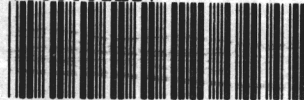


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SAGA PETROLEUM AS

# WELLFILE

NORSK HYDRO a.s

FINAL REPORT

WELL 15/5-2

LICENCE 048

No 20

FC



Norsk Hydro

Saga Petroleum a.s.  
INFORMASJONSSENTRET

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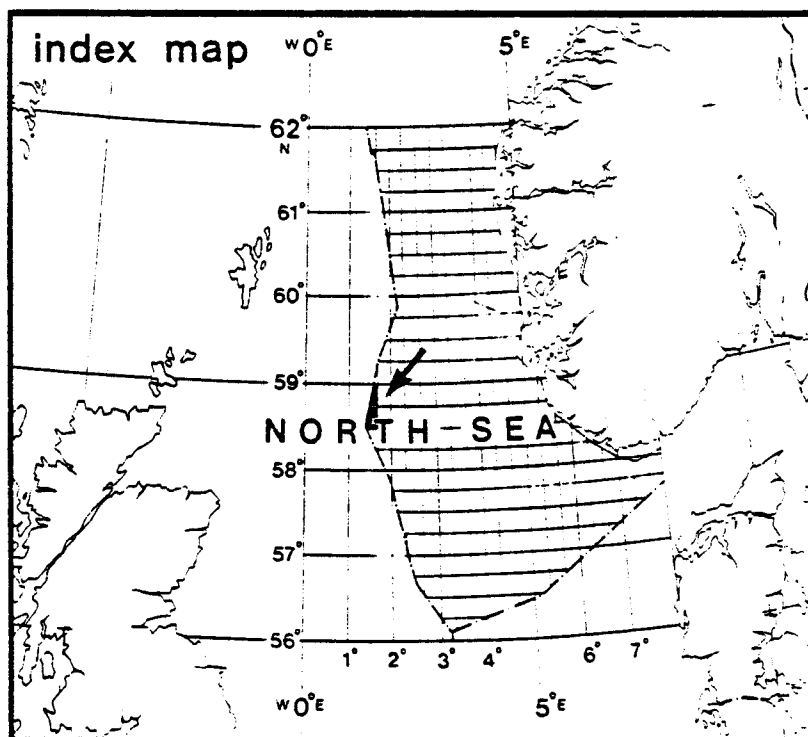
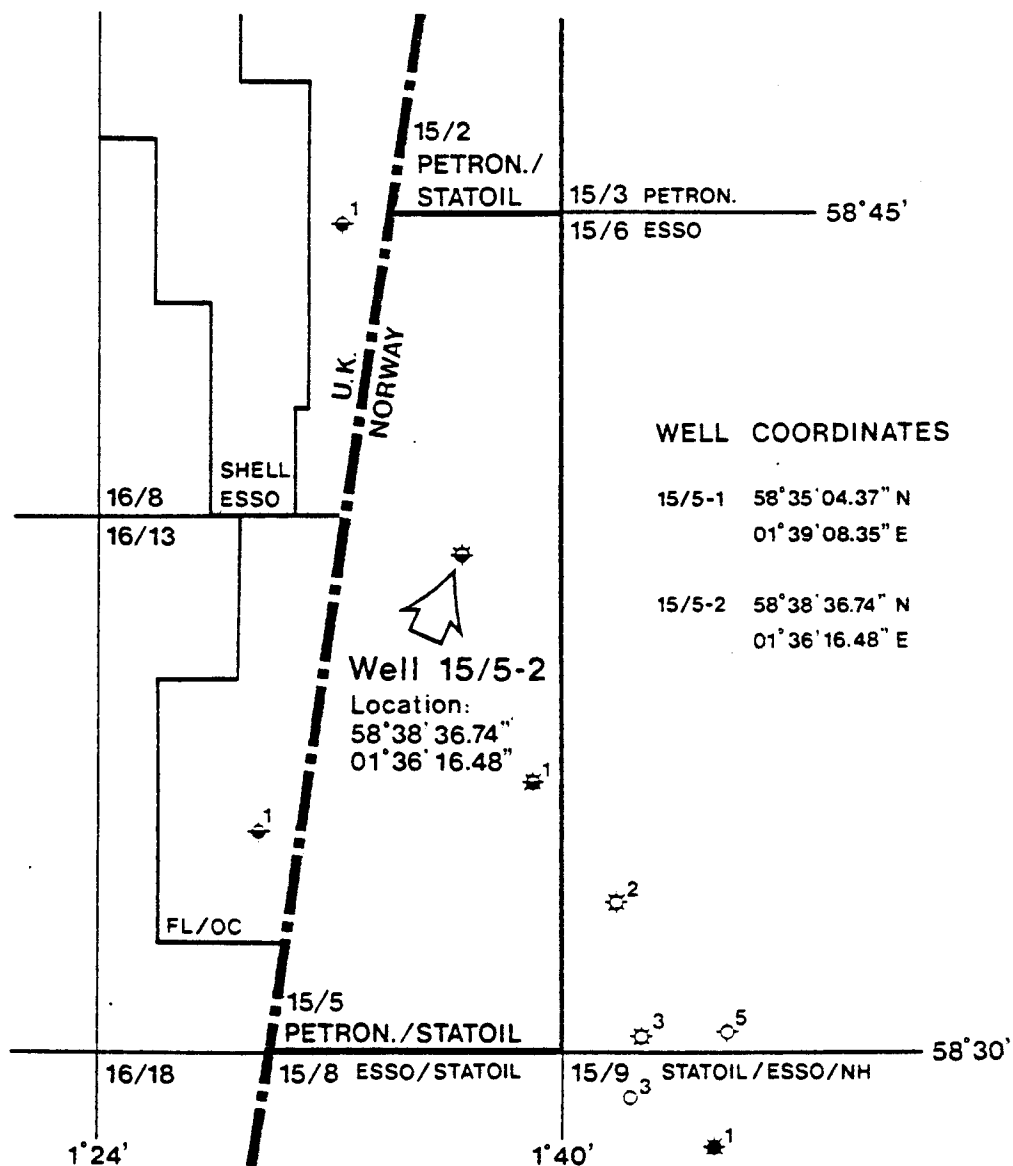
PREFACE

Licence 048 was awarded the Statoil/Petronord group February 18, 1977 with Norsk Hydro Produksjon a.s as operator. The licence includes the blocks 15/2 and 15/5 on the Norwegian continental shelf.

The group consists of the following companies:

|                              |       |
|------------------------------|-------|
| Den norske stats oljeselskap | 50%   |
| Elf Aquitaine Norge a.s      | 21.8% |
| Norsk Hydro Produksjon a.s   | 17.3% |
| Total Marine Norsk a.s       | 10.9% |

The well 15/5-2 was drilled by Norsk Hydro Produksjon a.s on behalf of the Statoil/Petronord Group.



## location map

5 km

5 miles



Norsk Hydro



TABLE 1  
SUMMARY OF WELL DATA

|                        |                               |
|------------------------|-------------------------------|
| Location:              | 58°38'36.7" N<br>1°36'16.5" E |
| Operator:              | Norsk Hydro<br>Produksjon a.s |
| Rig:                   | Treasure Seeker               |
| Contractor:            | Wilh.      Wilhelmsen         |
| RKB elevation (to MSL) | 25 m                          |
| Water depth            | 120.5 m MSL (145.5 m RKB)     |

Phase I

|                           |  |
|---------------------------|--|
| Start of operations:      | August 15, 1978  |
| Well spudded:             | August 16, 1978  |
| Well temporary abandoned: | December 16, 1978  |
| T.D. (Driller):           | 4322 m   |
| T.D. (Logger):            | 4326 m   |
| Formation at T.D.:        | Triassic sandstones  |
| Status:                   | Temporarily abandoned<br>with oil and gas shows<br>in Jurassic and Triassic<br>sandstones. |

Well program

|              |                   |
|--------------|-------------------|
| Hole record: | 36" to 194.5 m    |
|              | 26" to 469 m      |
|              | 17½" to 1615 m    |
|              | 12-1/4" to 3714 m |
|              | 8-3/8" to 4322 m  |

Casing record: 30" set at 194 m  
20" set at 454 m  
13-3/8" set at 1598 m  
9-5/8" set at 3696 m  
7" liner set at 4300 m

All depths are given with reference to RKB.

