

Denne rapport  
tilhører

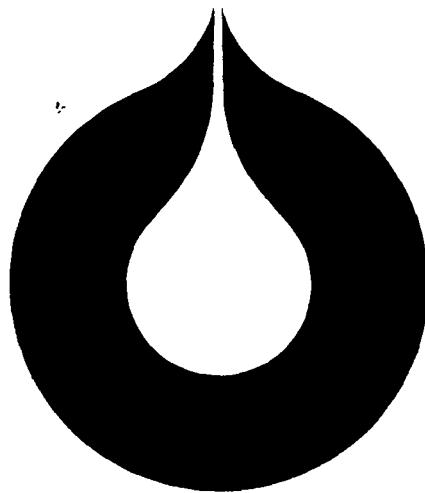


**L&U DOK.SENTER**

L.NR. 30284070019

KODE WELL 31/2-5 NC 53

Returneres etter bruk



**statoil**

Quick-look evaluation

Well: 31/2-5

Operasjonsteknologi - Stavanger

Statoil - January 1981

Engineer: J.I. Skagen

**Den norske stats oljeselskap a.s**

Quick-look evaluation

Well: 31/2-5

Operasjonsteknologi - Stavanger

Statoil - January 1981

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## Preliminary petrophysical evaluation of 31/2-5

Two methods have been applied for this evaluation, the shaly sand method by using the Nigeria-equation and the Waxman - Smith method by using the cation - exchange - capacity theory.

The main problem with this evaluation is the high mica-content which effects the GR-log and the grain density.

No shale was observed in this reservoir and therefore the shale volume is set to zero.

Three zones of interest have been evaluated, the gas zone from 1535 to 1579 m RKB, the oil zone from 1579 to 1602 m RKB and the water zone from 1602 to 1610 m RKB.

Most of the parameters used for the evaluation are based on the 31/2-1 well.

The plots needed for the Waxman - Smith evaluation are based on 31/2-1 data.

## INPUT DATA

LOGS:           Laterolog Deep                             (RLLD)  
              Laterolog Shallow                             (RLLS)  
              Microspherical Focused Log                     (RXO)  
              Formation Density Log                         (RHOB)  
              Compensated Neutron Log                         (PHIN)  
              Induction Log Deep                             (RILD) (RT)  
              Gamma Ray Log                                     (GR)

Core data:      No core data is used.

## EVALUATION

The evaluation has been devided into the intervals:

1535 - 1579 m RKB ; gas zone

1579 - 1602 m RKB ; oil zone

1602 - 1610 m RKB ; water zone

The MSFL-log is used as RXO log. The RT log is evaluated by using:

$$RT = 1.7 \text{ RLLD} - 0.7 \text{ RLLS} \text{ in h.c. zones}$$

$$RT = \text{RILD} \text{ in water bearing zones}$$

The shale content in this reservoir sand is very small and VSH is set to zero.

Micaceous sandstones: GR > 53,  $\delta G = 2.67$

Clean sandstones:      GR < 53,  $\delta G = 2.65$

Mud filtrate resistivity:  $Rmf = 0.07$  (60 000 ppm)

Formation water resistivity:  $Rw = 0.06$  (70 000 ppm)

Formation temperature:   T = 125°F ?

Gas density:            0.12

Oil density:            0.7

Water density:          1.045

Mud filtrate density:   1.035

The final porosity (PHIF):

$$\phi = \frac{\gamma_G - \rho_{\text{HOB}}}{\gamma_G - \gamma_{f1}}$$

for all three zones, with different fluid densities. The fluid densities are found from several steps of SXO calculations ( $F = 8.5$ ).

$$SXO = \sqrt{\frac{F \cdot Rmf}{RXO}}$$

Cut off values applied to this well:

$\phi > 24\%$  (i.e.  $k = 1 \text{ md}$ )

$V_{sh} < 40\%$  (unimportant,  $V_{sh} = 0$ )

$S_w > 65\%$

#### Nigeria formula exponents

Lithology factor (a) = 0.62

Cementation exponent (m) = 2

Saturation exponent (n) = 2

#### Waxman - Smith exponents

B-factor: 9.0 at  $125^{\circ}\text{F}$  6.4 @  $101^{\circ}\text{F}$

Saturation exponent (n) = 2

$F^* = A \cdot (\text{PHIF}) \text{ EXP } (-B)$

A = .532618

B = -0.188956

$Qv = C (\text{PHI}) \text{ EXP } (-E)$

C = .001495 0.0004

E = -3.748 4.9

(see attached plots of data from 31/2-1).

