Denne rapport tilhører

STATOIL

L&U DOK. SENTER

L. NR. 20088390021

KODE WELL 31/2-3

nc28

Returneres etter bruk

Reservoir Fluid Analysis

For

Norske Shell Exploration & Production

Well: 31/2-3

North Sea, Norway

CORE LABORATORIES UK LTD. Petroleum Reservoir Engineering ABERDEEN, SCOTLAND

Reservoir Fluid Analysis

For

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Well: 31/2-3

North Sea, Norway

Petroleum Reservoir Engineering

ABERDEEN, SCOTLAND

6th January, 1981

Norske Shell Exploration & Production, Damsle Ferusuei 43. P.O. Box 10, 40-33 Forus, Stavanger. Norway.

Attention: Mr. Dave Jolly

Subject: Reservoir Fluid Analysis

Well: 31/2-3North Sea, Norway

Our File Number: RFLA 80169

Gentlemen,

On 23rd June, 1980, samples of separator gas and condensate were collected during testing of the subject well and forwarded to our Aberdeen laboratory for analysis. The results of these analyses as requested by a representative of Norske Shell Exploration & Production are presented in the following report.

The hydrocarbon composition of the separator gas was determined by routine gas chromatography. The hydrocarbon composition of the condensate liquid was determined by low temperature fractional distillation.

After correcting the quoted producing gas-condensate ratio for the factors shown on page one a corrected gas-condensate ratio of 417947 SCF/BBL of separator condensate was calculated. Utilizing this gas-condensate ratio in conjunction with the experimentally determined hydrocarbon compositions of the separator products and the measured laboratory shrinkage of the condensate liquid, a wellstream composition was calculated. compositions are to be found on page two. The laboratory shrinkage data may be found on page five.

The separator products were physically recombined at the above gascondensate ratio and the resultant reservoir gas-condensate utilized for the remainder of the study.

A portion of the gas-condensate was placed in a high pressure visual cell and examined at the reservoir temperature of 154°F. At this temperature the system exhibited a retrograde dew point at 1842 psig. pressure-volume relations are shown on page three.

Continued/...

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Page Two

The wellstream composition was used to calculate the cumulative stock tank liquid and sales gas recovery using normal two stage separation. Also calculated are the plant liquid products on the primary and secondary stage separator gases. The total plant products in the wellstream are also shown. All recoveries are based on one MMSCF of original reservoir fluid. It must be remembered in applying these data that all recoveries are based on 100 percent plant efficiency. These data may be found on page four.

The extended hydrocarbon composition to eicosanes plus of the condensate fluid was determined by gas chromatography and this composition may be found on page six.

The extended composition to eicosanes plus of the reservoir fluid was calculated and this composition is presented on page seven.

In view of these results, the reservoir fluid would usually be considered a dry gas system, and consequently we would not normally perform a "step-wise" equilibrium (constant volume) depletion to simulate wellstream behaviour below the dew point. We will retain the samples in our laboratory pending further instructions from Norske Shell Exploration & Production.

It has been a pleasure to be of service to Norske Shell Exploration & Production. Should any questions arise concerning the data presented in this report, please do not hesitate to contact us.