SECTION A

GEOLOGY

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### SECTION A

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APPENDIX 1: Core descriptions

APPENDIX 2: Side wall core descriptions

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1. OBJECTIVES

The main objective of the well was to test possible hydrocarbon accumulations in Middle to Upper Jurassic Bathonian/Callovian transgressive sandstones and Middle Jurassic Bajocian deltaic sandstones. The well was located in a purposely off crestal position on an approx. 16 sq. km large structure some 7 km NW of the 15/5-1 discovery. The well was planned to penetrate into the Triassic with a projected total depth of 4500 m.

2. RESULTS

The 15/5-2 well encountered two hydrocarbon bearing sandstone intervals. In the Jurassic a thin Early to Middle Bathonian sandstone development was penetrated. Below in a formation interpreted to be of Triassic age a second hydrocarbon bearing sandstone interval was encountered. The prognosed well-developed Bathonian/Callovian and Bajocian sandstones were not found.

The Jurassic sandstone interval extended between 4035 m (depths ref.: loggers depths below K.B.) and 4055 m in the well. Interbeds of siltstones and shales reduced the 20 m gross pay to a net pay of 7.3 m from wireline log interpretation. Average porosity and average water saturation over the pay interval have been calculated to 14.3 and 41.7% respectively.

The top of the Triassic sandstones were encountered at 4141.3 m and continued with interbeds of varicoloured shales and siltstones to the T.D. of the well at 4326 m. From wireline log evaluation hydrocarbon bearing sandstones can be seen down to 4158.1 m. Below this a tight cemented sandstone appears, masking the exact hydrocarbon - water contact. Proved grosspay interval is thus 16.8 m while the net pay is 12.8 m. Average porosity over this interval has been calculated to 14.6 % and the average water saturation to 43 %.

RFTs were run to evaluate both reservoirs. In the Jurassic sandstone at 4053 m a formation pressure of 705.1 bars (10227 psig) was recorded. The Triassic sandstone reservoir had a formation pressure at 4143.5 m of 721.2 bars (10460 psig). Several segregated samples were taken, but all failed to recover any formation fluid.

The well was terminated at a depth of 4326 m in a formation interpreted to be of Triassic age. It is temporarily abandoned and will be re-entered to be production tested over the Triassic sandstone interval 4142 - 4158 m.

3.

### STRATIGRAPHY

The biostratigraphic evaluation of the well 15/5-2 has been performed by the laboratories of Robertson Research International Ltd., covering the interval 200 - 4323 m (KB).

The basic material for the analyses is ditch cutting samples, but also chips from conventional cores and a substantial number of side wall core samples have been studied.

Well site micropalaeontology was carried out during the drilling of the section from 3230 m to 3712 m, covering the Upper Cretaceous from Santonian and down into Hauterivian in the Lower Cretaceous. The objective of this service was to try to obtain a more precise stratigraphic breakdown of the formations while drilling into the Lower Cretaceous, to be able to run the 9 5/8" casing safely before penetrating the Upper Jurassic. The information thus obtained was also incorporated into the following analyses in the laboratory.

The final stratigraphic breakdown of the well has been obtained by comparing and adjusting the results of the biostratigraphy with wireline log correlations.

The drillers and the wireline logs depths are often at variance through the well. Since the ditch cuttings samples, which are the primary materials on which the stratigraphy is



based, are designated on the drillers depths, the biostratigraphic tops may be different from those picked on the wireline logs. From 3500 m and down to 4130 m the biostratigraphic tops, when based on ditch cuttings samples, have been adjusted to the wireline log depths (ISF/Sonic/GR runs) as follows:

Loggers depth = Drillers depth + 4 m.

The chrono- and lithostratigraphy of the well is shown on page 4 and 5 . The lithostratigraphic terminology applied is taken from Deegan and Scull: "A standard lithostratigraphic nomenclature for the Central and Northern North Sea" 1977.



Norsk Hydro

Oslo - Norway

WELL: 15/5-2

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DEPTH REF: K.B.

ELEVATION K B: 25 m

ALL DEPTH IN METERS (m)

| CRONOSTRATIGRAPHY |                |                       |                   | LITHOSTRATIGRAPHY |                    |      |
|-------------------|----------------|-----------------------|-------------------|-------------------|--------------------|------|
| SYSTEM            | SERIES / STAGE | DEPTH                 | THICKNESS         | GROUP             | FORMATION / MEMBER |      |
|                   |                | 145.5                 |                   | 145.5             |                    |      |
| QUATERNARY        | PLEISTOCENE    |                       | 334.5             |                   |                    |      |
| TERTIARY          |                | 480                   |                   | NORDLAND GROUP    |                    |      |
|                   | PLIOCENE       |                       | 220               |                   |                    |      |
|                   |                | 700                   |                   |                   | 758                |      |
|                   | MIOCENE        |                       | 360               |                   | UTSIRA FM          |      |
|                   |                | 1060                  |                   | 1040              | 1040               |      |
|                   | OLIGOCENE      |                       | 440               | HORDALAND GROUP   |                    |      |
|                   |                | 1500                  |                   |                   | 1603               |      |
|                   | EOCENE         |                       | 600               |                   | FRIGG FM           |      |
|                   |                | 2100                  |                   | 2128              | 2128               |      |
|                   | PALEOCENE      |                       | 682               | ROGALAND GROUP    | BALDER FM          | 2162 |
|                   |                | SELE FM               |                   |                   | 2204               |      |
|                   |                | LISTA FM              |                   |                   | 2252               |      |
|                   |                |                       | MONTROSE GR. 2606 | HEIMDAL FM        | 2606               |      |
|                   |                |                       | ROGALAND GR. 2705 | LISTA FM          | 2650               |      |
|                   |                |                       |                   | MAUREEN FM        | 2705               |      |
|                   |                |                       |                   | EKOFISK FM        | 2782               |      |
| CRETACEOUS        | UPPER          |                       |                   | CHALK GROUP       | TOR FM             | 2967 |
|                   |                | MAASTRICHTIAN         | 278               |                   |                    |      |
|                   |                | CAMPANIAN - SANTONIAN | 3060              |                   |                    |      |
|                   |                |                       | 3293              |                   |                    |      |



Norsk Hydro

Oslo - Norway

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WELL : 15/5 - 2

DEPTH REF. K.B.

ELEVATION K.B.: 25 m

ALL DEPTH IN METERS (m)

| CRONOSTRATIGRAPHY |                |                               |             | LITHOSTRATIGRAPHY |                  |                         |
|-------------------|----------------|-------------------------------|-------------|-------------------|------------------|-------------------------|
| SYSTEM            | SERIES / STAGE |                               | DEPTH       | THICKNESS         | GROUP            | FORMATION / MEMBER      |
| CRETACEOUS        | UPPER          |                               | 3293        | 295               | CHALK GROUP      | FLOUNDER FM 3440        |
|                   |                | CONIACIAN - TURONIAN          |             |                   |                  | HERRING FM 3507         |
|                   |                |                               | 3588        |                   |                  | PLENUS MRL FM 3588      |
|                   |                | CENOMANIAN                    |             |                   |                  | HIDRA FM 3647           |
|                   | LOWER          | ALBIAN                        | 3637        | 52                | CROMER KNOLL GR. | RØDBY FM 3689           |
|                   |                | EARLY ALB - APT.              | 3689        | 12                |                  | VALHALL FM 3759         |
|                   |                | EARLY BARREM.                 | 3701        | 10                |                  |                         |
|                   |                | HAUTERIVIAN                   | 3711        | 33                |                  |                         |
|                   |                | EARLY VALANG.                 | 3744        | 15                |                  |                         |
|                   |                | LATE - EARLY RYAZ.            | 3759        | 15                |                  |                         |
|                   |                |                               | 3774        |                   |                  |                         |
|                   |                | MID - EARLY VOLG.             |             | 30                | HUMBER GROUP     | KIMMERIDGE CLAY FM 3831 |
| JURASSIC          | UPPER          | KIMMERIDGIAN                  | 3804        | 15                |                  | HEATHER FM 3960         |
|                   |                |                               | 3819        |                   |                  |                         |
|                   |                | LATE OXFORDIAN                |             | 55                |                  |                         |
|                   |                | EARLY OXFORD.                 | 3869        | 25                |                  |                         |
|                   |                | LATE-MID. CALLOV.             | 3894        | 30                |                  |                         |
|                   |                | EARLY CALLOV.                 | 3924        | 36                |                  |                         |
|                   | MIDDLE         | LATE - MIDDLE BATHONIAN       | 3960        | 77                | BRENT FM.        |                         |
|                   |                | EARLY BATHON. - MID. BAJOCIAN | 4037        | 55                |                  |                         |
|                   |                | BAJOCIAN                      | 4087        | 24                |                  | 4113                    |
|                   |                |                               | 4113        |                   |                  |                         |
| TRIASSIC          | TRIASSIC       |                               |             | 210               |                  |                         |
|                   |                |                               | 4323 (T.D.) |                   | 4323             | 4323                    |

