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Den norske stats oljeselskap a.s



Gradering

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Laget av

Operation Technology, LET-Bergen

Undertittel

Tittel

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PETROPHYSICAL EVALUATION
WELL 30/3-3
NOVEMBER 1983
na se
Nov83 H. Buvik



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WELL DATA

Operator:	Statoil				
Well:	30/3-3				
Location:	60 ⁰ 46' 11.44" N 02 ⁰ 57' 05.58" E				
Classification	Exploration Well				
Drilling rig:	Ross Isle				
Spudded:	02.04.83				
Rig released:	31.05.83				
KB-elevation:	22.0 m				
Water depth:	182 m				
Total depth:					
Drillers depth:	3419 mRKB				
Sclumberger depth:	3425 mRKB				
Objective:	Middle and Lower Jurassic Sandstones				

FIGURE 1



- 3 -



INTRODUCTION

The well 30/3-3 was drilled in a down faulted block between the wells 30/6-5 and 30/3-2. The well was considered dry. The purpose of this "quick-look" analysis is to define the petrophysical parameters of the Drake and Brent Group and to look for hydrocarbons. Since Statfjord was considered dry and just partly penetrated, (32 m), no analysis was performed.





LITHOLOGY

The Brent Group (2978 m - 3048 mKB)

Ness Formation (2978 - 3034 mKB)

The Ness Formation consists predominantly of sandstones with beds of shale and coal. The sandstone is light to medium grey, very fine to medium grained, mostly friable, angular to subrounded with a fair visible porosity. The shale is micaceous, carbonaceous and none to slightly calcareous. The coal is black, hard, brittle and shiny.

The Etive Formation (3034 - 3048 mKB)

The Etive Formation consists of sandstone which is clear to transparent quartz, fine to medium grained, occasionally coarse, subrounded to subangular loose and friable.

The Dunlin Group (3048 - 3387 mKB)

The Drake Formation (3048 - 3241 mKB)

The Drake Formation consists of mostly sandsone on top, composed of clear to transparent quartz, medium to coarse, subangular to subrounded, mostly friable and occasionally slightly calcareously cemented.

The lower part of the formation is interbedded shale and sandstone.



	1 Ju/3-	,			Ā	RETEST	RECORDE	D DATA	<u>Kina an</u>		BLF TAB
DATI	3 20.05	. 83									
RUN	NO. 1								Мах	· recorded te	ոթ.։ 135 ⁰ Ը
Test No.	Depth	Tem	Log hydr. before t.	Corr. hydr. before t.	Draw down	Build up time	Log Pretest pressure	Cor. Pretest pressure	Log hydr. after t.	Cor. hydr. after t.	Remarks
	E	υ	bar	bar	bar	sec	bar	bar	bar	bar	
-	3007.2	121.1	378.074	377.936	318.676	9	331.396	331.190	377.936	377.798	18 sec. to stabilize
2	3013.0	117.2	378.143	378.005	318.883	12	331.810	331.603	378.626	378.488	
e	3042.0	117.2	382.280	382.177	326.226	3	334.430	334.258	382.142	382.039	
4	3036.2	117.2	381.660	381.556	138.481	50	334.706	334.534	381.522	381.418	
2	3086.2	118.9	388.072	387.968	316.608	12	339.188	339.015	388.003	386.899	
9											New tool
7	3036.2	1.1.4	379.660	380.625	189.572	56	333.672	334.568	379.729	380.694	-
8	3086.2	117.3	385.865	386.831	320.606	4	338.016	338.912	385.796	386.762	8
6	3243.8	120	404.619	405.584	26.717	245	356.011	356.976	404.550	405.515	Not so good
10	3396.8	120	422.752	423.718	40.300	54	361.113	362.078	422.752	423.718	
11	3389.9	120	421.856	422.821	170.197	105	361.527	362.492	421.856	422.821	
12	3402.4	120	421.959	423.924	3.413	785	361.182	362.147	422.890	423.855	
13											
14											
15											
16											
17											
18											
19											
20											



SUMMARY

Only residual hydrocarbons were encountered in the Brent and Drake sands of 30/3-3. The logs indicate an average watersaturation of 93% and an average porosity of 17%.

The RFT plot suggests a watergradient of 1.02 g/cc.

The well was not tested.

One interval from 2979 to 2992.5 mRKB was cored.



LOG QUALITY

The logs are generally of good quality.

The caliper presented, reads a slightly too high value and the caliper of the LDL-CNL log slightly too low.



INPUT PARAMETERS

Formation Temperature

A temperature of 116^OC was used in the calculations. This temperature was obtained from the ISF-SONIC log.

The LDL-CNL log was corrected for a temperature of 122°C.

Formation Water Resistivity, Rw

A value of 0.07 (at 116° C) was chosen after a comparison with 30/3-2, R_{wa} calculations, ratio method and calculations from the SP log.

Mud Properties

R _m	=	0.544	ohmm	at	14.4 [°] C
R _{mf}	=	0.349	ohmm	at	14.4°C
Rmc	=	1.000	ohmm	at	13.3 ⁰ C
R	=	0.143	ohmm	at	116 ⁰ C
R _{mf}	=	0.091	ohmm	at	116 ⁰ C
Rmc	=	0.255	ohmm	at	116 ⁰ C

Shale Parameters

The shale parameters were picked from cross plots and visual inspection of the logs.



COMPUTATIONS

Shale Volume

Of the standard shale indicators the GR and the LDL-CNL crossplot are considered applicable. The final shale volume used for further computations is picked as a minimum.

An exception are the intervals 2991 - 2999 mRKB and 3016.5 -3029 mRKB. These intervals are the coal beds of the Ness Formation which are not considered productive. By using the GR as the only indicator, these intervals were excluded from our statistics.

Porosity

The shale-corrected PHID and PHIS crossplot was used as a primary porosity and in addition as a final porosity, since the hydrocarbon effect was considered zero.



Water Saturation

The induction log is used as a R_t curve and a manually mudcake corrected RMSFL as a R_{xo} -curve. The modified Nigeria equation is used for the water saturation calculation.

$$\frac{1}{\sqrt{R_{f}}} = \left[\frac{V_{sh}^{c}}{\sqrt{R_{sh}}} + \frac{\varphi_{\cdot}^{m/2}}{\sqrt{aR_{w}}}\right] S_{w}^{n/2}$$

$$R_t = True Resistivity$$

 $R_w = Formation Water Resistivity$
 $S_w = Water Saturation$
 $R_{sh} = Shale Resistivity$
 $V_{sh} = Shale Volume$
 $\emptyset = Porosity$
 $C = Shale Exponent (1.6)$
 $m = Cementation Exponent (2)$
 $n = Saturation Exponent (2.0)$
 $a = Lithology Factor (1.0)$

First the $S_{xo}-S_{hr}$ -values were computed, then the PHIF and finally the S_w-S_h values.

In the coalbeds S_h was given the value 0 and S_w the value 1.