> Very truly yours, Core Laboratories U.K. Ltd.,

LKS/HG 15 cc addressee L. K. Sebborn, Laboratory Manager - RFL

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Company Norske Shell Exploration & Prod. Da	ate Sampled 23rd June, 1980
21 /2-2	North Sea
	Norway
Tied	11C
FORMATION CHARA	
Formation Name	Micaceous Sand
Date First Well Completed	19
Original Reservoir Pressure	PSIG @Ft.
Original Produced Gas-Liquid Ratio	SCF/Bbl
Production Rate	Bbls/Day
Separator Pressure and Temperature	PSIG°F.
Liquid Gravity at 60°F.	° API
Datum	Ft. Subsea
WELL CHARACT	ERISTICS
Elevation	Ft.
Total Depth	Ft.
Producing Interval	1520-1535 m
Tubing Size and Depth	5 In. to 1491 m
Open Flow Potential	MMSCF/Day
Last Reservoir Pressure	2275 PSIG @Ft.
Date	, 19
Reservoir Temperature	° F. @ Ft.
Status of Well	
Pressure Gauge	
SAMPLING CON	DITIONS
Flowing Tubing Pressure	PSIG
Flowing Bottom Hole Pressure	PSIG
Primary Separator Pressure	
Primary Separator Temperature	65 ° F.
Secondary Separator Pressure	PSIG
Secondary Separator Temperature	°F.
Field Stock Tank Liquid Gravity	° API @ 60° F.
Primary Separator Gas Production Rate	18377MSCF/Day
Pressure Base 14.696 PSIA	
Temperature Base 60 °F Compressibility Factor (F) 1.0358	•
Gas Gravity (Laboratory) 0.597	
Gas Gravity Factor (F) 1.2942	
Primary sepLiquid Production Rate @ 65°F	43.97
Primary Separator Gas/Primary sepLiquid Ratio	
or	2.39 Bbls/MMSCF
Sampled by	Flopetrol

REMARKS:

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Hydrocarbon Analyses of Separator Products and Calculated Well Stream

	Separator Liquid +	Separator (Gas *	Well Stream
Component	Mol Per Cent	Mol Per Cent	GPM	Mol Per Cent
				-
Hydrogen Sulfide	NIL	NIL		NIL
Carbon Dioxide	0.29	0.57		0.57
Nitrogen	0.05	1.59		1.59
Methane	14.12	93.46		93.27
Ethane	3.14	3.45		3.45
Propane	1.14	0.38	0.104	0.38
iso-Butane	2.02	0.28	0.091	0.28
n-Butane	0.42	0.04	0.013	0.04
iso-Pentane	1.22	0.03	0.011	0.03
n-Pentane	0.42	0.01	0.004	0.01
Hexanes	3.77	0.04	0.006	0.05
Heptanes plus	73.41	0.15	0.068	0.33
	100.00	100.00	0.307	100.00
Properties of Heptanes plus				
API gravity @ 60° F.	47.4			
Specific gravity @ 60/60° F.	0.7912			0.750
Molecular weight	120	103		112

Calculated separator gas gravity (air=1.000)=...0.597... Calculated gross heating value for separator gas=....1037...BTU per cubic foot of dry gas @ 14.696 psia and 60° F.

Primary separator gas collected @...480...psig and ...65....°F. Primary separator liquid collected @...480...psig and ...65....°F.

Primary separator gas/separator liquid ratio ...417.947.....SCF/Bbl @ 480 psig and 65°F

Primary separator liquid/stock tank liquid ratio ...1.1246....Bbls @ 480 psig and 65°F/BBl at 0 psig and 60°F

+ Cylinder Number: 20584/57

* Cylinder Number: A8643

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Pressure-Volume Relations at ...154.... °F.

Pressure PSIG		Relative Volume (1)	Compressibility Factor Z
3000		0.6988	0.876
2500		0.8266	0.865
2275	Reservoir	0.9092	0.866
2200	Pressure	0.9409	0.867
2100		0.9869	0.868
2074	Dew Point	1.0000	0.869
2000	Pressure	1.0391	
1900		1.0972	
1800		1.1616	
1700		1.2346	
1600		1.3174	
1400		1.5190	
1200		1.7890	
1000		2.1728	
800		2.7463	
600		3.6737	

(1) Relative Volume: V/Vsat is barrels at indicated pressure per barrel at saturation pressure.