Shaly sand evaluation

Nigeria equation

## STATISTICO

FIELD: . . . . . BLOCK 31/2  
 WELL: . . . . . 31-2-5  
 DATE: . . . . . 13.05.50 6 JANUARY 1981  
 ENGINEER: . . . . . JIS

DEPTH INTERVAL: . . . 1535.00 TO 1602.00

## APPLIED CUTOFFS:

.	MWH:	GREATER THAN	0.40
.	PHIF:	LESS THAN	0.24
.	SW:	GREATER THAN	0.65

## TOTAL DEPTH

THICKNESS: . . . . . 67.000  
 AVERAGE . . . . . PHIF . . . . . 0.306  
 AVERAGE . . . . . MWHALE . . . . . 0.000  
 AVERAGE . . . . . SW . . . . . 0.015  
 M.AVERAGE . . . . . SW \* . . . . . PHIF . . . . . 0.015  
 AVERAGE . . . . . ICH . . . . . 0.395  
 VOID VOLUME: . . . . . PHIF . . . . . 19.069  
 HC VOID VOLUME . . . . . ICH . . . . . 18.789  
 REC HC VOID VOLUME (IHP) . . . . . 17.611  
 MWV HC VOID VOLUME . . . . . 1.178

## NET PAY

THICKNESS: . . . . .	57.250	Total h.c. zone
AVERAGE . . . . . PHIF . . . . .	0.306	1535 - 1602 m
AVERAGE . . . . . MWHALE . . . . .	0.000	
AVERAGE . . . . . SW . . . . .	0.015	
M.AVERAGE . . . . . SW * . . . . . PHIF . . . . .	0.014	
AVERAGE . . . . . ICH . . . . .	0.395	
VOID VOLUME: . . . . . PHIF . . . . .	17.493	
HC VOID VOLUME . . . . . ICH . . . . .	17.242	
REC HC VOID VOLUME (IHP) . . . . .	16.154	
MWV HC VOID VOLUME . . . . .	1.038	

## NET SPHID

THICKNESS: . . . . . 57.250  
 AVERAGE . . . . . PHIF . . . . . 0.306  
 AVERAGE . . . . . MWHALE . . . . . 0.000  
 AVERAGE . . . . . SW . . . . . 0.015  
 M.AVERAGE . . . . . SW \* . . . . . PHIF . . . . . 0.014  
 AVERAGE . . . . . ICH . . . . . 0.395  
 VOID VOLUME: . . . . . PHIF . . . . . 17.493  
 HC VOID VOLUME . . . . . ICH . . . . . 17.242  
 REC HC VOID VOLUME (IHP) . . . . . 16.154  
 MWV HC VOID VOLUME . . . . . 1.038

## NET : GROSS RATIO

HNETPAY : HGRDCC (IHP) = 0.85448  
 HNETPAY : HGRDCC (IHP) = 0.95448  
 HNETPAY : HMETIAND = 2.06000

## STATISTICS

FIELD: . . . . . BLOCK 31/2  
 WELL: . . . . . 31-2-5  
 DATE: . . . . . 13.16.84 6 JANUARY 1981  
 ENGINEER: . . . . . JIS

DEPTH INTERVAL: . . . 1535.00 TO 1579.00

## APPLIED CUTOFFS:

.	VSH:	GREATER THAN	0.40
.	PHIF:	LESS THAN	0.24
.	SUM:	GREATER THAN	0.65

## TOTAL DEPTH

THICKNESS: . . . . . 44.000  
 AVERAGE . . . . . PHIF: . . . 0.276  
 AVERAGE . . . . . VSHALE: . . . 0.000  
 AVERAGE . . . . . SUM: . . . 0.013  
 M.AVERAGE . . . . . SUM + PHIF: 0.012  
 AVERAGE . . . . . VSH: . . . 0.987  
 VOID VOLUME: . . . . . PHIF: 12.141  
 HC VOID VOLUME . . . . . VSH: 11.993  
 REC HC VOID VOLUME (VSH\*%) 11.245  
 MOV HC VOID VOLUME . . . . . 0.748

