



# statoil

PETROPHYSICAL REPORT  
RFT REPORT  
WELL 6610/7-1  
BY LET - HARSTAD  
OCTOBER 1983

ENGINEER: JAN RAFDAL

**Den norske stats oljeselskap a.s**

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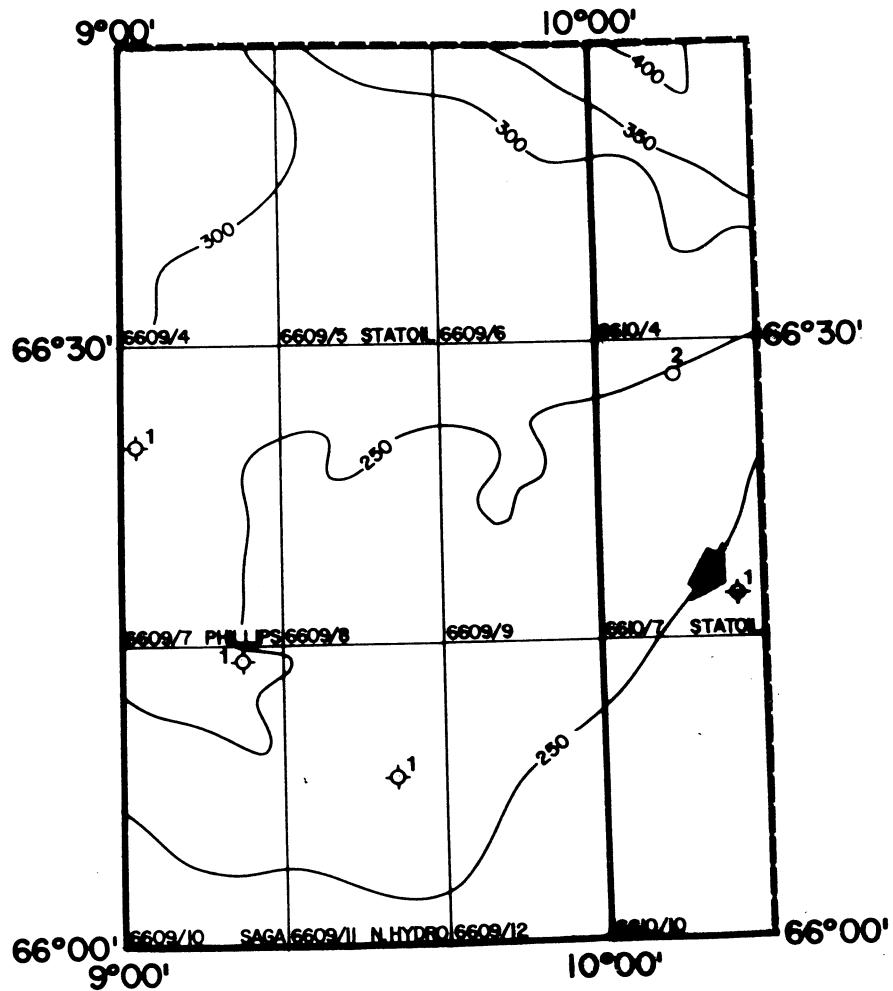
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GENERAL WELL DATA

License : PL 084  
Wildcat well : 6610/7-1  
Location : N  $66^{\circ} 17' 32,3''$ , E  $10^{\circ} 16' 52,5''$   
Spudded : 18. April 1983  
Rig released : 19. June 1983  
Rig : Neptuno Nordraug  
KB-elevation : 25m  
Water depth : 265m  
Total depth : 3333m  
Objective : Jurassic sandstones  
Operator : Statoil  
Partners : Agip, Elf  
Status : Plugged and abandonned



### Introduction

6610/7-1 was the first well drilled on TRÆNABANKEN. The main objective was to test JURASSIC sandstones for hydrocarbon accumulations. The well was however dry and was drilled to a total depth of 3333m RKB in rocks of Triassic age. The objective of the report is to evaluate the reservoir properties of Jurassic and Triassic formations using well logs, RFT-measurements and conventional core data.

### SUMMARY

The evaluation shows the well to be waterbearing. Some residual oil has been found on the core and can also be evaluated from the logs.

