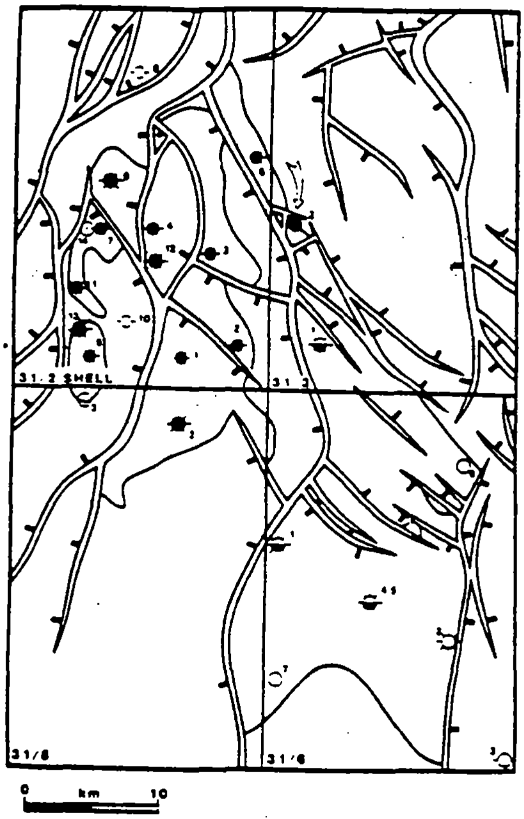
PETROPHYSICAL EVALUATION
WELL 31/3-2



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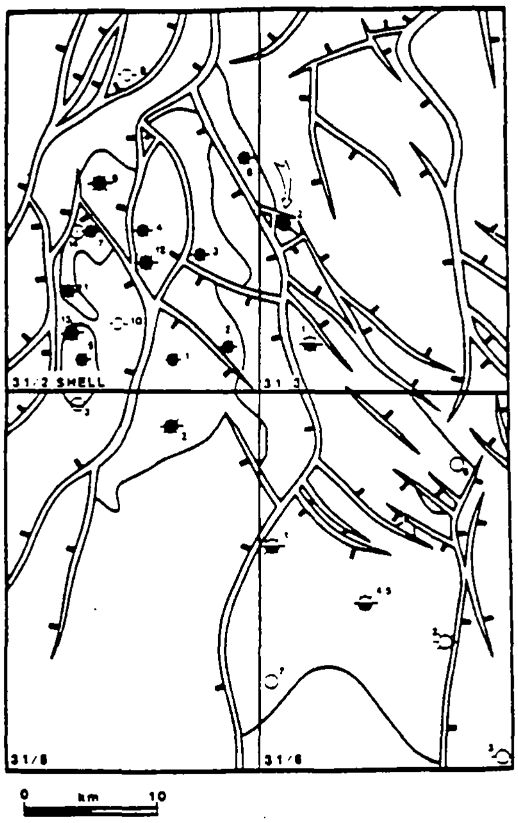

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PREFACE

This report proposes a preliminary petrophysical interpretation for well 31/3-2. The well was located close to the border line of Block 31/2, about midways of the Block 31/3. The well was spudded on March 5,1984 by the H-3 drilling vessel Treasure Seeker. The reservoir was reached at 1567 mRKB where the Sognefjord formation was identified. Hydrocarbons were encountered in the interval 1567 - 1578.5 mRKB.Coring was performed in the interval 1565.00 - 1640.00 mRKB. A production test was conducted in the intercval 1567.3 - 1577.3 mRKB. TD was reached at 2090 mRKB.

GENERAL DATA

Licence :	PL085	
Owners :	Statoil/Hydro/Saga	
Operator:	Hydro	
Field :	Troll East	
Coordinates :	60 52'11.41" N	6 748 639 mN
	03 40'41.79" E	536 836 mE
Rig :	TREASURE SEEKER	
Elevation KB :	25 m	
Water depth :	340 m (RKB)	
Date spudded :	MAR 5 , 1984	
Date completed :	APR 30, 1984	
TD Driller :	2090 m	
TD Logger :	2088 m	
Logging company :	Schlumberger	
Mud Logger :	Exploration Logging	

Well location is shown in figure 1.

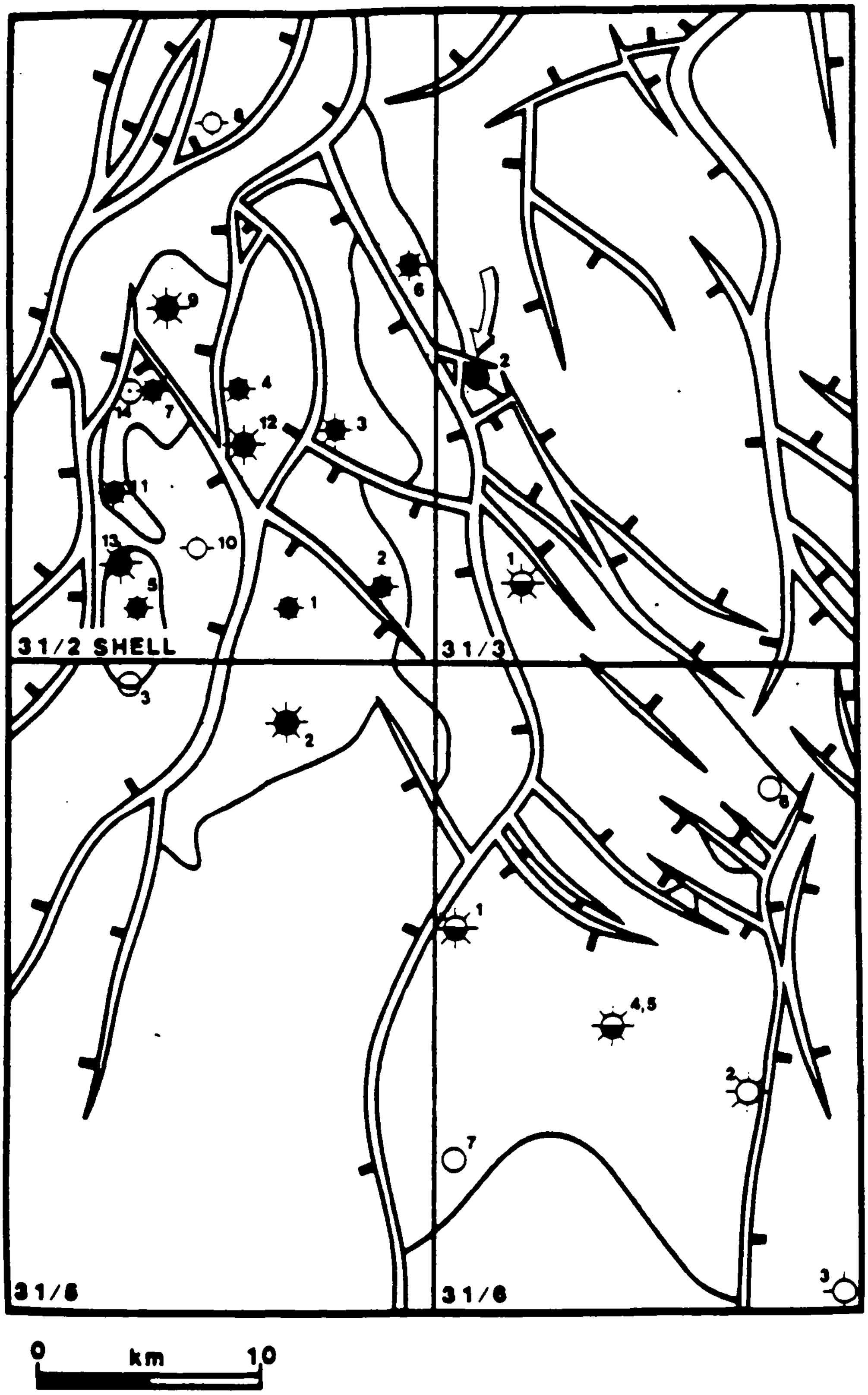


figure 1. Well location

OBJECTIVES

The primary objective for this well was to test if hydrocarbons are present close to the boundary fault between Troll-West and Troll-East and to evaluate the degree of communication between the to structures.

RESULT SUMMARY

Well 31/3-2 encountered hydrocarbons in the interval 1567-1579 mRkb.

The CPI results are summarized below:

FORMATION	INTERVAL mRkb	GROSS m	NET m	N/G	PHIE %	SW %	KHlog mD
SOGNEFJORD	1567.0-1706.0	139.0	131.0	0.94	26.9	84.4	1166.
U.HEATHER	1706.0-1725.0	19.0	17.5	0.92	18.6	81.9	2.6
FENSFJORD	1725.0-1850.5	125.5	107.5	0.86	21.4	91.7	241.
KROSSFJORD -top DRAKE	1850.5-2005.5	155.0	124.5	0.80	23.8	97.2	793.

* CORE DATA *

FORMATION	INTERVAL mRkb	PHI %	KLH mD (Arit)	KLV mD	KLV/KLH
SOGNEFJORD	1567.0-1706.0	29.9	3129.	1996.	0.64

The hydrocarbon interval was identified from the resistivity logs and density/neutron logs. The following contacts were established:

GOC = 1567.5 mRKB (1542.5 mMSL) Probable.
OWC = 1579.0 mRKB (1554.0 mMSL)

yielding a net hydrocarbon oil column of 11.5 meters. GOC is not conclusively determined from the logs, although the density/neutron separation at the very top of Sognefjord fm. could be interpreted as gas. A well test match verifies a GOC at 1567.5 mRKB.

The hydrocarbon net pay results:

INTERVAL	GROSS m	NET m	N/G	PHIE %	SW %	KHLOG mD	KVLOG mD	KLH mD	KLV mD
1567-1580	13.0	11.5	0.88	25.3	30.5	1511	1456	3024	1729

CORE DATA

Cores were taken in the interval 1565 - 1640 mRkb.The cores were depth corrected to logs.All cores were shifted down 1.50m and an acceptable agreement with logs was achieved.

Core recovery is shown below:

CORE NUMBER	DEPTH MRKB	REC.DEPTH MRKB	RECOVERY %
core 1	1565.00-1581.00	1565.00-1575.50	65.6
core 2	1581.00-1593.00	1581.00-1590.70	80.8
core 3	1593.00-1608.00	1593.00-1606.25	88.3
core 4	1608.00-1626.00	1608.00-1626.00	100.0
core 5	1626.00-1640.00	1626.00-1640.00	100.0

ROUTINE CORE MEASUREMENTS

Routine core measurements were performed every 0.25m throughout the cored interval.Measurements of air horisontal and vertical permeability,porosity and grain density were done.Air permeability was Klinkenberg corrected.

1 1/2 " plugs were taken approximately every meter.Table 1.

Seal peals were taken in 0.25 m sampling intervals approximately every two meter.Table 2.

OBJECTIVES

The primary objective for this well was to test if hydrocarbons are present close to the boundary fault between Troll-West and Troll-East and to evaluate the degree of communication between the to structures.

11.04.84. HYDRO WELL: 31/3-2

Table 1 1½" Plugger

CORE NO. 1:

1568.10
1569.10
1570.10
1571.10
1572.15
1573.10
1574.90

CORE NO. 2:

1581.10
1582.10
1583.10
1584.10
1585.10
1586.10
1587.10
1588.10
1589.10
1590.10

CORE NO. 3:

1593.10
1594.10
1595.10
1596.30
1597.30
1598.10
1599.15
1600.10
1601.10
1602.10
1603.20
1604.10
1605.10
1606.10

CORE NO. 4:

1608.10
1609.10
1610.60
1611.10
1612.10
1613.10
1614.10
1615.10
1616.10
1617.10
1618.10
1619.10
1620.10
1621.10
1622.10
1623.10
1624.10
1625.10

Table 2 **Seal Peal**

CORE NO. 1:

1568.75 - 1569.00
1570.75 - 1571.00
1572.75 - 1573.00
1574.00 - 1574.25

CORE NO. 2:

1582.75 - 1583.00
1584.75 - 1585.00
1586.75 - 1587.00
1588.75 - 1589.00

CORE NO. 3:

1594.75 - 1595.00
1596.00 - 1596.25
1598.75 - 1599.00
1600.75 - 1601.00
1602.75 - 1603.00
1604.75 - 1605.00

CORE NO. 4:

1609.75 - 1610.00
1611.75 - 1611.00
1615.75 - 1616.00
1619.75 - 1620.00
1621.75 - 1622.00
1623.75 - 1624:00

CORE NO. 5:

1626.75 - 1627.00
1628.75 - 1629.00
1630.75 - 1631.00
1632.75 - 1633.00
1634.75 - 1635.00
1636.75 - 1637.00
1638.75 - 1639.00

LOG EVALUATION

The log evaluation was performed with the IN HOUSE CPI program over the interval 1565 - 2025.0 mRKB.

Petrophysical model

The lithology of the 31/2-area is complex regarding the log evaluation, and is built up from a changing mixture of quartz, clay minerals, mica, carbonate cemented horizons, and presence of heavy minerals like pyrite. The presence of mica affects all the porosity logs and due to its radioactivity it appears as shaly on the gamma ray log. If a "standard" evaluation was to be performed - a shaly - sand evaluation - we would derive porosities too low and water saturations too high.

NGS - log - approach

The NGS - log has been used for the quantification of the mica content (ref. J. Suau 1). Due to the mud-effects on the logs in the presence of KCl-mud it has been normalized to the wells 31/2-11 and 31/2-12 which were drilled with a $CaCl_2/CaCO_3$ mud without barite. The quality of the logs in these wells are considered to be very good. Based on the Th/K cross plot (see fig. 2) with selected matrix values of clay, mica and feldspar the bulk volume of total solids of clay, mica and feldspar is calculated. Assuming a porosity, the volume of the different minerals are determined. Porosity is then calculated from the density log corrected for the mica and feldspar content. There is also a correction applied for the silt content. Due to the presence of silt together with mica there is a tendency of calculating too high mica content, since the silt is assumed to be containing an increased Thorium content. To take this into consideration the thorium curve is used as a silt indicator. The mica and feldspar volumes are reduced for this silt fraction and added to the shale volum.

The NGS - log has not been corrected for environmental effects nor the presence of KCl and barite. These corrections will allegedly shortly be possible to perform from Schlumberger and will be evaluated as soon as data becomes available.

In Fig. 3 the normalized and corrected Thorium and Potassium values are shown plotted in the Sognefjord, U. Heather and Fens formations.

SH	SILT	MI	FE	QZ	Ø

Matrix-model. Silt is calculated from Mica and Feldspar and added to shale.

Porosity determination

Porosity has been calculated from the density log corrected for the mica effect and hydrocarbons. Due to the high density of the mica (varies between 2.85 - 3.10 g/cc) it is assumed that the density log is the easiest log to correct. For the calculations based on the NGS - log the density log is corrected for the computed amounts of mica and feldspar through the equation:

$$Rhob_{corr} = Rhob + V_{mica}\ (Rhoma-Rhomica) + V_{FELD}\ (Rhoma-Rhofeld)$$

Hydrocarbon correction is applied after shale correction on the corrected density log according to the equation:

$$\emptyset = \frac{Rhoma - Rhob_{corr}}{Rhoma - Rhofl} - \frac{Rhoma - Rhoch}{Rhoma - Rhofl} \cdot V_{SH}$$

and based on the RXO-curve for a water saturation in the flushed zone, Sxo:

$$\frac{1}{\sqrt{R_{xo}}} = \frac{VSH^{(1-VSH/2)}}{\sqrt{R_{SH}}} + \emptyset^{m/2}\sqrt{a \cdot R_{mf}} \cdot S_{xo}^{n/2}$$

An iterative process is achieved until the effect on porosity is less than 0.004.

A comparison between calculated porosity and core porosity shows acceptable agreement. In situ-core porosities have to be depth corrected properly and corrected for the overburden effect.

TRUE RESISTIVITY

Rt - resistivity of the virgin formation was taken from the borehole corrected and invasion corrected laterolog.In the water zone the deep induction was used. The MSFL corrected for mudcake and SFL was used as RXO in the HC-bearing and water- bearing intervals respectively.