## NET PAY

## Gas zone

THICKNESS: . . . . . 35.000 1535 - 1579 m  
 AVERAGE . . . . . PHIF: . . . 0.306  
 AVERAGE . . . . . VSHALE: . . . 0.000  
 AVERAGE . . . . . SUM: . . . 0.012  
 M.AVERAGE . . . . . SUM + PHIF: 0.011  
 AVERAGE . . . . . VSH: . . . 0.988  
 VOID VOLUME: . . . . . PHIF: 10.715  
 HC VOID VOLUME . . . . . VSH: 10.595  
 REC HC VOID VOLUME (VSH\*%) 9.986  
 MOV HC VOID VOLUME . . . . . 0.669

## NET SAND

THICKNESS: . . . . . 35.000  
 AVERAGE . . . . . PHIF: . . . 0.306  
 AVERAGE . . . . . VSHALE: . . . 0.000  
 AVERAGE . . . . . SUM: . . . 0.012  
 M.AVERAGE . . . . . SUM + PHIF: 0.011  
 AVERAGE . . . . . VSH: . . . 0.988  
 VOID VOLUME: . . . . . PHIF: 10.715  
 HC VOID VOLUME . . . . . VSH: 10.595  
 REC HC VOID VOLUME (VSH\*%) 9.986  
 MOV HC VOID VOLUME . . . . . 0.669

## NET TO GROSS RATIO

HNETPAY/HGROSS SAND = 0.79545  
 HNETSAND/HGROSS SAND = 0.79545  
 HNETPAY/HNETSAND = 1.00000

# STATISTICS

FIELD: . . . . . BLOCK 31/2  
WELL: . . . . . 31-2-5  
DATE: . . . . . 13.31.53 6 JANUARY 1991  
ENGINEER: . . . . . JIG

DEPTH INTERVAL: . . . 1579.00 TO 1602.00

APPLIED CUTOFFS:

. VCH: GREATER THAN 0.40  
. PHIF: LESS THAN 0.24  
. CW: GREATER THAN 0.65

## TOTAL DEPTH

THICKNESS: . . . . . 23.000  
AVERAGE . . . PHIF: . . . 0.301  
AVERAGE . . . VCHALE: . . . 0.000  
AVERAGE . . . CW: . . . 0.020  
M.AVERAGE . . . CW + PHIF: . . . 0.019  
AVERAGE . . . CH: . . . 0.980  
VOID VOLUME: . . . (PHIF)\*: . . . 6.928  
HC VOID VOLUME . . . (CH)\*: . . . 6.796  
REL HC VOID VOLUME (CH)\*: . . . 6.366  
MOV HC VOID VOLUME . . . . . 0.431

## NET PAY

THICKNESS: . . . . . 22.250  
AVERAGE . . . PHIF: . . . 0.305  
AVERAGE . . . VCHALE: . . . 0.000  
AVERAGE . . . CW: . . . 0.020  
M.AVERAGE . . . CW + PHIF: . . . 0.019  
AVERAGE . . . CH: . . . 0.980  
VOID VOLUME: . . . (PHIF)\*: . . . 6.778  
HC VOID VOLUME . . . (CH)\*: . . . 6.647  
REL HC VOID VOLUME (CH)\*: . . . 6.228  
MOV HC VOID VOLUME . . . . . 0.419

Oil zone

1579 - 1602 m

## NET SAND

THICKNESS: . . . . . 22.250  
AVERAGE . . . PHIF: . . . 0.305  
AVERAGE . . . VCHALE: . . . 0.000  
AVERAGE . . . CW: . . . 0.020  
M.AVERAGE . . . CW + PHIF: . . . 0.019  
AVERAGE . . . CH: . . . 0.980  
VOID VOLUME: . . . (PHIF)\*: . . . 6.778  
HC VOID VOLUME . . . (CH)\*: . . . 6.647  
REL HC VOID VOLUME (CH)\*: . . . 6.228  
MOV HC VOID VOLUME . . . . . 0.419

## NET SAND / RATIO

HNETPAY / HNETSAND = 0.96739  
HNETSAND / HNETPAY = 0.96739  
HNETPAY / HNETSAND = 1.00000

Waxman - Smith evaluation

Cation - exchange - capacity

31/2-1

$$Qv = a \cdot \phi^{-b}$$

Sample no.	Porosity	Qv
2	.341	0.06
8	.309	0.12
14	.380	0.05
17	.287	0.23
19	.323	0.02
21	.358	0.10
22	.248	0.25
24	.292	0.13

