202034R

FLOPETROL JOHNSTON

Schlumberger

DIVISION : NEU

BASE : NWB

REPORT N°: 86.95.WT.02

Well Testing Report

Client = Statoil

Rig: Dyvi Delta

Field = Heidrun

Well = 6507/8-1

Zone = Aldra

Date = 01-DEC-86 To 05Dec 1986

DST nr. 2

— MAIN RESULTS —

Tested interval : Aldra Formation Perforations : 2387 - 2406m

| Operation | Duration | Bottom hole pressure | Well head pressure | Oil prod. rate | Gas prod. rate | G.O.R. |
|---------------------------------------------------|----------|----------------------|--------------------|-------------------|-------------------|--------------------------------|
| Units | hrs/min | KPa | KPa | M ³ /D | M ³ /D | M ³ /M ³ |
| Clean up flow 12.7mm fixed choke | 6.09 | 23205 | 5850 | 519.5 | 28920 | 56 |
| First build up | 6.08 | 24292 | N/A | - | - | - |
| Low rate flow 7.938mm fixed choke | 9.11 | 23997 | 6200 | 204.5 | 11870 | 58 |
| Second build up | 15.06 | 24318 | N/A | - | - | - |
| Bottom hole sampling 3.175mm fixed choke | 1.40 | 24281 | 5300 | N/A | N/A | N/A |
| High rate flow 12.7mm fixed choke | 3.10 | 23268 | 5840 | 507.5 | 28910 | 57 |
| 19.05mm fixed choke | 6.48 | 22428 | 5090 | 905.6 | 50080 | 55 |

Depth of bottom hole measurements: 2314.47m Reference: RKB. Dyvi Delta

Temperature: Max 81°C at: 2314.47m depth

Separator gas gravity (air: 1) at choke size: 12.7mm: .630, 7.938mm: .630, 1905mm: .615

STO gravity at choke size 12.7mm: .919, 7.938mm: .9196, 1905mm: .9170

BSW: 3% Sand at 19.05mm Water cut: 0

REMARKS AND OTHER OPERATIONS

All measure ments are those last recorded in each event

H₂S = 0.5 ppmCO₂ = 1.5%

DIVISION : NEU

BASE : NWB

REPORT N°: 86.95.WT.01

Well Testing Report

| | | |
|--------|---------------|----------------------------------|
| Client | = STATOIL | RIG: DYVI DELTA |
| Field | = HEIDRUN | Well = 6507/8-1 |
| Zone | = LOWER ALDRA | Date = 24-NOV-86 TO 30-NOV-86 |

DST no.1.

— MAIN RESULTS —

Tested interval : Lower Aldra Perforations : 2444m - 2463m

| Operation | Duration | Bottom hole pressure | Well head pressure | Oil prod. rate | Gas prod. rate | G.O.R. |
|---------------------------|----------|----------------------|--------------------|-------------------|-------------------|--------------------------------|
| Units | MIN | KPa | KPa | M ³ /D | M ³ /D | M ³ /M ³ |
| | | | D.S.T. # 1 | | | |
| Clean up | | 24638 | 4500 | | | |
| 6.35mm fixed choke | 20 | 22647 | 2250 | 161.3 | - | - |
| 7.940mm fixed choke | 45 | 22146 | 1800 | 201.6 | - | - |
| 9.525mm fixed choke | 101 | 22130 | 3820 | - | - | - |
| 11.11mm fixed choke | 242 | 21124 | 3620 | 272.6 | 12500 | 46 |
| 14.3mm fixed choke | 112 | 22311 | 3230 | 402.8 | 18120 | 45 |
| First build up | 597 | 22939 | 3020 | - | - | - |
| Low Rate flow | | | | | | |
| 11.11mm fixed choke | 540 | 22571 | 3860 | 267.7 | 13770 | 51 |
| Second build up | 1110 | 24627 | N/A | - | - | - |
| Bottom hole sampling flow | | | | | | |
| 3.175mm fix. | 149 | 24336 | 4830 | N/A | N/A | N/A |

Depth of bottom hole measurements: 2332.11m Reference: RKB, DYVI DELTA

Temperature: Max 84.9°C at: 2332.11m depth

Separator gas gravity (air: 1) at choke size: 11.11mm: .601, 14.3mm: .60

STO gravity at choke size 11.11mm: .9337, 14.3mm: .9337

BSW: 0% Water cut: 0%

REMARKS AND OTHER OPERATIONS

All Measurements are those last taken in each event.