WATER SATURATION

The Poupon equation was applied for the water saturation computation:

$$\frac{1}{RT^{1/2}} = \frac{VSH^{(1-VSH/2)}}{RSH^{1/2}} + \frac{PHIE^{m/2}}{(a\ RW)^{1/2}}\ SW^{n/2}$$

Symbols used:

Rt	=	Resistivity of virgin zone
VSH	=	Bulk volume shale
RSH	=	Shale resistivity
PHIE	=	Porosity
a	=	Lithology constant
m	=	Cementation exponent
n	=	Saturation exponent
RW	=	Formation water resistivity

THORIUM-POTASSIUM CROSSPLOT

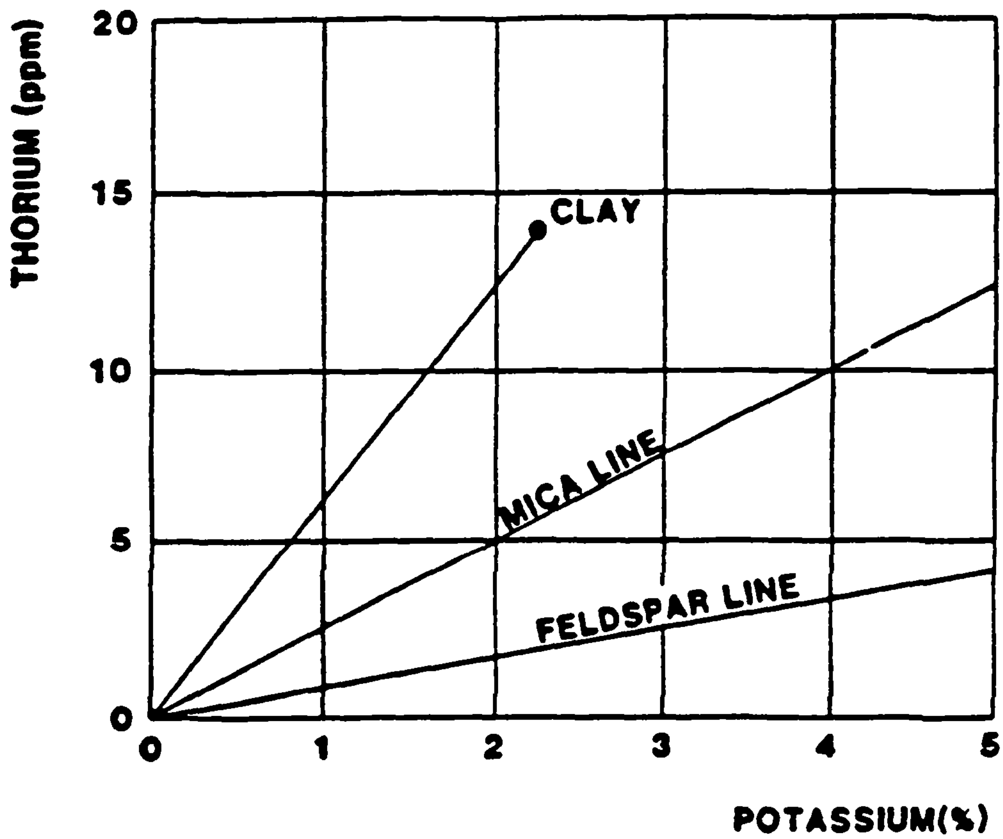


Figure 2 Thorium - Potassium Crossplot

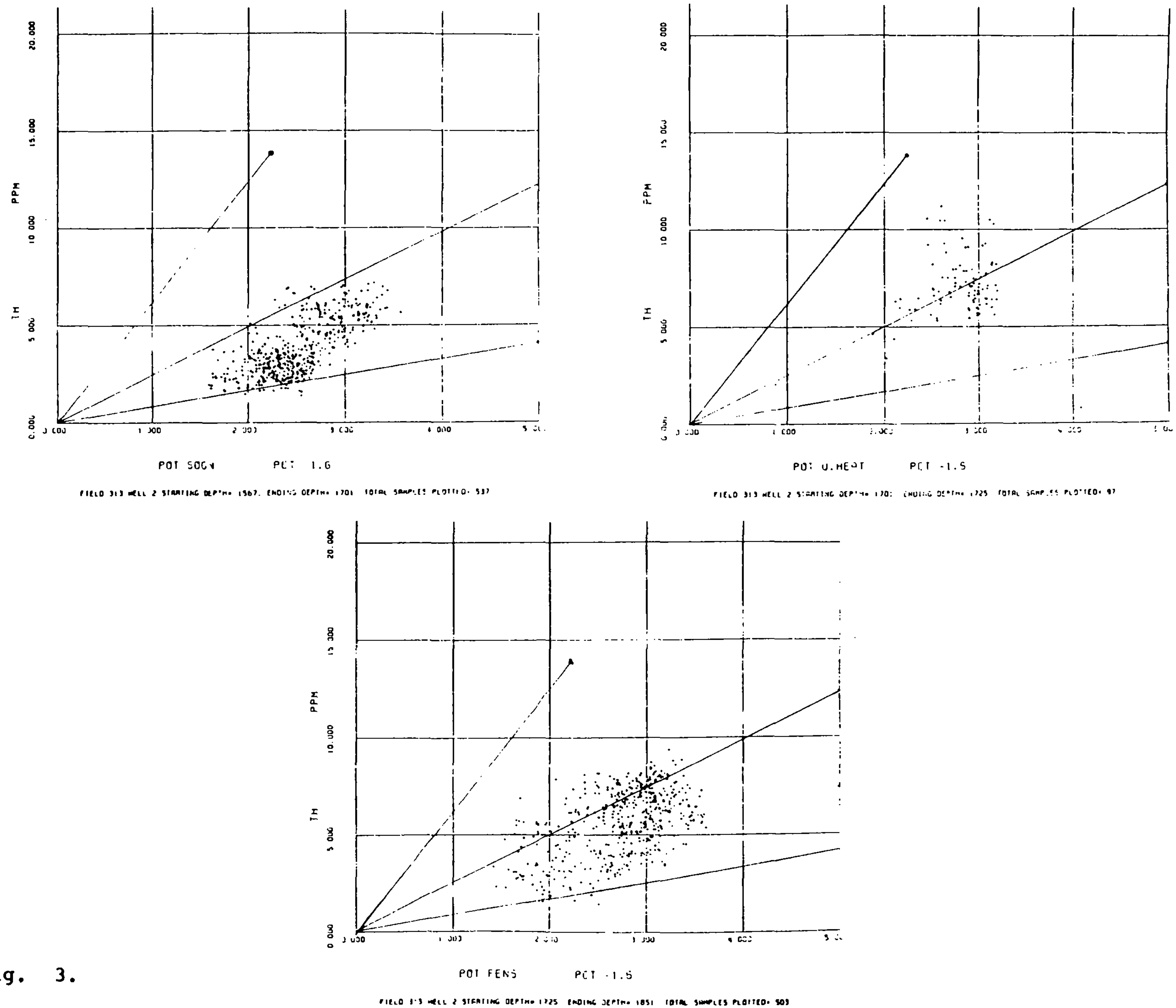

TH PPM
POT SOGN PCT 1.6
FIELD 313 WELL 2 STARTING DEPTH= 1567. ENDING DEPTH= 1701 TOTAL SAMPLES PLOTTED= 537
POT U.HEAT PCT -1.5
FIELD 313 WELL 2 STARTING DEPTH= 1701 ENDING DEPTH= 1725 TOTAL SAMPLES PLOTTED= 97
POT FENS PCT -1.5
FIELD 313 WELL 2 STARTING DEPTH= 1725 ENDING DEPTH= 1851 TOTAL SAMPLES PLOTTED= 503

Fig. 3.

PERMEABILITY

The log derived pemeability calculation was based on a regression between horisontal Klinkenberg corrected permeability versus porosity and gamma ray.The following relation was found:

Interval 1560.0 - 1579.0 mRKB

$$\log KH = 13.6661 + 1.3074*\log PHI - 2.3866*\log SW - 6.3994*\log GR$$
$$\log KV = -35.3623 - 37.2462*\log PHI - 12.2123*\log SW + 4.1953*\log GR$$

Interval 1579.0 - 2025.0 mRKB

$$\log KH = 21.3647 + 8.2158*\log PHI - 7.5960*\log GR$$
$$\log KV = 22.0281 + 7.4545*\log PHI - 8.3992*\log GR$$

GEOLOGICAL ZONING

The geological zonation is based on correlations made for the Troll area and the following formation tops are used in the evaluation

FORMATION	ZONE	FORMATION INTERVAL mRkb
SOGNEFJ.FM		1567.0 - 1706.0
	2B	1567.0 - 1616.0
	2A	1616.0 - 1620.0
	3	1620.0 - 1706.0
U.HEATHER FM	4	1706.0 - 1725.0
FENSFJORD FM	5	1725.0 - 1850.5
KROSS FM		1850.5 - 1929.0
L.HEATHER		1929.0 - 1939.0
BRENT		1939.0 - 2005.5

LOG EVALUATION DATA

LOG QUALITY AND PERFORMANCE

The log quality was acceptable for most of the logs.The MSFL log was edited in the interval 1536 - 1568 mRKB due to bad pad contact on main log. The repeat section was used for this interval. The DLL/MSFL was run over the interval 1502 - 1639 mRKB as an intermediate run with different mud properties than the main log run, from which logs have been evaluated.

NORMALIZATIONS

The well was drilled with a KCl mud containing 57 ppg Barite.This requires normaliztation of the thorium and potassium curves from the N G S - log. Comparision of the Th/K crossplots from this well with 31/2-11,12 and other wells in the area was performed to establish corrections.
The following normalizations were made:

LOG	SHIFT
K	- 1.6 pct.

RW-CALCULATION

Formation water resistivity was based on crossplot techniques from logs and from RW - calculations from nearby wells. RW - values varied from 0.065 - 0.088 ohmm at 137 DF. This is in good agreement with resistivity of a water sample from well 31/5-3 which is believed to be representative for the Troll Field.

No reliable water sample was retrieved from this well.

The formation water resistivity, RW, used in the evaluation:

RW = 0.080 ohmm Ø 135 DF (1570 mRKB)

which corresponds to an equivalent NaCL concentration of 46700 ppm.

COMPUTATION DATA

MUD PROPERTIES

Type of mud : KCL/POLYMER

Additives : Barite 57 ppg

RM	: 0.101 ohmm 14.4 C (58 DF)	RESERVOIR INTERVAL
RMF	: 0.090 ohmm 11.1 C (52 DF)	
RMC	: 0.400 ohmm 4.4 C (40 DF)	

Salinity: 55000 ppm Cl-

RM	: 0.115 ohmm 15.5 C (60 DF)	WATER INTERVAL
RMF	: 0.092 ohmm 7.2 C (45 DF)	
RMC	: 0.397 ohmm 5.0 C (41 DF)	

TEMPERATURE

Temperature,BHT,from logs:

DLL-MSFL	= 89 DF	1634 MRKB
ISF-LSS	= 121 DF	2085 MRKB
LDL-CNL	= 141 DF	2086 MRKB
SHDT-GR	= 159 DF	2087 MRKB

Temperature,BHT,from Horner plot :
Circulation time: 1 hrs 35 min

	Log	Depth	T1	T2	Time since circ.		Static temp
1/	ISF-LSS	2085	120	121	4 hr 25 min	(1,2)	152.7
2/	LDL-CNL	2086	141	142	13 hr 10 min	(2,3)	170.2
3/	SHDT-GR	2087	159	159	35 HR 40 MIN	(1,3)	165.3

Temperature used in the evaluation: 163 DF at 2086 mRKB
and a gradient of 0.054 is automatically implied.
Formation temperature : 72.8 C / 1570 mRKB (135 DF)

PARAMETERS USED IN THE LOG EVALUATION

Parameters used in the log evaluation have been based on log readings cross-plots, histograms and experiences from adjacent wells.

FLUID

RW = 0.080 ohmm
RHOFL = 1.03 g/cc
SALINITY = 28470 ppm Cl-
NACL = 46700 ppm

MATRIX

RHOMA = 2.65 g/cc
PHINMA = -4 PU
DTMA = 55 microsec/ft

CLAY

RHOBSH = 2.36 g/cc
PHINSH = 37 PU
DTSH = 115 microsec/ft
RSH = 1.0 OHMM

EXPONENTS

a = 1.0
m = 1.9
n = 2.0

TH/K VALUES

	TH	K
MICA	24	9.5
FELDSPAR	11	14
SHALE	14	2.25

RESULTS

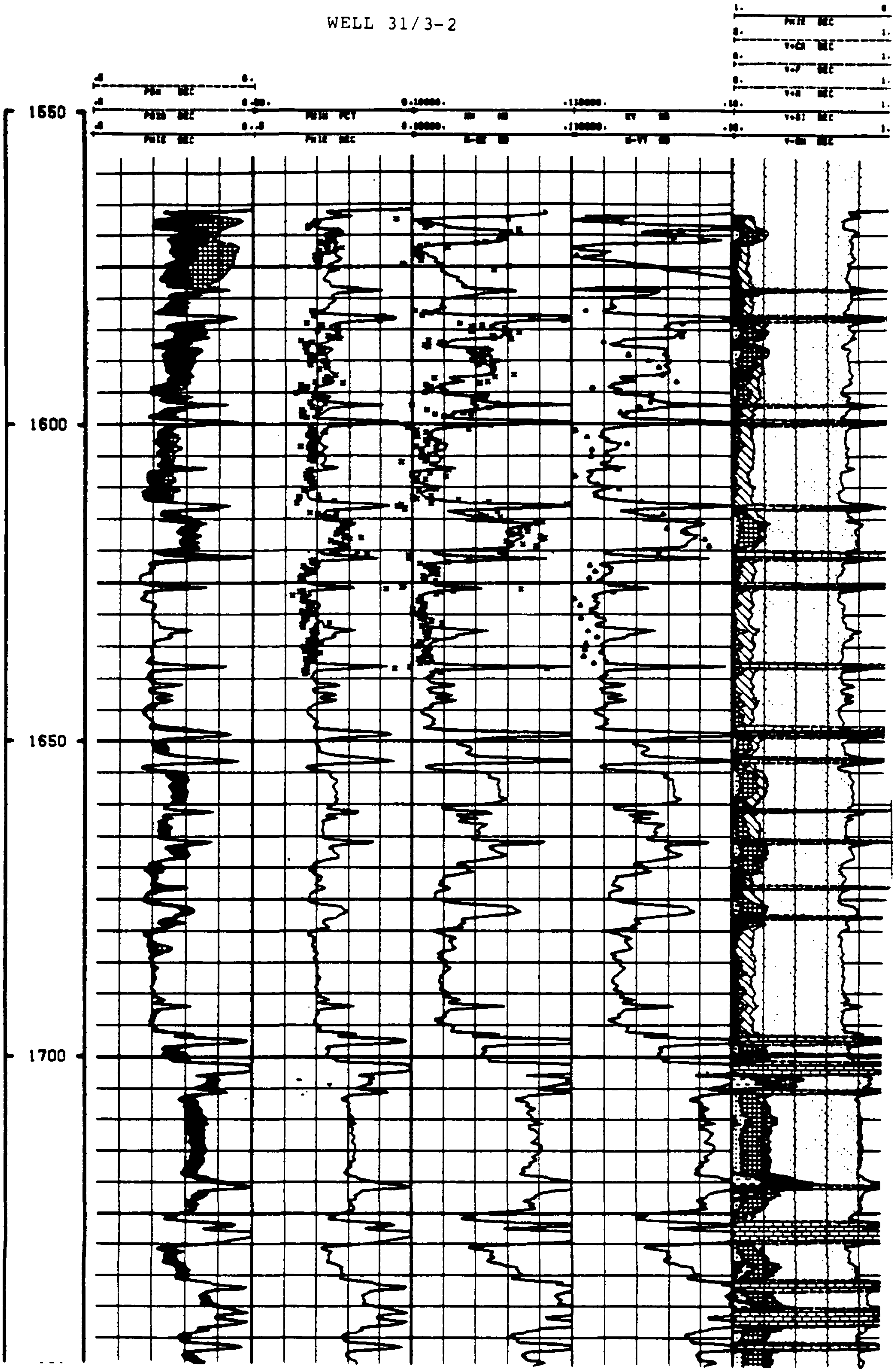
The evaluation results are presented for each geological zone.Porosity and water saturations were averaged arithmetically.Permeability was calculated as arithmetic-,geometric- and harmonic average.

CUT OFFS applied:

Porosity	<	0.12
VSH	>	0.40
SW	>	0.65

No overburden corrections on permeability is performed. Core porosity reduction for overburden effects is estimated to 0.96 based on data from nearby wells.