Linear regression:  $a = 14.915 \times 10^{-4}$

$$b = -3.748$$

$$F^* = F (1 + R_w \cdot B \cdot Qv)$$

$$R_w = 0.06$$

$$B = 9 \text{ at } 125^\circ\text{F}$$

Qv	F	F*	$\phi$ , Porosity
0.0623	6.4	6.615	0.3659
0.0958	14.3	15.040	0.3294
0.1028	13.3	14.039	0.3232
0.0621	6.4	6.615	0.3698
0.1616	20.6	22.397	<u>0.2865</u>
0.0852	13.2	13.808	0.3398
0.1025	12.0	12.664	<u>0.3235</u>
0.0865	11.2	11.723	0.3385
0.2787	21.6	24.851	<u>0.2477</u>
0.1510	21.0	22.713	<u>0.2917</u>

$$F^* = a \cdot \phi^{-m}$$

Linear regression:  $a = .532618$

$$m = -0.188956$$

31/2 - 1

$\phi$ : porosity fraction

1.0

.9

.8

.7

.6

.5

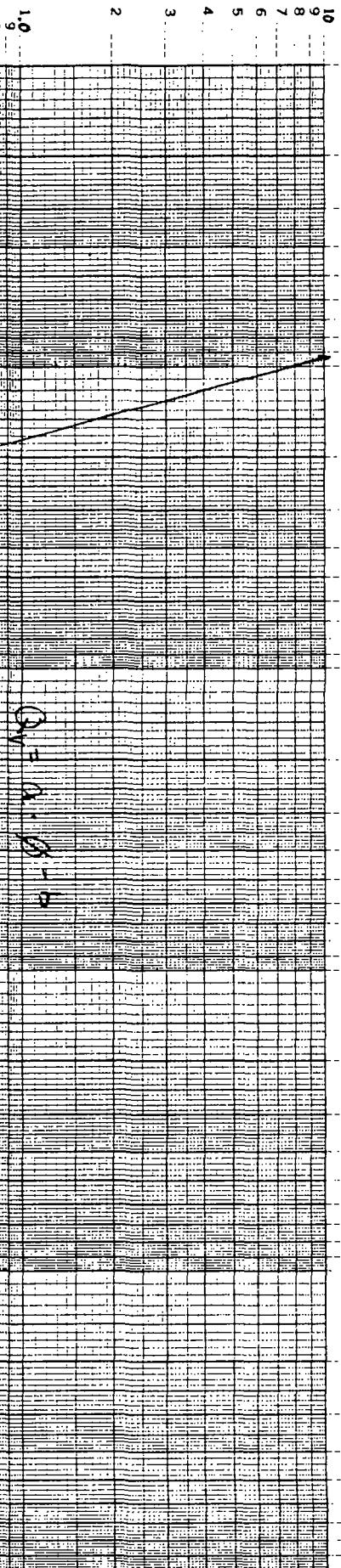
.4

.3

.2

.1

.01

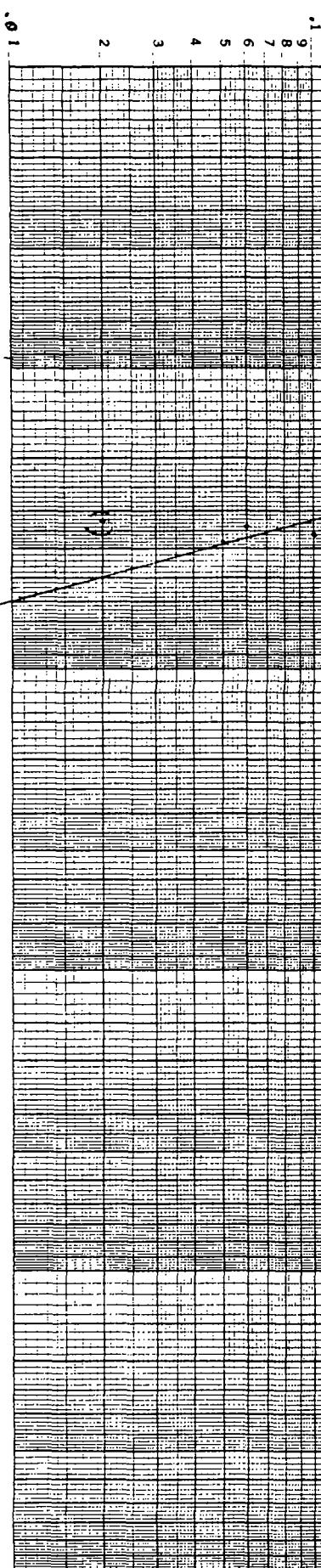


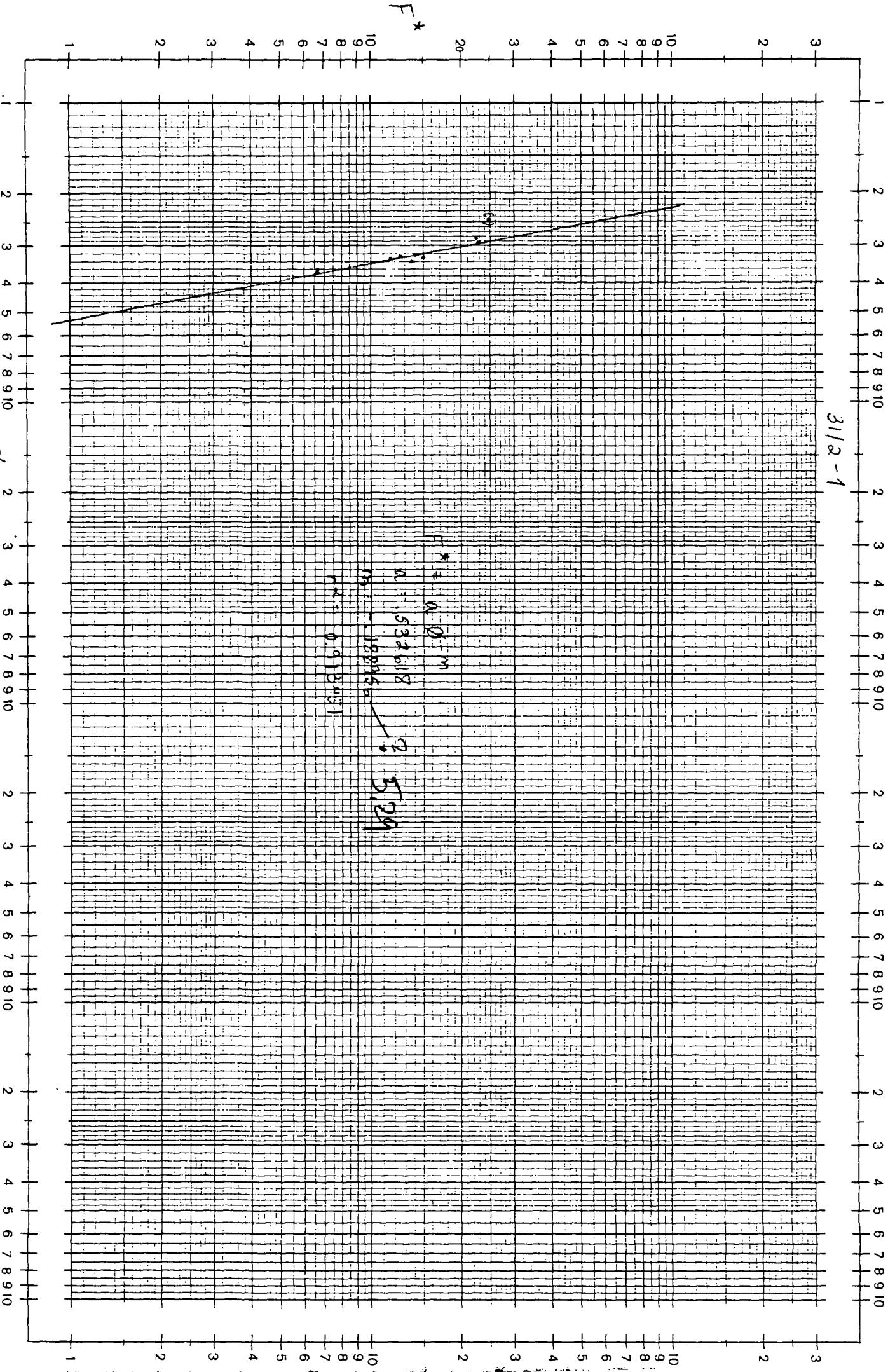
$$Q_V = \alpha \cdot \phi^{-\beta}$$

$$R = 0.814$$

$$D = 1.195 \times 10^{-4} = 0.001195$$

$Q_V$   
CFC





BFRONN  
31-2-5

DYBDE 1      DYBDE 2  
1535.00      1610.00

THIS IS THE CALCULATION OF SW  
USING THE MAXMAN-SMITH METHOD

\*\*\*\*\*

GIVE SATURATION EXPONENT N! 72.0

GIVE THE FACTOR B! 79.0

GIVE A IN THE RELATION F=A♦(PHIF)EXP(-B)!

