Denne rapport tilhører

L&U DOK. SENTER

L. NR. 20085170014

KODE Well 34110-11 w-29

Returneres etter bruk

L,71/24 Avd. 2,	8207 93	Statoil Sentralarkiv						
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STATOIL

EVALUATION OF CORE DATA

WELL. 34/10-11

DATE: JANUARY 1982



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COMMENTS.

The samples were extracted with methanol, followed by toluene and finally methanol. The samples were dried at 60° C and 40% relative humidity.

Helium Porosity and Klinkenberg corrected air permeability were measured.

The samples were saturated with simulated formation-water containing the following ions, Na 14400 ppm, Ca 1000 ppm, Mg 295 ppm, Ba 50 ppm, K 320 ppm, and Sr 216 ppm. All Chlorid-salts.

The measurements of gas/water capillary pressure were performed with air and the simulated formation-water. Stability time at each pressure level varied from 2 to 3 days. An air trap showed that no production of gas occured. The different water saturations were determined by the weights of the samples.

The resistivity index and capillary pressure were measured at the same time.

After resaturation formation resistivity factor, porosity and brine permeability reduction were measured.

During the tests sample 2A and 40 broke down and could not be replaced.



SAMPLE LIST

Sample no.	Depth (m)
2A	1899.25-30
40	1900.34-57
42	1900.80-88
50	1891.55
53	1893.45



POROSITY AND GRAIN DENSITY

Sample no.	% Porosity	Grain Density	
2A	32.4	2.63	
40	25.4	2.62	
42	22.0	2.58	
50	32.6	2.65	
53	24.5	2.61	

CAPILLARY PRESSURE AND RESISTIVITY INDEX.

Determination of n-exponent

Resistivity of brine at $20^{\rm O}{\rm C}$: 0.176 Ω m

 $RI = b \cdot Sw^{-n}$

Sample no.		2A			40			42			50			53	
Pressure, Bar	Sw.Frac.of Pore Space	ഥ	RI	Sw.Frac.of Pore Space	된급	RI	Sw.Frac.of Pore Space	된	RI	Sw.Frac.of Pore Space	FF R	RI S	Sw.Frac.of Pore Space	귶	RI
0	1.00	6.81		1.00	14.7		1.00	16.9		1.00	7.05		1.00	15.3	
0.025	0.952		1.03	0.963		1.03	0.956	, ¬	1.01	0.964	1.	1.05	0.968		1.06
0.05	0.950		1.04	0.961		1.04	0.950	17	1.01	996.0	1.	1.05	0.970		1.05
0.10	0.835		1.84	0.954		1.09	0.944	• •	1.02	0.945	1.	1.11	0.964		1.09
97.0	0.452		4.60	0.925		1.23	906.0	• •	1.21	0.612	3.	3.47	0.907		1.19
0.50	0.386		7.82	0.850		1.54	0.827	₹-1	1.52	0.508	5.	5.83	0.828		1.53
1.00	00:300	1	10.77	0.729		1.97	0.680	. 7	2.14	0.400	7.	7.77	0.709		1.98
2.00	0.294	1	13.94	0.695		2.15	699.0		2.18	0.377	8	8.70	0.683	•	2.04
10.0	0.246	1	19.42	0.621		2.40	0.646	. 1	2.21	0.360	10.16		0.579	•	2.89
15.0	0.234	2	20.12	đưu		dwu	0.628	· N	2.24	0.347	11.00		0.544	.,	3.43
	-		-			-									

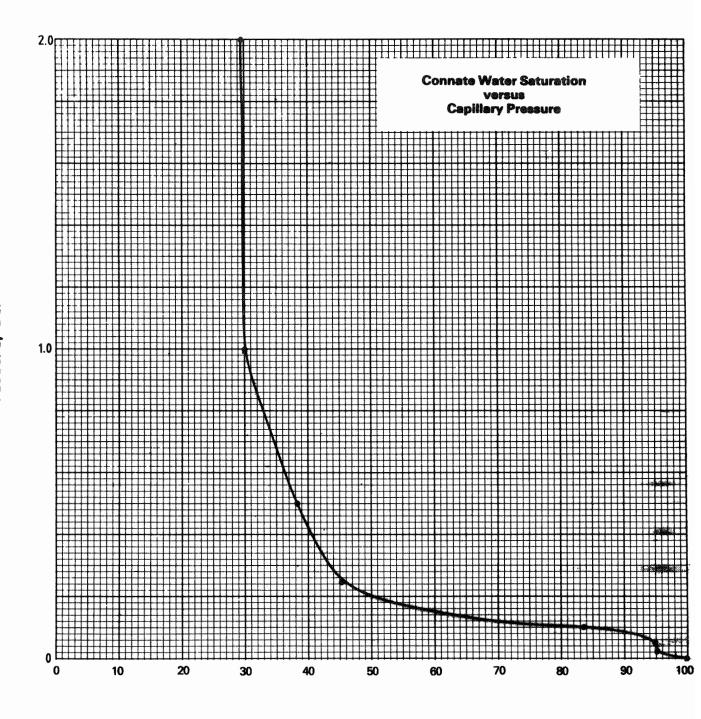
By weighted least squares method, forced through RI = 1.0, Sw = 1.0

1.00	1.98
1.01	2.29
76.0	1.94
1.01	1.99
1.01	2.08
Q	и



No. . ZA...... Kair . 417. III.