WELL 31/3-2



WELL 31/3-2
TROLL FIELD

NORSK HYDRO PETROPHYSICAL STUDY (AUG 1984)

NET SAND

	logs N/G alph	CORE DATA			LOG DATA			
ZONE		PHI	ARITH K-HZ	ARITH K-VT	PHI	S.W.	ARITH K-HZ	ARITH K-VT
1	-	-	-	-	-	-	-	-
2b	.95	29.6	2533.6	1416.1	26.5	67.9	1309.4	756.6
2a	1.00	22.1	4.1	3.8	21.6	84.3	70.5	29.5
3	.94	32.1	4933.3	3654.1	27.3	93.6	1137.0	454.2
4	.92	nd	nd	nd	18.6	81.9	2.6	1.1
5	.86	nd	nd	nd	21.4	91.7	241.4	92.1
KR-DR	.80	nd	nd	nd	23.8	97.2	739.2	335.1
2b hcarb	.98	27.6	3024.7	1728.8	25.0	35.3	1382.8	1325.5
2b water	.94	30.1	2407.5	1328.6	27.0	79.6	1275.4	535.4

NET PAY

	logs N/G alph	CORE DATA			LOG DATA			
ZONE		PHI	ARITH K-HZ	ARITH K-VT	PHI	S.W.	ARITH K-HZ	ARITH K-VT
1	-	-	-	-	-	-	-	-
2b	.26	28.0	2657.9	1533.9	25.4	33.1	1395.7	1344.4
2a	nd	nd	nd	nd	nd	nd	nd	nd
3	nd	nd	nd	nd	nd	nd	nd	nd
4	nd	nd	nd	nd	nd	nd	nd	nd
5	nd	nd	nd	nd	nd	nd	nd	nd
KR-DR	nd	nd	nd	nd	nd	nd	nd	nd
2b hcarb	.26	28.0	2657.9	1533.9	25.4	33.1	1395.7	1344.4
2b water	nd	nd	nd	nd	nd	nd	nd	nd

"nd" = "no data" : (1) data was not recorded in the interval or, (2) all data failed to pass discriminator cutoffs

"-" = zone was not present in this well

WELL 31/3-2
TROLL FIELD

NORSK HYDRO PETROPHYSICAL STUDY (AUG 1984)

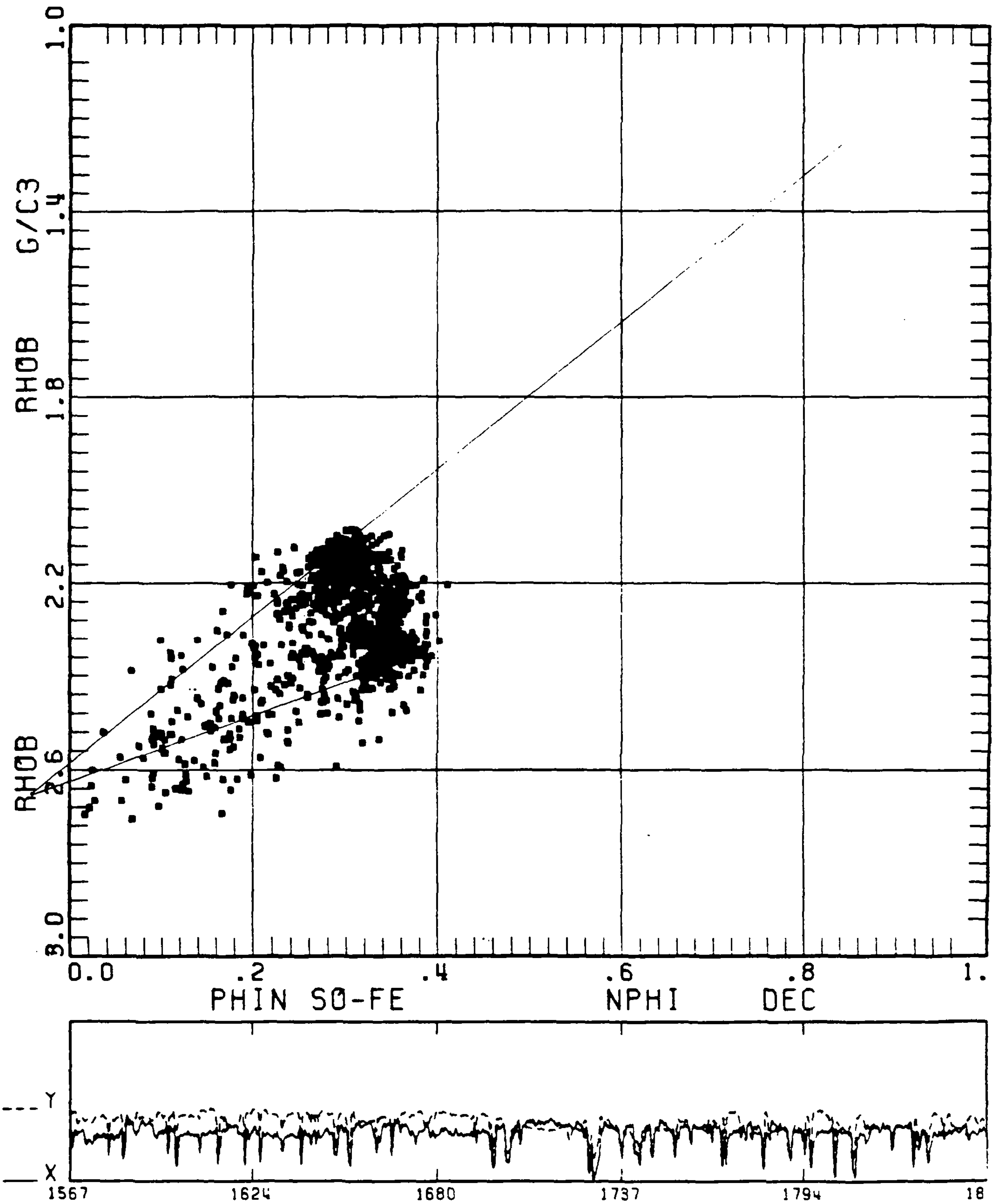
	logs N/G	NET SAND							
	alph	CORE DATA			LOG DATA				
ZONE		PHI	GEOM K-HZ	GEOM K-VT	PHI	S.W.	GEOM K-HZ	GEOMH K-VT	
1	-	-	-	-	-	-	-	-	
2b	.95	29.6	404.4	140.7	26.5	67.9	340.5	88.7	
2a	1.00	22.1	2.8	1.8	21.6	84.3	9.5	3.7	
3	.94	32.1	3257.8	2254.1	27.3	93.6	311.8	123.8	
4	.92	nd	nd	nd	18.6	81.9	1.6	0.7	
5	.86	nd	nd	nd	21.4	91.7	9.8	4.1	
KR-DR	.80	nd	nd	nd	23.8	97.2	138.2	64.5	
2b hcarb	.98	27.6	442.2	94.0	25.0	35.3	365.6	29.0	
2b water	.94	30.1	395.6	157.5	27.0	79.6	332.3	133.8	

	logs N/G	NET PAY						
	alph	CORE DATA			LOG DATA			
ZONE		PHI	GEOM K-HZ	GEOM K-VT	PHI	S.W.	GEOM K-HZ	GEOMH K-VT
1	-	-	-	-	-	-	-	-
2b	.26	28.0	357.8	101.3	25.4	33.1	353.8	25.3
2a	nd	nd	nd	nd	nd	nd	nd	nd
3	nd	nd	nd	nd	nd	nd	nd	nd
4	nd	nd	nd	nd	nd	nd	nd	nd
5	nd	nd	nd	nd	nd	nd	nd	nd
KR-DR	nd	nd	nd	nd	nd	nd	nd	nd
2b hcarb	.26	28.0	357.8	101.3	25.4	33.1	353.8	25.3
2b water	nd	nd	nd	nd	nd	nd	nd	nd

"nd" = "no data" : (1) data was not recorded in the interval or,
(2) all data failed to pass discriminator cutoffs

"-" = zone was not present in this well

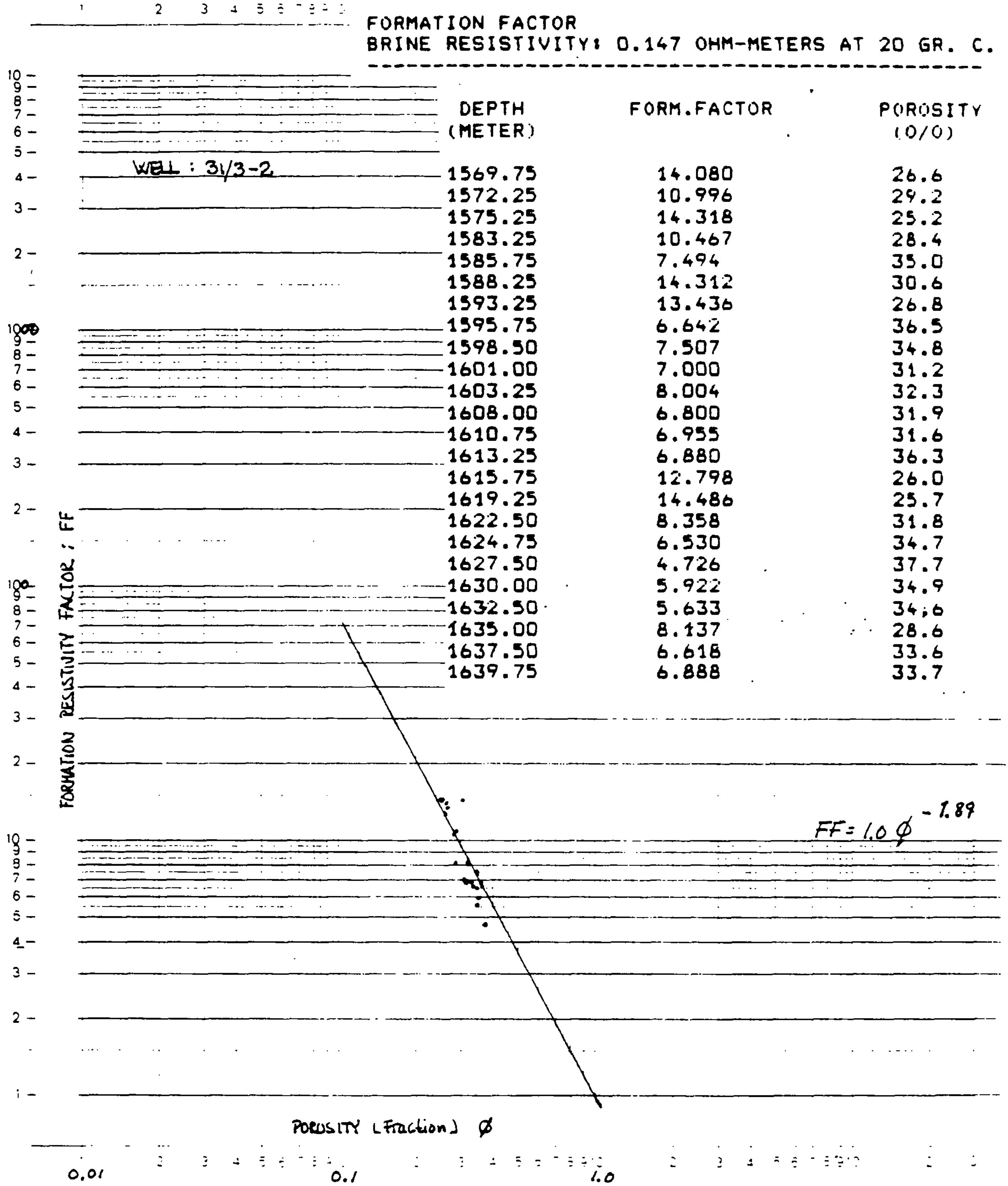
DENSITY/NEURTON CROSS PLOT
SOGN - FENS FM.(1567 - 1851 MRKB)



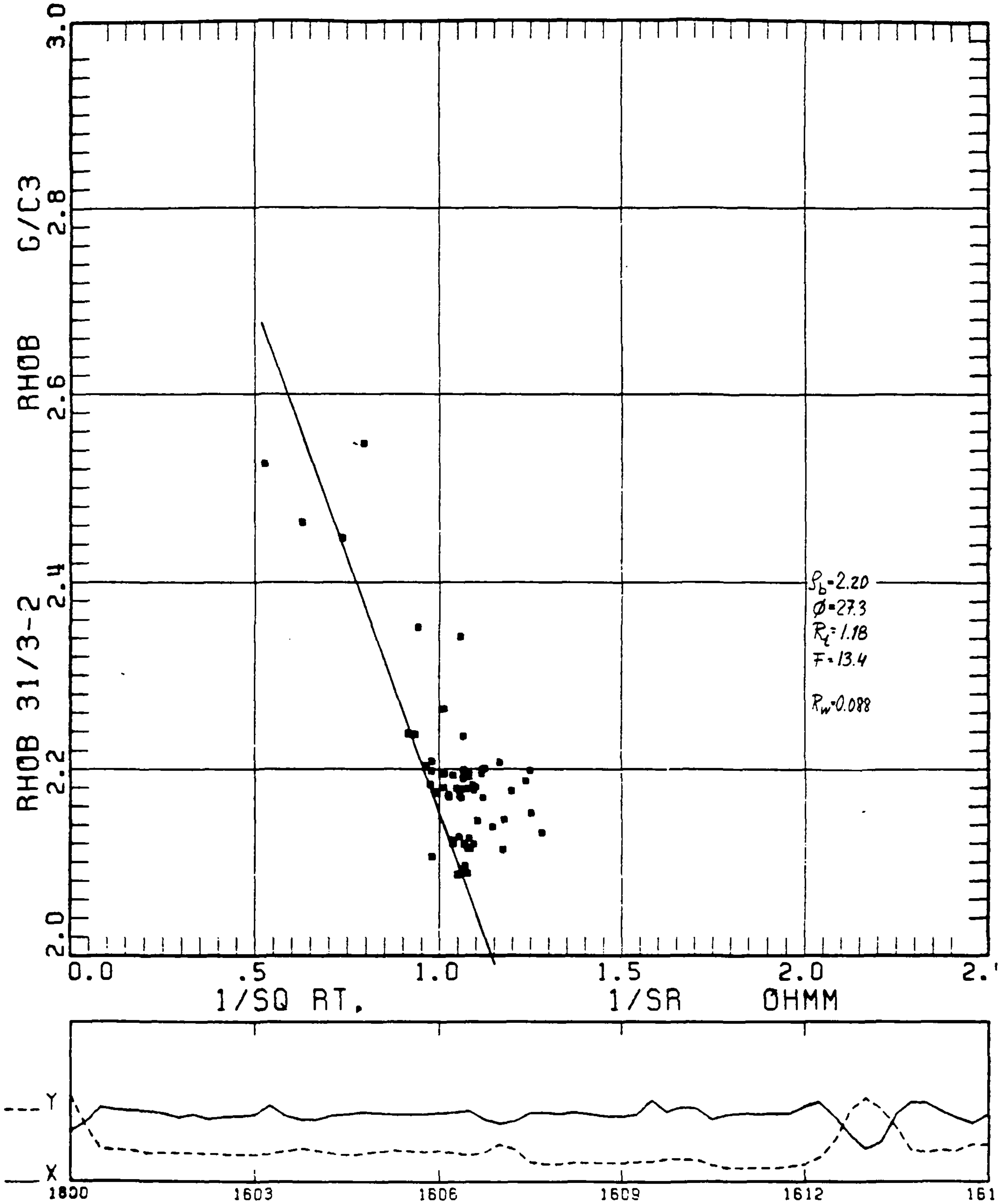
FORMATION RESISTIVITY FACTOR, FF
VS POROSITY (FRACTION) 31/3-2

FORMATION FACTOR
BRINE RESISTIVITY: 0.147 OHM-METERS AT 20 GR. C.