.532618

GIVE B IN THE SAME RELATION! ?-.188956

GIVE RESISTIVITY OF FORMATION (WATER)! 7.06

IS CURVE QV ALREADY CALCULATED (YES/NO) : NO

GIVE CONST C IN QV=C(PHI)EXP(-E)! ?.0014915

GIVE THE EXPONENT E! ?-3.748

SW-SH ARE FINISHED

## STATISTICS

FIELD: . . . . . BLOCK 31/2  
 WELL: . . . . . 31-2-5  
 DATE: . . . . . 13.59.44 6 JANUARY 1981  
 ENGINEER: . . . . . JIS

DEPTH INTERVAL: . . . 1535.00 TO 1602.00

## APPLIED CUTOFFS:

.	VSH:	GREATER THAN	0.40
.	PHIF:	LESS THAN	0.24
.	SW:	GREATER THAN	0.65

## TOTAL DEPTH

THICKNESS: . . . . . 67.000  
 AVERAGE . . . 'PHIF' . . . 0.285  
 AVERAGE . . . 'VSHALE' . . . 0.000  
 AVERAGE . . . 'SW' . . . . 0.082  
 W.AVERAGE . . . 'SW' + 'PHIF' 0.078  
 AVERAGE . . . 'SH' . . . . 0.918  
 VOID VOLUME: . . . ('PHIF') . 19.069  
 HC VOID VOLUME . . ('SH') . 17.700  
 RES HC VOID VOLUME ('SHR') . 12.340  
 MOV HC VOID VOLUME . . . . 5.360

## NET PAY

THICKNESS: . . . . . 57.250  
 AVERAGE . . . 'PHIF' . . . 0.306  
 AVERAGE . . . 'VSHALE' . . . 0.000  
 AVERAGE . . . 'SW' . . . . 0.067  
 W.AVERAGE . . . 'SW' + 'PHIF' 0.065  
 AVERAGE . . . 'SH' . . . . 0.933  
 VOID VOLUME: . . . ('PHIF') . 17.493  
 HC VOID VOLUME . . ('SH') . 16.364  
 RES HC VOID VOLUME ('SHR') . 11.687  
 MOV HC VOID VOLUME . . . . 4.677

Total h.c. zone  
1535 - 1602 m

## NET SAND

THICKNESS: . . . . . 57.250  
 AVERAGE . . . 'PHIF' . . . 0.306  
 AVERAGE . . . 'VSHALE' . . . 0.000  
 AVERAGE . . . 'SW' . . . . 0.067  
 W.AVERAGE . . . 'SW' + 'PHIF' 0.065  
 AVERAGE . . . 'SH' . . . . 0.933  
 VOID VOLUME: . . . ('PHIF') . 17.493  
 HC VOID VOLUME . . ('SH') . 16.364  
 RES HC VOID VOLUME ('SHR') . 11.687  
 MOV HC VOID VOLUME . . . . 4.677

## NET/GROSS RATIO

HNETPAY/HGROSS SAND = 0.85448  
 HNETSAND/HGROSS SAND = 0.85448  
 HNETPAY/HNETSAND = 1.00000

## STATISTICS

FIELD: . . . . . BLOCK 31/2  
 WELL: . . . . . 31-2-5  
 DATE: . . . . . 14.03.05 6 JANUARY 1981  
 ENGINEER: . . . . . JIS

DEPTH INTERVAL: . . . 1535.00 TO 1579.00  
 APPLIED CUTOFFS:

VSH:	GREATER THAN	0.40
PHIF:	LESS THAN	0.24
SWI:	GREATER THAN	0.85

## TOTAL DEPTH

THICKNESS: . . . . . 44.000  
 AVERAGE . . . (PHIF) . . . 0.276  
 AVERAGE . . . (VSHALE) . . . 0.000  
 AVERAGE . . . (SWI) . . . 0.077  
 W.AVERAGE . . . (SWI + PHIF) . . . 0.063  
 AVERAGE . . . (VSH) . . . 0.923  
 VOID VOLUME: . . . (PHIF) . . . 12.141  
 HC VOID VOLUME . . . (VSH) . . . 11.375  
 RES HC VOID VOLUME (VSH) . . . 7.881  
 MOV HC VOID VOLUME . . . . . 3.494