CO₂ = 1.5%H₂S = 0.5ppm

STATOIL WELL NO.6507/8-1

DRILLING MUD PROPERTIES RECORD

| MUD SYSTEM: | | SPUD MUD/KCl-POLYMER/GEL-LIGN. | | | | | | | | AREA RIG | | HALTENBANKEN DYVI DELTA | | | | | | | | | | | |
|-------------|-----------|--------------------------------|---------|-----------|-----|-----|----------|----------|------|----------|--------|-------------------------|-----------|------------|----------|---------------|-----------|----------|------|-------|---------|---------|-------|
| DAY No. | DATE 1986 | DEPTH metre | M.W. sg | F.V. s/qt | 600 | 300 | A.V. cps | P.V. cps | Y.P. | GEL 0 | GEL 10 | pH | API Filt. | CAKE 32nds | HTHP ml. | Chl.ppm *1000 | Calc. ppm | Pf %Sol. | %Oil | %Sand | MRT ppb | KCl ppb | |
| 1 | 10/28 | 447 | 1.05 | 80 | 61 | 53 | 30.5 | 8 | 45 | 36 | 38 | 10.60 | N.C | | | | | | | | | | |
| 2 | 10/29 | 447 | 1.05 | 92 | 66 | 56 | 33 | 10 | 46 | 34 | 35 | 10.80 | N.C | | | | | | | | | | |
| 3 | 10/30 | 447 | 1.05 | 120 | 88 | 66 | 44 | 22 | 44 | 42 | 48 | 10.90 | N.C | | | | | | | | | | |
| 4 | 10/31 | 610 | 1.05 | 150 | 92 | 70 | 46 | 22 | 48 | | 11.00 | N.C | | | | | | | | | | | |
| 5 | 11/ 1 | 1050 | 1.05 | 120 | 88 | 65 | 44 | 23 | 42 | | 11.00 | N.C | | | | | | | | | | | |
| 6 | 11/ 2 | 1050 | 1.12 | 62 | 44 | 32 | 22 | 12 | 20 | 2 | 5 | 9.00 | 4.5 | 1 | | 46 | 140 | .2 | 4 | | | | 42.00 |
| 7 | 11/ 3 | 1050 | 1.12 | 62 | 44 | 30 | 22 | 14 | 16 | 2 | 5 | 9.50 | 4.2 | 1 | | 46 | 140 | .2 | 4 | Tr. | 0 | | 42.00 |
| 8 | 11/ 4 | 1398 | 1.15 | 63 | 42 | 28 | 21 | 14 | 14 | 3 | 5 | 9.90 | 4 | 1 | | 67 | 320 | .3 | 6 | .25 | 3 | | 40.00 |
| 9 | 11/ 5 | 1675 | 1.35 | 60 | 57 | 36 | 28.5 | 21 | 15 | 3 | 5 | 9.10 | 3.5 | 1 | | 68 | 300 | .1 | 13 | .5 | 5 | | 42.00 |
| 10 | 11/ 6 | 2131 | 1.35 | 55 | 52 | 33 | 26 | 19 | 14 | 3 | 5 | 8.80 | 3.3 | 1 | | 72 | 440 | .1 | 14 | .75 | 10 | | 44.00 |
| 11 | 11/ 7 | 2235 | 1.35 | 51 | 51 | 32 | 25.5 | 19 | 13 | 3 | 7 | 8.40 | 3.5 | 1 | | 72 | 520 | .05 | 14 | .75 | 12 | | 45.00 |