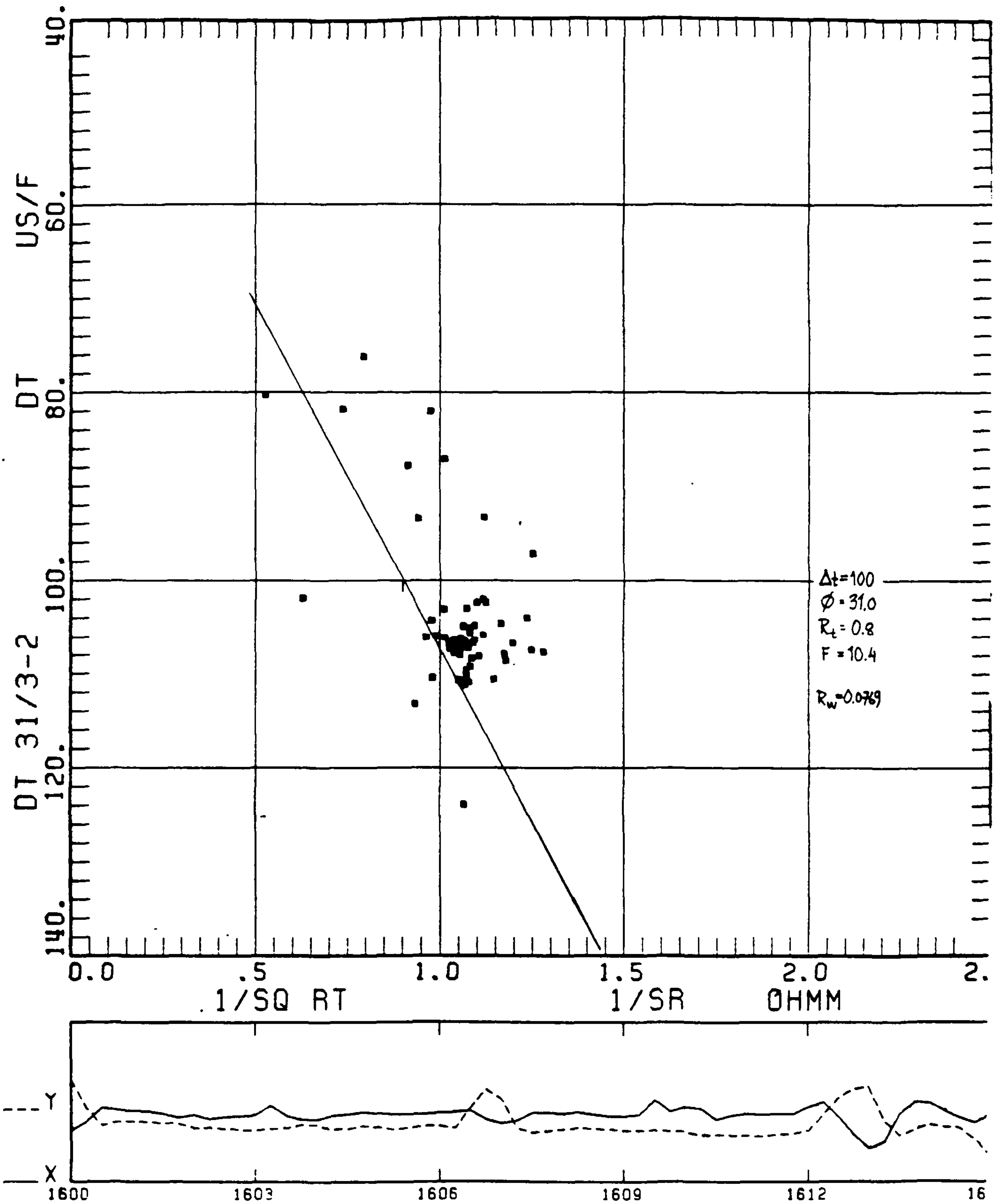
DEPTH (METER)	FORM.FACTOR	POROSITY (0/0)
1569.75	14.080	26.6
1572.25	10.996	29.2
1575.25	14.318	25.2
1583.25	10.467	28.4
1585.75	7.494	35.0
1588.25	14.312	30.6
1593.25	13.436	26.8
1595.75	6.642	36.5
1598.50	7.507	34.8
1601.00	7.000	31.2
1603.25	8.004	32.3
1608.00	6.800	31.9
1610.75	6.955	31.6
1613.25	6.880	36.3
1615.75	12.798	26.0
1619.25	14.486	25.7
1622.50	8.358	31.8
1624.75	6.530	34.7
1627.50	4.726	37.7
1630.00	5.922	34.9
1632.50	5.633	34.6
1635.00	8.137	28.6
1637.50	6.618	33.6
1639.75	6.888	33.7



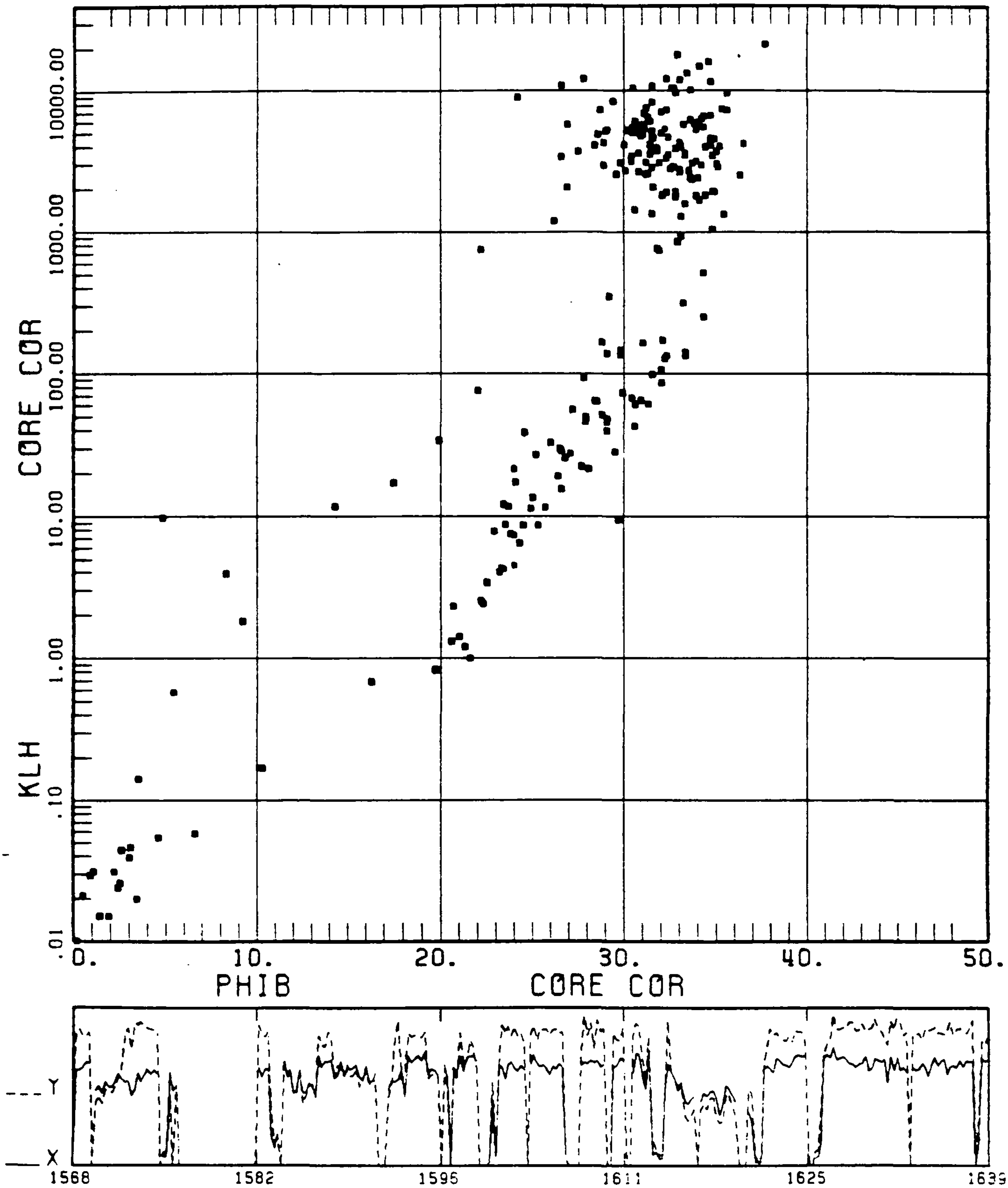
DENSITY VS $1/\sqrt{RT}$ (1600 -1615 MRKB)



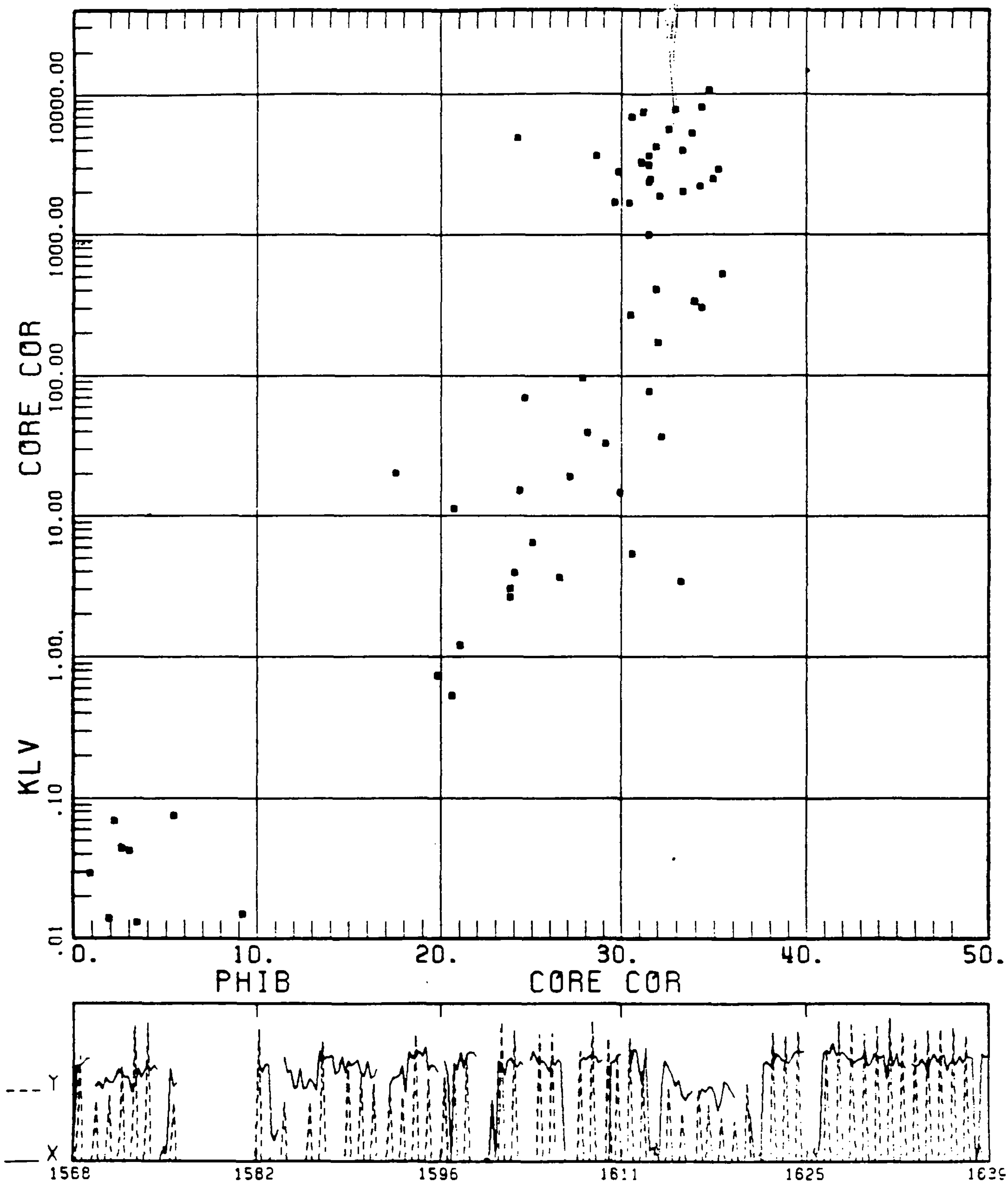
SONIC VS 1/√RT (1600 - 1615 MRKB)