DISCUSSION

The difficulties of log-interpretation in this well are the coalbeds in the Ness Formation. There are several beds fairly close together. The logs are not able to resolve the single non-coalbed in between without strong edge-effects. Due to this effect, the porosity, shale volume and especially the water saturation would give rather incorrect values, since the induction log has a long spacing.

To improve the CPI some "cosmetic" work was applied; filtering the porosity to zero where coal was present. The payzones of 1.75 m is believed to be just edge-effects of the induction log and not actual pay. The RFT pressures suggests a pure. watergradient.

There might be some residual gas in between the coal, but this gas would not be relevant to production.

The HC-residual curve is the product of SH * PHIF.



CORE SUMMARY

There is one core, 2979 - 2992.5 mRKB in the top of the Ness Formation.

The porosity range from 4.8% to about 17.1% with a single value of 25.4% which agrees with the log porosity.

The grain density is in the area of 2.66 g/cc - 2.68 g/cc and the permeability, both vertical and horisontal, rather low about 1 mD.

The zone about 2987 - 2988 mRKB is a high porosity and permeability zone.

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RESULTS

TABLE

PETROPHYSICAL PARAMETERS

FROM WELL LOGS

WELL 30/3-3

Formation interval (m RKB)	Sand (m)	Average Porosity %	Average Water Saturation %	Average Shale Volume %	Net/Gross %
BRENT and DRAKE	1.75 *	-	-	-	-
(2978 - 3116)	56.50	0.17	0.93	0.15	0.41
NESS Formation (2978 - 3034)	1.00*	- 0.20	- 0.91	- 0.11	- 0.28
ETIVE Formation	0.75 *	- 0.17	- 0.89	- 0.11	- 0.96
DRAKE Group	0.00	-	-	-	-
(3048 - 3116)	27.50	0.16	0.97	0.21	0.40



Cutoff values: $S_w = 0.65$ PHIF = 0.12 $V_{sh} = 0.40$



APPENDIX

Statistics

Sensitivity Plot

Crossplots

Listing

CPI

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	•	•	

30-3 5-05

• DATE:

8 ci 6 DEPTH INTERVAL: . . 2978.00 TO 3116.00 APPLIED CUTOFFS: ¢ NOCATED TUAN ------

0	°.	0.	
THAN	THAN	THAN	
GREATER	LESS	GREATER	
:HSO	PHIF:	54:	
	•	•	

DEPTH TOTAL

-

**********	138.000 0 104	0.442	0.935	0.887	0.065	14.391	1.628	0.345	1.283	*********
よよよすよよよよよよよよよよよよよよよよよよよよよよよよよ CUNICC-		RACE 'USHALE'	RAGE 'SU'	VERAGE 'SW' # 'PHIF'	PAGE 'SH'	D VOLUME: ('PHIF').	UOID VOLUME ('SH'X) .	HC VOID VOLUME ('SHR'X).	HC VOID VOLUME	************************

7 A 4 + 11 X

XXXXXXXXXXXX	1.750	0.224	0.215	0.484	0.469	0.516	0.391	0.208	0.066	0.142	*****
************	•	PHIF'	'USHALE'	, 'Su',	'SU' * 'BHIF'	, 'SH'	· · · ('PHIF').	· (* HS,) · · :)LUME ('SHR'X).)LUME	(*****************
**********	THICKNESS:	AVERAGE	AVERAGE	AUERAGE	U.AVERAGE	AVERAGE	VOID VOLUME: .	HC VOID VOLUME	RES HC VOID VO	MOV HC UDID UC	**********

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xxxxxxxxxxx	56.500	0.171	0.156	0.934	0.924	0.066	9.677
xxxxxxxxxxxxxxx	• • • •	'PHIF'	'USHALE'	'Su'	'SU' * 'PHIF'	, SH,	('PHIF').
**	٠	٠	•	•	٠	٠	٠
*****	THICKNESS: .	AUERAGE	AUERAGE	AVERAGE	U.AVERAGE .	AVERAGE	UOID VOLUME:

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0.01268 0.40342 0.03097 1.************
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8HE-E-ØE €-0€	18 NOV 1983	3034.00	0.40 0.12 0.65
 	10.25	. 2978.00 TO	GREATER THAN Less than Greater than
FIELD:	ENGINEER* • • • • • • • • • • • • • • • • • • •	DEPTH INTERVAL:	

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	*******	1.000	0.235	0.302	0.448	0.430	0.552	0.235	0.134	0.029	0.105	****
	*****	• • • •	PHIF'	USHALE'	SW/	SU' X 'PHIF'	SH'	. ('PHIF').	. (*'HS') .	ME ('SHR'X).	雨・・・・ 第	********
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2 1	********	THICKNESS	AUERAGE .	AUERAGE .	AVERAGE .	J.AUERAGE	AVERAGE .	JOID VOLUP	HC VOID VC	RES HC VOI	TOU HC VOI	*******

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**********		15.500	0.197	0.105	0.906	0.895	0,094	3.057
	************	• • • • • •	'PHIF'	'USHALE'	'Su'	'SU' X 'PHIF'	, sh'	('PHIF').
	*****	THICKNESS:	AVERAGE	AUERAGE	AVERAGE	U.AVERAGE	AVERAGE	UOID VOLUME: .

30-3-348 18 NOU 1983	3048.00 0.40 0.12 0.65
•••• ••• HB ••• 10.86	. 3034.00 TO Greater Than Less Than Greater Than
FIELD:	DEPTH INTERVAL: APPLIED CUTOFFS:

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*********	14.000	0.170	0.124	0.884	0.868	0.116	e. 373	0.314	0.072	0.242	*******
A L	++++++++++++++++++++++++++++++++++++++	E 'PHIF'	E 'USHALE'	E, SU/	AGE 'SU' * 'PHIF'	E'SH'	OLUME: ('PHIF').	D VOLUME ('SH'X) .	: VOID VOLUME ('SHR'X).	: VOID VOLUME	****************
~ ~ ~ ~	THICKN	AUERAG	AUERAG	AUERAG	U.AUER	AVERAG	VOID U	HC UOI	RES HC	MOU HC	****

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*********	********** 0.750	0.208	0.100	0.532	0.526	0.468	0.156	0.074	0.037	0.037	********
A 7 ******************	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	. 'PHIF'	. 'USHALE'	. 'SW'	. 'SU' # 'PHIF'	. , SH,	('PHIF').	1E ('SH'*) .	JOLUME ('SHR'X).	JOLUME	***********
N E T P	THICKNESS:	AVERAGE	AVERAGE	AUERAGE	U.AVERAGE .	AVERAGE	VOID VOLUME:	HC VOID VOLUT	RES HC VOID (MOU HC VOID (**********

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 PHIF
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 VSHALE
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 AUERAGE
 SU
 0.972