#### 4. LITHOSTRATIGRAPHY

This summary is compiled predominantly from ditch cuttings descriptions. Wire line logs are used as assistance in the lithological interpretation and to place boundaries of rock formations. Supplementary side wall core samples are available from Eocene in the Tertiary, through the Cretaceous and Jurassic and down into the Triassic.

##### 4.1 QUATERNARY

###### Pleistocene (194 - 480 m)

The interval is predominantly clay, medium to dark grey, soft to firm, slightly sticky, slightly to moderately calcareous, with thin silty stringers. The clay is rarely glauconitic and contains traces of pyrite and shell fragments which occur throughout the interval.

Interbeds of sand are found between 194 to 283 m. These are composed of clear occasionally frosted quartz grains, very fine to coarse, occasionally very coarse, angular to subrounded, poorly sorted, with dark grey to dark green to black lithic fragments and occasional shell fragments. Thin beds of dark brown woody lignite occur between 277 and 283 m.

The interval from sea bed and down to 1040 m is included in the Nordland Group.

##### 4.2 TERTIARY

###### Pliocene (480 - 700 m)

Continuation of the medium to dark grey clays, occasionally silty and lignitic with locally abundant shell fragments and traces of glauconite.

Miocene (700 - 1060 m)

700 - 758 m

Continuation of clays as described above.

758 - 910 m

The abrupt break from the overlying clays to the sands which form the upper part of the Utsira Formation occurs at 758 m. These sands are clear, very fine to fine grained angular to sub-angular, moderately well sorted, loose quartz with traces of glauconite, pyrite, mica and shell fragments. Occasionally minor clays which are olive grey, soft, sticky and slightly calcareous occur.

910 - 1060 m

This is a dominantly clay interval with some thin sands in the top 20 m and represents a transition from the Utsira Formation of the Norland Group (base at 1040 m) to the underlying Hordaland Group.

The clays are olive grey to olive green becoming various shades of brown, soft, sticky, slightly to moderately silty occasionally sandy and none to slightly calcareous with traces of glauconite, mica and shell fragments. The sand stringers consist of clear to milky quartz, very fine to medium grained, subangular to subrounded with moderate sorting. Thin stringers of a hard, grey brown dolomitic limestones also occur.

Oligocene (1060 - 1500 m)

This interval consists mainly of brown claystones as described above except for increased induration and the appearance of siltstone laminations below 1250 m. These siltstones are medium grey, brown grey and brown green, firm, micro micaceous, moderately calcareous and occasionally grade to very fine sandstone.

Two coarser clastic beds occur in this interval; an upper sand bed between 1180 and 1190 m composed of clear, very fine to medium grained quartz, occasionally becoming coarse grained, angular to sub-angular, poorly sorted with lithic fragments; and a lower sandstone bed, 1272 to 1278 m consisting of clear, white, very fine to medium grained quartz, angular to subangular, with moderate sorting, moderately hard calcareous cement and poor visible porosity.

Eocene (1500-2100 m)

1500 - 1603 m

Claystones continue dominant but have become olive green to olive grey, blocky and silty. With increasing induration they grade to shales in the lower part of the interval. They are non- to slightly calcareous. Foraminifera are fairly common. The interval is characterized by the appearance of thin stringers of light grey to brown, argillaceous limestones. These are moderately hard and micro to cryptocrystalline.

Rare stringers of brown grey, micromicaceous siltstone occur as do traces of sandstone, formed of clear, white, very fine grained, angular to sub-angular quartz, moderately hard with a calcareous cement. Traces of glauconite and pyrite occur.



1603--1783\_m

Sandstones become dominant and characterize this interval at the top part of the Frigg Formation. These are formed from clear, some frosted, very fine to coarse, occasionally very coarse grained, angular to sub-angular quartz, loose and hard, with a calcareous or siliceous cement. Interbeds of claystones and shales of various shades of green and brown occur. These are blocky to sub-fissile, slightly micro-micaceous, waxy, non-calcareous, silty in parts grading to stringers of brown black siltstone.

Traces of pyrite, glauconite and micro-fossils were found as were occasional thin stringers of white to light grey and light yellow brown, firm to hard, micro to crypto-crystalline limestone, which is occasionally dolomitic and argillaceous.

1783--1871\_m

This interval is composed mainly of medium to dark grey or grey black shales with minor green black stringers. This shale is similar to the shale in the upper unit. Traces of dusky red, soft to firm, sub-fissile, non-calcareous shale occur, as do stringers of micro-crystalline limestone and occasional interbeds of sand and sandstone as described in the above unit.

1871--1916\_m

This is a sand unit made up of clear, milky, fine to coarse grained, sub-angular to sub-rounded, loose quartz with thin interbeds of yellow brown to light grey argillaceous dolomitic limestone. Traces of pyrite and micro-fossils occur throughout the unit.

1916 - 2063 m

Shales light dark grey, green grey and grey brown, subfissile, occasionally silty and sandy, and non-calcareous constitute the main lithology in this interval. Thin stringers of dolomitic limestones described as above occur, becoming dolomite in the lower part which also is marked by the appearance of red brown, light grey and green, non-calcareous shales. Rare pyrite occurs throughout the unit.

2063 - 2100 m

The red brown shales occurring towards the base of the interval above become the dominant lithology in this interval. Minor grey, grey green and light grey blue shales which are soft to hard and non-calcareous occur as well and traces of light to medium grey, grey brown tuffaceous material are reported. The interval also contains traces of black carbonaceous material, pyrite, glauconite and micro-fossils.

Paleocene (2100 - 2782 m)

2100 - 2128 m

This is a continuation of the above interval and differs only in the occurrence of light grey to grey brown, soft to firm, argillaceous, dolomitic, limestone stringers. The base of this unit at 2128 m forms the junction of the Hordaland Group and the Rogaland Group.

2128 - 2204 m

Varicoloured shales with traces of tuff and thin limestone stringers and traces of pyrite as described above (except predominantly light-medium grey and grey brown in colour)

constitute the lithology in this interval which comprises the Balder Formation (2128 - 2162 m) and the Sele Formation (2162 - 2204 m) within the Rogaland Group.

2204 - 2252 m

This interval consists dominantly of medium to dark grey, grey brown to medium brown, grey green and light blue grey, non-tuffaceous, fissile to blocky, non- to slightly calcareous shales with traces of grey to brown grey, hard, calcareous siltstone and loose, fine to medium grained sand.

The interval forms the upper part of the Lista Formation within the Rogaland Group, which is separated from the lower part by the intervening arenaceous fan deposits of the Heimdal formation.

2252 - 2606 m

This interval consists mainly of thick sands and sandstones with minor interbeds of shales and occasional thin stringers of limestone and dolomite.

The sand consists of clear, fine to medium grained quartz, occasionally becoming very fine and coarse grained. It ranges from sub-rounded to angular and is moderately to poorly sorted. The sandstone is dominantly finer grained ranging from fine to very fine grained and occasionally grading to siltstone. It shows moderate sorting and a calcareous cement.

The shales are grey, grey brown and grey green, firm to moderate hard, fissile to blocky, occasionally silty and micro-micaeous and slightly to non-calcareous.