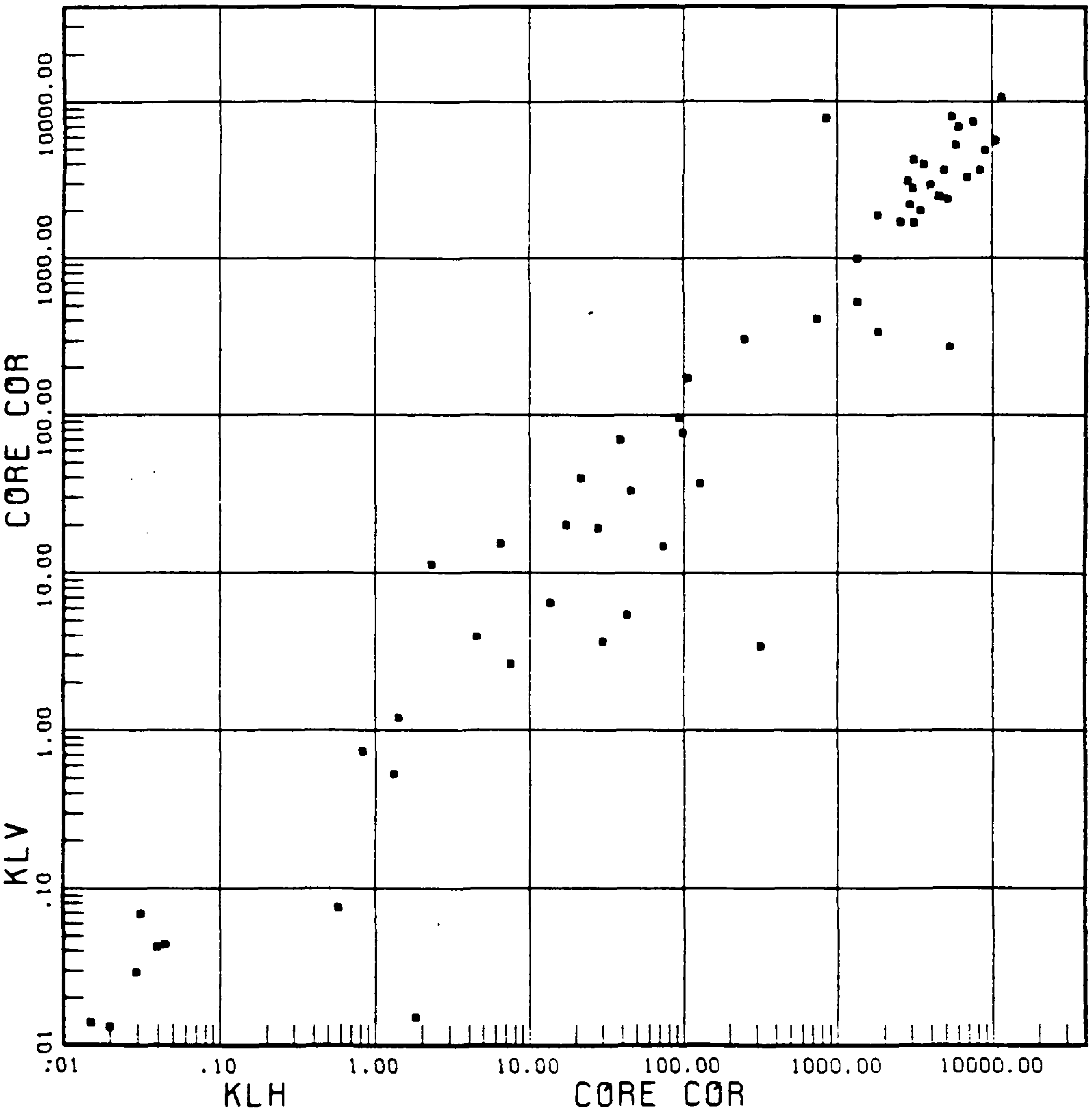
HORISONTAL PERMEABILITY VS POROSITY
DEPTH CORRECTED CORE DATA 31/3-2

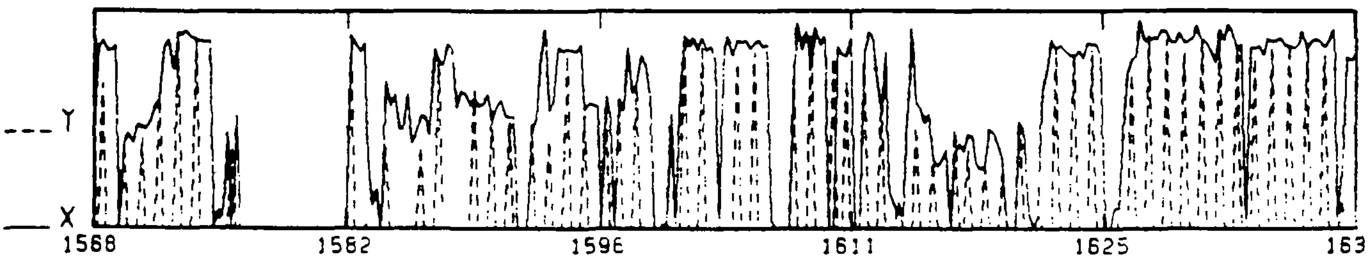


VERTICAL PERMEABILITY VS POROSITY
DEPTH CORRECTED CORE DATA 31/3-2

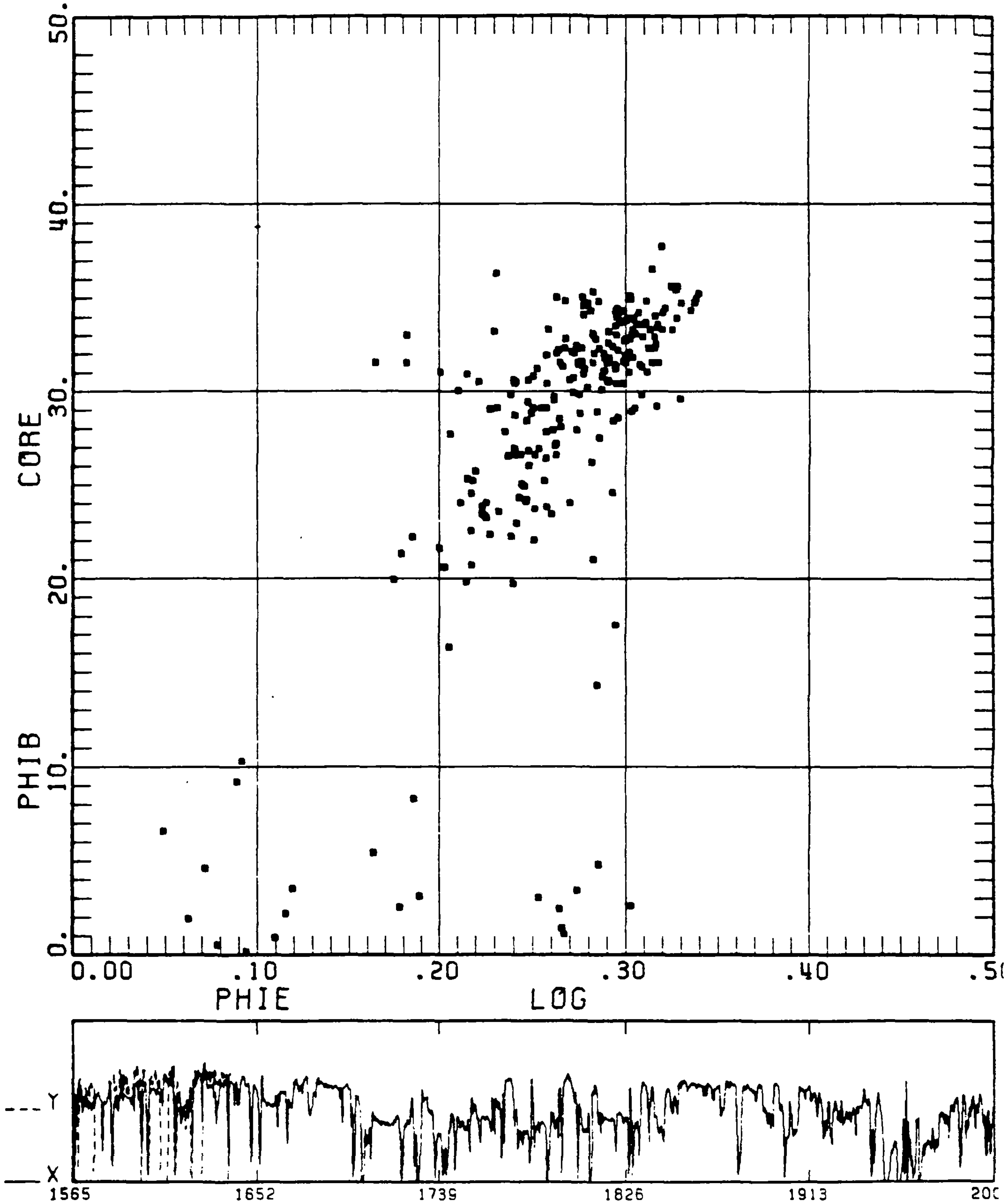


VERTICAL AND HORISONTAL CORE PERMEABILITY
31/3-2





CORE POROSITY VS LOG POROSITY
31/3-2



LISTING OF COMPUTED RESULTS
(1567 - 1850 MRKB)

FIELD = 312. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIE %	Sw %	VSH %	KLOGH MD
1567.0	19.0	50.1	1.1	4.2
1567.3	24.1	27.5	2.1	233.0
1567.5	28.2	12.2	2.0	4101.5
1567.8	29.4	10.1	2.0	8972.7
1568.0	29.0	14.3	2.1	3300.4
1568.3	29.4	16.6	2.1	1969.1
1568.5	30.0	22.0	2.4	1122.2
1568.8	30.0	26.3	2.9	725.5
1569.0	27.4	33.4	3.4	194.2
1569.3	22.5	41.9	4.9	22.6
1569.5	21.6	46.9	5.7	7.4
1569.8	22.6	47.8	6.1	6.8
1570.0	24.0	46.7	5.6	3.9
1570.3	24.4	44.3	5.1	10.1
1570.5	24.5	45.2	4.6	10.6
1570.8	25.7	43.7	4.1	12.1
1571.0	25.0	40.1	2.4	13.6
1571.3	23.5	32.9	2.0	63.4
1571.5	24.4	21.9	1.0	1339.5
1571.8	24.0	15.6	0.9	3356.9
1572.0	23.2	17.6	1.0	4396.1
1572.3	24.7	17.1	1.1	5440.3
1572.5	24.7	18.0	1.1	5659.8
1572.8	25.1	19.9	1.0	4408.7
1573.0	24.0	21.4	1.1	3316.9
1573.3	24.0	21.9	1.2	3118.6
1573.5	22.8	23.0	1.2	2500.5
1573.8	22.2	24.5	0.7	1745.5
1574.0	23.1	24.1	0.8	1692.3
1574.3	24.5	23.2	1.0	2017.9
1574.5	25.3	22.3	1.0	1319.5
1574.8	26.4	22.5	1.0	973.1
1575.0	26.1	24.3	0.7	1047.7
1575.3	25.7	25.6	0.7	1047.9
1575.5	25.6	27.2	0.7	1151.4
1575.8	26.3	28.4	1.0	1157.2
1576.0	25.7	29.4	1.1	623.7
1576.3	26.7	30.6	1.2	507.8
1576.5	27.2	31.5	1.4	563.6
1576.8	27.4	33.4	1.5	333.1
1577.0	23.0	35.8	1.3	343.2
1577.3	27.0	37.3	1.3	355.0
1577.5	26.2	43.2	1.3	287.4
1577.8	25.7	49.2	1.6	257.1
1578.0	25.7	34.0	1.7	234.6
1578.3	25.3	50.4	1.8	272.6
1578.5	17.6	56.0	2.1	134.5
1578.8	9.6	100.0	3.1	5.3
1579.0	15.9	99.3	3.6	5.5
1579.3	23.7	77.0	3.2	62.2

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1579.5	25.2	91.3	2.1	89.3
1579.8	25.1	91.5	1.9	193.2
1580.0	24.5	90.0	1.3	513.4
1580.3	24.2	94.0	1.0	1014.6
1580.5	24.3	90.4	1.4	1006.0
1580.8	25.4	75.1	1.9	1127.6
1581.0	25.9	89.0	2.1	1104.4
1581.3	26.3	76.9	1.6	1250.2
1581.5	26.3	73.6	1.7	872.6
1581.8	27.3	85.3	1.3	1227.7
1582.0	23.2	86.5	1.9	1965.4
1582.3	29.3	77.6	1.6	2358.0
1582.5	28.7	89.0	1.5	1615.5
1582.8	21.5	86.5	2.1	132.7
1583.0	8.9	100.0	3.2	0.1
1583.3	4.9	100.0	5.0	0.0
1583.5	9.1	100.0	5.9	0.0
1583.8	17.1	34.3	5.4	3.9
1584.0	23.0	75.1	5.1	25.6
1584.3	24.7	73.0	5.5	23.7
1584.5	25.7	72.8	4.6	36.0
1584.8	26.0	70.7	4.9	34.7
1585.0	25.1	67.6	5.6	20.8
1585.3	23.9	67.4	6.7	13.7
1585.5	22.8	69.5	6.2	7.7
1585.8	23.1	70.0	6.3	11.2
1586.0	23.7	70.5	4.9	15.9
1586.3	21.9	83.9	4.4	14.9
1586.5	24.1	96.3	2.3	116.0
1586.8	26.3	87.0	2.6	569.5
1587.0	26.4	81.3	2.1	655.0
1587.3	28.2	82.3	2.5	800.4
1587.5	30.4	93.6	3.3	1637.7
1587.8	29.7	73.1	5.3	683.3
1588.0	26.0	75.4	6.4	66.1
1588.3	24.9	65.7	6.9	27.3
1588.5	25.9	60.1	7.0	38.5
1588.8	26.4	61.9	7.1	37.4
1589.0	27.2	61.9	5.9	44.0
1589.3	26.9	65.0	5.6	29.4
1589.5	26.6	56.4	4.3	29.7
1589.8	26.7	59.1	4.4	34.3
1590.0	26.5	56.6	4.4	27.2
1590.3	25.2	65.0	4.3	24.0
1590.5	26.3	66.7	5.0	29.4
1590.8	26.2	70.6	4.6	38.6
1591.0	26.2	72.3	3.7	34.6
1591.3	25.1	74.1	3.9	29.5
1591.5	26.2	74.1	4.5	25.9
1591.8	25.7	78.2	3.0	25.2

FIELD = 313. WELL = 2. START = 1587.00 STOP = 2025.00

DEPTH M	PHIE %	SW %	VSH %	KLOGH MD
1592.0	25.2	76.7	3.7	30.7
1592.3	24.3	74.5	3.3	47.5
1592.5	24.7	72.7	3.0	224.3
1592.8	23.3	75.7	3.3	705.9
1593.0	25.7	73.7	3.0	445.0
1593.3	24.7	75.1	3.0	229.0
1593.5	25.0	75.5	2.8	391.2
1593.8	27.7	72.5	2.6	1283.9
1594.0	29.5	68.1	3.1	1574.0
1594.3	30.7	66.4	3.3	1900.0
1594.5	30.3	70.3	3.7	921.2
1594.8	30.6	74.3	4.0	773.5
1595.0	31.4	73.6	3.5	1323.0
1595.3	30.5	74.8	3.6	1130.3
1595.5	27.7	77.7	3.3	376.5
1595.8	25.7	84.0	3.6	95.8
1596.0	27.5	74.7	2.9	91.5
1596.3	23.0	79.9	2.6	32.5
1596.5	26.4	81.5	2.2	57.8
1596.8	20.6	84.0	2.3	15.9
1597.0	9.4	100.0	2.3	0.1
1597.3	16.4	100.0	2.5	3.1
1597.5	25.5	86.5	1.9	54.1
1597.8	26.7	87.7	1.5	68.2
1598.0	27.5	84.1	1.6	166.6
1598.3	28.1	83.2	1.8	534.9
1598.5	28.5	83.7	2.3	472.0
1598.8	31.1	78.4	1.4	745.9
1599.0	31.0	80.9	1.1	801.6
1599.3	27.9	85.0	1.2	392.0
1599.5	15.5	100.0	1.8	3.6
1599.8	4.5	100.0	2.2	0.0
1600.0	6.2	100.0	1.7	0.0
1600.3	17.5	100.0	1.4	16.0
1600.5	26.5	86.3	1.7	450.3
1600.8	27.1	91.4	1.3	1235.8
1601.0	27.8	93.6	1.5	1948.3
1601.3	28.6	85.0	1.4	2597.7
1601.5	28.3	92.4	1.4	2585.2
1601.8	28.2	79.1	1.4	2394.7
1602.0	28.0	91.2	1.3	3080.0
1602.3	29.7	76.1	1.6	1810.4
1602.5	28.9	73.6	1.9	1580.0
1602.8	29.0	79.0	1.7	1980.6
1603.0	29.1	79.7	1.9	1373.1
1603.3	23.6	92.1	2.0	737.4
1603.5	28.2	90.9	1.7	877.0
1603.8	28.0	80.2	1.3	834.0
1604.0	27.4	79.4	1.7	597.6
1604.3	28.3	81.4	1.5	1500.6

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH M	PHIE %	SW %	VSH %	KLOGH MD
1604.5	29.9	31.1	1.5	2163.9
1604.8	28.4	54.9	1.4	1926.3
1605.0	27.6	56.4	1.2	1521.9
1605.3	27.2	86.5	1.3	1123.2
1605.5	27.9	85.9	1.4	1277.4
1605.8	27.4	85.5	1.2	1346.7
1606.0	27.4	57.0	1.5	1376.7
1606.3	28.2	55.2	1.4	2711.4
1606.5	29.3	55.0	1.3	2709.2
1606.8	29.2	76.3	1.4	1434.0
1607.0	23.6	54.9	1.3	422.2
1607.3	25.7	52.3	1.1	1751.2
1607.5	30.5	77.9	0.9	7717.8
1607.8	31.6	76.6	0.7	5675.7
1608.0	31.7	75.8	0.7	5512.4
1608.3	31.6	77.4	0.5	6123.2
1608.5	31.7	75.1	0.8	7694.9
1608.8	31.8	72.6	1.1	6589.3
1609.0	31.6	73.1	0.9	7010.7
1609.3	31.3	74.8	0.9	6848.8
1609.5	30.9	92.2	1.0	4490.3
1609.8	30.7	79.7	1.1	3174.6
1610.0	29.8	87.0	2.0	1242.5
1610.3	30.1	84.0	1.5	1575.6
1610.5	32.0	67.9	1.3	3503.8
1610.8	33.2	70.3	1.5	4342.8
1611.0	33.1	72.5	1.4	5469.6
1611.3	33.0	72.0	1.3	4689.5
1611.5	32.8	72.3	1.1	3825.7
1611.8	32.5	73.6	0.8	3693.1
1612.0	31.7	82.6	0.5	1623.9
1612.3	29.3	95.1	0.7	624.0
1612.5	23.1	95.9	1.0	151.9
1612.8	11.9	100.0	1.1	1.7
1613.0	7.2	100.0	1.4	0.7
1613.3	11.5	100.0	1.6	1.5
1613.5	17.6	100.0	1.9	68.4
1613.8	27.0	100.0	1.9	745.1
1614.0	27.6	97.7	2.3	351.6
1614.3	27.2	89.6	2.4	227.3
1614.5	27.4	90.6	2.6	173.0
1614.8	24.6	81.3	3.2	51.0
1615.0	24.9	91.5	4.1	60.3
1615.3	28.2	83.7	4.7	139.8
1615.5	23.9	88.4	5.1	24.2
1615.8	17.9	80.5	6.1	1.6
1616.0	17.5	91.7	4.9	2.0
1616.3	20.1	84.3	5.0	3.8
1616.5	21.8	82.5	5.0	7.3
1616.8	22.3	92.7	5.2	9.8

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIE %	SW %	VSH %	KLOGH MD
1617.0	22.7	81.4	5.0	11.1
1617.3	22.4	84.3	4.6	10.8
1617.5	21.2	84.4	4.6	5.8
1617.8	20.0	84.5	5.0	3.1
1618.0	20.5	81.1	4.4	3.5
1618.3	21.5	82.3	4.2	4.9
1618.5	22.0	83.0	3.7	5.8
1618.8	21.9	85.8	3.0	6.3
1619.0	21.7	82.3	3.4	7.0
1619.3	20.2	84.9	2.4	6.4
1619.5	19.6	94.3	1.7	10.3
1619.8	23.3	96.3	1.2	102.5
1620.0	28.0	78.5	0.5	997.7
1620.3	29.5	69.9	0.9	2253.3
1620.5	23.5	59.7	1.1	2013.6
1620.8	26.7	47.5	1.6	1109.1
1621.0	18.4	58.6	2.4	50.7
1621.3	10.9	100.0	3.0	0.6
1621.5	20.1	94.9	2.1	30.4
1621.8	29.1	76.3	1.9	465.1
1622.0	31.1	86.2	1.4	1926.3
1622.3	30.3	93.7	1.7	3377.0
1622.5	29.5	100.0	1.9	1853.7
1622.8	29.5	100.0	1.4	1282.2
1623.0	31.2	100.0	1.8	1857.5
1623.3	30.2	100.0	2.1	1454.1
1623.5	30.8	100.0	1.9	1563.3
1623.8	32.5	100.0	1.7	1967.4
1624.0	33.7	100.0	1.5	3056.1
1624.3	34.0	100.0	1.7	3267.4
1624.5	33.7	100.0	1.3	3309.1
1624.8	33.8	100.0	1.4	4614.9
1625.0	33.1	99.0	1.2	2983.8
1625.3	33.0	91.5	1.4	2280.1
1625.5	30.3	94.0	1.5	1827.9
1625.8	18.9	100.0	2.2	94.3
1626.0	18.5	100.0	2.6	66.4
1626.3	29.4	95.5	2.1	973.2
1626.5	32.7	93.9	1.5	2158.5
1626.8	32.1	100.0	1.6	3383.7
1627.0	31.9	100.0	1.2	5230.4
1627.3	32.8	100.0	1.0	5592.7
1627.5	33.5	98.7	1.6	4332.9
1627.8	33.0	98.0	1.2	5159.3
1628.0	31.1	99.7	1.2	4790.7
1628.3	29.9	100.0	1.2	5249.4
1628.5	29.1	100.0	1.6	3474.0
1628.8	28.9	100.0	1.3	4111.3
1629.0	28.3	100.0	0.9	3460.1
1629.3	30.2	100.0	0.7	6147.9