| 12 | 11/ 8 | 2235 | 1.35 | 51 | 39 | 25 | 19.5 | 14 | 11 | 3 | 5 | 8.30 | 3.5 | 1 | | 70 | 580 | 0 | 14 | .75 | 12 | | 44.00 |
| 13 | 11/ 9 | 2235 | 1.2 | 80 | 35 | 22 | 17.5 | 13 | 9 | 3 | 20 | 10.30 | 5 | 1 | | 3.5 | 80 | .05 | 5 | Tr. | 17 | | |
| 14 | 11/10 | 2250 | 1.2 | 110 | 72 | 44 | 36 | 28 | 16 | 5 | 27 | 9.20 | 3.7 | 1 | 13.00 | 3.7 | 300 | .05 | 6 | Tr. | 19 | | |
| 15 | 11/11 | 2249 | 1.2 | 110 | 63 | 39 | 31.5 | 24 | 15 | 5 | 24 | 9.30 | 3.8 | 1 | 14.00 | 4.8 | 300 | .05 | 6 | .5 | 20 | | |
| 16 | 11/12 | 2290 | 1.2 | 90 | 53 | 33 | 26.5 | 20 | 13 | 4 | 19 | 9.10 | 4.2 | 1 | 14.50 | 4.8 | 260 | .05 | 6 | .5 | 22 | | |
| 17 | 11/13 | 2350 | 1.2 | 107 | 61 | 38 | 30.5 | 23 | 15 | 3 | 22 | 9.70 | 4.2 | 1 | 14.00 | 4.2 | 280 | .1 | 6 | .5 | 20 | | |
| 18 | 11/14 | 2467 | 1.21 | 105 | 62 | 38 | 31 | 24 | 14 | 4 | 22 | 9.20 | 3.6 | 1 | 12.00 | 4.5 | 210 | .1 | 7 | 1.5 | 23 | | |
| 19 | 11/15 | 2600 | 1.2 | 95 | 58 | 36 | 29 | 22 | 14 | 4 | 24 | 9.00 | 4.2 | 1 | 12.00 | 4.6 | 260 | .1 | 9 | .75 | 20 | | |
| 20 | 11/16 | 2600 | 1.2 | 95 | 58 | 36 | 29 | 22 | 14 | 4 | 23 | 9.00 | 4.2 | 1 | | 4.6 | 260 | .1 | 9 | .75 | 20 | | |
| 21 | 11/17 | 2600 | 1.2 | 95 | 53 | 33 | 26.5 | 20 | 13 | 4 | 17 | 9.00 | 4 | 1 | | 4.5 | 280 | .05 | 9 | .75 | 18 | | |
| 22 | 11/18 | 2600 | 1.2 | 118 | 55 | 35 | 27.5 | 20 | 15 | 4 | 20 | 9.20 | 4 | 1 | | 4.5 | 280 | .05 | 9 | .75 | 18 | | |
| 23 | 11/19 | 2600 | 1.2 | 102 | 55 | 35 | 27.5 | 20 | 15 | 4 | 18 | 9.40 | 4.1 | 1 | | 4.6 | 280 | .05 | 9 | .75 | 18 | | |
| 24 | 11/20 | 2600 | 1.2 | 98 | 51 | 32 | 25.5 | 19 | 13 | 3 | 22 | 9.10 | 4.2 | 1 | | 4.5 | 280 | .1 | 9 | .75 | 17 | | |
| 25 | 11/21 | 2600 | 1.2 | 90 | 50 | 30 | 25 | 20 | 10 | 3 | 12 | 8.70 | 4 | 1 | | 4.5 | 280 | .05 | 9 | .75 | 17 | | |
| 26 | 11/22 | 2600 | 1.2 | 57 | 41 | 26 | 20.5 | 15 | 11 | 3 | 14 | 9.90 | 5.8 | 1 | | 6 | 120 | .15 | 9 | .75 | 17 | | |