The limestones occur as white, soft, chalky and occasionally argillaceous stringers while the dolomite stringers are pale to dark yellow brown, hard and micro-crystalline.

This interval represents the Heimdal Formation of the Montrose Group.

2606-2650\_m

The sands and sandstones of the Heimdal Formation are underlain by the lower part of the Lista Formation consisting of medium grey to brown grey, soft, non-calcareous clays, medium to dark grey, green grey and some red brown micro-micaeous shales with minor interbeds of white to light yellow, soft to firm, micro-crystalline, occasionally dolomitic limestone.

Danian 2650 - 2782\_m

2650 - 2705\_m

This interval is similar to the previous one except that the clays are becoming light grey and have an increasing calcareous content. The sand/sandstone interbeds are white to light grey as above and become dominant with depth. There are thin stringers of limestone as described above.

This interval represents the Maureen Formation and forms the lower part of the Rogaland Group. Both this formation and the Lista contain traces of pyrite and glauconite.

2705 - 2782\_m

A major change occurs at the base of the Maureen Formation. The underlying Ekofisk Formation forms the upper unit of the Chalk Group and is markedly more calcareous.

The Ekofisk Formation consists predominantly of cream to white, occasionally pink, micro-crystalline to chalky limestones. These are argillaceous in part and grade to marlstones which are glauconitic in the lower part. These marlstones are predominantly medium grey to green grey, firm and blocky but occasionally red in colour. Thin stringers of dark grey to black calcareous shale occur.

4.3

CRETACEOUS

Upper Cretaceous (2782 - 3637 m)

Maastrichtian (2782 - 3060 m)

2782 - 2967 m

This interval comprises the Tor Formation consisting mainly of limestone with occasional marl interbeds and minor shale stringers.

The limestone is white to cream coloured, firm to moderately hard, crypto-crystalline and clean, some is chalky and argillaceous in part and grades to marl which is light to medium grey and soft to firm. The thin shale interbeds are light to dark grey with black laminations, firm to hard, subfiss and calcareous. Traces of pyrite and glauconite were seen in lower parts of the interval.

2967 - 3060 m

A marked decrease in the limestone and corresponding increase in amount of marlstone marks this interval which forms the upper part of the Flounder Formation.

The limestone is the same as that in the overlying Tor Formation except some appears as shades of beige and brown, micro to crypto-crystalline and hard. The marlstone is

predominantly red to red brown and firm with minor interbeds of light to medium grey marl as in the Tor Formation. The shale stringers reported above almost totally disappear.

Santonian / Campanian (3060 - 3293 m)

3060 - 3255 m

This interval is a continuation of the Flounder Formation and is marked by a continuing increase in the amount of marlstone and decrease in the amount of limestone. The marlstone forms thick dominant beds separated by usually thin stringers of limestone.

The marlstones are mainly light to medium grey with minor light to medium red brown and occasionally very argillaceous becoming shales. The limestones are cream, off-white, hard and micro to crypto-crystalline. A thin stringer of light red to brown calcareous siltstone occurs at 3208 m.

3255 - 3293 m

Shales, dark grey, hard, sub-fissile to blocky and calcareous become dominant. Interbeds of light to medium grey marlstone with fine argillaceous laminations occur.

This interval forms a continuation of the Flounder Formation.

Coniacian / Turonian (3293 - 3588 m)

3293 - 3440 m

This interval forms the base of the Flounder Formation and is marked by an increase in limestone.

The marlstone is light to medium grey, red, red brown and some light brown, soft to hard with local fine argillaceous laminations and grades to limestone. The limestone is white



to grey, with some light tan, and is basically similar to the overlying limestones, some chalky and argillaceous, some hard and crypto to micro-crystalline. It contains rare finely disseminated pyrite and traces of pyrite aggregates, some rare glauconite and rare very finely crystalline dolomite rhombs.

Shale stringers occur throughout the interval and are described as being red/brown, medium to dark grey, blocky to sub-fissile, moderately hard to hard, silty, earthy occasionally slightly carbonaceous and calcareous.

3440 - 3507 m

The overlying limestones continue down into this interval becoming more chalky and less marly, with an increase in glauconite. Both the marl and the shale become thin and minor.

This interval represents the Herring Formation.

3507 - 3588 m

This interval is marked by an increase in the amount of argillaceous material and consists of thinly interbedded marls and limestones in the upper part becoming thicker downwards with the marls becoming dominant. Some thin shales being light grey green, dark grey, micro-micaceous and slightly calcareous occur in the lower part.

This interval is defined as the Plenus Marl Formation.

Cenomanian (3588 - 3637 m)

This interval consists of the bulk of the Hidra Formation and can be divided into an upper marly section (3588 - 3610 m) and a lower limestone section.

The marls can be distinguished from the overlying grey Plenus marls by the appearance of red brown to pink interbeds.

Traces of clear, very fine grained, well sorted, glauconitic, calcareous sandstone occur in the upper marly section.

The lower limestone is similar to that described for the rest of the Chalk Group to which this Hydra Formation forms the lowest unit.

Lower Cretaceous (3637 - 3774 m)

The Lower Cretaceous comprises the Cromer Knoll Group which is divided into the Rødby Formation and the underlying Valhall Formation.

Albian (3637 - 3689 m)

The upper 10 m of the Albian (3637 - 3647 m) comprises the lowest part of the Hydra Formation as described above. The rest of the Albian consists of the Rødby Formation (3647 - 3689 m) and is predominantly light to dark grey, pink and red brown marls as described above, with thin, light grey, chalky and micro-crystalline limestone stringers which become more common downwards. Thin shale and sand stringers occur and glauconite is common in the lower part of the interval.

Early Albian - Aptian (3689 - 3701 m)

Early Barremian (3701 - 3711 m)

Hauterivian (3711 - 3744 m)

Early Valanginian (3744 - 3759 m)

This section forms the Valhall Formation and is marked by a more shaley lithology than in the overlying formations.

The shale is light to dark grey with minor red brown and occasional green grey laminations. It is firm to moderately

hard, blocky to sub-fissile, silty in parts with traces of finely disseminated pyrite and is non - to very calcareous. Thin interbeds of micro-crystalline limestone occur throughout the section and a thick marl unit occurs between 3729 and 3741 m. A thin very fine grained glauconitic sandstone occurs at 3713 - 3715 m.

Late-Early Ryazanian (3759 - 3774 m)

This interval forms the upper section of the Kimmeridge Clay Formation and consists of a dark brown, soft to firm, earthy, silty, carbonaceous, pyritic, non-calcareous shale. The Kimmeridge Clay Formation is the highest unit of the Humber Group.

4.4

JURASSIC

Upper Jurassic (3774 - 3960 m)

Middle-Early Volgian (3774 - 3804 m)

Kimmeridgian (3804 - 3814 m)

This interval is a continuation of the overlying dark brown shales and forms a part of the Kimmeridge Clay Formation. However, in this interval the shales are interbedded with two thin sandstone stringers consisting of clear to white, very fine to very coarse grained, angular to rounded, friable to hard, poorly sorted, calcareous cemented quartz with traces of glauconite.

Late Oxfordian (3814 - 3869 m)

Early Oxfordian (3869 - 3894 m)

The top 11 m of this section is a continuation of the dark brown shales of the Kimmeridge Clay Group.

Below 3831 m the shale is interbedded with medium to dark

brown micro-crystalline limestone stringers and is identified as part of the Heather Formation.

Late-Middle Callovian (3894 - 3924 m)

Early Callovian (3924 - 3960 m)

This is a continuation of the Heather Formation and forms the lowest interval of the Humber Group.

It comprises dark brown shales as described above with some medium grey, slightly calcareous shales and interbeds of dark brown, micro-crystalline dolomite. Below 3927 m the dolomite disappears and the shale is interbedded with thin stringers of light to medium brown, calcareous, silty sandstone and limestones.

Middle Jurassic (3960 - 4113 m)

This entire section is described as the Brent Formation.

Late-Middle Bathonian (3960 - 4037 m)

This section comprises the upper part of the Brent Formation and consists of dark brown and medium grey shales with interbeds of light to medium brown siltstone as described in the Heather Formation grading downwards into light brown, very fine to fine grained, calcareous sandstone interbeds and stringers. This section also contains interbeds of black, hard, vitreous coal beds up to 5 m thick.