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

* DEPTH *	PHIE %	SW %	VSH % *	KLOGH MD *
1629.5	30.2	100.0	0.9	5921.2
1629.8	29.9	100.0	1.1	3735.0
1630.0	29.5	100.0	1.1	3324.9
1630.3	29.6	100.0	1.0	4178.0
1630.5	30.0	100.0	1.0	3699.4
1630.8	30.3	100.0	1.0	2240.9
1631.0	29.5	100.0	0.7	2108.1
1631.3	29.2	100.0	0.9	2358.3
1631.5	27.9	100.0	0.9	3577.8
1631.8	27.9	100.0	1.0	3676.6
1632.0	27.7	99.9	1.1	2537.8
1632.3	24.1	100.0	1.6	612.1
1632.5	13.1	100.0	2.6	40.9
1632.8	21.1	100.0	2.3	76.4
1633.0	24.6	100.0	1.6	181.3
1633.3	25.2	100.0	1.4	431.3
1633.5	24.0	100.0	1.2	372.6
1633.8	25.0	100.0	1.2	505.3
1634.0	28.4	100.0	1.6	1677.5
1634.3	29.4	100.0	1.5	1952.1
1634.5	29.5	100.0	1.8	2494.3
1634.8	29.5	100.0	1.9	2955.3
1635.0	29.9	100.0	2.0	2626.4
1635.3	30.4	100.0	1.9	2482.1
1635.5	30.4	100.0	1.4	2368.6
1635.8	30.4	100.0	1.0	3053.3
1636.0	30.2	100.0	1.2	3323.3
1636.3	30.0	100.0	1.4	2592.9
1636.5	30.0	100.0	1.5	2233.8
1636.8	30.2	100.0	1.4	2267.8
1637.0	30.9	100.0	1.1	2707.4
1637.3	31.4	100.0	1.2	1965.7
1637.5	32.0	90.3	1.5	2390.7
1637.8	29.0	83.9	1.7	1710.7
1638.0	18.2	100.0	1.3	76.5
1639.3	7.3	100.0	2.4	0.1
1638.5	16.3	100.0	2.5	25.8
1638.8	27.7	90.6	2.4	1074.5
1639.0	30.5	97.0	1.7	2130.4
1639.3	31.1	100.0	2.0	2122.4
1639.5	31.1	100.0	1.2	1945.6
1639.8	31.6	100.0	1.4	3213.6
1640.0	31.5	99.3	1.2	3573.7
1640.3	30.7	100.0	1.1	3031.9
1640.5	30.7	96.2	1.0	2730.4
1640.8	30.2	93.4	1.2	2211.6
1641.0	24.1	100.0	1.2	451.6
1641.3	23.3	100.0	1.3	457.2
1641.5	26.9	100.0	1.1	2196.1
1641.8	31.1	95.6	1.1	3295.1

FIELD = 313. WELL = 2. START = 1557.00 STOP = 2025.00

DEPTH	PHIF %	Sw %	VSH %	KLOGH MD
1642.0	31.2	95.5	1.2	2673.4
1642.3	30.5	99.3	1.3	2900.7
1642.5	24.9	100.0	1.7	759.3
1642.8	23.6	100.0	1.5	522.4
1643.0	29.0	100.0	1.5	1785.4
1643.3	28.6	100.0	1.8	1583.5
1643.5	23.9	100.0	1.9	405.6
1643.8	25.5	100.0	2.4	578.8
1644.0	30.0	96.0	2.3	2324.9
1644.3	31.1	92.1	2.5	2526.4
1644.5	31.6	91.5	1.9	2142.9
1644.8	32.4	92.2	1.5	3646.7
1645.0	32.9	95.5	1.9	4653.2
1645.3	32.8	98.9	1.3	4589.9
1645.5	32.3	100.0	1.4	4934.7
1645.8	32.3	100.0	1.9	3452.4
1646.0	31.6	100.0	2.0	2603.2
1646.3	31.1	100.0	1.9	2210.1
1646.5	30.9	100.0	1.9	1319.1
1646.8	29.7	100.0	1.5	2211.0
1647.0	29.7	100.0	1.4	2246.3
1647.3	30.4	95.7	1.4	1885.5
1647.5	30.6	87.9	1.7	2536.6
1647.8	30.7	80.2	2.0	3536.7
1648.0	30.8	66.3	2.1	4372.8
1648.3	25.4	66.3	2.9	866.2
1648.5	13.9	91.7	3.9	4.5
1648.8	7.9	100.0	3.6	0.1
1649.0	6.4	100.0	3.2	0.0
1649.3	9.3	100.0	4.9	0.1
1649.5	19.6	94.9	3.7	12.0
1649.8	27.0	84.7	3.6	99.0
1650.0	28.4	93.1	3.4	141.9
1650.3	29.7	94.0	3.3	292.4
1650.5	30.5	93.2	3.0	307.1
1650.8	29.9	94.5	3.4	245.1
1651.0	29.1	96.1	3.4	144.7
1651.3	29.0	95.3	2.7	126.0
1651.5	29.0	93.9	2.3	[illegible]
1651.8	28.6	92.5	2.0	186.3
1652.0	27.9	90.9	1.7	196.1
1652.3	25.1	92.0	1.6	135.4
1652.5	21.1	93.7	2.0	67.1
1652.8	14.9	100.0	2.2	6.4
1653.0	9.1	100.0	1.9	0.1
1653.3	5.6	100.0	1.5	0.0
1653.5	12.6	100.0	1.7	3.9
1653.8	27.3	100.0	1.3	1395.8
1654.0	32.3	97.8	2.3	3613.3
1654.3	33.2	100.0	2.3	3284.2

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1654.5	31.6	100.0	2.3	1860.2
1654.8	26.6	100.0	3.5	213.5
1655.0	25.2	95.9	4.2	53.6
1655.3	26.0	90.9	4.5	38.0
1655.5	25.7	76.7	4.7	34.0
1655.8	25.5	75.0	5.5	39.3
1656.0	24.5	79.4	5.5	22.8
1656.3	23.7	81.7	5.0	17.7
1656.5	23.6	82.7	4.9	18.4
1656.8	24.3	81.4	5.7	19.3
1657.0	24.7	81.5	5.6	19.5
1657.3	24.9	81.9	5.7	19.0
1657.5	24.5	82.5	4.9	18.3
1657.8	24.2	82.6	5.1	16.7
1658.0	24.0	81.3	5.5	17.0
1658.3	23.5	83.5	4.7	17.9
1658.5	23.6	82.9	4.6	15.0
1658.8	24.2	81.1	4.2	13.3
1659.0	24.2	81.5	3.3	15.7
1659.3	23.3	85.4	2.1	10.7
1659.5	23.6	86.2	2.9	14.4
1659.8	24.2	92.5	2.9	18.9
1660.0	24.0	100.0	1.9	36.3
1660.3	25.4	100.0	2.5	353.9
1660.5	26.6	97.6	2.0	1054.4
1660.8	26.5	96.3	1.6	1027.5
1661.0	24.0	100.0	2.1	621.1
1661.3	16.9	100.0	1.8	43.7
1661.5	17.6	100.0	2.2	30.2
1661.8	26.3	95.2	1.7	377.5
1662.0	27.1	96.9	1.7	292.3
1662.3	23.7	100.0	1.9	30.9
1662.5	26.4	100.0	2.4	251.9
1662.8	28.1	90.4	2.7	335.4
1663.0	27.9	91.9	3.0	126.3
1663.3	27.8	92.6	3.1	42.3
1663.5	27.9	89.0	3.2	52.2
1663.8	28.0	87.1	3.4	71.2
1664.0	28.0	87.1	3.6	76.2
1664.3	28.2	87.3	3.3	82.3
1664.5	27.6	91.7	3.3	67.3
1664.8	27.6	94.5	3.4	78.4
1665.0	28.0	95.7	3.3	77.6
1665.3	28.4	89.1	3.4	91.4
1665.5	27.5	85.0	3.0	132.5
1665.8	21.1	100.0	3.0	54.4
1666.0	12.1	100.0	4.4	0.7
1666.3	14.0	100.0	5.3	1.0
1666.5	21.8	93.6	5.2	18.4
1666.8	25.7	75.3	5.3	35.6

FIELD = 313. WELL = 2. START = 1667.00 STOP = 2025.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1667.0	25.9	79.6	5.4	34.9
1667.3	24.3	82.0	6.2	26.7
1667.5	24.6	79.0	6.5	21.4
1667.8	24.1	76.3	6.8	16.0
1668.0	23.4	81.7	5.2	10.4
1668.3	23.1	99.8	3.9	13.5
1668.5	23.2	96.6	8.8	27.5
1668.8	25.9	99.2	4.9	49.1
1669.0	28.1	97.1	4.7	110.1
1669.3	29.7	94.8	4.2	316.7
1669.5	30.9	90.4	4.9	371.7
1669.8	30.5	86.5	5.0	184.9
1670.0	30.9	85.7	4.3	163.7
1670.3	32.0	81.3	4.2	191.0
1670.5	32.1	83.3	3.7	150.6
1670.8	30.7	86.5	3.8	113.1
1671.0	30.8	92.7	2.0	262.1
1671.3	29.6	97.9	1.7	528.7
1671.5	28.2	100.0	1.3	994.9
1671.8	29.3	100.0	1.8	950.3
1672.0	28.9	100.0	1.7	1045.4
1672.3	29.7	100.0	2.0	1254.1
1672.5	30.1	96.0	1.9	1267.2
1672.8	30.2	98.8	1.9	1378.0
1673.0	29.7	89.0	1.9	880.7
1673.3	27.3	92.3	1.6	607.1
1673.5	27.7	92.3	1.6	646.6
1673.8	30.2	99.8	1.7	1382.7
1674.0	31.3	93.7	1.9	1879.3
1674.3	31.8	100.0	1.5	1826.3
1674.5	32.1	100.0	2.4	1806.7
1674.8	32.1	100.0	2.8	1984.0
1675.0	32.6	100.0	3.5	1509.6
1675.3	32.7	96.6	3.3	1084.7
1675.5	32.0	92.8	4.1	768.2
1675.8	30.1	97.7	4.9	227.8
1676.0	23.9	88.2	5.3	33.3
1676.3	22.6	95.3	6.4	7.5
1676.5	21.6	91.9	5.6	5.5
1676.8	21.1	91.7	5.6	5.1
1677.0	20.5	94.9	5.5	3.9
1677.3	21.6	96.2	5.3	7.0
1677.5	22.9	91.2	4.7	17.9
1677.8	23.4	97.7	5.0	49.4
1678.0	25.9	97.9	4.9	141.8
1678.3	26.2	87.9	4.7	265.1
1678.5	27.8	92.6	4.4	264.1
1678.8	27.9	93.1	4.9	202.6
1679.0	27.2	83.4	9.9	260.6
1679.3	26.7	97.0	5.3	345.0

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2023.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1679.5	25.9	95.2	2.7	229.8
1679.8	27.8	93.1	2.1	671.0
1680.0	30.4	95.2	1.5	1973.7
1680.3	31.9	93.3	1.3	1583.0
1680.5	32.5	92.6	2.0	1043.0
1680.8	32.3	96.5	1.6	905.0
1681.0	30.9	100.0	1.5	547.1
1681.3	30.3	100.0	1.5	405.1
1681.5	31.0	100.0	1.5	639.5
1681.8	30.9	96.5	1.5	639.8
1682.0	30.9	91.7	1.5	548.8
1682.3	31.4	86.4	1.4	529.5
1682.5	31.1	80.9	1.4	491.0
1682.8	30.7	75.1	1.1	402.1
1683.0	30.7	79.5	0.9	540.5
1683.3	30.7	80.6	1.2	907.3
1683.5	29.7	87.6	1.3	1363.3
1683.8	29.4	93.5	1.1	1505.7
1684.0	30.2	95.6	1.6	1097.0
1684.3	30.9	97.6	2.0	1418.0
1684.5	30.7	100.0	2.1	1345.9
1684.8	30.1	100.0	2.2	809.2
1685.0	29.2	100.0	1.3	735.5
1685.3	29.6	100.0	1.7	898.0
1685.5	30.2	99.2	2.1	835.8
1685.8	29.6	99.0	2.1	685.9
1686.0	29.1	100.0	1.7	592.3
1686.3	29.6	99.2	1.9	705.0
1686.5	29.8	99.4	2.4	876.2
1686.8	29.7	98.4	2.5	904.0
1687.0	29.9	97.9	1.6	1054.1
1687.3	29.5	99.4	1.6	1211.3
1687.5	28.3	100.0	1.5	1231.5
1687.8	29.0	100.0	1.1	1349.0
1688.0	29.3	100.0	1.2	1253.7
1688.3	29.4	100.0	1.3	1327.3
1688.5	29.5	100.0	1.4	1091.6
1688.8	30.1	100.0	1.6	995.2
1689.0	30.1	100.0	1.6	1006.4
1689.3	30.1	99.1	2.0	1322.4
1689.5	29.5	98.3	2.4	1004.4
1689.8	29.4	98.9	2.2	657.6
1690.0	29.1	99.6	2.4	627.5
1690.3	29.7	100.0	2.0	691.7
1690.5	29.2	99.4	1.3	873.5
1690.8	27.4	100.0	1.7	471.1
1691.0	25.9	100.0	1.7	290.3
1691.3	28.0	100.0	1.5	609.8
1691.5	29.4	95.8	2.0	709.2
1691.8	25.3	100.0	2.3	193.9

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1692.0	18.3	100.0	2.5	12.9
1692.3	22.5	100.0	2.4	64.3
1692.5	28.2	96.2	1.9	524.8
1692.8	29.3	92.9	1.8	697.2
1693.0	29.3	94.9	1.6	683.4
1693.3	29.3	97.5	1.2	942.8
1693.5	29.9	96.5	1.2	855.4
1693.8	30.1	96.4	1.3	837.9
1694.0	30.0	95.2	1.5	1505.4
1694.3	30.5	97.6	2.1	1877.2
1694.5	30.7	97.4	2.0	1342.4
1694.8	30.0	99.7	1.7	920.7
1695.0	29.5	100.0	1.5	617.4
1695.3	28.9	100.0	1.7	456.9
1695.5	28.5	100.0	1.7	470.8
1695.8	29.1	95.1	1.5	507.0
1696.0	28.8	99.3	1.9	565.6
1696.3	22.9	100.0	2.4	173.3
1696.5	17.3	100.0	2.9	17.0
1696.8	23.2	79.7	3.7	120.8
1697.0	18.6	80.8	4.0	22.7
1697.3	4.6	100.0	4.7	0.0
1697.5	1.5	100.0	5.8	0.0
1697.8	3.1	100.0	5.2	0.0
1698.0	9.7	100.0	6.0	0.0
1698.3	20.0	87.0	5.2	9.1
1698.5	26.4	76.2	5.5	53.2
1698.8	26.8	84.2	5.3	56.6
1699.0	25.8	88.2	5.6	44.9
1699.3	25.9	84.8	6.2	44.2
1699.5	26.4	79.3	8.4	62.1
1699.8	26.9	78.7	5.3	55.8
1700.0	26.3	80.6	4.8	49.0
1700.3	24.4	80.0	12.8	40.2
1700.5	24.0	77.6	12.5	36.0
1700.8	23.8	77.5	6.8	35.2
1701.0	15.4	100.0	5.6	2.6
1701.3	2.3	100.0	11.4	0.0
1701.5	0.0	100.0	16.8	-9999.0
1701.8	0.3	100.0	17.0	0.0
1702.0	0.2	100.0	12.5	0.0
1702.3	1.1	100.0	9.9	0.0
1702.5	3.2	100.0	15.0	0.0
1702.8	10.8	90.9	15.7	0.1
1703.0	16.7	74.3	13.9	2.5
1703.3	13.1	85.3	24.7	0.3
1703.5	11.5	86.2	34.7	0.1
1703.8	13.4	80.4	36.9	0.2
1704.0	13.4	94.5	25.1	0.1
1704.3	12.2	96.7	27.8	0.1

