Denne rapport tilhører

STATOIL

L&U DOK. SENTER

L. NR. 20088390018

KODE Well 31/2-3 11/25

Returneres etter bruk

Reservoir Fluid Analysis

For

Norske Shell Exploration & Production

Well: 31/2-3

North Sea, Norway

CORE LABORATORIES UK LTD. Petroleum Reservoir Engineering ABERDEEN, SCOTLAND

Reservoir Fluid Analysis

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North Sea, Norway

Petroleum Reservoir Engineering ABERDEEN, SCOTLAND

5th January, 1981

Norske Shell Exploration & Production, Damsle Ferusuei 43, P.O. Box 10, 40-33 Forus, Stavanger, Norway.

Attention: Mr. Dave Jolly

Subject: Reservoir Fluid Analysis

Well: 31/2-3 North Sea, Norway

Our File Number: RFLA 80167

Gentlemen,

On 8th July, 1980, samples of separator gas and condensate were collected during testing of the subject well and forwarded to our Aberdeen laboratory for analysis. The results of these analyses as requested by a representative of Norske Shell Exploration & Production are presented in the following report.

The hydrocarbon composition of the separator gas was determined by routine gas chromatography. The hydrocarbon composition of the condensate liquid was determined by low temperature fractional distillation.

After correcting the quoted producing gas-condensate ratio for the factors shown on page one a corrected gas-condensate ratio of 415567 SCF/BBL of separator condensate was calculated. Utilizing this gas-condensate ratio in conjunction with the experimentally determined hydrocarbon compositions of the separator products and the measured laboratory shrinkage of the condensate liquid, a wellstream composition was calculated. These compositions are to be found on page two. The laboratory shrinkage data may be found on page five.

The separator products were physically recombined at the above gas-condensate ratio and the resultant reservoir gas-condensate utilized for the remainder of the study.

A portion of the gas-condensate was placed in a high pressure visual cell and examined at the reservoir temperature of $154^{\circ}F$. At this temperature the system exhibited a retrograde dew point at 2067 psig. The pressure-volume relations are shown on page three.

Continued/...

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Norske Shell Exploration & Production Continued/...

Page Two

The wellstream composition was used to calculate the cumulative stock tank liquid and sales gas recovery using normal two stage separation. Also calculated are the plant liquid products on the primary and secondary stage separator gases. The total plant products in the wellstream are also shown. All recoveries are based on one MMSCF of original reservoir fluid. It must be remembered in applying these data that all recoveries are based on 100 percent plant efficiency. These data may be found on page four.

The extended hydrocarbon composition to eicosanes plus of the condensate fluid was determined by gas chromatography and this composition may be found on page six.

The extended composition to eicosanes plus of the reservoir fluid was calculated and this composition is presented on page seven.

In view of these results, the reservoir fluid would usually be considered a dry gas system, and consequently we would not normally perform a "step-wise" equilibrium (constant volume) depletion to simulate wellstream behaviour below the dew point. We will retain the samples in our laboratory pending further instructions from Norske Shell Exploration & Production.

It has been a pleasure to be of service to Norske Shell Exploration & Production. Should any questions arise concerning the data presented in this report, please do not hesitate to contact us.