Early Bathonian - Middle Bajocian (4037 - 4090 m)

4037 - 4055 m

This interval is composed dominantly of sandstone beds (up to 7 m thick) with dark brown and medium grey shale interbeds. The sandstone is clear, occasionally brown, very fine to fine, occasionally medium and coarse to very coarse grained, very poorly sorted and friable with a weak calcareous cement. It has moderate to good porosity and abundant hydrocarbon shows.

4055 - 4090 m

This interval is distinguished from the sandstones above by a marked increase in shale and the appearance of dolomitic limestone interbeds.

The shale is brown to greyish brown, with minor dark grey and traces of light green and it is calcareous. The limestone is micro to crypto-crystalline, hard and dolomitic in parts. In the lower part of this interval thick coal beds of similar descriptions as above occur.

Bajocian (4090 - 4113 m)

This is the lowest interval of the Brent Formation and consists of interbedded sandstones, siltstones and thin coal beds.

The sandstones show a marked change from those above and are light grey, very fine to fine grained, well sorted with moderate porosity. They grade into siltstone which is dusky yellowish brown, blocky and non-calcareous. Both the shale and coal are as described for the upper intervals of the Brent Formation. Traces of pyrite occur in this as well as in the other intervals in the Jurassic.

4.5

TRIASSIC (4113 - 4326 m (T.D.))

Changes in lithology and in log character marks the top of this interval which consists of sandstones, in places grading to siltstones, and interbedded shales. The sandstones are pale yellowish brown, yellowish grey, occasional green grey and red stained, very fine to medium, in parts silty and poorly to well sorted. They are generally loose to friable, but are occasionally hard with calcareous and siliceous cement and some clay matrix. Porosity is usually poor to fair. The shales are brownish grey, greyish red, dusky brown, light to dark grey, occasional dark greenish grey, moderate hard, micro-micaceous and slightly to non-calcareous. In places they become very fine sandy and silty grading to siltstones. Traces of a light grey, chalky limestone, a dark brown, crypto-crystalline dolomite and pyrite occur through the interval.

5. HYDROCARBON SHOWS

Evaluation of hydrocarbon shows at the well site was carried out in a conventional manner.

Below 195 m a complete hydrocarbon total gas detector (50 units = 1 %) and a gas chromatograph for automatic and continuous gas analysis, recorded as ppm by volume of C1 through C5, were operational.

Hydrocarbon shows on ditch cuttings were evaluated according to Norsk Hydro's geologist's well site manual.

5.1 GAS RECORD

195 - 310 m

Throughout this interval the continuous ditch gas recording varies between 0.1 and 4 % and the chromatograph shows methane (C1) only. The higher readings correspond to sand or lignite layers.

310 - 1300 m

In this interval the continuous ditch gas recording does not exceed 1.5 % except for the interval 520 - 570 m when the total gas recorded reaches 12 %. There is no evident lithological change to explain this gas peak.

The interval can be further subdivided on the basis of chromatograph analysis. Between 310 and 640 m and from 920 to 1190 m methane (C1) and ethane (C2) were recorded, C2 mostly as traces. For the rest of the interval C1 only was found.

1300 - 2789 m

This section is characterized by low ditch gas recordings, generally less than 0.2 %.



Down to 2510 m C1 is the only constituent recorded, except for the interval 2268 - 2278 m where ethane (C2) and propane (C3) are found in trace amounts.

Below 2510 m C2 and C3 become persistent but only as traces. The lithology in this section is dominated by sandstones, including the Heimdal Formation in the Paleocene, and shales.

2789 - 2793\_m

This zone, which coincides with the top of the Maastrichtian limestone (at 2782 m) shows a total gas recording of up to 6 %, and the first occurrence of iso-butane (iC4) and normal-butane (nC4) are noted. The chromatograph peaked at 29140, 5742, 455, 245 and 25 ppm C1, C2, C3, iC4 and nC4 respectively.

2793 - 3005\_m

The continuous ditch gas recordings varies between 0.2 and 2 % in this interval, with the exception of a 4 % peak at 2829 m. C1 and C2 are recorded throughout, with occasional traces of C3. Limestones and marlstones are dominating the lithology in this section.

3005 - 3759\_m

Throughout this interval the total gas is low, not exceeding 0.6 %. C1 is persistent throughout, whereas C2 is reported occasionally and in small quantities. From 3705 m C3 and traces of C4 is also reported.

3759 - 3956\_m

The top of this interval correlates with the kimmerian Unconformity below which extends the organic-rich shales of

the Upper Jurassic shales of the Kimmeridge Clay Formation.

The top is marked by a moderate increase in total gas, from 0.1 to 1 % and throughout the interval the ditch gas varies between these values. The chromatograph shows C1 - iC4 down to 3795 m, below this depth only C1, C2 and C3 were recorded. The average chromatograph values were 2000, 1000, 80, 60 ppm for C1, C2, C3 and iC4 respectively.

3956 - 4130 m

In this interval the occurrence of interbedded coal beds, sandstones and shales cause the nature of the continuous ditch gas curve to become much more erratic, with values ranging from 0.1 to 40 % total gas. A general decrease in total gas as we go downwards can be seen. This interval comprises the sandstones, coals and shales of the Middle Jurassic and the gas curve correlate generally with either coal or sandstone beds. The chromatograph recorded C1-C4 between 3990 - 4050 m, with maximum reading 134820, 5692, 3845, 500 and 1000 ppm for C1, C2, C3, iC4 and nC4 respectively, whereas for the rest of the interval only C1 - C3 were recorded.

4130 - 4270 m

From 4130 m a sharp increase in the total gas recording is again noted, with values ranging from 0.3 to 32 %. The chromatograph recorded C1 - C3 with occasional traces of C4. Below 4220 m C1 - C3 only was found. Trissic sandstones dominate this section and wireline log evaluation showed average hydrocarbon saturation of 57 % from 4141 to 4158 m. In general the total gas recording gradually decreases downwards over this interval.

4270 - 4323 m

This interval consisting of water-wet sandstones show total gas readings less than 0.2 % and the chromatograph recorded C1 with traces of C2 only.

5.2 OIL STAIN AND FLUORESCENCE

2792 - 2828 m

The top of this interval coincides roughly with the Tor Formation in the Maastrichtian and consists of limestones which occasionally grades to marls. The shows were reported as occasionally pale white to dull gold fluorescence, with trace of slow, pale yellow to blue crush fluorescence cut. The show is very weak and occurs at two distinct depths 2792 and 2828 m, this coincide with two small gas peaks.

3488 - 3588 m

This section covers the basal part of the Herring Formation and the entire Plenus Marl Formation within the Turonian-Cenomanian, and is characterized by marlstones and limestones. The limestones are reported to have pale yellow to yellowish white fluorescence, non-fast streaming, white to pale blue fluorescence cut. The show is most pronounced between 3488 and 3517 m. No definite increase in total gas can be attributed to these shows.

Note: Discrepancy drillers and loggers depth over the interval 3700 - 4130 m. Loggers depth = drillers depth + 4.5 m. Loggers depth is used in this report.

3707 - 3723 m

This zone consists of shales and marlstones with limestone stringers and is a part of the Valhall Formation in the Lower Cretaceous. The limestones show abundant white to yellowish white fluorescence, fast to instant streaming, white to blue white fluorescence cut. A small gas peak is associated with the show.

3759 - 3860 m

A marked lithological change occurs as we enter the Kimmeridge Clay Formation and passes into the Upper Jurassic. Dark, organic-rich shales predominate with occasional limestone stringers. In the shales a weak show is reported at various levels described as follows: No fluorescence, traces of slow, faint light yellow crush fluorescence cut, occasionally streaming cut.

4008 - 4055 m

In this interval Middle Jurassic sandstones, coals and shales predominate and within the sandstones the following shows were reported:

4008 - 4013 m: Abundant pale blue fluorescence, slow but extensive bluish white fluorescence cut.

4035 - 4055 m: 80 % pale brown hydrocarbon stain on clear quartz, abundant pale yellow to dull orange fluorescence, slow to fast yellow white streaming fluorescence cut.