Depth ø ... 32.4%

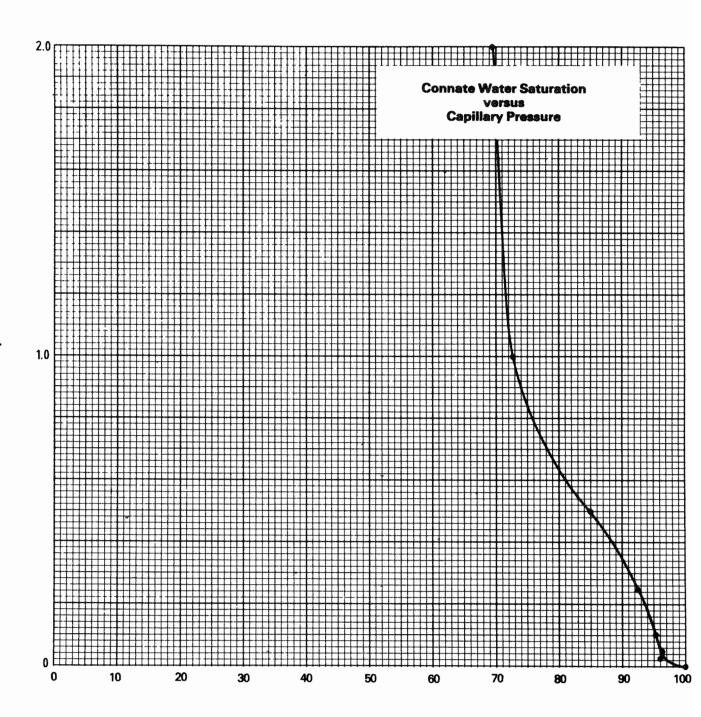




Well 34/10-11

Sample No. 40 Kair 11.4 md

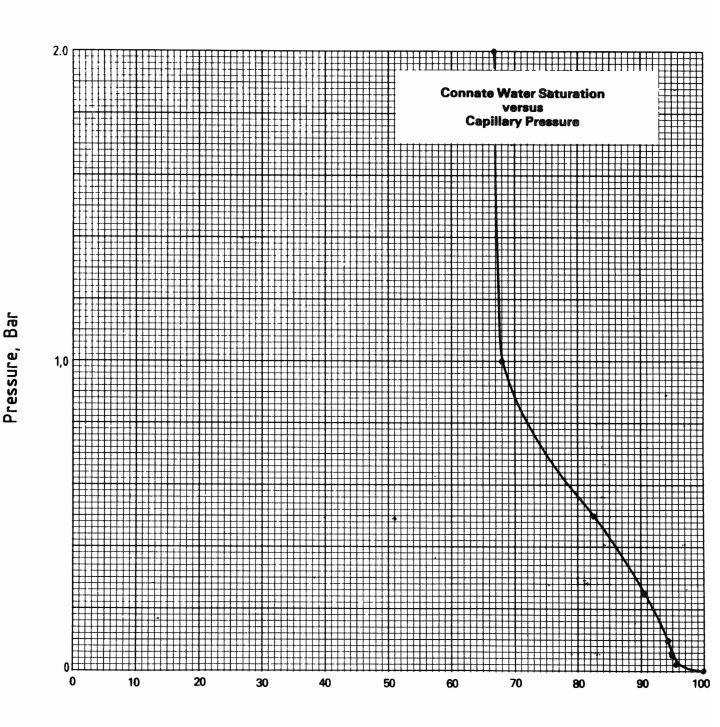
Depth Ø 25,4%





Well34/10-11

Depth ø ...22.0%

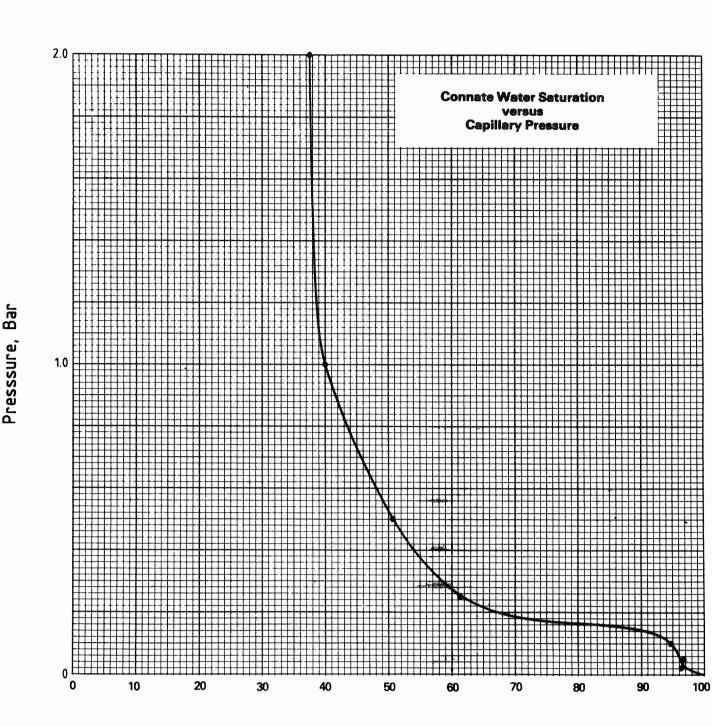




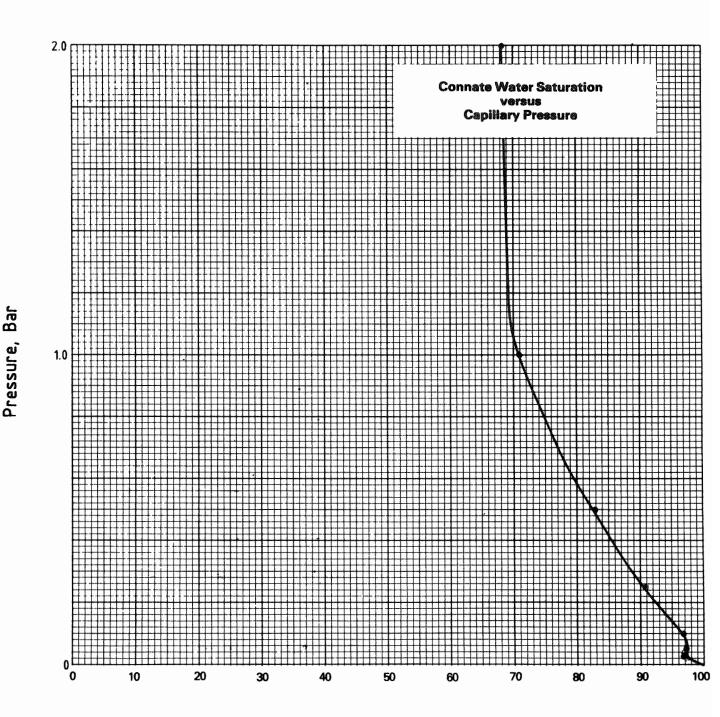
Well 34/10-11

Sample No. 50 Kair 205 md

Depth ø 32.6%





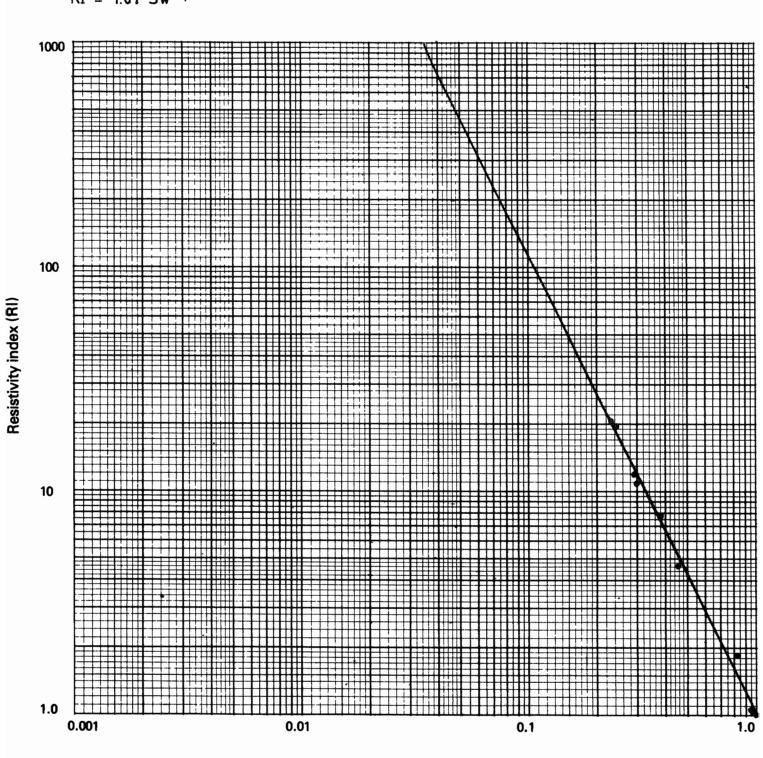