The petrophysical properties have been summarized in the table below:

| Interval             | 2650-2915 | 2915-3333 |
|----------------------|-----------|-----------|
| Net sand (m)         | 122.5     | 177.75    |
| Average porosity (%) | 18.5      | 16.5      |
| Net/Gross ratio      | 0.462     | 0.425     |

### STRATIGRAPHY

The descriptions of depositional environments and lithologies are based on log interpretations, paleontology and cuttings/core descriptions.

| INTERVAL                                 | DEPOSITIONAL ENVIRONMENT/LITHOLOGY                                                  | REMARKS                                    |
|------------------------------------------|-------------------------------------------------------------------------------------|--------------------------------------------|
| 2658m-2679m<br>(Toarcian sand)           | Marine sandstone. Offshore, very shallow inner shelf (near shore in uppermost part) | coarsening up sandstone                    |
| 2679m-2746m<br>(L. Jurassic shale)       | Shallow marine claystone.<br>(Possible lagoonal in parts)                           | Silty claystone                            |
| 2746m-2854m<br>(L. Jurassic sand)        | Littoral and brackish water sandstones with abundant terrestrial debris             | several coarsening up units                |
| 2746m-3152m<br>(L. Jur. coal sequ.)      | Coastal plain coal swamp association, non marine to shallow brackish environment    | clean sands interbedded w/shale-sand coals |
| 3152m-3234m<br>(Triassic grey beds)      | Same depositional environment as above, but without coal development                | interbedded sands and shales               |
| 3234m-3333m(T.D.)<br>(Triassic red beds) | None marine to deltaic environment, close to shore                                  | interbedded sands and shales               |

### LOG QUALITY

The overall quality of the logs is good. GR calibrations on ISF/SONIC run No. 5 is out of range, and this explains the relative high GR-readings on the final runs.

LOGS RUN ON 6610/7-1

| Name                     | Run | Interval      |
|--------------------------|-----|---------------|
| ISF/SONIC-SP-GR          | 1   | 353 - 813     |
| ISF/SONIC-SP-GR          | 2   | 801 - 1258    |
| ISF/SONIC-SP-GR          | 3   | 1251 - 2112,5 |
| ISF/SONIC-MSFL-SP-CAL-GR | 4   | 2098,0- 2921  |
| ISF/SONIC-MSFL-SP-CAL-GR | 5   | 2915 - 3328   |
|                          |     |               |
| LDL-PEF-CAL-GR           | 1   | 353 - 814     |
| LDL-PEF-CAL-GR           | 2   | 801 - 1259    |
| LDL-PEF-CAL-GR           | 3   | 1251 - 2108   |
| LDL-CNL-PEF-CAL-NGS      | 4   | 2098 - 3329   |
|                          |     |               |
| HDT                      | 1   | 801 - 1260    |
| HDT                      | 2   | 1251 - 1920   |
| S-HDT                    | 3   | 2098 - 3329   |
|                          |     |               |
| CST                      | 1   | 1583 - 2108   |
| CST                      | 2   | 1260 - 1570   |
| CST                      | 3   | 3053 - 3325   |
| CST                      | 4   | 2876 - 3045   |
| CST                      | 5   | 2850 - 3000,1 |
| CST                      | 6   | 2470 - 2876   |
| CST                      | 7   | 2117 - 2450   |
|                          |     |               |
| CBL-VDL-GR               | 1   | 550 - 1245    |
| CBL-VDL-GR               | 2   | 290 - 2092    |
|                          |     |               |
| RFT-GR                   | 1   | 1293,6- 1304  |
| RFT-GR                   | 2   | 2659 - 3111   |
|                          |     |               |
| VSP/CHECKSHOTS           |     | 315 - 3370    |

Input parameters

Input parameters are based on physical measurement and empirical relations.

Formation water resistivity

The salinity of the formation water seem to be different above and below the coaly sequence (2915-2970m RKB) :

1. Depth 2748m (ISF/SONIC # 4)  
SP= -26mV Temp= 81.1°C  
Rmf= 0.097 ohm m at 81.1°C  
Rw= 0.052 ohm m ~ 55 000 ppm NaCl
  
2. Depth 3295m (ISF/SONIC # 5)  
SP= -45mV Temp= 92.8°C  
Rmf= 0.097 ohm m at 92.8°C  
Rw= 0.03 ohm m ~ 95 000 ppm NaCl

This can be verified with the RFT plots which indicates two water gradients and different pressure regimes above and below the coaly shale sequence.