Two cores were cut in this interval, core 1 from 4018.1 to 4025.1 m and core 2 from 4037.0 to 4047.5 m. In core 1 from 4018.1 to 4019.6 m the following show was reported:

In sandstone abundant pale blue florescence and slow, but extensive bluish white fluorescence cut. Gas was seen bleeding from numerous hairline fractures throughout the core. In core 2 shows are reported as described in the interval 4035 to 4055 m, the colour of the fluorescence varying from pale yellow or dull orange to purple red.

4141 - 4158\_m

No shows were reported on the sandstone ditch cuttings while drilling this interval. Wire line logs run over the interval showed, however, average hydrocarbon saturation of 57 %.

6. CORING

6.1 CONVENTIONAL CORES

Two cores were cut in the Middle Jurassic sequence. Core 1 was taken from 4013.6 m to 4020.6 m and recovered 5.1 m (72.8 %). The core was decided to be cut based on sandstone occurrence in the ditch cuttings, but only shales and coal beds were found in the core. Core 2 was cut from 4032.5 m to 4043.0 m and recovered 9.8 m (93.3 %).

Over the interval in which the cores were taken there exists a discrepancy between the drillers and wireline log depths. To get the log depths of these cores, 4.5 m have to be added to the drillers depth.

Descriptions of the cores are shown in Appendix 1.

6.2 SIDE WALL CORES

Side wall cores were taken from 1655 m, in the Eocene, and down through the whole well with the last core recovered at 4323 m in the Triassic.

A total of 9 runs were made. The recovery varied from 3 to 30 out of 30 possible for each run. The low recoveries in run 3, 4 and 5 (see Well Summary, Appendix 3) were due to misfires which have not been explained by any technical malfunctions. A total of 174 out of 270 cores were recovered.

A detailed description of the cores is given in Appendix 2.

7. WIRELINE LOGGING

The following list contains a summary of the wireline logs run in the well 15/5-2 and shows the dates, logged intervals and run numbers for each log.

| LOG             | DATE     | LOGGED INTERVAL   | RUN NO. |
|-----------------|----------|-------------------|---------|
| BHC/GR          | 20.08.78 | 192 - 464.5 m     | 1       |
| ISF/SONIC/GR    | 31.08.78 | 455 - 1621.5 m    | 2       |
| "               | 31.08.78 | 1366 - 1620.5 m   | 2a      |
| "               | 15.10.78 | 1593 - 3610 m     | 3       |
| "               | 19.10.78 | 3500 - 3715 m     | 4       |
| "               | 9.11.78  | 3691 - 4134 m     | 5       |
| "               | 19.11.78 | 4000 - 4326 m     | 6       |
| FDC/CNL/GR      | 31.08.78 | 455 - 1612 m      | 1       |
| "               | 19.10.78 | 1593 - 3713.5 m   | 2       |
| "               | 9.11.79  | 3689 - 4134 m     | 3       |
| "               | 19.11.78 | 3691 - 4326 m     | 4a      |
| "               | 20.11.78 | 4000 - 4325.5 m   | 4b      |
| DLL/MSFL/GR     | 20.11.78 | 4000 - 4324.5 m   | 1       |
| HDT             | 19.10.78 | 1593 - 3712 m     | 1       |
| "               | 22.11.78 | 3690.5 - 4323.5 m | 2       |
| VELOCITY SURVEY | 21.11.78 | 500 - 4323 m      | 1       |
| RFT             | 22.11.78 | MISRUN            | 1       |
| "               | 24.11.78 | 4148.5 m          | 2       |
| "               | 24.11.78 | 4145 m            | 3       |
| "               | 25.11.78 | 4053 m            | 4       |
| "               | 25.11.78 | 4053 m            | 5       |
| "               | 29.11.78 | 4157.5 m          | 6       |
| "               | 29.11.78 | MISRUN            | 7       |
| "               | 29.11.78 | 4157.5 m          | 8       |

| LOG | DATE     | LOGGED INTERVAL |        |   | RUN NO. |
|-----|----------|-----------------|--------|---|---------|
| CST | 20.10.78 | 3000            | - 3710 | m | 1       |
| "   | 20.10.78 | 1655            | - 2990 | m | 2       |
| "   | 22.11.78 | 4052            | - 4315 | m | 3       |
| "   | 23.11.78 | 4114            | - 4323 | m | 4       |
| "   | 23.11.78 | 3925            | - 3961 | m | 5       |
| "   | 23.11.78 | 3753            | - 4275 | m | 6       |
| "   | 27.11.78 | 3912            | - 4149 | m | 7       |
| "   | 28.11.78 | 3720            | - 3992 | m | 8       |
| "   | 28.11.78 | 3758            | - 4140 | m | 9       |
| CCL | 19.11.78 | 0               | - 3696 | m | 1       |
| HRT | 3.09.78  | 541             | - 1589 | m | 1       |
| "   | 27.10.78 | 2655            | - 3652 | m | 2       |
| CPI | 12.02.79 | 4005            | - 4295 | m | 1       |



8. SPECIAL STUDIES

The biostratigraphic evaluation of the well has been performed by the laboratories of Robertson Research International Ltd. The results are presented in the report:

"Norsk Hydro Norwegian North Sea 15/5-2 well:  
Biostratigraphy of the interval 200 m - 4323 m".

A geochemical study of the well has been performed by the laboratories of Robertson Research International Ltd. Canned ditch cuttings samples over the interval 1450 m to 4323 m have been analysed for maturation level and source rock potential. Sampling intervals were 50 m between 1450 and 3750 m, 5 m between 3750 and 3755 m, 2 and 3 m between 3755 and 3770 m, 5 m between 3770 and 4000 m, and 25 m between 4000 and 4323 m. The results from this study are presented in the report:

"Report on a geochemical evaluation of the Norsk Hydro 15/5-2 well, Norwegian North Sea".

APPENDIX 1

CORE DESCRIPTIONS, CORE 1 AND 2



# Norsk Hydro

| Well no.<br>15/5 - 2          |               | Core report               |                                      |  | Core no s<br>1  |
|-------------------------------|---------------|---------------------------|--------------------------------------|--|---|
| Interval<br>4013.6 - 4020.6 m |               | Area<br>NORTH SEA, NORWAY | Cut<br>4013.6 - 4020.6 m             | Date<br>5-11-1979  |   |
| Scale<br>1:50                 |               | Well R.K.B.<br>25 m       | Recovery<br>4013.6 - 4018.7 m, 72,8% | Geologist<br>FAGERLAND/SKAAR   |   |
| Depth<br>scale                | Re-<br>covery | Lithological<br>column    | Depths                               | Lithological descriptions  | Shows   |
| 4013                          |               |                           |                                      |  |   |
| 4014                          |               |                           | 4013.6                               | <u>Sh</u> , beige gy-lt brn, hd, plty, v slty, occ tr coal lam, micro-mic, irr lam w/ bioturbation and slump texture w/ pocket incl of <u>Sst</u> , pale yel'sh brn, vf, hd, subang, silic, micro-mic, well srt'd, pr por. | Gas bleeding from numerous hairline thin frac throughout the core.          |
| 4015                          |               |                           | 4015.4                               | <u>Coal</u> , blk, shiny, vitreous, hd, frac, occ slickensides, occ thin intbds (1-5 cm) of <u>Sh</u> , blk, hd, fis, v carb.  | On <u>Sst</u> , abn pale blue flu and slow but extensive bluish wh flu cut. |
| 4016                          |               |                           | 4016.7                               | <u>Coal</u> , a/a intbd w/ <u>Sh</u> , blk-blk brn, fis, hd, v carb.   |   |
| 4017                          |               |                           |                                      |  |   |
| 4018                          |               |                           | 4018.7                               |  |   |
| 4019                          |               | NOT RECOVERED             |                                      |  |   |
| 4020                          |               |                           | 4020.6                               |  |   |
| 4021                          |               |                           |                                      |  |   |
|                               |               |                           |                                      | <div>NOTE: DISCREPANCY DRL'S AND LOGGER'S DEPTH. LOGGER'S DEPTH = DRL'S DEPTH + 4,5 m.</div>   |   |
| Well 15/5 - 2                 |               | Core report 1             |                                      |  | Core nos 1  |