Very truly yours,

Core Laboratories U.K. Ltd.,

LKS/HG 15 cc addressee

L. K. Sebborn,

Laboratory Manager - RFL

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	File RFLA 80167
Company Norske Shell Expl. & Prod.	Date Sampled 8th July, 1980
Well31/2-3	County North Sea
Field	N
	CHARACTERISTICS Closp Sand
Formation Name	Clean Sand
Date First Well Completed	19
Original Reservoir Pressure	PSIG @Ft.
Original Produced Gas-Liquid Ratio	SCF/Bbl
Production Rate	Bbls/Day
Separator Pressure and Temperature	°F.
Liquid Gravity at 60°F. Datum	Ft. Subsea
	RACTERISTICS
Elevation	
Total Depth	Ft.
Producing Interval	
Tubing Size and Depth	In. toFt.
Open Flow Potential	MMSCF/Day
Last Reservoir Pressure	2275PSIG @Ft.
Date	
Reservoir Temperature	154 ° F. @ Ft.
Status of Well	
Pressure Gauge	G CONDITIONS
Flowing Tubing Pressure	PSIG
Flowing Bottom Hole Pressure	PSIG
Primary Separator Pressure	325 PSIG
Primary Separator Tressure Primary Separator Temperature	
Secondary Separator Pressure	PSIG
Secondary Separator Temperature	° F.
Field Stock Tank Liquid Gravity	° API @ 60° F.
Primary Separator Gas Production Rate	20612MSCF/Day
Pressure Base 14.696	PSIA
Temperature Base 60 Compressibility Factor (F) 1.0201	
Gas Gravity (Laboratory) 0.602 Gas Gravity Factor (F) 1.2888	
Primary sep Liquid Production Rate @ 100°F	49.6
Primary Separator Gas/. Primary sep. Liquid Ratio	415567 SCF/BbI
or	2.41 Bbls/MMSCF
Sampled by	Flopetrol
REMARKS:	

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Hydrocarbon Analyses of Separator Products and Calculated Well Stream

	Separator Liquid *	Separator (Gas +	Well Stream
Component	Mol Per Cent	Mol Per Cent	GPM	Mol Per Cent
	<u> </u>	*		
Hydrogen Sulfide	NIL	NIL		NIL
Carbon Dioxide	0.16	0.57		0.57
Nitrogen	0.06	1.61		1.61
Methane	8.40	93.26		93.08
Ethane	1.47	3.45		3.45
Propane	0.44	0.38	0.104	0.38
iso-Butane	0.64	0.29	0.104	0.38
n-Butane	0.14	0.04	0.093	
iso-Pentane	0.59	0.04	0.013	0.04 0.04
n-Pentane	0.22	0.01	0.013	
Hexanes	3.18	0.01	0.004	0.01
Heptanes plus	84.70			0.09
Tropianos pras	100.00	$\frac{0.27}{100.00}$	$\frac{0.122}{0.386}$	$\frac{0.44}{100.00}$
	100.00	100.00	0.380	100.00
Properties of Heptanes plus				
API gravity @ 60° F.	44.0			
Specific gravity @ 60/60° F.	0.8063			0.7427
Molecular weight	130	103		114
Wolfer	************	••••••		
Calculated separator gas gravity (ai	r=1.000=0.602			
Calculated gross heating value for so	· · · · · · · · · · · · · · · · · · ·	BTU		
per cubic foot of dry gas @ 14.696)		
per cubic root of dry gas @ 14.070	psia anu oo v.			

Primary separator gas collected @...325.....psig and ...100.....°F. Primary separator liquid collected @...325....psig and ...100...oF.

Primary separator gas/separator liquid ratio415567....SCF/Bbl @ 325 psig and 100°F

Primary separator liquid/stock tank liquid ratio1.0872....Bbls @ 325 psig and 100°F/Bbl at 60°F

Cylinder Number: 16251/69

Cylinder Number:

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Pressure-Volume Relations at ...154... °F.

Pressure PSIG		Relative Volume (1)	Compressibility Factor Z
3000		0.6953	0.877
2500		0.8242	0.867
2275	Reservoir	0.9051	0.867
2200	Pressure	0.9369	0.868
2100		0.9835	0.870
2067	Dew Point	1.0000	0.871
2000	Pressure	1.0344	
1900		1.0913	
1800		1.1560	
1700		1.2277	
1600		1.3102	
1400		1.5102	
1200		1.7797	
1000		2.1600	
800		2.7309	
600		3.6782	

(1) Relative Volume: V/Vsat is barrels at indicated pressure per barrel at saturation pressure.