 AUERAGE
 SU
 0.972

 AUERAGE
 SU
 0.953

 AUERAGE
 SU
 0.963

 AUERAGE
 SU
 0.028

 AUERAGE
 SU
 0.132

 RES
 HC UOID UOLUME
 0.137

 RES
 HC UOID UOLUME
 0.107

 AUERAGE
 SU
 30-3-3HB 0.40 0.12 0.65 3116.00 ************************************ NET/GROSS RATIOS ... 3048.00 TO GREATER THAN LESS THAN GREATER THAN . HB 10.27 ٠ ٠ • • • SUS PHIF: STATIST STICS ٠ SAND DEPTH INTERVAL: APPLIED CUTOFFS: • • ٠ WELL: ENGINEER: DATE: FIELD: . . . N E



WELL 30/3-3 HB. INTERVAL 2978.00 - 3116.00 TIME 10.34 18. Nov. 1983



THE HEATHER FORMATION

(2950 - 2978 m RKB)

THE NESS MEMBER

(2978 - 3034 m RKB)

5314437233337345081111 000

+12 +10 +6 +8 +13 +9

+12

+1 +2 +1 +1 +

÷2

+ +1 +1 +1 +

202

+1 +5 +7

+8 +4 +17 +8 +7

+13

+++++++++++

+10 +13

+3

214

PLOTTED BY: HB

THE ETIVE MEMBER

(3034 - 3048 mRKB)

THE DRAKE FORMATION

(3048 - 3116 m RKB)

THE DUNLIN SHALE

(3116 - 3150 mRKB)

LISTING

SW	1.000	1.000	1.000	1.000	1.001	1.000	0.954	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
HIH	000-0	14.0	000.0	0.000	0.00.0	0.000	0.000	0.000	0.000	0.000	0.001	0.000	000-0	000.0	000-0	0000	000.0	0.000	0.000	000.0	u.ac1	U.009	0.115	0.013	0.010	0.000	0.062	0.000	0.000	0.000
N S H	0.956	0.937	0.920	6.? . D	0.435	0.995	1.000	1.000	1.000	1.000	0.960	0.935	1.000	1.000	1.000	1.000	1.000	0.983	1.000	1.000	0.962	0.918	n.3&1	0.922	n. 930	1.000	0.973	1 ó ö • 0	1.000	1.000
DEP TH	2967.50	2461.15	2968.00	2968 . 25	2968.50	2968.75	2969.00	2969.25	2969.50	2969 25	2970.00	2970.25	2070.50	2970.75	2°71.00	2971.25	2971.50	2971.75	2972.00	2972.25	2972.50	2972.75	2973.00	2973.25	2973.50	2973.15	2974.00	2974 - 25	2974.50	2974.75
SW	1.000	0.925	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	0.946	1.000	1.000	1.000	1.000	1.000	1.000	1.000	0.899	0.786	0.795	0.801	0.901	1.000	1.000	1.000
4 IEd	0.030	0.944	0.023	0.014	0.008	0.001	0.000	0.000	0.000	0.011	U.U20	0.022	0.015	0.017	0.038	0.016	0.000	000.0	0.000	00.C	00000	0.000	0.000	0.000	0.000	0.000	0.024	0.008	0000	0.000
NSN	0.384	0.943	0.967	0.942	0.755	n.981	1.000	1.000	0.996	0.981	0.930	0.887	0.395	0.887	0.845	0.889	1.000	1.000	0.091	0.980	1.000	1.000	1.000	1.000	1.000	1.000	0.987	0.927	0.967	0.990
0E1 11	2960.00	2960.25	2960.50	2960.75	2961.30	2961.25	2961.52	2901.75	2962.00	2062.25	2962.50	2962.75	2963.10	2963.25	2963.50	2963.75	2964.00	2964.25	2964.50	2964.75	2965.00	2965.25	2965.50	2965.75	2966.00	2960.25	2966.50	2966.75	2967.00	2967.25

DATE: 1%NOV23/HB

WELL: 30-3-3Hⁿ (2960 - 3150)

U. %00 U. %87 U. %87 0. %26 0. %28 0. %26 0. %26 0. %26 0. %26 0. %27 0. %26	0.000 0.090 0.101 0.118 0.117 0.117 0.117	0.552 0.552 0.552 0.503 0.503 0.503	2988.25 2988.50 2988.75 2989.75 2989.25 2989.50 2989.75	1.000 1.000 1.000 1.000 0.823	0.000 0.000 0.000 0.000 0.040	0.710 0.377 0.968 0.797
00-0	0.059 0.058 0.054	0.560 0.560 0.564	2987.25 2987.50 2987.75 2988.00	0.933 1.000 1.000 1.000 1.000	0.045 0.035 0.010 0.000 0.000 0.000	
204 °0	u.u14 0.035 0.055	u.840 0.743 0.574	2980.5U 2986.75 2987.00	1.000 1.000 1.000	0.031 0.031 0.034	MOS
1.000	0.017	0.769	2986.25	1.000 1.000	0.006 0.027	4 0
1.000	0.035	0_696 0_646	2985.75 2486 00	1.000	0.000	\sim
0.901 0.96	0.058 0.046	0.674 0.699	2985,25 2985,50	1.000 1.000	00000	96 01
0.90	U. U61 0. 060	U. 689 D. 673	2984.75	1.000 1.000	000.0	00
0.00	0.071	0.653	2984.50	1.000 1.000	0.000	00
7.33(0.000	0.628	2084 110	1.000	000.0	00
0.795	0.108	0.624	2983.75	1.000	0000	
0.733	0.146 0.127	0.579 0.579	2983.25 2983.50	1.000 1.000	0000-0	23
0.742	0.153	0.549	2983.00	1.000	J.002	400
0.73	0.151 0.158	U.552 D.547	2982.50 2982.75	1.000	004°0	00
S	d IH d	N S H	DEP TH	S ¼	ЫЦF	÷