Mud filtrate density

A mud filtrate density of 1.01 g/cc was used.

Shale parameters

Shale parameters are based on crossplots and visual inspection of the logs:

| Interval                        | 2650-2915 | 2915-3333 |
|---------------------------------|-----------|-----------|
| Density (LDT) (g/cc)            | 2.60      | 2.6       |
| Neutron porosity (frac)         | .35       | .35       |
| GR <sub>sand</sub> (API units)  | 40        | 40        |
| GR <sub>shale</sub> (API units) | 120       | 120       |
| R <sub>shale</sub> (ohm m)      | 5         | 11 .      |

Log corrections

No corrections was made to the log measurements.

Computations

Shale volume was calculated using the GR with the following parameters: GR<sub>sand</sub> = 40    GR<sub>shale</sub> = 120

Porosity was calculated from a combination of LDT and CNL with a standard sandstone model.

Watersaturation was calculated with the "Indonesia"  
(Schlumberger) equation:

$$\frac{1}{\sqrt{RT}} = \left[ \frac{V_{shale} \left( 1 - \frac{V_{shale}}{2} \right)}{\sqrt{R_{shale}}} + \frac{\phi^{m/2}}{a R_w} \right] S_w^{n/2}$$

Where:  
Sw = water saturation  
Rt = RILD  
 $V_{shale}$  = Shale volume  
 $R_{shale}$  = Resistivity of shale  
 $\phi$  = Porosity  
a = lithology factor (=1)  
m = cementation exponent (=2.15)  
n = saturation exponent (=2)  
Rw = formation water resistivity

#### Core measurements

Three cores were cut in the evaluated interval (core no. 2,3 and 4). The cores have been shifted to fit the log depth using GR from core and porosity. The enclosed core summary log (2650-2750m RKB) shows core data on reported depth and shifted depth compared to log results.

Comparison of core and log porosity

The porosity from logs and core has been compared in the cleanest part of the cored interval:

| <u>INTERVAL</u> | <u>LOG</u> | <u>CORE</u> |
|-----------------|------------|-------------|
| 2662-2675       | .171       | .169        |

Discussion

A relative high hydrocarbonsaturation is calculated in the shales and especially in the coaly/organic rich sequence. The formation is regarded as waterbearing which is proved by the RFT. High hydrocarbonsaturation in shales is also common further north at Tromsøflaket. This may be due to several reasons i.e.: we do not know the petrophysical parameters ( $m$ ,  $n$ ,  $a$ ) for the shales to correctly calculate the saturation or the saturation of hydrocarbons in the shales may be correct.

