

Reservoir Fluid Analysis For Norske Shell Exploration & Production Well: 31/2-3 North Sea, Norway

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Reservoir Fluid Analysis For Norske Shell Exploration & Production Well: 31/2-3 North Sea, Norway

6th January, 1981

Norske Shell Exploration & Production, Damsle Ferusuei 43, P.O. Box 10, 40-33 Forus, Stavanger, Norway.

Attention: Mr. Dave Jolly

Subject: Reservoir Fluid Analysis Well: 31/2-3 North Sea, Norway Our File Number: RFLA 80167B

Gentlemen,

On 8th July, 1980, samples of separator gas and condensate were collected during testing of the subject well and forwarded to our Aberdeen laboratory for analysis. The results of these analyses as requested by a representative of Norske Shell Exploration & Production are presented in the following report.

The hydrocarbon composition of the separator gas was determined by routine gas chromatography. The hydrocarbon composition of the condensate liquid was determined by low temperature fractional distillation.

After correcting the quoted producing gas-condensate ratio for the factors shown on page one a corrected gas-condensate ratio of 420310 SCF/BB1 of separator condensate was calculated. Utilizing this gas-condensate ratio in conjunction with the experimentally determined hydrocarbon compositions of the separator products and the measured laboratory shrinkage of the condensate liquid, a wellstream composition was calculated. These compositions are to be found on page two. The laboratory shrinkage data may be found on page five.

The separator products were physically recombined at the above gascondensate ratio and the resultant reservoir gas-condensate utilized for the remainder of the study.

A portion of the gas-condensate was placed in a high pressure visual cell and examined at the reservoir temperature of 154°F. At this temperature the system exhibited a retrograde dew point at 2118 psig. The pressure-volume relations are shown on page three.

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Norske Shell Exploration & Production Continued/...

Page Two

The wellstream composition was used to calculate the cumulative stock tank liquid and sales gas recovery using normal two stage separation. Also calculated are the plant liquid products on the primary and secondary stage separator gases. The total plant products in the wellstream are also shown. All recoveries are based on one MMSCF of original reservoir fluid. It must be remembered in applying these data that all recoveries are based on 100 percent plant efficiency. These data may be found on page four.

The extended hydrocarbon composition to eicosanes plus of the condensate fluid was determined by gas chromatography and this composition may be found on page six.

The extended composition to eicosanes plus of the reservoir fluid was calculated and this composition is presented on page seven.

In view of these results, the reservoir fluid would usually be considered a dry gas system, and consequently we would not normally perform a "step-wise" equilibrium (constant volume) depletion to simulate wellstream behaviour below the dew point. We will retain the samples in our laboratory pending further instructions from Norske Shell Exploration & Production.

It has been a pleasure to be of service to Norske Shell Exploration & Production. Should any questions arise concerning the data presented in this report, please do not hesitate to contact us.

> Very truly yours, Core Laboratories U.K. Ltd.,

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LKS/HG 15 cc addressee L. K. Sebborn, Laboratory Manager - RFL

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Company Norske Shell Expl. & Prod.	Date Sampled 8th July, 1980
Well	County North Sea
Field	State Norway

FORMATION CHARACTERISTICS

Formation Name	Clean Sand
Date First Well Completed	19
Original Reservoir Pressure	PSIG @Ft.
Original Produced Gas-Liquid Ratio	SCF/Bbl
Production Rate	Bbls/Day
Separator Pressure and Temperature	PSIGºF.
Liquid Gravity at 60°F.	° API
Datum	Ft. Subsea

Datum

WELL CHARACTERISTICS

Elevation	Ft.
Total Depth	Ft.
Producing Interval	1435-1460 m
Tubing Size and Depth	$\frac{5}{1405.6}$ m
Open Flow Potential	MMSCF/Day
Last Reservoir Pressure	
Date	19
Reservoir Temperature	
Status of Well	
Pressure Gauge	