Company Statoil

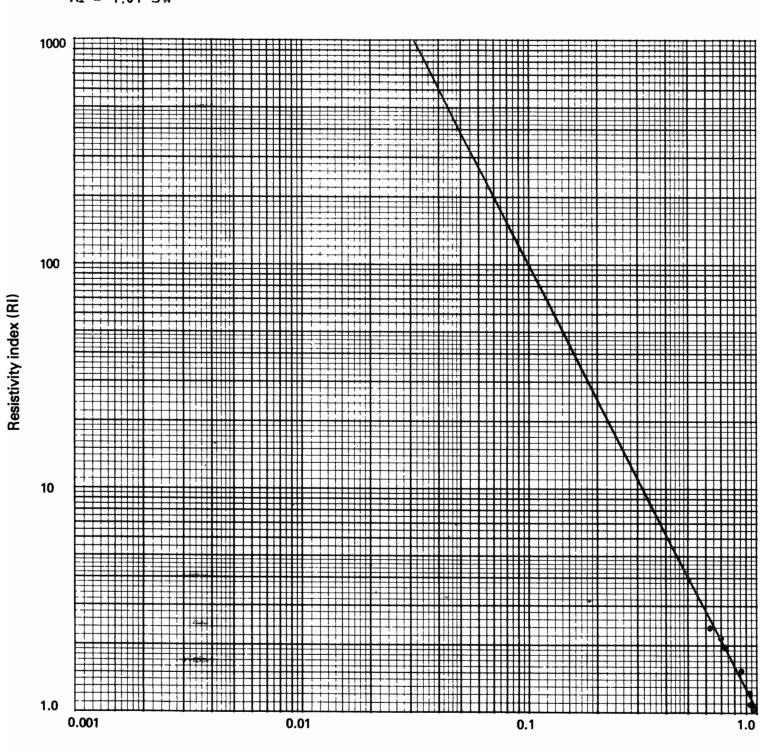
Well 34/10-11 Sample : 2A

RI = 1.01 Sw^{-2,08}



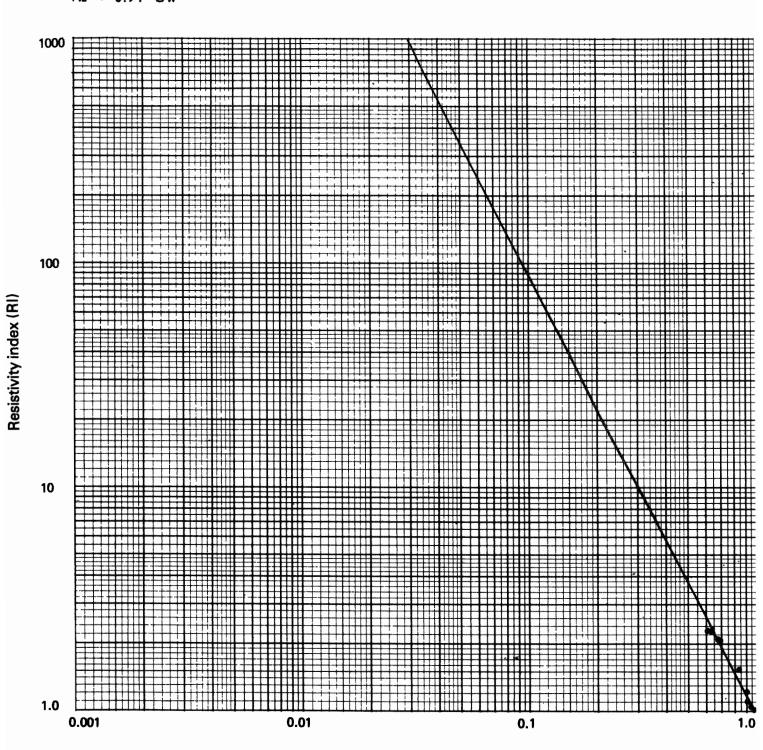


Company .	Statoil	
Well	34/10-11	Sample: 40
R1 = 1 01	Sw-1.99	



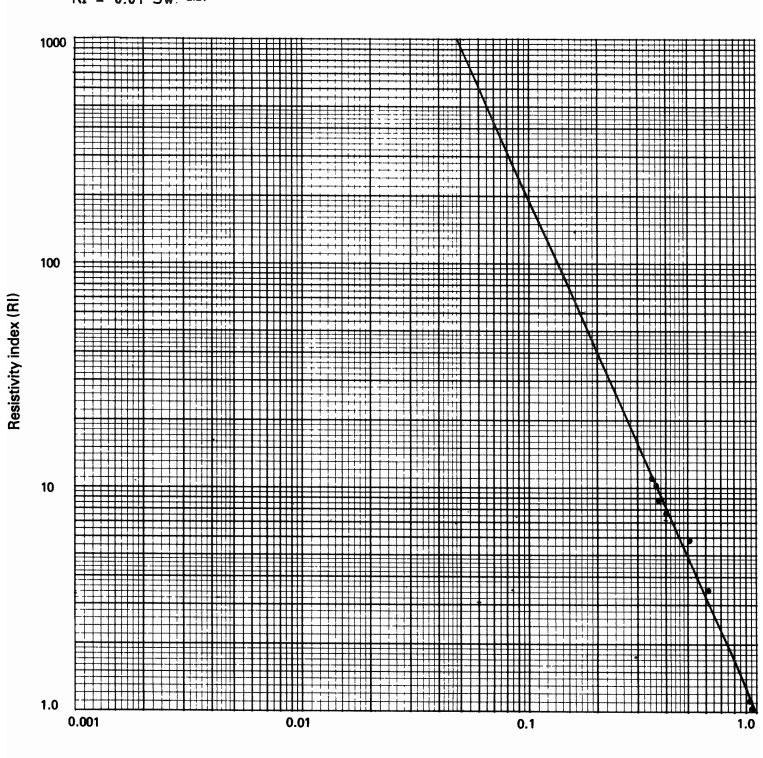


Company .	Statoil			
Well	34/10-11	Sample :	42	
RI = 0.97	Sw-1.94			





Company .	Statoil			 	 ٠.
Well	34/10-11	Sample :	.50	 	