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CALCULATED RECOVERY PER MMSCF OF ORIGINAL FLUID

Wellstream MSCF	1000
Normal Temperature Separation*	
Stock Tank Liquid - Barrels Primary Separator Gas - MSCF Second Stage Gas - MSCF Stock Tank Gas - MSCF	5.27 991.36 2.56 1.60
Total Plant Products in Primary Separator Gas - Gallons**	
Propane Butanes (Total) Pentanes Plus	101 100 65
Total Plant Products in Second Stage Gas - Gallons**	
Propane Butanes (Total) Pentanes Plus	0.34 0.30 0.14
Total Plant Products in Wellstream - Gallons**	
Propane Butanes (Total) Pentanes Plus	105 107 280

^{*} Recovery Bases: Primary separation at 1250 psig and 40°F Second Stage at 500 psig and 40°F Stock Tank at 0 psig and 27°F

^{**} Recovery assumes 100% plant efficiency

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SEPARATOR TESTS OF Separator Liquid SAMPLE

SEPARATOR PRESSURE PSI GAUGE	SEPARATOR TEMPERATURE OF	SEPARATOR GAS/OIL RATIO	STOCK TANK GAS/OIL RATIO	STOCK TANK GRAVITY API # 60°F	SHRINKAGE FACTOR VR/VSAT (2)	FORMATION VOLUME FACTOR (3)	SPECIFIC GRAVITY OF FLASHED GAS
0	65		90	44.4	0.9198	1.0872	0.873

⁽¹⁾ Separator and Stock Tank Gas/Oil Ratio in cubic feet of gas @ 60°F and 14.7 PSI absolute per barrel of stock tank oil @ 60°F.

⁽²⁾ Shrinkage Factor: Vr/Vsat. is barrels of stock tank oil @ 60°F per barrel of saturated oil @ ...325...... PSI gauge and ...100...... F.

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HYDROCARBON ANALYSIS OF SEPARATOR LIQUID SAMPLE

Component:	Mol Percent:	Weight Percent:
Hydrogen Sulphide	NIL	NIL
Carbon Dioxide	0.16	0.06
Nitrogen	0.06	0.01
Methane	8.40	1.16
Ethane	1.47	0.38
Propane	0.44	0.17
Iso-Butane	0.64	0.32
N-Butane	0.14	0.07
Iso-Pentane	0.59	0.37
N-Pentane	0.22	0.14
Hexanes	3.18	2.35
Methyl Cyclopentane	2.74	1.93
Benzene	NIL	NIL
Cyclohexane	4.16	2.94
Heptanes	3.75	3.15
Methyl Cyclohexane	9.55	7.86
Toluene	0.80	0.62
Octanes	7.96	7.62
Ethylbenzene	1.20	1.07
Meta and Para Xylene	4.31	3.84
Orthoxylene	0.55	0.49
Nonanes	7.31	7.86
1, 2, 4 Trimethylbenzene	3.00	3.02
Decanes	10.31	12.31
Undecanes	10.86	13.42
Dodecanes	4.80	6.49
Tridecanes	4.65	6.84
Tetradecanes	3.44	5.49
Pentadecanes	2.57	4.45
Hexadecanes	1.02	.1.90
Heptadecanes	0.80	1.59
Octadecanes	0.44	0.93
Nonadecanes	0.23	0.51
Eicosanes plus	0.25	0.64
	100.00	100.00

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HYDROCARBON ANALYSIS OF WELLSTREAM SAMPLE

Component:	Mol Percent:	
Hydrogen Sulphide	NIL	
Carbon Dioxide	0.57	
Nitrogen	1.61	
Methane	93.08	
Ethane	3.45	
Propane	0.38	
Iso-Butane	0.29	
N-Butane	0.04	
Iso-Pentane	0.04	
N-Pentane	0.01	
Hexanes	0.09	
Methyl Cyclohexane	0.01	
Benzene	NIL	1.8
Cyclohexane	0.02	
Heptanes	0.02	
Methyl Cyclohexane	0.06	c C 8
Toluene	TRACE	
Octanes	0.05	
Ethylbenzene	0.01	ت. <u>۲</u> ۰۱۵۰
Meta and Para Xylene	0.02	
Orthoxylene	TRACE	
Nonanes	0.04	<i>ن ت \</i> د ټل
1, 2, 4 Trimethylbenzene	0.02	
Decanes	0.06	د نان
Undecanes	0.08	
Dodecanes	0.03	
Tridecanes	0.01	
Tetradecanes	0.01	
Pentadecanes	TRACE	
Hexadecanes	TRACE	
Heptadecanes	TRACE	
Octadecanes	TRACE	
Nonadecanes	TRACE	
Eicosanes plus	TRACE	
	100.00	

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L. K. Sebborn,

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