Su	0.834	0.610	1.000	0.472	0.450	0.894	1.000				1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	0.973	0.987	9.980	0.919	0.934	U.933	1.000	0.987	0.937
PHIF	000-0	0.000	0.000	0.000	0.000	0.00.0	0.000				0.000	000.0	0.018	0.000	000.0	0.000	0.012	0.000	0.000	0.000	0.000.0	0.003	U.O60	0.100	0.133	0.141	0.154	0.171	0.172	0.164	U.15U	0.169	0.184
HS A	1.000	1.000	1.000	1.000	1.000	1.000	1.000				0,999	0.847	0.661	0.607	1.858	0.814	0.486	0.520	0.734	0.456	0.229	0.162	0.147	0.149	0.136	0.238	0.202	0.143	0.100	0.164	0.265	0.170	0.105
DEPTH	2997.50	2997.75	2998.00	2998.25	2998.50	2998.75	2999.00				2999.25	2999.50	2999.75	3000-00	3000.25	3000.50	3000.75	3001.00	3001.25	3001.50	3001.75	3002.00	3002.25	3002.50	3002.75	3.)03.00	3003.25	3003.50	3003.75	3004.00	3004.25	3004.50	3004.75
SW	0.803	0.824	0.929	1.000	1.000	1.000	0.747	1.000	1.000	1.000	1.000	0.478	0.766				0.768	0.762	1.000	1.000	1.000	1.000	1.000	0.702	0.312	1.000	1.000	0.409	0.460	0.498	1.000	1.000	1.000
PHIF	110	0 104	0.088	0.069	0.017	0.000	0.000	000.0	0.000	0.000	0.000	0.252	0.176				0.192	0.195	0.000	0.000	0.000	0.000	0.061	0.114	0.000	0.000	0.000	0.000	0.000	0.000	0000.0	0.000	00000
ΝSΗ	007-0	0.495	0.551	0.641	0.939	1.000	1.000	1.000	1.000	0.870	0.826	0.602	0.254				0.067	0.125	0.424	0.937	1.000	1.000	0.912	0.935	1.000	1.000	1.000	1.000	1.300	1.000	1.000	1.000	1.000
DEPTH	2990-00	2990.25	2000.50	2990.75	2991.00	2991.25	2091.50	2491.75	2092.00	2992.25	2992.50	2992.75	2993.00				2993.25	2993.50	2993.15	2094.00	2994.25	2994.50	294.75	2995.00	2995.25	2995.50	2995.75	2996.00	2996.25	2996.50	2996.15	2997.00	2997.25

0EP 14	V SH	H I H d	SW				
3005 . 00	U.081	u.195	0.908	DEPTH	NSH	HIH	SW
				3012.50	0.045	0.198	1.000
20.05 25	0.009	0.204	0.864	C1=210C	0-040	0.210	776 U
	0.011	0.220	0.791	3013.25	700-0	0.216	0.936
3005-75 3005-75	0.099	0.214	0.806	3013 50	0.069	0.207	0.972
3006-00	0.146	0.224	0.785	3013.75	0.098	0.193	1.000
3006.25	0.157	0.245	0-740	5014.00	0.032	0.200	1.000
3000.50	0.167	0.239	0.779	3014.25	0.303	0.206	0.998
3006.75	0.142	0.225	0.843	3014.50	0.007	0.213	1.000
3007.00	0.039	0.225	0.837	3014.75	0.020	0.213	1.000
3007.25	0.034	0.204	0.893	3015.00	0.014	0.209	1.000
3007.50	0.074	0.169	1.000	3015.25	0.018	0.215	1.000
3007.75	0.075	0.136		3015.50	0.035	0.222	1.000
3008.00	0.061	0-140		3015.75	0.000	0.228	920-()
3008.25	0.043	0.159	1.000	3116.00	U.000	0.228	0.934
3008.50	0.031	0.185		3016.25	0.032	0.227	0.886
3068.75	0.013		0.407	3016.50	0.503	0.170	0.971
3009.00	0.030	0.211	044°	3110.75	1.000	000.0	0.841
3009.25	0.126	0. × US		3017-00	1.000	0.000	0.632
3009.50	0.151	0.190		3017.25	1.000	0.000	0.389
31)09.75	0.129	0.175		3017.50	1.000	000.0	1.000
3010.00	0.126	1.61.0	0. 242	3017.75	1.000	JUC .	1.000
3010.25	0.123	0.195	0.023	3018.00	1.000	00(1.0	1.000
3010.50	0.112	0.197	126.0	3018.25	1.000	0.000	1.000
3010.75	0.109	0.196	000 U	3018.50	1.000	0.000	1.000
3011.00	0.147	0.189	0.907	3018.75	1.000	000.0	1.000
3011.25	0.124	0.189		3019-00	0.788	0.000	1.000
3011.50	0.127	0.190	1-962	3019-25	n.931	000 . 0	1.000
3011.15	0.154	U.186	1.000	3019-50	1.000	0.000	1.000
3012.00	0.146	0.183	1.000	3019.75	1.000	000.0	0.482
3012.25	0.094	U.138	1.000				

N S	1.000 1.000	1.000	0.379	U. 493	Ú - ÓÓ4	0.591	0.396	1.000	1.000	1.000	1.000	1.000	0.455	0.312	1.000	1.000	1.000	1.000	1-000	1.000	1.000	1.000	1-000	1.000	1.000	0.449			U.453	0.512
HILF	00000 0000	0.000	U. 255	0.160	0.107	0.199	0.320	0,000	000.0	0.000	0.000	0.000	0.197	0.107	0.068	U.061	0.052	0.043	0.043	000.0	00000	0.000	0.000	0.000	0.000 n	0.221			0.228	0.211
N S H	1.000	1.000	0.570	0.324	0.549	0.329	0.175	0.523	0.743	0.728	0.829	0.843	0.835	0.719	0.663	0.663	0.713	0.781	0.879	1.000	1.000	1.000	0.959	0.723	0.492	0.467			0.248	0.045
DEPTH	3027-50 3027-75 2028-00	3028-25	3028-50	3028.75	3029.00	51129-25	5U29-50	C/ - 520C	5050 00		5020.50	50.50.75	5051.00	50.51.25	3031.50	51151-75	3032.00	3132.25	3032.50	3032.75	3033.00	5055.25	3033.50	3033.75	3034.00	3034 25			3034.50	3034.75
S N	U.679 0.782	1.000		1.000	0.260	0.289	0.385	0.553	0.669	1.000	1.000	1.000	0-465	0.729	0.756	1_000	1_000	1.000	1_000	1.000	1.000	0.426	0.684	0.639	0.475	0.398	0.363	1.000		
J IHd	0.000 0.000	0000		0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	00000	000 0	0.000	0.000	000-0	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	00000		
ΝSΗ	1.000	0.759		1.000	1.000	1.000	1.000	0.992	1.000	1.000	1.000	1.000	1 - 000	1.000	1.000	1.000	1_000	1.000	1_000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000		
DEPTH	3020.00 3026.25	3020.50	57-J2N5	3021.25	3021.50	3021.75	3022.00	3022.25	3022.50	3022.75	3023.00	3023.25	3023-50	3023.75	3024-00	3024.25	3024-50	3024 75	3025_00	5025.25	3025.50	3025.75	3026.00	3020.25	3026.50	3026.75	3027.00	3027.25		