RT = 0.01	S₩ -2.29				

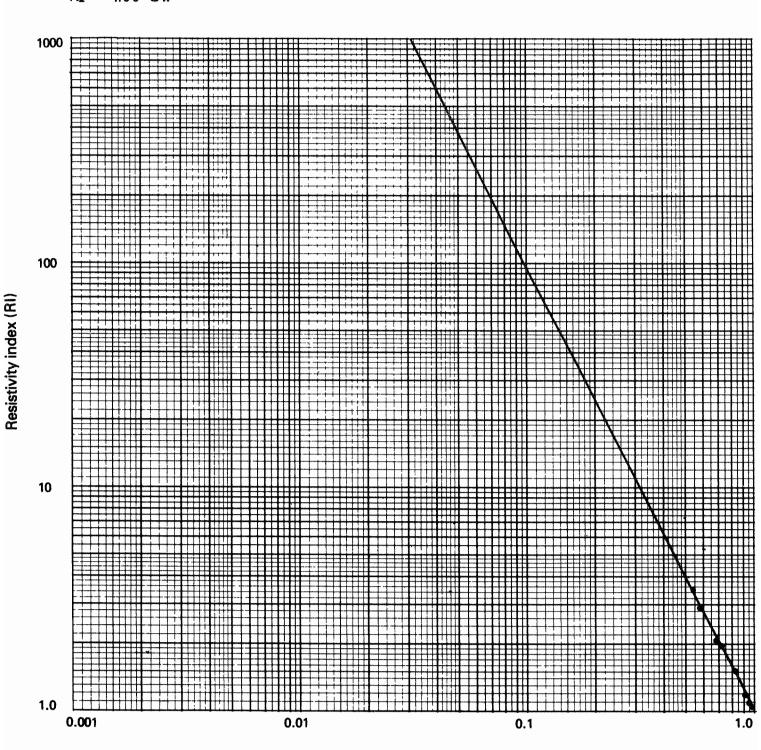




Company Statoil

Well 34/10-11 Sample : 53

RI = 1.00 Sw -1.98



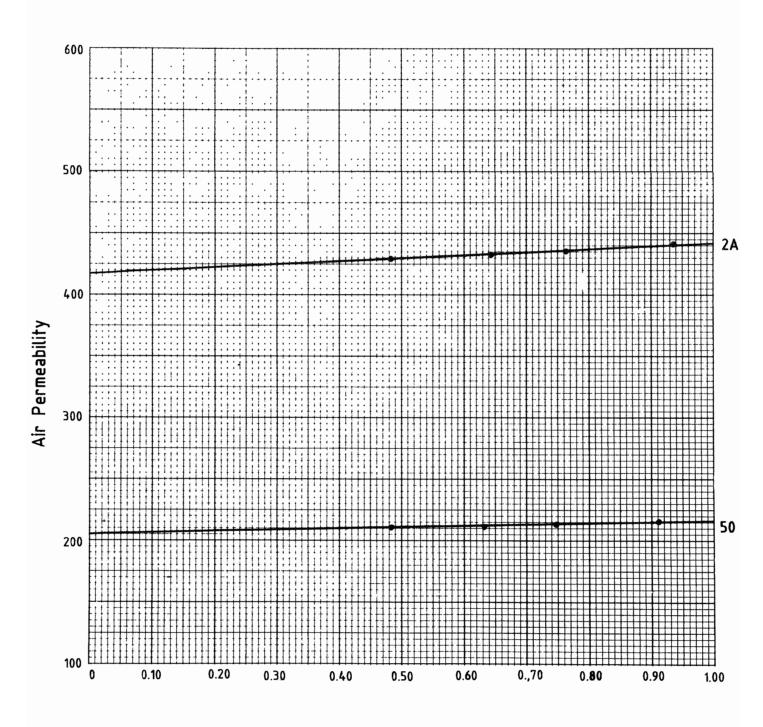


KLINKENBERG CORRECTED AIR PERMEABILITY

	Sett:		
Sample no.	(Mean pressure) -1	Air permeability	Klinkeberg corrected
	(atm. abs.) -1	md	permeability md
2 A	0.938	441	
	0.765	436	
	0.645	433	
	0.492	430	417