# Norsk Hydro

| Well no.<br>15/5-2          |          | Core report               |                                  |  | Core no's<br>2  |
|-----------------------------|----------|---------------------------|----------------------------------|--|---|
| Interval<br>4032.5 - 4042 m |          | Area<br>NORTH SEA, NORWAY | Cut<br>4032.5 - 4043 m           | Date<br>7-11-1978  |   |
| Scale<br>1:50               |          | Well R.K.B.<br>25 m       | Recovery<br>4032.5-4042.31m, 94% | Geologist<br>FAGERLAND/SKAAR   |   |
| Depth scale                 | Recovery | Lithological column       | Depths                           | Lithological descriptions  | Shows   |
| 4032                        |          |                           |                                  |  |   |
|                             |          |                           | 4032.5                           | <u>Sst</u> , dk yel'sh brn, vf, hd-fri, subang, slty incr towards bottom, arg, mica on bedding planes, reg                               | Abn orng-rd purple flu, fast yel-wh flu cut.                    |
| 4033                        |          |                           |                                  | lam w/low dip, calc cmt, minor silic cmt, mod srt'd, pr-mod por  |   |
|                             |          |                           | 4033.5                           | <u>Sst</u> , olv gy, hd, micro-mic enriched on bedding planes, v arg grdg <u>Sh</u> toward bottom, reg bedding.                          | Abn flu a/a but more dull and slow cut.                         |
| 4034                        |          |                           |                                  |  |   |
|                             |          |                           | 4034.5                           | <u>Sh</u> , olv blk-brn blk, v hd, blk, occ slty, occ frac w/slickensides.   | No shows  |
| 4035                        |          |                           |                                  |  |   |
|                             |          |                           | 4036.0                           | <u>Sst</u> , a/a.  | Abn faint flu and cut a/a.                                      |
| 4036                        |          |                           | 4036.2                           | <u>Sh</u> , a/a w/minor <u>Sst</u> a/a.  | Tr of shows in slst a/a.  |
|                             |          |                           |                                  |  |   |
| 4037                        |          |                           | 4037.0                           | <u>Sh</u> , slty else gen a/a, but v foss, mainly bivalves, calc w/moldic and frac fillings of calc.                                     |   |
|                             |          |                           |                                  |  |   |
| 4038                        |          |                           | 4038.0                           | <u>Sst</u> , gy brn, vf-f, fri, subang, slty, sl arg, sl micro-mic dispersed, homogeneous texture, tr calc cmt, mod-well srt'd, mod por. | Abn orng (90%) grdg rd-purple flu, with fast yel-wh cut.        |
|                             |          |                           |                                  |  |   |
| 4039                        |          |                           |                                  |  |   |
|                             |          |                           |                                  |  |   |
| 4040                        |          |                           |                                  |  |   |
|                             |          |                           | 4040.9                           | <u>Sst</u> , olv gy, hd, blk, occ sl micro-mic lam, mainly dispersed, tr vf <u>Sst</u> grns, v arg, occ steep dip frac slickensided.     | Abn show a/a, but more pale and with more slow yel-grn flu cut. |
| 4041                        |          |                           |                                  |  |   |
| 4042                        |          |                           |                                  |  |   |
| Well 15/5-2                 |          | Core report 2/1           |                                  |  | Core nos 2  |



# Norsk Hydro

|  |   |   |         |                                    |                |  |
|--|---|---|---------|------------------------------------|----------------|--|
| Well no.<br>15/5-2   |   | Core report   |         |                                    | Core no.s<br>2 |  |
| Interval<br>4042 - 4043 m.   |   | Area<br>NORTH SEA, NORWAY   |         | Cut<br>4032.5 - 4043 m.            |                |  |
| Scale<br>1:50  |   | Well R.K.B.<br>25m  |         | Date<br>7-11-1978                  |                |  |
|  |   |   |         | Recovery<br>4032.5 - 4042.31m, 94% |                |  |
|  |   |   |         | Geologist<br>FAGERLAND/ SKAAR      |                |  |
| Depth<br>scale   | Re-<br>covery   | Lithological<br>column  | Depths  | Lithological descriptions          | Shows          |  |
| 4042   |  |  | 4042 31 | <u>Sist</u> , a/a.                 | Shows a/a.     |  |
| 4043   |  | NOT<br>RECOVERED  | 4043    |                                    |                |  |
| <div style="border: 1px solid black; padding: 5px; margin: 10px auto; width: fit-content;">NOTE: DISCREPANCY DRL'S<br/>AND LOGGER'S DEPTH.<br/>LOGGER'S DEPTH =<br/>DRL'S DEPTH + 4.5 m.</div> |   |   |         |                                    |                |  |
| Well<br>15/5-2   |   | Core report<br>2/2  |         |                                    | Core no.s<br>2 |  |

APPENDIX 2

SIDE WALL CORE DESCRIPTIONS



# Norsk Hydro

|                             |                       |                      |        |
|-----------------------------|-----------------------|----------------------|--------|
| SIDE WALL CORES DESCRIPTION |                       | SERVICE COMPANY      | Schlum |
|                             |                       | ASKED                | 30     |
|                             |                       | SHOT                 | 30     |
|                             |                       | LOST                 | 3      |
|                             |                       | EMPTY                | 1      |
| WELL: 15/5-2                | RUN N°: 1             | SAMPLES RECOVERED 26 |        |
| LICENCE: 048                | PAGE N°: 1 of 2       |                      |        |
|                             | DATE: 20 October 1978 | GEOLOGIST: Fagerland |        |

tr: trace - M: medium - G: good

| N° | DEPTHS<br>m | REC<br>% | LITHOLOGY   | Fluorescence |     |
|----|-------------|----------|---|--------------|-----|
|    |             |          |   |              | CUT |
| 1  | 3701        | 60       | Mrlst/Lst, m gy, hd, blk, no vis por, 100% bright vel flu, instant to v fast wh-milky cut, no resd.           |              |     |
| 2  | 3705        | 95       | sh, dk gy, firm, subfis, calc.  |              |     |
| 3  | 3700        | /        | Lost  |              |     |
| 4  | 3690        | /        | Lost  |              |     |
| 5  | 3685        | 50       | Sst, prnish gy, mod hd, vf-slt, arg, v calc, calc mrx and cmt, arg, abn glau, tr mica, well strd, no vis por. |              |     |
| 6  | 3655        | 50       | Mrlst, dk gy, firm, blk-subfis, v arg, sl slty.   |              |     |
| 7  | 3630        | 60       | Mrlst, m dk gy, As No. 6.   |              |     |
| 8  | 3605        | 85       | Mrlst, olv gy-lt olv gy, firm, subfis, v arg as No. 7.  |              |     |
| 9  | 3595        | 45       | Slst, m gy-lt olv gy, firm-hd, blk, arg, v calc grd to Mrlst.   |              |     |
| 10 | 3587        | 85       | Sh, m gy-grnish gy, firm, subfis, sl-non calc w tr inter-lam Sh rd, firm, sl-non calc.                        |              |     |
| 11 | 3575        | 40       | Slst, m gy, mod hd, blk, v calc grd to Mrlst, mod arg.  |              |     |
| 12 | 3545        | 40       | Sh/Mrlst, m gy, firm-mod hd, subfis, sl slty.   |              |     |
| 13 | 3535        | 40       | Mrlst, m gy, mod hd, subfis, slty.  |              |     |
| 14 | 3510        | 60       | As No. 13.  |              |     |
| 15 | 3505        | /        | Lost  |              |     |
| 16 | 3490        | 100      | Sh, m dk gy-dk gy, firm, blk, calc, sl slty.  |              |     |
| 17 | 3477        | /        | Empty   |              |     |
| 18 | 3460        | 40       | Lst, lt gy-wh, firm-mod hd, crypto xln, 100% bright vel flu prob mainly mineral, tr v slow wh cut.            |              |     |