## NET PAY

THICKNESS: . . . . .	35.000	Gas zone
AVERAGE . . . (PHIF) . . .	0.306	1535 - 1579 m
AVERAGE . . . (VSHALE) . . .	0.000	
AVERAGE . . . (SWI) . . .	0.052	
W.AVERAGE . . . (SWI + PHIF)	0.050	
AVERAGE . . . (VSH) . . .	0.948	
VOID VOLUME: . . . (PHIF) . . .	10.715	
HC VOID VOLUME . . . (VSH) . . .	10.181	
RES HC VOID VOLUME (VSH) . . .	7.891	
MOV HC VOID VOLUME . . . . .	2.890	

## NET SAND

THICKNESS: . . . . .	35.000
AVERAGE . . . (PHIF) . . .	0.306
AVERAGE . . . (VSHALE) . . .	0.000
AVERAGE . . . (SWI) . . .	0.052
W.AVERAGE . . . (SWI + PHIF)	0.050
AVERAGE . . . (VSH) . . .	0.948
VOID VOLUME: . . . (PHIF) . . .	10.715
HC VOID VOLUME . . . (VSH) . . .	10.181
RES HC VOID VOLUME (VSH) . . .	7.891
MOV HC VOID VOLUME . . . . .	2.890

## NET/GROSS RATIOS

HNETPAY/HGROSS SAND = 0.79545  
 HNETCARB/HGROSS SAND = 0.79545  
 HNETPAY/HNETSAND = 1.00000

## STATISTICS

FIELD: . . . . . BLOCK 31-2  
 WELL: . . . . . 31-2-5  
 DATE: . . . . . 14.46.41 6 JANUARY 1981  
 ENGINEER: . . . . . JID

DEPTH INTERVAL: . . . 1579.00 TO 1602.00

## APPLIED CUTOFFS:

. VSH: GREATER THAN 0.40  
 . PHIF: LESS THAN 0.24  
 . SW: GREATER THAN 0.65

## TOTAL DEPTH

THICKNESS: . . . . . 23.000  
 AVERAGE . . . "PHIF": . . . 0.301  
 AVERAGE . . . "VSHALE": . . . 0.000  
 AVERAGE . . . "SW": . . . 0.091  
 W.AVERAGE . . . "SW" + "PHIF": 0.087  
 AVERAGE . . . "SH": . . . 0.908  
 VOID VOLUME: . . . "PHIF": 6.928  
 HC VOID VOLUME . . . "SH": 6.325  
 RES HC VOID VOLUME ("SH":) 4.459  
 MOV HC VOID VOLUME . . . 1.866

## NET PAY

THICKNESS: . . . . .	22.250	Oil zone
AVERAGE . . . "PHIF": . . .	0.305	1579 - 1602 m
AVERAGE . . . "VSHALE": . . .	0.000	
AVERAGE . . . "SW": . . .	0.092	
W.AVERAGE . . . "SW" + "PHIF":	0.088	
AVERAGE . . . "SH": . . .	0.908	
VOID VOLUME: . . . "PHIF":	6.778	
HC VOID VOLUME . . . "SH":	6.184	
RES HC VOID VOLUME ("SH":)	4.396	
MOV HC VOID VOLUME . . .	1.788	

## NET SAND

THICKNESS: . . . . . 22.250  
 AVERAGE . . . "PHIF": . . . 0.305  
 AVERAGE . . . "VSHALE": . . . 0.000  
 AVERAGE . . . "SW": . . . 0.092  
 W.AVERAGE . . . "SW" + "PHIF": 0.088  
 AVERAGE . . . "SH": . . . 0.908  
 VOID VOLUME: . . . "PHIF": 6.778  
 HC VOID VOLUME . . . "SH": 6.184  
 RES HC VOID VOLUME ("SH":) 4.396  
 MOV HC VOID VOLUME . . . 1.788

## NET / GROSS RATIO

HNETPAY / HGROSS SAND = 0.96739

HNETAND / HGROSS SAND = 0.96739

HNETPAY / HNETSAND = 1.00000