SAMPLING CONDITIONS

	PSIG
	PSIG
325	PSIG
100	° F.
	PSIG
	• F .
	° API @ 60° F.
00	MSCF/Day

Field Stock Tank Liquid Gravity		
Primary Separator Gas Production Ra	ate	
Pressure Base	14.696	PSIA
Temperature Base	60	°F.
Compressibility Factor (F)	1.0201	
Gas Gravity (Laboratory)	0.606	
Gas Gravity Factor (F)	1.2846	
Bringer g	0_	

Primary sep. Liquid Production Rate @ 100°F Primary Separator Gas/. Primary sep... Liquid Ratio

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49.55	Bbls/Day
	SCF/Bbl
	Bbls/MMSCF
Flopetrol	

Sampled by

Flowing Tubing Pressure Flowing Bottom Hole Pressure Primary Separator Pressure Primary Separator Temperature Secondary Separator Pressure Secondary Separator Temperature

REMARKS:

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Component	Separator Liquid * Mol Per Cent	Separator Gas Mol Per Cent	+ Well Stream GPM Mol Per Cent
Hydrogen Sulfide	NIL	NIL	NIL
Carbon Dioxide	0.15	0.56	0.56
Nitrogen	0.06	1.59	1.59
Methane	8.31	93.14	92.88
Ethane	1.45	3.45	3.45
Propane	0.44	0.39	0.39
iso-Butane	0.65	0.30	0.30
n-Butane	0.13	0.04	0.04
iso-Pentane	0.57	0.04	0.04
n-Pentane	0.21	0.01	0.01
Hexanes	3.11	0.15	0.16
Heptanes plus	84.92	0.33	0.58
	100.00	100.00	100.00
Properties of Heptanes plus			
API gravity @ 60° F.	43.9		
Specific gravity @ 60/60° F.	0.8068		0.7375
Molecular weight	130	103	112
Calculated separator gas gravity (a Calculated gross heating value for s per cubic foot of dry gas @ 14.696	eparator gas = $\dots 1050$	BTU	
Primary separator gas collected @ Primary separator liquid collected @		.00°F. .00°F.	
Primary separator gas/separator liq Primary separator liquid/stock tanl		SCF/Bbl@ 325 psi Bbls@ 325 psig a	ig and 100 ⁰ F and 100 ⁰ F per Bbl at (
* Cylinder Number	: 20524/83		

These analyses, opinions or interpretations are based on observations and material supplied by the client to whom, and for whose exclusive and confidential use, this report is made. The interpretations or opinions expressed represent the best judgement of Core Laboratories, Inc. (all errors and omissions excepted); but Core Laboratories, Inc. and its officers and employees, assume no responsibility and make no warranty or representations as to the productivity, proper operation, or profitableness of any oil, gas or other mineral well or sand in connection with which such report is used or relied upon.

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+ Cylinder Number: A7588

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Well	31/2-3

Relative Pressure Compressibility PSIG Volume (1) Factor Z 3000 0.7140 0.878 2500 0.8463 0.868 0.868 2275 Reservoir 0.9295 Pressure 0.9622 0.869 2200 Dew Point 1.0000 0.870 2118 Pressure 2000 1.0610 1900 1.1200 1800 1.1857 1700 1.2610 1600 1.3449 1.5497 1400 1200 1.8270 2.2160 1000 800 2.8010 600 3.7725

(1) Relative Volume : V/Vsat is barrels at indicated pressure per barrel at saturation pressure.

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CALCULATED RECOVERY PER MMSCF OF ORIGINAL FLUID

Wellstream MSCF	1000
Normal Temperature Separation*	
Stock Tank liquid - Barrels Primary Separator Gas - MSCF Second Stage Gas - MSCF Stock Tank Gas - MSCF	7.55 987.53 3.70 2.31
Total Plant Products in Primary Separator Gas - Gallons**	
Propane Butanes (Total) Pentanes Plus	102 100 75
Total Plant Products in Second Stage_Gas - Gallons**	
Propane Butanes (Total) Pentanes Plus	0.50 0.43 0.23
Total Plant Products in Wellstream - Gallons**	
Propane Butanes (Total) Pentanes Plus	107 111 380
 Recovery Bases: Primary separation at 1250 psig Second Stage at 500 psig and 40 Stock Tank at 0 psig and 27 F 	g and 40 ⁰ F)F
** Recovery assumes 100% plant efficiency	