SUJ	0.944	0.870	9020	074 1	665 0	707 n	0.983	1.030	1.000	1.000	1.000	0.959	0.000	0.870	0.850	0.767					1.000	U-981	0.982	1.000	1.000	0.894	0.881	1.000	1.000	1 000					(int. •)
JIH4	u.125	CH2 n	141.0				0.148	U.139	0.139	0.137	0.140].146	0.159	0.168	0.167	0.150				1 T F C		0-150	0.146	0.142	1].148	0.150	0.146	0.095	0°030	000		000-0		600 U	
ΝSΝ	0.163		000				500°0	0.110	0.120	U.158	0.158	0.134	0.101	0.057	0.063	0.200				190 U			0.217	0.191	0.143	0.148	0.139	0.268	0.548	0.731	0 704	0/9/0			
DEP TH	3042-50							00444.00		51144 - 75	3045.00	51145.25	3045.50	5145.75	3046.00	3046 25				3046 50			5947.00	3()47.25	3047.50	3047.75	3048-00	3048.25	31)48_50	3048.75	3049-00	21140 25		2140-75	
SW	0.632 0.822	0.836	0.787	0.757	0.764	0.790	0.805	0.803	0.840	0.852	0.878	0 884	0_875	0.957				n-997	1.000	0.993	0 922	0.865				0.65		0.869		0.861	0.856	0.905	0.927	0.950	
FILF	0.186 0.172	0.175	0.192	0.204	0.201	0.193	0.193	0.191	0.184	0.181	0_180	173	0.168	154	0 1 35			0.140	0.148	0.148	0.163	0.183						0.191	0.200	0.204	0.208	0.204	0.200	0.195	
VSH	0.006 0.031	0.113	0.045	0.009	0.030	0.059	0.052	0.338	0.059	0.081	0-104	0-140	0.157	0 150	0 15×			761.U	0.206	0.233	0.179	0.119	-				40n•n	0.078	0.00%	0.093	0.077	U.051	0.017	0.039	
DFPTN	3035.00 3035.25	3035.50	3035.75	31136.00	3036.25	3136.50	3.036.75	3037.00	3037.25	3037-50	3037.75	2078 00	31138.25	21128 50	3038 75		00.4000 70.70	51159 65	3039.50	3039.75	3040.00	3040-25					00*0*n0	3040.75	5041-30	3.041.25	3041.50	31141.75	3042.00	31)42.25	

DEPTH	ЧSН	PHIF	SW				
				DEPTH	VSH	PHIF	SW
3050.00	0.082	0.033	1.000				
3050.25	0.629	0.044	1.000	3057.50	0.615	u.025	1.000
3050.50	0.602	0.048	1.000	3057.75	0.636	0.022	1.000
3050.75	J.593	u.∪43	1.000	3058.00	0.088	0.015	1.000
3051.00	0.573	0.139	1.000	3058-25	0.533	0.055	1.000
3051.25	0.595	0.039	1.000				
3051.50	0.599	0.037	1.000				
3051.75	0.596	0.032	1.000				
3052.00	0.635	0.030	1.000	3054.50	0.339	0.111	0.870
3052.25	0_544	0.032	1.000	31158.75	0.364	0.105	0.939
				3059.00	9.463	0.076	1.000
				3059 25	0.537	0.057	1.000
				31159-50	0.540	0.057	1.000
3052.50	0.626	0.034	1.000	3059.75	0.474	0.075	1.000
3052.15	0.616	0.037	1.000	3060.00	0.390	0.108	1.000
3053.00	0.564	0.049	1.000	3060.25	0.288	0.137	1.000
3053.25	0.519	0.065	1.000	3060.50	0.248	0.141	1.000
3053.50	0.486	0.077	1.000	3060.75	0.306	0.114	1.000
3053.75	0.501	0.070	1.000	3()61.00	0.327	0.099	1.000
3054.00	0.505	0.064	1.000	3061.25	0.334	0.101	1.000
3054.25	0.524	0.058	1.000	3061.50	0.393	0.102	1.000
3054.50	0.569	0.062	1.000	3061.75	0.351	0.122	1.000
3054.75	0.494	0.086	0.788	3062.00	0.281	0.138	1.000
3055.00	0.390	0.107	0.899	3062.25	0.257	0.137	0.989
3()55.25	0.411	260.0	0.945	3062.50	0.261	0.117	1.000
3055.50	0.445	0.085	0.994	3062.75	0.346	0.080	1.000
3055.75	0.474	0.070	1.000	3063.00	0.425	0.065	1.000
3056.00	0.490	0.063	1.000	3063-25	0.385	0.093	1.000
3056.25	0.520	0.057	1.000	3063.50	0.345	0.110	1.000
3050.50	0.522	0.057	1.000	3063.75	0.334	0.108	1.000
3056.75	0.557	0.046	1.000	3064 - 00	0.395	0.074	1.000
3.157.00	0.636	0.036	1.000	3064.25	0.495	0.041	1.000
3057.25	0.650	0.028	1.000	3064.50	0.555	0.035	1.000
				3064.75	n.645	0.019	1.000

SW	1.n00	0.977	0.750	0.960	0.997	1.000	1.000	1.000	0.978	0.887	0.939	1.000	1.000	1.000	1.000	1.000	0.998	1.000	1.000	1.000	1.000	1.000	1_000	1.000	1.000	1.000	1.000	1.000	626 ° 0	0.950
PHIF	11.166	0.176	0.182	0.177	0.166	U.152	0.160	J.162	0.174	0.184	0.163	0.131	0.093	0.075	0.110	0.149	ŋ . 158	0.151	0.133	0.108	0.064	0.042	0.064	0.099	0.130	0.138	0.147	0.150	0.164	U . 165
ΝSΗ	0-244	0.237	0.176	148	0_167	0 159	0-149	0.150	0.103	n_170	0.229	0.177	0.163	0.178	0.221	197	0.216	0.232	0.237	0.238	0.351	0.240	0.193	0.209	0.208	0.213	0.234	0.254	0.161	0.169
DEPTH	1070 ED				50100-C20 2022 - C20	36 2602		2014-00		2014-202			2012.50			2024 25	2076.50	20176 75	202 2202	3077.25	30.77.50	z1177.75	3078-00	20128 25	2010 10 10 10 10 10 10 10 10 10 10 10 10	2028 75			2017-62	3079.75
SU	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	0.999	0.967	0.943	0.933	0.928	0.944	0.980	1.000	1.000	1.000	1.000
PHIF	010-0	0.000	0.000	0.014	0.057	J.U86	0.105	0.119	0.120	0.100	0.086	0.081	0.068	0.051	0.056	0.089	0.113	0.141	0.157	0.159	0.165	0.169	0.166	0.161	U.149	0.138	0.122	0.097	U.082	0.124
NSN	0.340	0.928	0.677	0.549	n.433	0.352	0.302	0.259	0.208	0.236	0.248	0.223	197	0.236	0.228	0.191	0.222	0.217	0.221	0.254	0.225	0.166	0.142	0.150	0.133	0.175	0.193	0.262	0.330	0.316
DEP TH	3065-00	50 65 . 25	3065.50	3065.15	5066.00	3u66.25	3000.50	3066.75	3067.00	3067.25	3067.50	3067.75	3008.00	31168.25	3068.50	31168.75	3069.00	3069.25	3009.50	3069.75	3070.00	3070.25	3070.50	3070.75	3971.00	3071.25	3071.50	3071.75	3072.90	3072.25