FIELD = 313. WELL = 2. START = 1557.00 STOP = 2025.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1704.5	14.5	79.7	33.7	0.3
1704.8	15.4	70.4	36.2	0.4
1705.0	17.1	69.9	24.5	0.9
1705.3	15.8	65.5	6.4	1.0
1705.5	9.1	100.0	3.5	0.0
1705.8	7.3	100.0	5.0	0.0
1706.0	14.7	93.3	6.9	0.6
1706.3	19.6	80.3	6.4	2.2
1706.5	20.7	63.5	5.1	2.8
1706.8	21.9	81.3	4.7	5.5
1707.0	21.4	82.7	4.8	5.2
1707.3	19.9	66.7	5.3	2.7
1707.5	19.4	86.1	5.5	2.0
1707.8	20.0	80.6	6.4	2.7
1708.0	20.4	77.7	7.1	2.2
1708.3	19.5	80.1	6.9	1.3
1708.5	19.3	79.8	7.5	1.5
1708.8	19.7	78.2	7.1	2.2
1709.0	19.6	77.3	7.4	2.3
1709.3	19.5	76.8	7.7	1.8
1709.5	19.2	77.2	8.0	1.7
1709.8	18.3	76.6	11.5	1.5
1710.0	19.9	74.7	10.8	2.1
1710.3	19.4	74.5	12.4	1.5
1710.5	18.6	77.5	8.5	1.2
1710.8	17.4	76.8	13.6	0.7
1711.0	18.9	75.6	9.3	2.1
1711.3	19.7	76.5	9.3	2.1
1711.5	19.7	77.8	7.3	2.0
1711.8	18.4	78.7	7.7	1.3
1712.0	18.6	78.1	7.2	1.2
1712.3	18.8	77.6	6.5	1.0
1712.5	18.4	75.8	6.0	1.0
1712.8	18.0	80.3	6.0	1.1
1713.0	17.9	80.9	5.5	1.2
1713.3	18.2	79.6	5.4	1.3
1713.5	18.6	77.3	6.5	1.5
1713.8	18.6	77.8	6.1	1.7
1714.0	17.9	80.5	5.7	1.0
1714.3	17.6	81.2	6.4	0.9
1714.5	17.6	81.0	6.1	0.8
1714.8	17.5	80.5	7.2	0.9
1715.0	17.5	80.8	6.7	0.9
1715.3	17.9	80.5	6.3	0.9
1715.5	17.9	80.9	5.5	1.1
1715.8	18.1	80.2	5.2	1.2
1716.0	18.4	75.9	6.7	1.7
1716.3	18.1	79.8	6.7	1.5
1716.5	17.8	80.4	5.9	1.2
1716.8	18.6	77.4	7.3	1.6

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1717.0	19.3	75.3	7.4	2.1
1717.3	12.8	79.1	6.7	1.9
1717.5	18.8	81.2	6.9	2.0
1717.8	19.7	81.2	7.2	2.9
1718.0	20.3	82.2	6.9	3.6
1718.3	20.1	84.2	7.9	2.7
1718.5	21.0	84.9	5.6	3.5
1718.8	20.7	81.5	11.1	3.8
1719.0	19.8	79.1	17.0	2.5
1719.3	17.3	77.1	27.7	0.6
1719.5	16.7	77.1	26.0	0.5
1719.8	14.5	72.6	32.5	0.2
1720.0	12.1	67.7	40.7	0.0
1720.3	8.4	67.0	48.6	0.0
1720.5	4.2	73.0	56.0	0.0
1720.8	0.7	100.0	61.3	0.0
1721.0	2.0	87.3	53.2	0.0
1721.3	11.8	85.7	19.3	0.0
1721.5	15.9	83.8	10.1	0.4
1721.8	15.9	81.2	16.1	0.7
1722.0	16.9	79.6	17.2	1.1
1722.3	18.1	81.2	14.1	1.4
1722.5	17.1	59.7	12.5	1.3
1722.8	17.4	93.4	9.4	1.8
1723.0	19.4	88.9	6.4	3.1
1723.3	19.3	89.3	6.1	1.9
1723.5	18.8	89.3	6.4	1.5
1723.8	19.1	86.3	5.5	2.2
1724.0	18.1	91.4	4.5	1.5
1724.3	17.9	97.8	4.6	1.4
1724.5	18.4	100.0	4.2	2.6
1724.8	19.2	100.0	3.0	9.3
1725.0	21.9	100.0	2.0	53.9
1725.3	23.6	100.0	1.3	124.1
1725.5	24.1	100.0	2.2	104.2
1725.8	26.2	99.2	1.5	261.7
1726.0	25.8	88.4	1.6	245.9
1726.3	20.1	96.9	1.6	47.8
1726.5	13.2	100.0	1.1	3.9
1726.8	6.8	100.0	1.1	0.0
1727.0	5.2	100.0	1.6	0.0
1727.3	9.0	100.0	1.7	0.4
1727.5	14.6	76.4	1.4	13.3
1727.8	10.7	93.3	1.5	1.3
1728.0	0.5	100.0	1.5	0.0
1728.3	0.0	100.0	1.5	-9999.0
1728.5	0.0	100.0	1.5	-9999.0
1728.8	0.0	100.0	1.3	-9999.0
1729.0	1.7	100.0	1.4	0.0
1729.3	4.6	100.0	1.6	0.0

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIE %	Sw %	VSH %	KLOGH MD
1729.5	7.4	100.0	2.2	0.0
1729.8	9.7	100.0	2.4	0.2
1730.0	12.7	100.0	3.2	1.3
1730.3	21.3	96.6	4.0	39.5
1730.5	27.8	98.0	4.1	162.7
1730.8	29.6	90.2	3.8	131.9
1731.0	26.8	93.4	4.1	50.1
1731.3	25.0	94.9	4.7	26.9
1731.5	25.6	89.9	4.9	29.8
1731.8	26.1	85.4	5.9	34.9
1732.0	25.3	86.0	6.4	25.8
1732.3	25.7	87.2	6.9	25.9
1732.5	25.9	86.1	7.2	41.2
1732.8	26.3	84.2	6.3	40.4
1733.0	26.4	83.8	6.8	31.9
1733.3	23.7	84.5	15.4	14.3
1733.5	23.0	90.3	9.9	12.7
1733.8	21.7	88.0	14.7	5.0
1734.0	22.6	84.5	12.4	5.3
1734.3	21.6	85.1	13.8	4.5
1734.5	22.1	87.3	9.1	4.7
1734.8	21.7	90.7	7.1	4.0
1735.0	21.1	90.0	10.2	3.0
1735.3	22.3	89.6	5.3	5.2
1735.5	22.2	86.3	5.1	7.6
1735.8	20.4	90.2	3.3	3.8
1736.0	16.6	94.1	6.0	1.1
1736.3	12.2	99.8	11.9	0.2
1736.5	11.6	100.0	4.7	0.2
1736.8	7.7	100.0	5.2	0.0
1737.0	1.6	100.0	12.5	0.0
1737.3	2.6	100.0	16.2	0.0
1737.5	11.2	100.0	7.4	0.0
1737.8	13.4	100.0	6.9	0.1
1738.0	14.3	100.0	6.9	0.3
1738.3	15.4	97.5	9.1	0.4
1738.5	15.1	94.5	10.5	0.3
1738.8	15.2	99.2	10.1	0.3
1739.0	14.8	99.2	9.6	0.2
1739.3	14.6	92.8	14.0	0.2
1739.5	15.2	75.7	17.5	0.3
1739.8	14.4	76.9	19.1	0.2
1740.0	12.1	80.4	22.7	0.0
1740.3	9.6	76.8	33.4	0.0
1740.5	6.4	61.1	32.1	0.0
1740.8	3.9	100.0	21.3	0.0
1741.0	1.1	100.0	20.4	0.0
1741.3	5.6	99.2	17.7	0.0
1741.5	9.2	81.8	12.6	0.1
1741.8	10.9	87.9	2.7	0.6

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIE %	SW %	VSH %	KLOGH MD
1742.0	10.6	85.3	3.8	0.6
1742.3	5.9	100.0	8.4	0.0
1742.5	1.3	100.0	15.2	0.0
1742.8	3.0	100.0	21.4	0.0
1743.0	6.7	99.0	29.8	0.0
1743.3	12.6	89.7	21.8	0.1
1743.5	16.0	93.2	15.1	1.0
1743.8	15.3	95.2	19.3	1.2
1744.0	16.5	100.0	6.1	2.8
1744.3	17.2	100.0	6.2	3.0
1744.5	20.4	93.9	6.3	6.9
1744.8	21.6	91.3	6.6	7.8
1745.0	21.3	94.7	6.5	5.6
1745.3	21.1	94.6	5.9	4.5
1745.5	21.0	91.9	4.4	5.2
1745.8	19.0	94.3	3.9	4.0
1746.0	12.3	100.0	4.4	0.3
1746.3	5.4	100.0	4.5	0.0
1746.5	2.5	100.0	3.4	0.0
1746.8	6.2	100.0	7.0	0.0
1747.0	13.5	100.0	12.8	0.2
1747.3	18.6	91.5	9.2	2.0
1747.5	19.9	91.3	7.2	3.0
1747.8	20.6	87.5	7.2	3.5
1748.0	20.2	85.5	7.2	2.7
1748.3	19.4	84.6	7.1	2.8
1748.5	18.6	83.2	7.9	2.4
1748.8	17.3	86.5	7.3	1.0
1749.0	16.9	84.2	3.0	0.7
1749.3	17.5	81.8	6.5	1.4
1749.5	17.9	81.5	6.0	1.5
1749.8	18.5	79.2	7.2	2.0
1750.0	19.0	77.0	7.9	2.4
1750.3	19.0	77.0	7.6	2.0
1750.5	18.8	78.2	8.0	2.2
1750.8	16.7	82.9	13.3	0.9
1751.0	16.3	82.7	13.7	0.5
1751.3	17.4	78.2	17.0	0.7
1751.5	17.1	77.8	20.5	0.9
1751.8	16.0	81.4	24.4	0.5
1752.0	16.5	82.6	22.7	0.9
1752.3	16.6	84.4	24.7	1.0
1752.5	18.7	82.7	16.4	3.8
1752.8	19.4	73.6	15.1	10.5
1753.0	15.2	87.2	11.9	4.2
1753.3	10.2	100.0	7.2	0.3
1753.5	9.1	100.0	5.6	0.1
1753.8	15.6	91.1	5.9	3.5
1754.0	20.1	86.6	5.7	14.9
1754.3	20.5	95.6	5.3	17.6

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1754.5	25.0	87.7	7.1	137.9
1754.8	26.2	84.1	11.3	137.3
1755.0	23.7	92.4	13.1	28.2
1755.3	21.3	91.4	21.1	7.8
1755.5	22.9	89.5	15.5	13.3
1755.8	24.4	87.9	9.3	20.4
1756.0	24.2	88.2	7.2	20.5
1756.3	23.9	86.2	6.0	24.5
1756.5	23.6	80.0	10.4	13.5
1756.8	22.3	83.3	7.4	8.2
1757.0	19.9	85.0	12.0	3.7
1757.3	19.7	80.7	15.1	2.9
1757.5	19.8	80.5	12.3	2.9
1757.8	17.9	82.4	14.5	1.1
1758.0	17.0	95.4	6.3	1.2
1758.3	12.6	100.0	5.8	0.2
1758.5	12.4	100.0	14.6	0.1
1758.8	16.9	85.8	15.2	1.0
1759.0	19.1	85.3	9.6	3.5
1759.3	20.1	86.6	6.0	3.7
1759.5	20.4	85.9	5.2	4.1
1759.8	20.7	83.0	7.1	4.2
1760.0	20.1	94.5	7.7	2.3
1760.3	20.0	85.3	6.9	2.9
1760.5	19.9	85.4	6.9	3.6
1760.8	19.2	89.6	6.3	2.3
1761.0	19.6	87.0	6.5	2.4
1761.3	20.2	83.7	9.3	3.1
1761.5	20.5	83.3	7.7	2.9
1761.8	20.7	81.8	7.8	3.2
1762.0	19.7	81.5	9.3	2.3
1762.3	19.2	80.3	9.2	2.0
1762.5	19.0	77.3	8.4	2.0
1762.8	19.2	75.9	7.6	1.7
1763.0	18.0	74.1	6.9	1.4
1763.3	15.6	78.0	13.5	0.4
1763.5	16.2	95.7	10.9	0.9
1763.8	20.6	89.9	9.1	5.6
1764.0	26.3	79.2	7.2	31.9
1764.3	25.4	79.5	13.1	16.3
1764.5	23.5	96.4	12.9	10.7
1764.8	16.6	100.0	10.9	2.2
1765.0	14.5	100.0	7.9	1.2
1765.3	22.5	92.3	6.9	27.9
1765.5	25.9	94.8	6.9	49.8
1765.8	25.9	95.9	9.1	39.2
1766.0	24.6	86.7	11.3	27.3
1766.3	23.7	91.4	7.3	17.5
1766.5	22.8	91.2	3.6	12.1
1766.8	23.3	90.2	4.9	18.5

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1767.0	25.0	84.2	5.4	30.0
1767.3	24.0	83.7	7.7	16.9
1767.5	22.3	85.6	3.5	10.8
1767.8	17.7	98.0	3.7	6.3
1768.0	7.3	100.0	1.5	0.0
1768.3	7.2	100.0	1.1	0.0
1768.5	17.5	100.0	1.1	45.8
1768.8	27.2	61.3	0.8	1890.8
1769.0	23.3	76.0	0.7	534.6
1769.3	12.1	100.0	0.8	2.3
1769.5	14.1	100.0	1.1	5.7
1769.8	26.0	73.8	1.2	443.3
1770.0	31.3	78.3	1.0	1842.2
1770.3	31.4	90.7	0.7	1876.4
1770.5	31.4	95.2	1.2	1662.8
1770.8	31.5	97.0	1.9	3024.9
1771.0	31.5	99.9	1.8	2995.8
1771.3	32.1	100.0	1.9	3242.2
1771.5	31.6	100.0	1.8	3154.8
1771.8	31.6	100.0	2.0	2493.0
1772.0	31.4	100.0	2.2	2744.9
1772.3	31.6	100.0	2.0	2906.5
1772.5	32.2	100.0	2.2	2245.9
1772.8	31.5	100.0	2.4	2036.6
1773.0	30.9	100.0	2.6	1910.6
1773.3	30.7	93.0	2.8	1312.2
1773.5	28.9	86.6	3.6	474.8
1773.8	22.9	93.9	4.4	51.0
1774.0	17.2	100.0	5.7	3.2
1774.3	13.0	91.6	6.4	2.6
1774.5	20.8	76.2	7.2	5.3
1774.8	22.2	73.1	6.4	7.4
1775.0	23.0	71.2	5.8	15.6
1775.3	17.3	90.3	6.2	2.9
1775.5	10.2	100.0	10.8	0.0
1775.8	11.3	100.0	16.9	0.0
1776.0	15.2	95.9	11.6	0.2
1776.3	16.1	87.4	8.3	0.4
1776.5	15.6	88.5	7.3	0.3
1776.8	15.5	96.7	7.3	0.3
1777.0	15.4	84.9	7.9	0.3
1777.3	13.7	90.1	9.5	0.1
1777.5	11.4	100.0	9.1	0.0
1777.8	12.4	97.2	9.3	0.1
1778.0	14.3	87.7	8.9	0.1
1778.3	15.9	83.2	8.1	0.5
1778.5	16.0	85.1	7.8	0.6
1778.8	15.5	87.3	8.1	0.3
1779.0	15.3	89.7	7.4	0.2
1779.3	14.9	88.6	8.7	0.2