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SEPARATOR TESTS OF Separator Liquid SAMPLE +

SEPARATOR PRESSURE PSI GAUGE	SEPARATOR TEMPERATURE OF	SEPARATOR GAS/OIL RATIO (1)	STOCK TANK GAS'OIL RATIO (1)	STOCK TANK GRAVITY APJ 40 60°F	SHRINKAGE FACTOR VR/VSAT (2)	FORMATION VOLUME FACTOR (3)	SPECIFIC GRAVITY OF FLASHED GAS
0	65		89	44.5	0.9204	1.0865	0.841

+ Cylinder Number: 20524/83

- (1) Separator and Stock Tank Gas/Oil Ratio in cubic feet of gas @ 60°F and 14.7 PSI absolute per barrel of stock tank oil @ 60°F.
- (2) Shrinkage Factor : Vr/Vsat. is barrels of stock tank oil @ 60°F per barrel of saturated oil @325..... PSI gauge and ...100...... F.

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HYDROCARBON ANALYSIS OF SEPARATOR LIQUID SAMPLE

Component:	Mol Percent:	Weight Percent:
Hydrogen Sulphide	NIL	NIL
Carbon Dioxide	0.15	0.06
Nitrogen	0.06	0.02
Methane	8.31	1.15
Ethane	1.45	0.38
Propane	0.44	0.17
Iso-Butane	0.65	0.33
N-Butane	0.13	0.07
Iso-Pentane	0.57	0.35
N-Pentane	0.21	0.13
Hexanes	3.11	2.30
Methyl Cyclopentane	2.76	1.94
Benzene	NIL	NIL
Cyclohexane	4.17	2.93
Heptanes	3.73	3.13
Methyl Cyclohexane	9.62	7.91
Toluene	0.78	0.59
Octanes	7.95	7.61
Ethylbenzene	1.17	1.04
Meta and Para Xylene	4.36	3.88
Orthoxylene	0.59	0.52
Nonanes	7.29	7.83
1, 2, 4 Trimethylbenzene	3.04	3.06
Decanes	10.40	12.38
Undecanes	10.67	13.16
Dodecanes	4.78	6.45
Tridecanes	4.80	7.04
Tetradecanes	3.51	5.60
Pentadecanes	2.51	4.32
Hexadecanes	1.00	1.86
Heptadecanes	0.83	1.64
Octadecanes	0.44	0.92
Nonadecanes	0.26	0.56
Eicosanes plus	0.26	0.67
	100.00	100.00

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HYDROCARBON ANALYSIS OF WELLSTREAM SAMPLE

Component:	Mol Percent:
Hydrogen Sulphide	NIL
Carbon Dioxide	0.56
Nitrogen	1.59
Methane	92.88
Ethane	3.45
Propane	0.39
Iso-Butane	0.30
N-Butane	0.04
Iso-Pentane	0.04
N-Pentane	0.01
Hexanes	0.16
Methyl Cyclopentane	0.05
Benzene	NIL
Cyclohexane	0.06
Heptanes	0.07
Methyl Cyclohexane	0.06
Toluene	TRACE
Octanes	0.05
Ethylbenzene	TRACE
Meta and Para Xylene	0.03
Orthoxylene	TRACE
Nonanes	0.05
1, 2, 4 Trimethylbenzene	0.02
Decanes	0.05
Undecanes	0.04
Dodecanes	0.02
Tridecanes	0.02
Tetradecanes	0.02
Pentadecanes	0.02
Hexadecanes	0.01
Heptadecanes	0.01
Octadecanes	TRACE
Nonadecanes	TRACE
Eicosanes plus	TRACE
	100.00

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Norske Shell Exploration & Production RFLA 80167B

Core Laboratories U.K. Ltd., Reservoir Fluid Analysis,

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L. K. Sebborn, Laboratory Manager - RFL

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