40	0.747	15.0	
	0.633	14.4	
	0.549	14.0	
	0.434	13.5	11.4
42	0.703	7.17	
	0.600	6.99	
	0.524	6.88	
	0.418	6.63	5.87
50	0.912	216	
	0.747	213	
	0.633	212	
	0.484	211	205
53	0.767	13.6	
	0.647	13.0	
	0.560	12.8	
	0.440	12.2	10.4

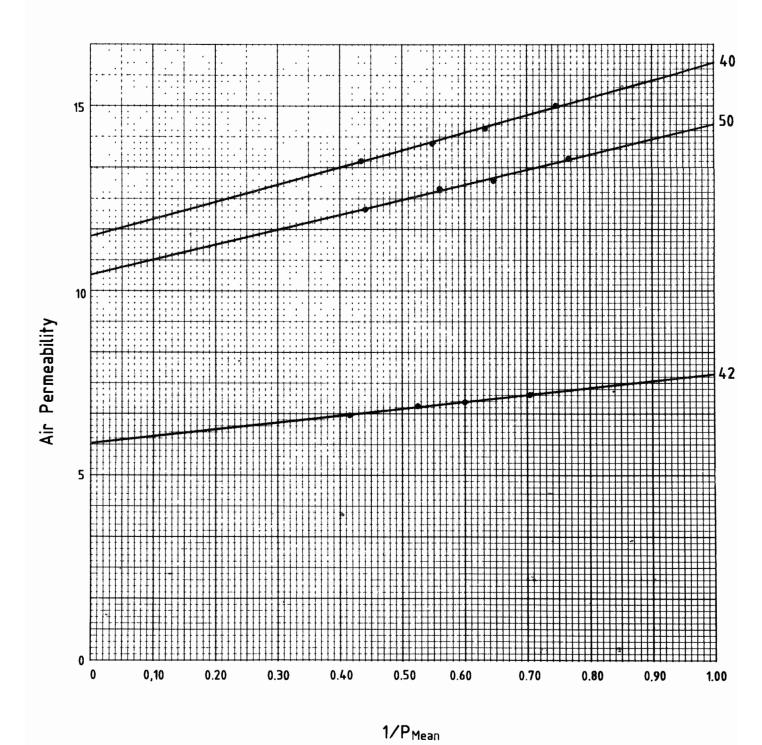


Klinkenberg Correction





Klinkenberg Correction





BRINE PERMEABILITY REDUCTION AT FOUR DIFFERENT CONFINING PRESSURES.