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CALCULATED RECOVERY PER MMSCF OF ORIGINAL FLUID

Wellstream MSCF	1000
Normal Temperature Separation*	
Stock Tank liquid - Barrels Primary Separator Gas - MSCF Second Stage Gas - MSCF Stock Tank Gas - MSCF	3.41 994.14 1.74 1.08
Total Plant Products in Primary Separator Gas - Gallons**	
Propane Butanes (Total) Pentanes Plus	102 99 56
Total Plant Products in Second Stage Gas - Gallons**	
Propane Butanes (Total) Pentanes Plus	0.23 0.20 0.08
Total Plant Products in Wellstream - Gallons**	
Propane Butanes (Total) Pentanes Plus	105 104 195

^{*} Recovery Bases: Primary separation at 1250 psig and 40°F Second Stage at 500 psig and 40°F Stock Tank at 0 psig and 27°F

^{**} Recovery assumes 100% plant efficiency

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SEPARATOR TESTS OF Separator Liquid SAMPLE

SEPARATOR PRESSURE PSI GAUGE	SEPARATOR TEMPERATURE OF	SEPARATOR GAS/OIL RATIO	STOCK TANK GAS/OIL RATIO (1)	STOCK TANK CRAVITY API "# 60°F	SHRINKAGE FACTOR VR/VSAT (2)	FORMATION VOLUME FACTOR (3)	SPECIFIC GRAVITY OF FLASHED GAS
0	65		210	50.0	0.8892	1.1246	0.876

- (1) Separator and Stock Tank Gas/Oil Ratio in cubic feet of gas @ 60°F and 14.7 PSI absolute per barrel of stock tank oil @ 60°F.
- (2) Shrinkage Factor: Vr/Vsat. is barrels of stock tank oil @ 60°F per barrel of saturated oil @480..... PSI gauge and
- (3) Formation Volume Factor: Vsat/Vr is barrels of saturated oil @480..... PSI gauge and65...... F per barrel of stock tank oil @ 60°F.

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HYDROCARBON ANALYSIS OF SEPARATOR LIQUID SAMPLE

Component:	Mol Percent:	Weight Percent:
Hydrogen Sulphide	NIL	NIL
Carbon Dioxide	0.29	0.14
Nitrogen	0.05	0.02
Methane	14.12	2.36
Ethane	3.14	0.98
Propane	1.14	0.52
Iso-Butane	2.02	1.23
N-Butane	0.42	0.25
Iso-Pentane	1.22	0.92
N-Pentane	0.42	0.31
Hexanes	3.77	3.39
Methyl Cyclopentane	5.16	4.53
Benzene	NIL	NIL
Cyclohexane	7.29	6.40
Heptanes	5.94	6.20
Methyl Cyclohexane	13.00	13.32
Toluene	0.96	0.92
Octanes	8.81	10.49
Ethylbenzene	0.83	0.92
Meta and Para Xylene	3.94	4.36
Orthoxylene	0.49	0.53
Nonanes	6.53	8.72
1, 2, 4 Trimethylbenzene	1.52	1.91
Decanes	6.63	9.83
Undecanes	4.66	7.15
Dodecanes	2.64	4.44
Tridecanes	1.97	3.60
Tetradecanes	1.42	2.81
Pentadecanes	0.84	1.80
Hexadecanes	0.38	0.87
Heptadecanes	0.23	0.57
Octadecanes	0.10	0.28
Nonadecanes	0.03	0.10
Eicosanes plus	0.04	0.13
	100.00	100.00

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HYDROCARBON ANALYSIS OF WELLSTREAM SAMPLE

Component:	Mol Percent:
Hydrogen Sulphide	NIL
Carbon Dioxide	0.57
Nitrogen	1.59
Methane	93.27
Ethane	3.45
Propane	0.38
Iso-Butane	0.28
N-Butane	0.04
Iso-Pentane	0.03
N-Pentane	0.01
Hexanes	0.05
Methyl Cyclopentane	0.03
Benzene	NIL
Cyclohexane	0.05
Heptanes	0.04
Methyl Cyclohexane	0.05
Toluene	TRACE
Octanes	0.04\
Ethylbenzene	TRACE (
Meta and Para Xylene	0.01)
Orthoxylene	TRACE
Nonanes	0.03
1, 2, 4 Trimethylbenzene	TRACE
Decanes	0.02
Undecanes	0.01
Dodecanes	0.01
Tridecanes	0.01
Tetradecanes	0.01
Pentadecanes	0.01
Hexadecanes	0.01
Heptadecanes	TRACE
Octadecanes	TRACE
Nonadecanes	TRACE
Eicosanes plus	TRACE
-	100.00

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