RFT-SUMMARY

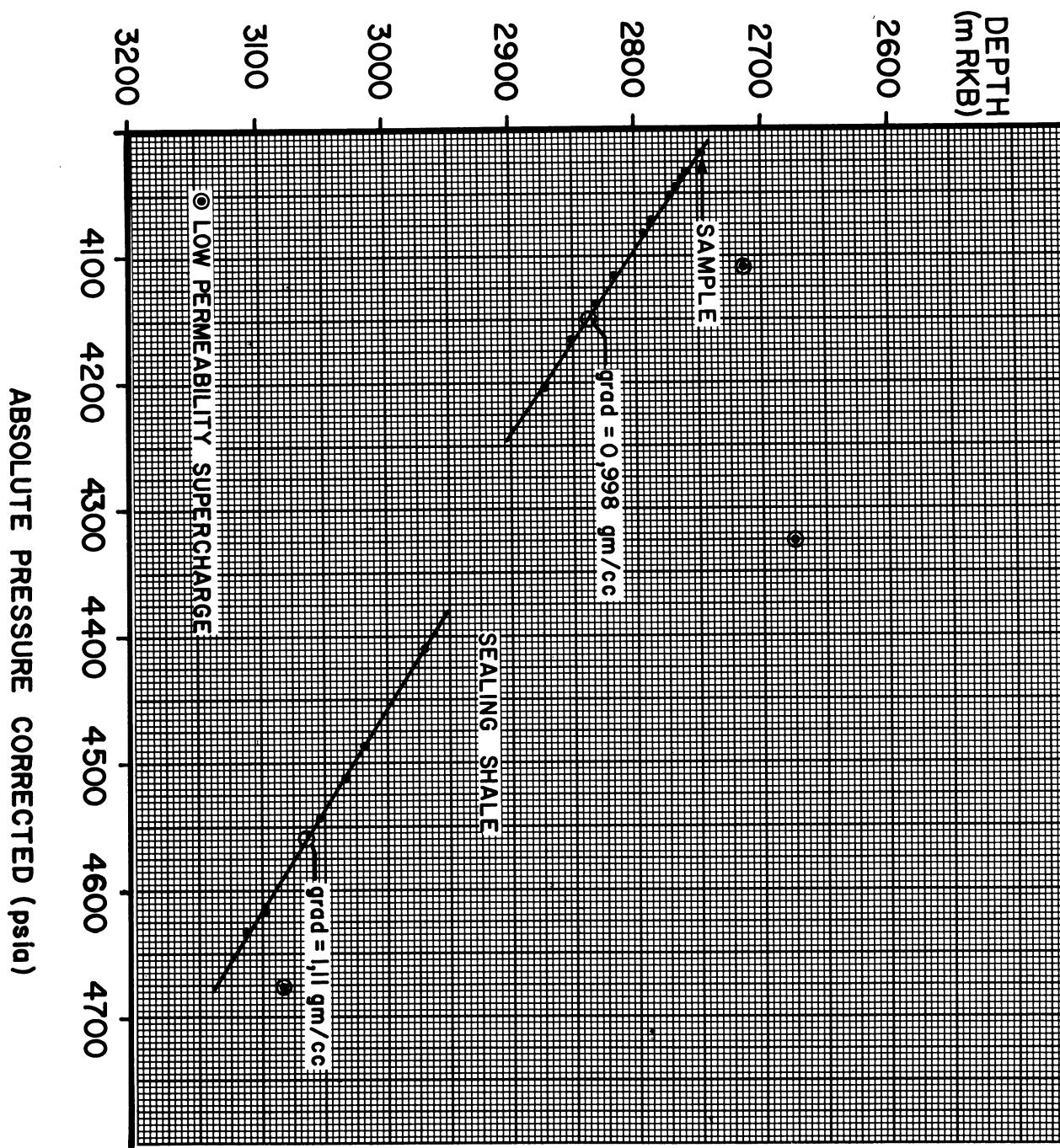
21 pressure readings were measured from 2672.5 to 3110 m RKB. One segregated sample was taken at 2748m. No pressures were measured below 3110m due to operational problems of the tool. The sand from 2652-2675m was very tight, hence the sample was taken lower.

The RFT-plot indicates two water gradients in the well (see plot).

The sample consisted of mud filtrate:

|          | 2 3/4 gal | 1 gal | mudfiltrate | .     |
|----------|-----------|-------|-------------|-------|
| cl-, ppm | :         | 11000 | 10500       | 13000 |
| ca+, ppm | :         | 160   |             | 260   |
| density  | :         |       | 1.015       |       |
| ph       | :         |       | 7.8         | 10.5  |