IF SW		53 0.958	56 1.000	22 1.000	1/ 1.000	23 1.000	29 1.000	38 1.000	47 1.000	56 1.000	40 1.000	1.000	59 1.000	83 1.000	27 1.000	50 0.967	77 0.905	81 0.887	72 0.906	58 0.942	33 1.000	1.000	13 1.000	51 1.000	39 0.896	82 0.888				41 1.000	0.0 1.000	91 1.000	79 1.000
ГНЧ		0.15	0.15	0.12	0.11	0.12	0.12	0.13	0.14	0.15	0.14	0.10	0.06	0.08	0.12	0.16	0.1	0.18	0.17	0.15	0.13	0.10	0.11	0.15	0.18	0.18				0.14	0.10	5G • 0	0.07
H S N		0.183	0.195	0.201	0.178	n.169	0.188	0.198	0.225	0.201	0.179	0.172	0.159	0.130	0.154	0.200	0.182	0.160	0.144	0.153	0.194	0.272	0.373	0.310	0.190	0.200				0.261	0.238	0.205	0.216
DEPTH		3087.50	3087.75	3088.00	3088.25	3088.50	3088.75	3089.00	3089.25	3089.50	3089.75	3090.00	3090.25	3090.50	3090.75	3091.00	3091.25	3091.50	3091.75	3092.00	3092.25	3092.50	3092.75	3093.00	3093.25	3093.50				3093.75	3094.00	3094.25	3094.50
	MS		0°-014	0.923	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	0.995	0.952	0.972	0.955	0.961	0.934	0.970	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	0.974	
	PHIF		n.163	0.141	0.088	0.024	0000	0.000	0.000	0.000	0.000	0.000	0.032	0.104	0.143	0.163	0.167	0.168	.0.176	0.180	0.171	0.161	0.159	0.163	0.165	0.172	0.175	0.177	0.169	0.170	0.181	0.185	
	V SH		0.212	(1.254	0.367	0.495	0.708	0.830	0.838	0.873	0.896	0.809	0.575	0.330	0.204	0.144	0.153	0.154	0.129	0.146	0.169	0.192	0.172	0.186	0.184	0.180	0.165	ŋ . 150	0.158	0.178	0.169	9.168	
	DEPTH		3080.00	3080.25	3020.50	308u.75	3081.00	3081.25	3081.50	3081.75	3082.00	3082.25	3082.50	3082.75	3083.00	31)83.25	31183.50	3083.75	3034.00	3084.25	3084.50	3084.75	3085.00	3085.25	3085.50	3085.75	3486.00	3:180.25	3080.50	3086.75	31187.00	31167.25	