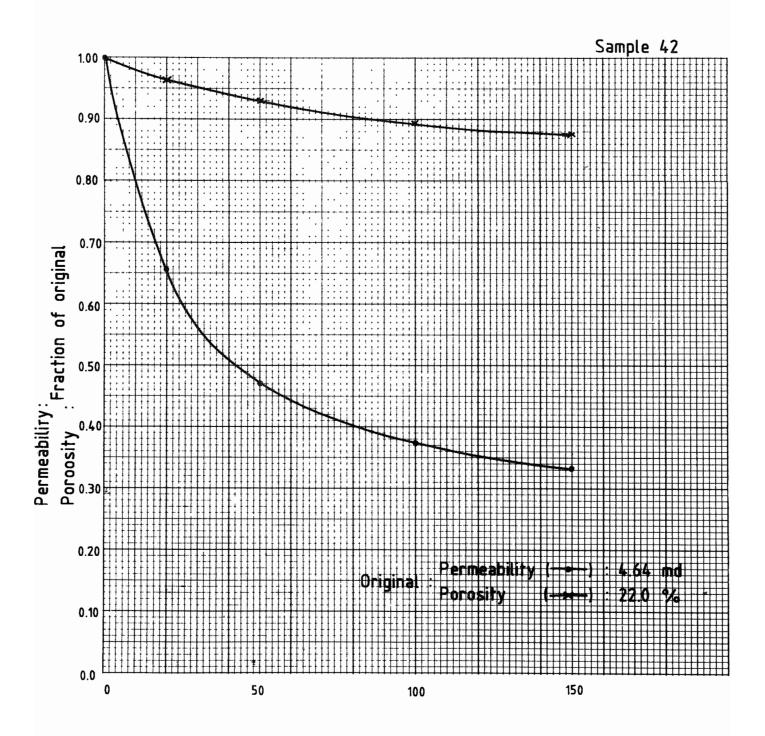
Sample	Room	, 2	O Bar	50	Bar	100	Bar	150	O Bar
no.	KBrine original,md	KBrine md	Fraction of orig.	KBrine md	Fraction of orig.	KBrine md		KBrine md	Fraction of orig.
42	4.64	3.05	0.657	2.19	0.472	1.76	0.379	1.54	0.332
50	178	142	0.798	94.6	0.531	61.3	0.344	44.0	0.247
53	8.28	5.84	0.705	4.67	0.564	3.91	0.472	3.57	0.431

BRINE POROSITY REDUCTION AT FOUR DIFFERENT CONFINING PRESSURES.

Sample	Room	ļ	20 Bar	50	Bar	10	0 Bar		l50 Bar
no.	Ø % orig.	Ø %	Fraction of orig.	Ø %	Fraction of orig.	•	Fraction of orig.	Ø %	Fraction of orig.
42	22.0	21.2	0.964	20.5	0.932	19.7	0.895	19.3	0.877
50	32.6	27.3	0.837	26.2	0.807	25.4	0.779	24.8	0.761
53	24.5	23.4	0.955	22.5	0.918	21.7	0.886	21.4	0.871



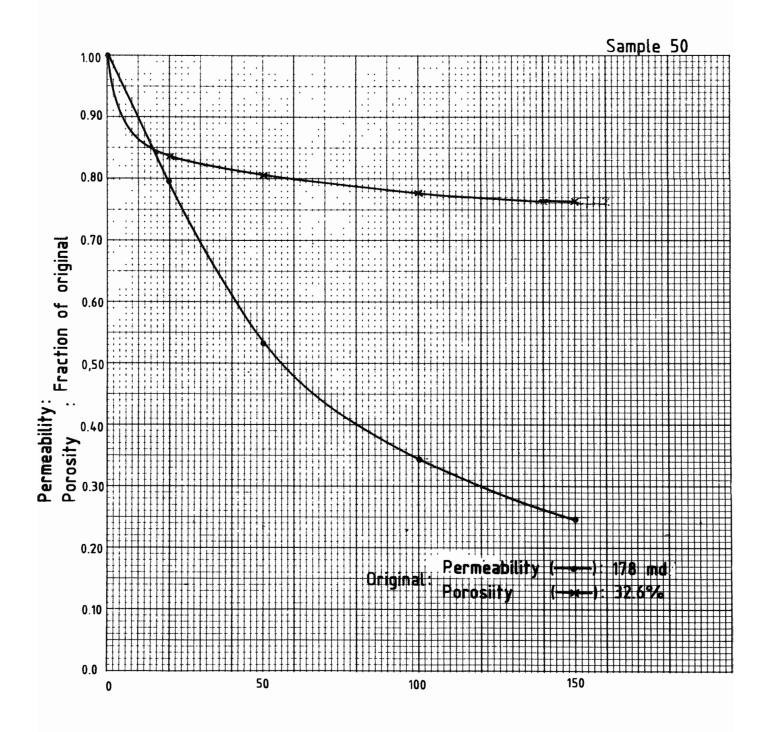
Permeability, Porosity versus Net Overburden