## 6610/7-I RFT. MEASUREMENTS



## 6610/7-1 REPEAT FORMATION TESTER

RUN NO. 2

| DEPTH<br>m RKB | MEASURED PRESSURE CORRECTED (bara) | HYDROSTATIC<br>BEFORE | FORMATION<br>PRESSURE | HYDROSTATIC<br>AFTER | REMARKS      |
|----------------|------------------------------------|-----------------------|-----------------------|----------------------|--------------|
| 2659           | 322.3                              | -                     | 322.3                 | 322.3                | tight        |
| 2661           | 322.5                              | -                     | 322.5                 | 322.5                | "            |
| 2665           | 322.9                              | -                     | 322.9                 | 323.8                | supercharge  |
| 2672.5         | 323.8                              | 298.3                 | 323.8                 | 328.9                |              |
| 2715           | 329.3                              | 283.4                 | 328.9                 |                      |              |
| 2748           | 332.8                              | 277.0                 | 332.8                 | 332.8                | very good    |
| 2759           | 333.9                              | 278.1                 | 334.1                 | 334.1                | good         |
| 2763           | 334.6                              | 278.5                 | 334.6                 | 334.6                | good         |
| 2766           | 334.8                              | 278.8                 | 332.9                 | 332.9                | very good    |
| 2772           | 335.5                              | 279.4                 | 335.6                 | 335.6                | "            |
| 2787.5         | 337.6                              | 280.9                 | 337.4                 | 337.4                | "            |
| 2794           | 338.1                              | 281.5                 | 338.2                 | 338.2                | "            |
| 2817.5         | 341.4                              | 283.9                 | 341.0                 | 341.0                | "            |
| 2832.5         | 342.6                              | 285.4                 | 342.8                 | 342.8                | good/fair    |
| 2850           | 344.9                              | 287.2                 | 344.9                 | 344.9                | good         |
| 2874           | 348.0                              | 289.7                 | 347.7                 | 347.7                | "            |
| 2967           | 358.7                              | 303.9                 | 358.7                 | 358.7                |              |
| 3017           | 364.9                              | 309.5                 | 364.6                 | 364.6                | good/fair    |
| 3032.5         | 366.7                              | 311.2                 | 366.7                 | 366.7                | "            |
| 3051           | 368.9                              | 313.2                 | 368.7                 | 368.7                | "            |
| 3080.5         | 372.2                              | 322.5                 | 372.1                 | 372.1                | supercharge  |
| 3095           | 373.9                              | -                     | -                     | -                    | seal failure |
| 3097           | 374.0                              | 318.2                 | 374.0                 | 374.0                | good         |
| 3110           | 375.4                              | 319.4                 | 375.5                 | 375.5                | fair         |
| 3135           | 378.9                              | -                     | 378.5                 | 378.5                | seal failure |
| 3136           | 378.5                              | -                     | -                     | "                    | "            |
| 3142           | 379.3                              | -                     | -                     | "                    | "            |
| 3169           | 382.5                              | -                     | -                     | -                    |              |
| Sample:        |                                    |                       |                       |                      |              |
| 2748           | 333.0                              | 277.2                 | 332.8                 | 332.8                | very good    |

6610-7-1 RHOB VS PHIN

111  
15822754332323322111  
11 11167487517612956443315972753111

-0.050 0.050 0.150 0.250 0.350 0.450

S6610-7-1 PHIN DEPTH: 2650.00 2915.00 TOTAL: 1055  
0.2266 Y.AU: 2.4452

LOTTED BY: JRA

6610-7-1 RHOB US PHIM

-0.050 0.050 0.150 0.250 0.350 0.450

56610-7-1 PHIN DEPTH: 2915.00 3330.00 TOTAL: 1587  
0.2283 Y.AU: 2.4691

• PLOTTED BY : JRA







6610-7-1 RHOB US GR

1234442223334455223312232222331  
9874870861684802771981156934128415532

+ + 348123 5782 112 1+ 1 + 1 + 1  
 + + 3244256A465122 1+1 1 11+1 +  
 + + 2611134718A1 311+ 1 11 +  
 + + 1456A13289578431 1 + 11 +  
 2.400 -++++++1+4252252245463+1+++1+++++1+++++1+++++1  
 + + 1 111 121429654413 1 11+ 1 +  
 + + 1 +113436851+ 11 + +  
 + + 2 + 1468A4535 11 1 +  
 + + 11324691522 1 11111453 +

[View Details](#) [Edit](#) [Delete](#)

**0.000      30.000      60.000      90.000      120.000      150.000**

DEPTH: 2650.00 2915.00 TOTAL: 105  
2.445

6610-7-1 RHOB VS GR

3345345446565343332111111122112112122223  
93829259114324122012136877981795696697889

693820259114324128912138811382195535510000  
\*\*\*\*\*1\*\*\*\*\*1\*\*\*\*\*1\*\*\*\*\*1\*\*\*\*\*1\*\*\*\*\*1\*\*\*\*\*3