0.402 1.000			0.000 1.000	0.000 1.000	0.000 1.000	0.000 1.000	0.000 1.000	0 0 0 1 0 0 0		0.000 1.000	0.000 1.000 0.000 1.000									0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 1.000 0.000 1.000 0.000 1.000 0.000 1.000 0.000 1.000 0.0000 0.0000 0.0000 0.0000 0.000000										
0-845			0.354	ŋ.911	0.912	J.958	ŋ.942	0.899		0.377	0.940	0.377 0.940 0.898	0.377 0.940 0.898 0.830	0.877 0.940 0.898 0.880 0.880	0.877 0.940 0.898 0.830 1.939 0.939 0.942	0.377 0.940 0.898 0.830 0.830 0.939 0.920	0. 377 0. 940 0. 898 0. 880 1. 939 0. 920 0. 958	0. 377 0. 940 0. 898 0. 880 1. 939 0. 958 0. 958 0. 958	0. 377 0. 940 0. 898 0. 830 0. 939 0. 942 0. 953 0. 953 0. 950 0. 950	0.877 0.898 0.898 0.880 0.988 0.958 0.958 0.958 0.958 0.958 0.952 0.952	0.877 0.840 0.898 0.880 0.880 0.958 0.958 0.958 0.958 0.958 0.958 0.958	0.877 0.8940 0.8940 0.880 0.939 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958	0. 377 0. 940 0. 898 0. 830 0. 928 0. 952 0. 952 0. 952 0. 952 0. 922 0. 922	0. 877 0. 878 0. 880 0. 880 0. 980 0. 952 0. 950 0. 952 0. 950 0. 950 0. 950 0. 950 0. 950 0. 950 0. 950 0. 950 0. 950	0.877 0.898 0.880 0.880 0.988 0.942 0.958 0.958 0.958 0.958 0.950 0.951 0.950 0.951 0.950 0.951 0.952 0.951 0.952 0.951 0.952 0.951 0.952 0.952 0.952 0.951 0.952 0.951 0.952 0.951 0.952 0.9510 0.9510 0.9510 0.9510 0.95100000000000000000000000000000000000	0.877 0.898 0.898 0.880 0.958 0.958 0.958 0.958 0.958 0.958 0.958 0.958 1.000 1.000	0.877 0.878 0.8980 0.880 0.958 0.958 0.958 0.958 0.958 0.957 0.957 0.957 1.000 1.000 1.000	0.877 0.898 0.898 0.880 0.958 0.952 0.958 0.958 0.958 0.958 0.958 1.000 1.000 1.000	0.877 0.898 0.880 0.880 0.988 0.958 0.958 0.958 0.958 0.958 0.958 0.957 1.000 1.000 1.000 1.000	0.877 0.898 0.880 0.880 0.988 0.958 0.958 0.958 0.958 0.958 0.958 0.958 1.000 1.000 1.000 1.000 1.000 1.000
116.1118			3117.75	3113.00	3118.25	3118.50	3118.75	3119.00	2110 25	C 7 8 6 1 1 C	3119.50	3119-50 3119-75	3119.50 3119.75 3120.00	3119.50 3119.75 3120.00 3120.25	3119.50 3119.75 3120.00 3120.25 3120.50	3119.50 3119.75 3120.00 3120.25 3120.25 3120.75	3119.50 3120.00 3120.25 3120.25 3120.25 3121.00	3119.50 3120.00 3120.25 3120.50 3121.00 3121.25	3119.50 3120.00 3120.25 3120.50 3121.25 3121.25 3121.25	3119.50 3120.00 3120.25 3120.25 3121.25 3121.25 3121.25	3119.50 3120.25 3120.25 3120.25 3121.25 3121.25 3121.25 3121.25 3122.00	3119.50 3120.75 3120.25 3120.25 3121.25 3121.25 3121.25 3122.25 3122.25	3119.50 3120.00 3120.25 3120.50 3121.25 3121.25 3121.25 3122.50 3122.50 3122.50	3119.50 3120.00 3120.25 3120.50 3121.25 3121.25 3122.50 3122.50 3122.50 3122.50 3122.50	3120-25 3120-25 3120-25 3121-25 3121-25 3121-25 3122-25 3122-25 3122-25 3122-25 3122-25 3122-25 3122-25	3119-50 3120-00 3120-25 3120-25 3121-25 3121-25 3122-25 3122-25 3122-25 3122-25 3122-25 3122-25	3119.50 3120.00 3120.55 3120.55 3121.25 3121.25 3122.25 3122.25 3122.50 3122.50 3122.55 3122.50 3122.55 3122.55	3119.50 3120.00 3120.25 3120.56 3121.25 3121.25 3122.55 3123.55	3119-50 3120-00 3120-55 3120-55 3121-25 3121-25 3122-55 3122-55 3122-55 3122-55 3122-55 3122-55 3122-55 3122-55 3122-75 3122-75 3122-75 3122-75 3122-75 3122-75	3120-25 3120-25 3120-25 3120-25 3121-25 3121-25 3122-25 3122-25 3122-25 3122-25 3122-25 3122-25 3122-25 3122-25 3122-25 3122-25 3122-25
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140°040	u. 180 0. 119	134	1].144	0.142	U.128					0.118	0.118 0.122	0.118 0.122 0.125	0.118 0.122 0.125 0.123	0.118 0.122 0.125 0.123 0.123	0.118 0.125 0.125 0.123 0.123	0.118 0.125 0.125 0.123 0.123 0.095 0.095	0.118 0.125 0.125 0.123 0.123 0.058 0.058	0.118 0.125 0.125 0.123 0.123 0.058 0.027 0.027	0.118 0.125 0.123 0.123 0.058 0.058 0.058 0.051 0.057 0.005	0.118 0.125 0.125 0.125 0.125 0.058 0.027 0.011	0.118 0.125 0.125 0.125 0.125 0.058 0.027 0.005 0.005 0.005 0.005	0.118 0.125 0.125 0.125 0.095 0.017 0.016 0.005 0005 0005 00000000	0.118 0.125 0.125 0.125 0.095 0.017 0.005 0005 0005 00000000	0.118 0.125 0.125 0.125 0.027 0.005 0.013 0.013 0.005 0005 0005 00000000	0.118 0.125 0.125 0.125 0.005 0.017 0.005 0005 0005 00000000	0.118 0.125 0.125 0.125 0.025 0.027 0.027 0.027 0.018 0.018 0.035 0.056	0.113 0.123 0.123 0.005 0.017 0.005 0.018 0.0000000000	0.113 0.125 0.125 0.125 0.095 0.017 0.006 0.018 0.000 0.018 0.000 0.018 0.000 0.018 0.000 0.018 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.000000	0.113 0.125 0.125 0.125 0.095 0.009 0.009 0.009 0.009 0.009 0.009 0.009 0.009 0.009 0.009 0.009 0.009 0.009 0.009 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.000000	0.112 0.125 0.125 0.125 0.005 0005 0005 0005 0005 0005 0005 000000
0.252	0.244	0.230	0.215	0.265	0.326					0.317	0.317 0.29ô	0.317 0.290 0.248	0.317 0.290 0.248 0.211	0.317 0.296 0.248 0.211 0.223	0.290 0.290 0.211 0.211 0.223 0.223	0.296 0.296 0.271 0.211 0.223 0.237	0.277 0.296 0.278 0.273 0.223 0.361	0.317 0.296 0.278 0.211 0.273 0.223 0.519 0.619	0.272 0.275 0.278 0.278 0.223 0.223 0.237 0.237 0.237 0.237 0.237 0.237 0.237	0.273 0.275 0.275 0.275 0.275 0.223 0.271 0.275 0.271 0.275 0.271 0.275	0.273 0.2750 0.2750 0.2750 00000000000000000000000000000000000	0.317 0.296 0.2737 0.2737 0.2237 0.266 0.2787 0.27877 0000000000000000000000000000000000	0.317 0.296 0.278 0.278 0.273 0.237 0.265 0.265 0.265 0.265 0.265 0.265 0.265 0.265 0.265 0.265 0.265 0.265 0.2788 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.278888 0.27888 0.278888 0.27888 0.278888 0.27888 0.278888 0.278888 0.27888888 0.2788888888 0.27888888888888888888888888888888888888	0.278 0.278 0.278 0.278 0.278 0.278 0.223 0.2788 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.27888 0.278888 0.27888 0.278888 0.27888 0.27888 0.278888 0.278888 0.278888 0.278888 0.2788888 0.27888888 0.278888888 0.27888888888888888888888888888888888888	0.223 0.248 0.273 0.273 0.273 0.223 0.223 0.223 0.223 0.245 0.223 0.245 0.223 0.245 0.253 0.2550 0.2550 0.2550 0.2550 0.2550 0.2550 0.2550 0.2550 0.2550 000	0.278 0.278 0.278 0.278 0.278 0.223 0.263 0.223 0.263 0.263 0.263 0.2710 0.263 0.270 0.270 0.263 0.270 0.263 0.263 0.265 0.2750 0.2750 0.2750 0.27500000000000000000000000000000000000	0.273 0.273 0.273 0.273 0.273 0.273 0.237 0.237 0.237 0.251 0.251 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.253	0.272 0.272 0.272 0.273 0.273 0.273 0.273 0.273 0.273 0.273 0.272 0.253 0.253 0.253 0.253 0.253 0.253 0.253 0.253 0.253 0.253 0.253 0.253 0.272	0.223 0.275 0.275 0.275 0.275 0.275 0.223 0.275 0.223 0.275 0.275 0.275 0.255 0.255 0.255 0.255 0.537 0.537 0.537	0.223 0.272 0.273 0.273 0.273 0.223 0.253
116.03	110.50 110.50	110 75	111 00	111.25	111.50					5111.75	5111.75 5112.00	3111.75 3112.00 3112.25	5111.75 5112.00 5112.25 5112.50	5111.75 5112.00 5112.25 5112.50 5112.75	5111.75 5112.00 5112.25 5112.50 5112.75 3113.00	5111-75 5112-00 5112-25 5112-50 3112-75 3113-00	5111.75 5112.00 5112.25 5112.25 5112.75 313.00 313.25 313.25	<pre>5111.75 5112.25 5112.25 5112.25 3112.25 3113.25 3113.25 5113.25 5113.25</pre>	<pre>5111.75 5112.25 5112.25 5112.25 5112.25 3113.25 3113.25 3113.25 3113.25 3113.75</pre>	<pre>%111.75 %112.00 %112.25 %112.75 %112.75 %112.75 %112.75 %113.50 %114.00 %114.25</pre>	<pre>5111.75 5112.25 5112.25 5112.25 3113.25 3113.25 3113.25 3114.25 5114.25 5114.25</pre>	<pre>\$111.75 \$112.00 \$112.25 \$112.25 \$112.25 \$113.25 \$113.25 \$113.25 \$114.25 \$114.25 \$114.25 \$114.25</pre>	<pre>5111.75 5112.25 5112.25 5112.25 5112.25 3113.25 3114.25 5114.25 5114.25 5114.25 5114.25 5114.25 5114.75 5115.10 5</pre>	<pre>%111.75 %112.25 %112.25 %112.25 %112.25 %112.25 %113.25 %114.25 %114.25 %114.25 %115.25 %115.25 %115.25 %115.25 %115.25</pre>	<pre>%111.75 %112.25 %112.25 %112.25 %112.25 %112.25 %113.50 %114.25 %114.25 %115.25 %115.25 %115.25 %115.25</pre>	<pre>%111.75 %112.25 %112.25 %112.25 %112.25 %112.25 %112.25 %114.00 %114.25 %114.25 %114.25 %115.25 %115.25 %115.25 %115.25</pre>	5111-75 5112-25 5112-25 5112-25 5112-25 5112-25 5113-25 5113-25 5114-25 5115-50 5115-50 5115-50 5115-50 5115-50 5115-50 5115-50 5115-50 5115-50	<pre>%111.75 %112.25 %112.25 %112.25 %112.25 %112.25 %113.20 %113.25 %115.25 %115.25 %115.25 %115.25 %115.25 %115.25 %115.25 %115.25 %115.25 %116.00</pre>	3111.75 3112.25 3112.25 3112.25 3112.25 3113.25 3114.25 3115.25 3115.25 3115.25 3115.25 3115.25 3115.25 3115.25 3115.25 3115.25 3115.25 3115.25 3115.25	5111.75 5112.25 5112.25 5112.25 5112.25 5113.50 5114.25 5115.50 5115.50 5115.50 5115.50 5115.50 5115.50 5115.50 5115.50 5115.50 5115.50 5116.25 5116.25