Net Overburden, Bar



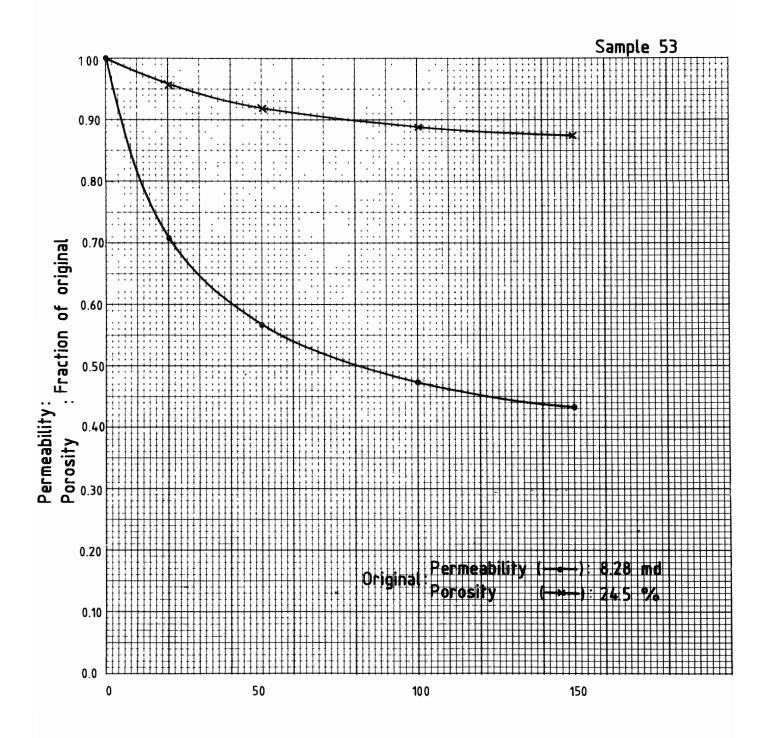
Permeability, Porosity versus Net Overburden



Net Overburden, Bar



Permeability, Porosity versus Net Overburden



Net Overburden, Bar



POROSITY AND FORMATION RESISTIVITY FACTOR MEASURED AT 4 DIFFERENT NET CONFINING PRESSURES.

 $\label{eq:ff} \text{FF = a } \emptyset^{-m}$ Brine Resistivity at 20 $^{\circ}\text{C: 0.176} \ \Omega\text{m}$

	No confining		20 Bar		50 Bar		100 Bar		150 Bar	
Sample no.	Ø%	FF	Ø%	FF	Ø٤	FF	Ø۶	FF	Ø%	FF
42	22.0	14.78	21.2	15.29	20.5	16.62	19.7	18.09	19.3	20.82
50	32.6	9.41	27.3	10.00	26.2	10.40	25.4	10.69	24.8	11.12
53	24.5	13.73	23.4	15.28	22.5	16.63	21.7	17.70	21.4	18.26