+ 136465784267A962333 1 1 + 11 1 +  
 + 11AAA9AAA937A75361 231 1 1 1 + 1 1 +  
 + 4135AA3AA886499634 211 112 1+ 2 1 11+  
 2.400 +++++++1+A4922A5948A44854121112++++1++++++13111+  
 + 54516545A7A4464412 +21 2 1+11 1 213+  
 + 12221 332645A33346 1412 111 121+ 1 1 +  
 + 1+ 1 3324226425413+312542121+ 12 1112+  
 + +111 2 41 32353123 221 1 14112 212+

silver pieces coins coins coins 120 coins 150 coins

0.000 30.000 60.000 90.000 120.000 150.000

: 96610-7-1 GR DEPTH: 2915.00 3330.00 TOTAL: 125  
: 78.5868 Y.AU: 2.4450

PLOTTED BY: JR

8610-7-1 PHIN VS GR  
 3345345446565343321121112221221121322223  
 6938202591143341221143308992907056946078895  
 0.500 -+++++  
 + + + 1 1 1 11 1+1 1 11+10  
 + + + + 11 1 111 1+1 +8  
 + + + + 1 + 1 11+1 1 +6  
 + + + + + 1 + +1 1 1 +3  
 + + + + + + 1 + 1 2 12+7  
 + + + + + + + 111 2 +5  
 + + + + + + + 2 +2  
 + + + + + + + 1 + 2 1 +4  
 + + + + + + + 1 +1 1 +3  
 0.400 -+++++  
 + + + + + + + 121 11 +6  
 + + + + + + + 11 141 + 11 13+14  
 + + + + + + + 1 1 1 11 212 +10  
 + + + + + + + 1 + 2 11 122+10  
 + + + + + + + 1 113 2 1 +11  
 + + + + + + + 1 1 +12 1121 4+14  
 + + + + + + + 11 113 1 34 +19  
 + + + + + + + 11 111 1 211225+19  
 + + + + + + + 1111 111 113 11+16  
 0.300 -+++++  
 + + + + + + + 1 1 1211 25414+25  
 + + + + + + + 11 2 +114211114+20  
 + + + + + + + 1 1 211 142211111 1212 +26  
 + + + + + + + 11 2 113+ 2221 121+20  
 + + + + + + + +111 22 15 322212+25  
 + + + + + + + 1 1 1 2 241+21 11221 +23  
 + + + + + + + 11 123 1+11 221 121 17 11 +32  
 + + + + + + + 1 1 1121 211 + 12 11 2 1 11 +21  
 + + + + + + + 1112 1 2113 313 +12 34 121 4 2 +40  
 0.200 -+++++  
 31+1+1+21312322214112+221++1131+11++1+1+48  
 4335231 213326114331221232 321 1 11 +72  
 4542112256773446663221 32321 22+ 1 +99  
 1375611457AAA62562211+3111111 1+ 11 1 +123  
 234544559459888778331 131212 11 + 1 2 2 +129  
 22698A9AA876AAA58453212421 1 + 1 +161  
 2336AA5AA67A7861121 3 1 1 11 + +117  
 3255335447464 41 11+ + +62  
 +1142A8 5 14 11 2 +1 + +41  
 + + 13 13 + 1 11 1+ 1 + +13  
 0.100 -+++++  
 + 11 1 1 1 + + +5  
 + + 1 1 + + + +2  
 + 1+ 1 + + + +2  
 + + 1 + + + +1  
 + 1+ + + + + +3  
 + + 21 + + + +  
 + + + + + + +  
 + + + + + + +  
 0.000 -+++++  
 0.000 30.000 60.000 90.000 120.000 150.000  
 GR DEPTH: 2915.00 3330.00 TOTAL: 1308  
 56610-7-1 Y.AU: 0.2091  
 78.7364

S6610-7-1 GR DEPTH: 2650.00 2915.00 TOTAL: 1058  
81.3275 Y.AU: 80.7867

LOTTED BY: JRE

0.000 30.000 60.000 90.000 120.000 150.000  
GR  
56810-7-1 DEPTH: 2915.00 3330.00 TOTAL: 1319  
78.9718 Y.AV: 76.3552

LOTTED BY : JRA

96610-7-1 GR DEPTH: 2650.00 2915.00 TOTAL: 1053  
81.1460 Y.A.U: 3.0579

LOTTED BY: JRA

0.000 90.000 60.000 90.000 120.000 150.000  
GR 610-7-1 DEPTH: 2915.00 3330.00 TOTAL: 11F  
1.2497 Y.AV: 2.5473

LOTTED BY: JRA