SW	1.000	1 000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.600	1.001	1.000
PHJF	000-0	0,000 0	000-0	0 • 0 0 5	0.000	0.000	0.100	0.000	000.0	000.0	0.000	0.000	000.0	0000	0.000	0.006	0.000	0.000	0.000	0.000	0.000	0.000	0.000	000.0	0.000	00000	0.000	000.0	0.000
NSH	0.954	0-770 1	0.967	0-344	0.908	1.000	0.966	0.921	n_868	0.898	0.924	0.384	0.900	0.912	0.888	0.912	1.000	1.000	1.000	1.000	1.000	0.995	1.000	1.000	1.000	1.000	1.000	1.000	1.000
DEPTH	3132.50	C/ 2/2/C	3133 25	3123.50	31 33.75	3134.00	3134.25	3134.50	3134.75	3135.00	3135.25	3135.50	3135.75	3130.00	3136.25	3136.50	3136.75	3137.00	3137.25	3137.50	3137.75	3138.00	3138.25	3138.50	3138.75	3139.00	3139.25	3139.50	3139.75
SW	1.000	1 - 000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	0 999	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000
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VSH	1.000 1.000	1.000	1.000	1.000	1.000	1.000	1.000	1.000	1-000	1 000						100-11	124 - 0	0 935	104.0			0 04 /	- 204 - 205		1.000	1.000	1.000	1.000	U- 902
DEP TH	3125 00 3125 25	3125.50	3125.75	5120.UU	C7 07 1 C	51 20.50	CJ 0710	3127.25	1	3127.75	3128 00	3128.25	3128_50	312× 75	3120 00	3120 25		3129.75	3130 00	31 30 25 31 35	3130 50	3130.75	21 21 21			JC•1710		00-2010 2120 35	

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	STI	ATØIL DATA	PROCESSING	CENTER	3			
PLOT MADE BI	:	30-3-3HB			DATE:	11.39.50	18 NÖVEMBER	1983
DEPARTMENT	:	LET/BER						
ADDRESS/BØX	:	HER						
ØTHER INFØ	:	-						

GRAPHICAL LOG-PRESENTATION

WELL : 30-3-3HB DEPTH INTERVALL :2960.00-3150.00 (METER)

ENGINEER :HB SCALE 1:200

DATE: 11.39.56 18 NOVEMBER 1983

. STRATIGRAPHY (REF. RKB=22M)

PETROPHYSICAL EVALUATION	= =		
NPUT PHRHMETERS 2950M-3034M RKB) RW=0.070 RMF=0.091 RSH=10.0 PHINSH=0.38 TEMP M=2 N=2 R=1 RH0BSH=2.57	= 116 (DEG C)		
TATISTICS			
INIERVHE (BHENI+UKHKE FM.)	AVG VSH		
		HVG PHIF	AVG SW
GRØSS THICKNESS	0.44 0.16	0.10 0.17	AVG SW 0.94 0.93
GRØSS THICKNESS 138.00 M NET SAND (VSH<0.40 PHIF>0.12) 56.50 M NET PAY (VSH<0.40 PHIF>0.12 SW<0.60)	0.44 0.16	0.10 0.17	AVG SW 0.94 0.93
GRØSS THICKNESS	0.44 0.16 AVG VSH	AVG PHIF	AVG SW D.94 D.93 AVG SW
GRØSS THICKNESS 138.00 M NET SAND (VSH<0.40 PHIF>0.12) 56.50 M NET PAY (VSH<0.40 PHIF>0.12 SW<0.60)	0.44 0.16 AVG VSH 0.61 0.11	AVG PHIF 0.10 0.17 AVG PHIF 0.10 0.20	AVG SW 0.94 0.93 AVG SW 0.88 0.91
GRØSS THICKNESS 138.00 M NET SAND (VSH<0.40 PHIF>0.12) 56.50 M NET PAY (VSH<0.40 PHIF>0.12 SW<0.60)	0.44 0.16 AVG VSH 0.61 0.11	O. 10 O. 17 AVG PHIF O. 10 O. 10 O. 20	AVG SW 0.94 0.93 AVG SW 0.88 0.91
GRØSS THICKNESS 138.00 M NET SAND (VSH<0.40 PHIF>0.12) 56.50 M NET PAY (VSH<0.40 PHIF>0.12 SW<0.60)	0.44 0.16 AVG VSH 0.61 0.11 AVG VSH	AVG PHIF 0.10 0.17 AVG PHIF 0.10 0.20 AVG PHIF	AVG SW 0.94 0.93 AVG SW 0.88 0.91 AVG SW
GRØSS THICKNESS 138.00 M NET SAND (VSH<0.40 PHIF>0.12) 56.50 M NET PAY (VSH<0.40 PHIF>0.12 SW<0.60)	0.44 0.16 AVG VSH 0.61 0.11 AVG VSH 0.12 C.11	AVG PHIF 0.10 0.17 AVG PHIF 0.10 0.20 AVG PHIF 0.17 0.17	AVG SW 0.94 0.93 AVG SW 0.88 0.91 AVG SW 0.88 0.91
GRØSS THICKNESS 138.00 M NET SAND (VSH<0.40 PHIF>0.12) 56.50 M NET PAY (VSH<0.40 PHIF>0.12 SW<0.60)	0.44 0.16 AVG VSH 0.61 0.11 AVG VSH 0.12 C.11	AVG PHIF 0.10 0.17 AVG PHIF 0.10 0.20 AVG PHIF 0.17 0.17 0.17	AVG SW 0.94 0.93 AVG SW 0.88 0.91 AVG SW 0.88 0.89