STATOIL WELL NO.6507/8-1

DRILLING MUD PROPERTIES RECORD

| MUD SYSTEM: | | SPUD MUD/KCl-POLYMER/GEL-LIGN. | | | | | | | | AREA RIG | | HALTENBANKEN DYVI DELTA | | | | | | | | | | |
|-------------|-----------|--------------------------------|---------|-----------|-----|-----|---------|---------|-----|----------|--------|-------------------------|-----------|------------|----------|---------------|-----------|----------|------|-------|---------|---------|
| DAY No. | DATE 1986 | DEPTH metre | M.W. sg | F.V. s/qt | 600 | 300 | A.V cps | P.V cps | Y.P | GEL 0 | GEL 10 | pH | API Filt. | CAKE 32nds | HTHP ml. | Chl.ppm *1000 | Calc. ppm | Pf %Sol. | %Oil | %Sand | MBT ppb | KCl ppb |
| 27 | 11/23 | 2600 | 1.2 | 55 | 38 | 24 | 19 | 14 | 10 | 3 | 25 | 12.50 | 5.2 | 1 | | 6 | 160 | .95 | 9 | .75 | 15 | |
| 28 | 11/24 | 2598 | 1.2 | 53 | 38 | 23 | 19 | 15 | 8 | 3 | 27 | 12.50 | 5.8 | 1 | | 6 | 160 | .95 | 9 | .75 | 15 | |
| 29 | 11/25 | 2598 | 1.2 | 54 | 37 | 23 | 18.5 | 14 | 9 | 3 | 24 | 12.50 | 5.8 | 1 | | 6 | 160 | .9 | 9 | .75 | 15 | |
| 30 | 11/26 | 2598 | 1.2 | 41 | 28 | 17 | 14 | 11 | 6 | 3 | 27 | 12.50 | 5.9 | 1 | | 6 | 160 | .65 | 9 | .75 | 15 | |
| 31 | 11/27 | 2598 | 1.2 | 39 | 27 | 17 | 13.5 | 10 | 7 | 3 | 14 | 11.80 | 6.2 | 1 | | 5.5 | 200 | .55 | 8 | .75 | 15 | |
| 32 | 11/28 | 2598 | 1.2 | 41 | 29 | 18 | 14.5 | 11 | 7 | 3 | 16 | 11.50 | 6.8 | 1 | | 6 | 240 | .45 | 8 | .75 | 15 | |
| 33 | 11/29 | 2598 | 1.2 | 42 | 27 | 17 | 13.5 | 10 | 7 | 3 | 14 | 12.00 | 6.2 | 1 | | 5.5 | 200 | .7 | 8 | .75 | 15 | |
| 34 | 11/30 | 2434 | 1.2 | 44 | 27 | 17 | 13.5 | 10 | 7 | 2 | 15 | 12.00 | 6 | 1 | | 5.5 | 220 | .6 | 8 | .5 | 15 | |
| 35 | 12/ 1 | 2420 | 1.2 | 39 | 24 | 15 | 12 | 9 | 6 | 2 | 12 | 12.30 | 7.5 | 1 | | 7.5 | 160 | .75 | 8 | Tr. | 15 | |
| 36 | 12/ 2 | 2420 | 1.2 | 40 | 24 | 15 | 12 | 9 | 6 | 2 | 15 | 12.00 | 8.2 | 1 | | 7.5 | 240 | .55 | 8 | .25 | 15 | |
| 37 | 12/ 3 | 2420 | 1.2 | 40 | 24 | 15 | 12 | 9 | 6 | 2 | 15 | 11.80 | 8 | 1 | | 7.5 | 240 | .4 | 8 | .25 | 15 | |
| 38 | 12/ 4 | 2420 | 1.2 | 40 | 24 | 15 | 12 | 9 | 6 | 2 | 14 | 11.80 | 7.4 | 1 | | 7.5 | 220 | .4 | 8 | Tr. | 15 | |
| 39 | 12/ 5 | 2000 | 1.2 | 43 | 27 | 17 | 13.5 | 10 | 7 | 3 | 19 | 12.10 | 8.2 | 1 | | 7.5 | 300 | .8 | 8 | .25 | 15 | |
| 40 | 12/ 6 | | 1.35 | 46 | 33 | 21 | 16.5 | 12 | 9 | 4 | 26 | 12.10 | 8.6 | 1 | | 8 | 360 | .6 | 12 | .75 | 15 | |

3.11 Drilling equipment failures