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIF %	Sw %	VSH %	KLOGH MD
1779.5	15.4	87.6	9.1	0.2
1779.8	16.2	85.9	9.3	0.4
1780.0	15.8	91.8	6.1	0.3
1780.3	14.1	94.8	5.4	0.3
1780.5	12.7	93.1	4.1	0.4
1780.8	9.9	100.0	5.5	0.1
1781.0	6.0	100.0	5.9	0.0
1781.3	7.1	100.0	5.8	0.0
1781.5	15.9	100.0	6.0	7.8
1781.8	26.4	97.4	9.0	317.1
1782.0	31.5	98.3	7.7	1254.3
1782.3	32.0	97.9	5.8	1275.8
1782.5	29.3	95.1	6.1	540.7
1782.8	19.9	100.0	6.4	12.2
1783.0	10.9	100.0	6.8	0.1
1783.3	11.0	100.0	7.8	0.0
1783.5	14.1	86.0	8.0	0.2
1783.8	16.2	79.7	7.8	0.5
1784.0	17.3	79.2	8.2	0.7
1784.3	17.2	81.8	7.6	0.6
1784.5	16.8	85.7	7.1	0.6
1784.8	17.3	84.0	7.0	0.6
1785.0	18.7	79.7	6.1	1.2
1785.3	17.5	86.1	5.9	1.0
1785.5	13.6	100.0	5.2	0.1
1785.8	15.3	99.3	4.5	0.3
1786.0	18.0	84.7	5.0	1.2
1786.3	19.1	87.7	5.7	1.3
1786.5	19.8	85.9	6.3	1.6
1786.8	18.9	87.6	5.2	1.4
1787.0	19.2	89.7	5.1	1.2
1787.3	18.5	89.2	4.3	1.4
1787.5	19.0	90.3	5.0	1.0
1787.8	17.8	89.6	5.8	1.0
1788.0	17.5	86.2	9.3	1.0
1788.3	17.2	87.0	8.4	0.7
1788.5	16.0	93.4	3.0	0.4
1788.8	10.5	100.0	1.8	0.0
1789.0	2.4	100.0	13.1	0.0
1789.3	0.0	100.0	13.9	-9999.0
1789.5	0.0	100.0	11.0	-9999.0
1789.8	1.3	100.0	6.9	0.0
1790.0	6.0	100.0	17.2	0.0
1790.3	14.2	100.0	14.3	0.2
1790.5	15.9	98.9	19.6	0.7
1790.8	19.6	95.9	5.9	4.3
1791.0	21.9	89.3	6.7	9.4
1791.3	21.7	90.0	6.5	7.1
1791.5	21.0	99.5	6.5	5.0
1791.8	20.0	82.1	15.7	3.9

FIELD = 313. WELL = 2. START = 1557.00 STOP = 2025.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1792.0	21.5	73.6	9.6	7.1
1792.3	19.6	83.5	8.2	3.0
1792.5	16.8	92.4	7.4	0.8
1792.8	16.4	95.6	7.2	0.6
1793.0	17.6	96.1	5.5	1.2
1793.3	18.4	100.0	3.4	3.7
1793.5	19.0	100.0	2.9	9.2
1793.8	19.7	100.0	2.5	22.9
1794.0	13.5	100.0	2.5	2.1
1794.3	14.8	100.0	2.0	3.4
1794.5	25.1	100.0	1.6	157.9
1794.8	28.4	100.0	1.4	442.3
1795.0	28.5	100.0	1.4	681.2
1795.3	29.1	87.8	1.7	1250.5
1795.5	21.0	100.0	1.5	80.9
1795.8	7.7	100.0	1.8	0.0
1796.0	2.7	100.0	2.5	0.0
1796.3	10.8	100.0	2.1	0.5
1796.5	23.8	83.2	1.2	424.9
1796.8	29.0	82.1	1.4	1608.7
1797.0	30.0	87.0	1.4	1825.0
1797.3	30.6	93.2	1.5	2143.5
1797.5	31.0	96.4	1.6	2110.3
1797.8	31.3	100.0	1.7	2374.6
1798.0	32.2	100.0	2.0	2432.6
1798.3	32.5	100.0	2.3	1660.3
1798.5	32.4	100.0	2.5	1762.5
1798.8	32.9	100.0	2.8	2185.7
1799.0	33.5	99.6	2.3	2700.2
1799.3	32.6	100.0	2.7	2067.1
1799.5	31.5	100.0	2.6	1322.3
1799.8	32.3	98.2	2.3	1615.2
1800.0	32.1	96.3	2.6	1315.5
1800.3	31.0	97.4	3.2	807.8
1800.5	31.0	95.9	3.1	665.1
1800.8	29.9	99.7	3.3	407.3
1801.0	28.6	100.0	3.7	257.8
1801.3	29.4	93.8	4.6	365.5
1801.5	28.9	90.0	4.9	235.3
1801.8	26.4	96.1	4.1	63.2
1802.0	23.2	98.2	4.2	37.0
1802.3	24.7	97.5	3.3	45.7
1802.5	26.6	83.0	2.7	135.6
1802.8	28.0	71.4	2.2	251.3
1803.0	21.6	80.7	2.7	71.7
1803.3	8.4	100.0	4.0	0.1
1803.5	1.2	100.0	4.6	0.0
1803.8	6.3	100.0	4.3	0.0
1804.0	20.4	89.6	5.1	14.2
1804.3	24.6	86.5	5.9	36.5

FIELD = 313. WELL = 2. START = 1557.00 STOP = 2025.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1804.5	23.0	95.6	6.0	14.3
1804.8	23.0	91.5	6.4	15.6
1805.0	21.6	87.4	7.9	8.5
1805.3	19.1	86.8	10.2	2.3
1805.5	16.7	88.6	9.1	0.9
1805.8	15.4	88.2	8.4	0.3
1806.0	15.7	82.3	9.2	0.3
1806.3	16.5	79.0	9.0	0.5
1806.5	16.3	80.4	9.6	0.5
1806.8	15.7	81.0	12.9	0.4
1807.0	16.0	83.2	10.7	0.5
1807.3	15.7	88.7	12.3	0.4
1807.5	16.6	100.0	8.6	0.6
1807.8	15.7	100.0	9.5	0.4
1808.0	17.9	100.0	9.7	1.7
1808.3	21.7	91.4	9.5	31.0
1808.5	20.4	95.3	5.4	34.5
1808.8	3.1	100.0	8.2	0.0
1809.0	0.0	100.0	13.1	-9999.0
1809.3	0.0	100.0	3.8	-9999.0
1809.5	0.0	100.0	2.9	-9999.0
1809.8	3.3	100.0	2.6	0.0
1810.0	16.3	100.0	3.1	16.1
1810.3	26.7	91.4	2.4	497.4
1810.5	28.0	100.0	2.0	760.4
1810.8	27.1	100.0	1.9	537.0
1811.0	27.6	100.0	2.1	517.3
1811.3	29.0	100.0	2.8	815.8
1811.5	30.1	100.0	3.5	816.0
1811.8	30.3	100.0	2.9	944.9
1812.0	29.5	100.0	3.5	925.2
1812.3	28.1	100.0	4.1	400.5
1812.5	27.0	98.8	4.4	184.5
1812.8	23.3	100.0	4.9	61.6
1813.0	18.1	100.0	5.1	8.8
1813.3	18.5	100.0	5.7	10.5
1813.5	21.2	92.0	5.0	24.5
1813.8	22.3	93.7	5.1	21.2
1814.0	16.7	100.0	6.1	1.9
1814.3	15.3	100.0	5.9	1.2
1814.5	20.1	85.6	5.5	6.4
1814.8	21.4	83.6	6.1	6.2
1815.0	20.5	89.2	5.3	4.0
1815.3	18.6	98.4	5.5	1.5
1815.5	19.0	95.2	5.8	2.0
1815.8	20.0	88.5	6.3	3.0
1816.0	20.2	87.4	6.3	2.7
1816.3	20.4	85.9	6.4	2.5
1816.5	20.5	84.1	5.9	2.3
1816.8	20.0	84.2	6.1	2.8

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIF %	SW %	VSH %	KLOGH MD
1817.0	19.6	84.2	6.5	2.5
1817.3	19.7	83.2	6.9	2.1
1817.5	19.4	85.6	7.0	2.0
1817.8	19.4	86.7	7.1	1.9
1818.0	19.1	88.4	6.3	1.7
1818.3	19.3	88.1	5.5	2.3
1818.5	19.5	87.6	5.4	2.2
1818.8	19.4	89.0	5.0	2.3
1819.0	19.0	90.5	5.2	2.1
1819.3	20.0	85.6	6.4	3.1
1819.5	20.2	86.6	5.5	3.5
1819.8	19.1	92.8	4.2	2.6
1820.0	19.7	87.3	4.3	4.5
1820.3	19.9	85.7	2.7	11.1
1820.5	18.7	90.7	3.0	17.7
1820.8	14.3	100.0	4.6	2.2
1821.0	9.5	100.0	4.9	0.0
1821.3	14.9	100.0	3.8	0.4
1821.5	20.1	93.1	3.6	4.2
1821.8	21.0	92.8	3.3	5.3
1822.0	21.1	94.7	4.0	5.0
1822.3	20.9	95.4	4.1	4.6
1822.5	21.6	91.5	4.3	7.1
1822.8	21.8	91.4	4.2	7.1
1823.0	21.5	93.9	4.3	7.0
1823.3	21.3	93.0	4.5	6.5
1823.5	21.5	90.1	5.4	6.3
1823.8	21.1	88.9	5.9	5.5
1824.0	20.6	89.5	5.4	3.9
1824.3	19.6	91.7	5.5	2.4
1824.5	18.4	96.5	5.5	1.5
1824.8	18.4	96.4	5.6	1.5
1825.0	19.6	89.7	6.4	1.8
1825.3	20.1	87.6	6.6	2.4
1825.5	19.7	89.4	6.1	2.5
1825.8	19.2	92.0	6.5	2.2
1826.0	18.9	95.6	5.1	2.1
1826.3	19.9	92.7	4.9	2.5
1826.5	20.2	89.9	4.0	2.7
1826.8	19.3	85.7	5.0	2.4
1827.0	12.0	100.0	10.3	0.1
1827.3	2.3	100.0	4.1	0.0
1827.5	8.0	100.0	4.2	0.0
1827.8	22.3	100.0	3.7	159.6
1828.0	28.5	93.3	3.9	1105.5
1828.3	29.2	95.4	4.1	695.6
1828.5	25.1	100.0	5.1	121.3
1828.8	14.1	100.0	6.3	0.9
1829.0	4.3	100.0	6.1	0.0
1829.3	2.4	100.0	6.3	0.0

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

DEPTH	PHIE %	SW %	VSH %	KLOGH MD
1829.5	8.1	100.0	6.0	0.0
1829.8	13.9	100.0	6.0	0.1
1830.0	17.2	100.0	5.3	0.7
1830.3	18.4	95.4	4.9	1.2
1830.5	18.6	95.1	3.8	1.3
1830.8	17.9	96.4	3.1	1.4
1831.0	16.8	96.8	2.9	1.9
1831.3	19.9	81.1	2.0	13.0
1831.5	19.0	71.6	2.0	51.6
1831.8	12.5	96.2	2.9	4.2
1832.0	7.9	100.0	3.4	0.1
1832.3	11.2	100.0	2.6	0.9
1832.5	16.0	100.0	1.4	11.1
1832.8	18.9	100.0	0.9	40.2
1833.0	21.2	100.0	1.1	69.4
1833.3	26.0	100.0	1.9	319.0
1833.5	28.8	100.0	1.9	1023.7
1833.8	29.4	100.0	2.3	1380.2
1834.0	30.5	100.0	2.2	1749.1
1834.3	31.1	100.0	2.0	1777.3
1834.5	30.9	100.0	2.1	1741.1
1834.8	30.6	100.0	2.4	1539.2
1835.0	30.2	100.0	2.7	1540.2
1835.3	29.9	100.0	2.7	895.8
1835.5	29.8	100.0	2.7	381.0
1835.8	28.7	100.0	2.9	291.9
1836.0	28.2	99.3	3.0	224.5
1836.3	27.4	93.3	2.9	152.9
1836.5	19.4	100.0	3.1	12.9
1836.8	12.0	100.0	3.2	0.4
1837.0	18.7	100.0	2.9	3.0
1837.3	22.8	100.0	2.9	17.4
1837.5	23.3	100.0	2.7	22.9
1837.8	25.5	100.0	2.7	61.3
1838.0	26.7	100.0	3.2	159.1
1838.3	28.6	100.0	3.7	359.2
1838.5	29.0	97.2	4.1	520.2
1838.8	29.4	94.7	5.2	257.5
1839.0	27.2	95.8	5.5	91.1
1839.3	23.0	100.0	6.4	13.7
1839.5	20.4	100.0	7.2	2.5
1839.8	20.8	92.3	6.3	3.3
1840.0	20.8	86.9	6.7	3.9
1840.3	20.4	84.4	7.8	3.1
1840.5	20.2	83.1	7.3	2.7
1840.8	18.6	85.4	8.7	1.0
1841.0	17.1	89.0	7.2	0.5
1841.3	16.2	92.0	6.5	0.3
1841.5	15.3	93.8	7.4	0.2
1841.8	15.7	92.3	7.3	0.3

FIELD = 313. WELL = 2. START = 1567.00 STOP = 2025.00

*	DEPTH *	PHIE %	Sw %	VSH % *	KLOGH MD *
*	1842.0 *	15.9	94.6	6.6 *	0.3 *
*	1842.3 *	16.6	92.9	6.6 *	0.4 *
*	1842.5 *	17.6	88.1	6.7 *	0.5 *
*	1842.8 *	17.5	36.0	8.0 *	0.5 *
*	1843.0 *	15.3	81.3	17.3 *	0.2 *
*	1843.3 *	14.0	83.0	18.9 *	0.1 *
*	1843.5 *	14.3	100.0	9.5 *	0.1 *
*	1843.8 *	12.5	100.0	16.6 *	0.0 *
*	1844.0 *	16.3	100.0	4.8 *	0.6 *
*	1844.3 *	20.7	100.0	2.5 *	35.4 *
*	1844.5 *	25.7	100.0	2.8 *	591.0 *
*	1844.8 *	26.0	100.0	4.0 *	490.1 *
*	1845.0 *	26.6	100.0	4.7 *	368.0 *
*	1845.3 *	28.2	100.0	4.2 *	376.8 *
*	1845.5 *	28.5	100.0	4.1 *	266.1 *
*	1845.8 *	28.5	100.0	4.3 *	253.1 *
*	1846.0 *	28.9	100.0	4.4 *	321.5 *
*	1846.3 *	29.1	100.0	4.1 *	270.4 *
*	1846.5 *	29.5	99.4	4.3 *	222.0 *
*	1846.8 *	28.0	94.5	4.4 *	167.3 *
*	1847.0 *	25.6	92.9	4.4 *	64.0 *
*	1847.3 *	23.8	97.3	4.2 *	31.6 *
*	1847.5 *	23.3	82.8	4.2 *	22.4 *
*	1847.8 *	22.4	84.0	4.2 *	17.4 *
*	1848.0 *	21.5	89.8	4.5 *	11.2 *
*	1848.3 *	21.7	94.0	4.6 *	12.2 *
*	1848.5 *	23.7	95.6	5.6 *	25.9 *
*	1848.8 *	25.9	95.8	6.1 *	46.3 *
*	1849.0 *	26.6	97.6	5.5 *	56.6 *
*	1849.3 *	26.9	96.0	5.7 *	50.1 *
*	1849.5 *	26.1	95.3	5.0 *	40.6 *
*	1849.8 *	24.3	96.5	4.2 *	29.2 *
*	1850.0 *	23.4	99.2	2.9 *	20.3 *
*	1850.3 *	21.0	100.0	2.9 *	15.1 *
*	1850.5 *	21.3	100.0	1.9 *	45.9 *
*	1850.8 *	26.4	100.0	1.7 *	356.5 *
*	1851.0 *	29.5	100.0	1.5 *	1537.5 *
*	1851.3 *	30.7	100.0	1.6 *	2297.3 *
*	1851.5 *	29.7	100.0	1.6 *	1708.6 *
*	1851.8 *	29.2	100.0	1.8 *	1968.2 *
*	1852.0 *	30.2	100.0	1.8 *	3127.7 *
*	1852.3 *	31.2	100.0	2.1 *	3374.9 *
*	1852.5 *	30.9	100.0	2.2 *	2405.1 *
*	1852.8 *	30.7	100.0	2.0 *	2440.2 *
*	1853.0 *	30.8	100.0	1.7 *	2664.7 *
*	1853.3 *	31.3	100.0	1.6 *	4242.3 *
*	1853.5 *	31.8	100.0	1.6 *	6134.8 *
*	1853.8 *	31.4	100.0	1.9 *	4209.4 *
*	1854.0 *	31.2	100.0	2.0 *	3013.6 *
*	1854.3 *	31.3	100.0	2.1 *	2629.4 *