By wighted least squares method, forced through FF = 1.0, \emptyset = 1.0

a	1.02	1.00	1.00	1.00	0.99
m	1.84	1.80	1.81	1.80	1.83

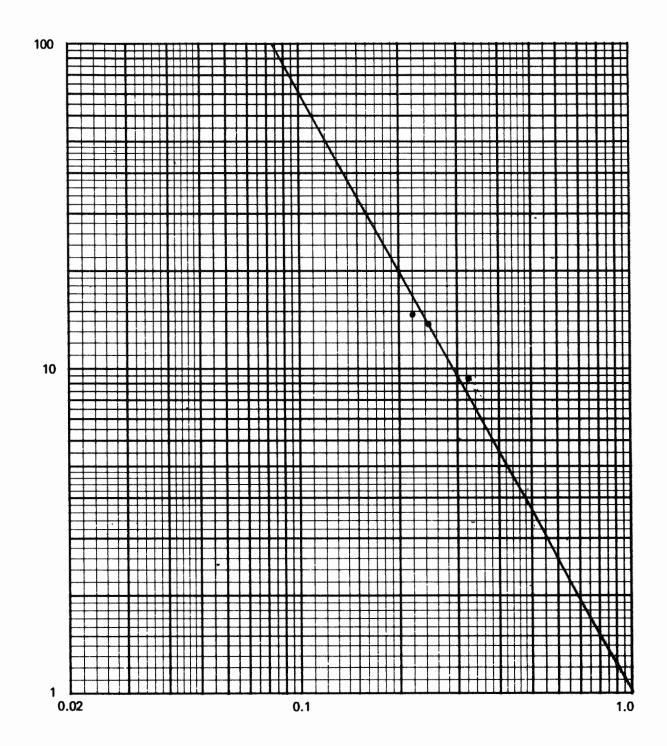


Company Statoil

Well 34/10-11

Room Condition

FF = 1,02¢-1.84



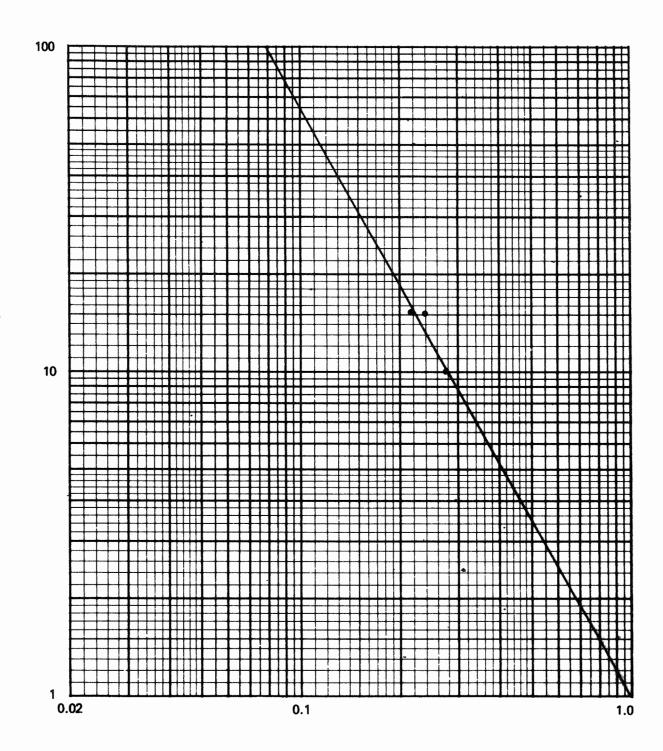


Company Statoil

Well 34/10-11

Net Overburden Pressure : 20 Bar

FF = 1,00¢,-1.80

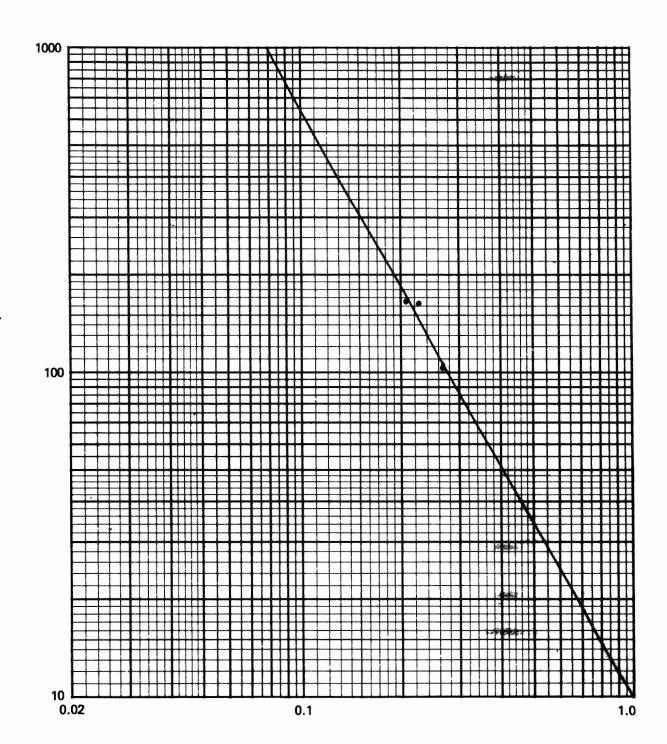




Company Statoil
Well 34/10-11

Net Overburden : 50 Bar

 $FF = 1,00\phi^{-1.81}$

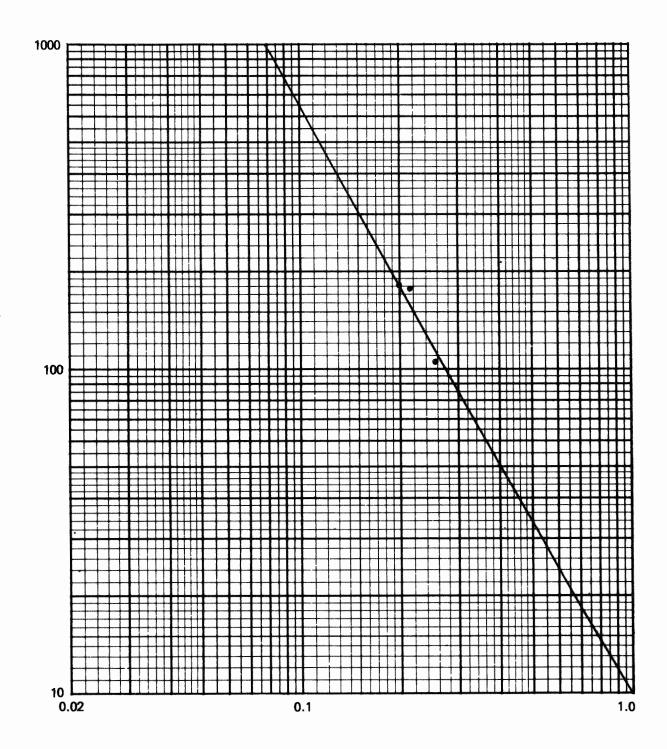




Company Statoil
Well 34/10-11

Net Overburden Pressure: 100 Bar

 $FF = 1,00\phi -1.80$





Company Statoil
Well 34/10-11

Net Overburden Pressure : 150 Bar

 $FF = 0.99\phi^{-1.83}$