tr : trace - M : medium - G : good

~~WFO~~ B2036





# Norsk Hydro

|                             |                        |                        |
|-----------------------------|------------------------|------------------------|
| SIDE WALL CORES DESCRIPTION |                        | SERVICE COMPANY Schlum |
|                             |                        | ASKED: 30'             |
|                             |                        | SHOT: 30               |
|                             |                        | LOST: 0                |
|                             |                        | EMPTY: 0               |
| WELL: 15/5-2                | RUN N°: 2              | SAMPLES RECOVERED: 30  |
| LICENCE: 048                | PAGE N°: 1 of 2        |                        |
|                             | DATE: October 20, 1978 | GEOLOGIST:             |
|                             |                        | N. Fagerland           |

tr: trace - M: medium - G: good

| N° | DEPTHS<br>m | REC<br>% | LITHOLOGY  | Fluorescence |  |     |
|----|-------------|----------|--|--------------|--|-----|
|    |             |          |  |              |  | CUT |
| 31 | 2990        | 50       | Lst. wh - lt gy. firm-mod hd. slarg. crypto-xln. no vis por.                         |              |  |     |
| 32 | 2980        | 60       | Mrlst. m gy. mod hd-firm. blkv.  |              |  |     |
| 34 | 2882        | 70       | Sh/Clyst. dk gy-gvish rd. sft. calc.   |              |  |     |
| 35 | 2796        | 40       | Lst. wh, mod hd, frac. crypto xln. no vis por.                                       |              |  |     |
| 36 | 2785        | 50       | As N° 35.  |              |  |     |
| 37 | 2780        | 95       | Sh. dk gy. firm. blkv. calc.   |              |  |     |
| 38 | 2765        | 60       | Mrlst. m blue'shgy-pale red. firm-sft, blkv.   |              |  |     |
| 39 | 2732        | 50       | Mrlst/Lst. lt gy. firm. blkv.  |              |  |     |
| 40 | 2710        | 75       | Sh. mdk gy. firm. blkv. v calc. slty.  |              |  |     |
| 41 | 2706        | 100      | As N° 40.  |              |  |     |
| 42 | 2695        | 75       | Sd/Sst. wh-lt gy. lse-firm. vf. ang. tr Glau. non calc. well<br>srtd, v gd por.      |              |  |     |
| 43 | 2685        | 90       | Sh. dk gy. firm. blkv. calc.   |              |  |     |
| 44 | 2655        | 100      | Sh. dk gy-blk. firm. blkv. carb. non calc.   |              |  |     |
| 45 | 2625        | 90       | Sh. dk gy. firm. blkv. non calc.   |              |  |     |
| 46 | 2569        | 75       | Sd/Sst. lt gy. firm. vf. slty. ang. tr mica. non calc. sl arc.<br>well srtd, gd por. |              |  |     |
| 47 | 2531        | 60       | As N° 46.  |              |  |     |
| 48 | 2244        | 100      | Sh. m gy-dk gy. firm. blkv. sl micro-mic. non calc.                                  |              |  |     |
| 49 | 2203        | 100      | Sh. dk gy-blk. firm. blkv. carb. non calc. sl slty.                                  |              |  |     |
|    |             |          |  |              |  |     |



tr : trace - M : medium - G : good

~~W~~ B2C36



# Norsk Hydro

|                             |  |                         |
|-----------------------------|--|-------------------------|
| SIDE WALL CORES DESCRIPTION |  | SERVICE COMPANY: Schium |
|                             |  | ASKED: 30               |
|                             |  | SHOT: 11                |
|                             |  | LOST: 0                 |
|                             |  | EMPTY: 3                |
| WELL: 15/5-2                |  | SAMPLES RECOVERED 8     |
| LICENCE: 048                |  | Misfire: 19             |
| RUN N°: 3                   |  | GEOLOGIST:              |
| PAGE N°: 1 of 2             |  |                         |
| DATE: 22 November 1978      |  |                         |

tr: trace - M: medium - G: good

| N° | DEPTHS<br>m | REC<br>% | LITHOLOGY  | Fluorescence |     |  |
|----|-------------|----------|--|--------------|-----|--|
|    |             |          |  |              | CUT |  |
| 1  | 4315        | 50       | Sst/Sst. gy blue, vf. sl mica, w/f pyr incl. blk flks. arg. fri.                     |              |     |  |
| 2  | 4300,5      | 50       | Sh, rd brn, slty, sl mic.  |              |     |  |
| 3  | 4288,5      | 30       | Sh. rd brn. slty to sd. w/f incl of Sst. gybl. vf-f. subang.                         |              |     |  |
| 4  | 4275        | 20       | Sst. brn rd brn. f. rr m. subang. v. fri. calc w/incl of Sh. gybl.                   |              |     |  |
| 5  | 4263,5      | 30       | Sst. as No. 4, f, loc m, subang, w/incl of Sh, gybl, sd.                             |              |     |  |
| 6  | 4183        | /        | Empty  |              |     |  |
| 7  | 4155        | 40       | Sst. brn. rd brn. f to m. subang. v. fri, w/pyr incl, arg w/rr incl of Sh gybl, pyr. |              |     |  |
| 8  | 4150        | 20       | Sst. brn. lt brn. f. rr m. subang. v. fri. sl calc.                                  |              |     |  |
| 9  | 4147        | /        | Empty.   |              |     |  |
| 10 | 4076,5      | /        | Empty.   |              |     |  |
| 11 | 4052        | 50       | Sst. dk brn. f-m. subang w/blk flk (coal?). fri. arg cmt, loc calc cmt.              |              |     |  |
| 12 | 4047,5      | /        | Misfire.   |              |     |  |
| 13 | 4014        | /        | "  |              |     |  |
| 14 | 3984        | /        | "  |              |     |  |
| 15 | 3970        | /        | "  |              |     |  |
| 16 | 3955        | /        | "  |              |     |  |
| 17 | 3946,5      | /        | "  |              |     |  |
| 18 | 3935        | /        | "  |              |     |  |



tr : trace - M : medium - G : good

~~WFO~~ 82036



# Norsk Hydro

|                             |                        |                         |
|-----------------------------|------------------------|-------------------------|
| SIDE WALL CORES DESCRIPTION |                        | SERVICE COMPANY: Schlum |
|                             |                        | ASKED: 30               |
|                             |                        | SHOT: 18                |
|                             |                        | LOST: 7                 |
|                             |                        | EMPTY: 1                |
| WELL: 15/5-2                | RUN N°: 4              | SAMPLES RECOVERED: 10   |
| LICENCE: 048                | PAGE N°: 1 of 2        | Misfire: 12             |
|                             | DATE: 23 November 1978 | GEOLOGIST: A. Davies    |

tr: trace - M: medium - G: good

| N° | DEPTHS<br>m | REC<br>% | LITHOLOGY  | Fluorescence |     |
|----|-------------|----------|--|--------------|-----|
|    |             |          |  | IR           | CUT |
| 1  | 4323        | 40       | Sst, pale rd w/brn tinge, vf-f, ang-subrnd, slty, occ hematite stn, firm, w/calc cmt, fri, no show.                |              |     |
| 2  | 4315        | 15       | Sst, dk yel brn-gy yel grn, vf, occ f, ang-suhang, grdg to slst, firm, v fri, weak calc cmt, fair por, no show.    |              |     |
| 3  | 4300,5      | 15       | Sh, dk rd brn, firm, fis-subfis, occ slty, micro mic, non calc.  |              |     |
| 4  | 4275        | /        | Lost   |              |     |
| 5  | 4265        | /        | Lost   |              |     |
| 6  | 4253        | /        | Lost   |              |     |
| 7  | 4228        | 50       | Sst, lt olv gy-lt grn gy, vf-f, rnd-subrnd, firm, fri, calc, clay mtx, low por, no show.                           |              |     |
| 8  | 4203        | 40       | Sst, lt olv gy, vf-f, rnd-subrnd, firm, fri, weak calc, cmt, sme dk grn frags, clr + dk brn mica flakes, no shows. |              |     |
| 9  | 4183        | 30       | Sst, lt gy-lt brn, vf, occ f, rnd-subrnd, firm, v fri, calc, clay mtx, low-mod por, no show.                       |              |     |
| 10 | 4169        | 30       | Sst, lt brnsh olv gy, vf-f, occ m, rnd-subrnd, occ subang, firm, v fri, w/non calc cmt, mod-gd por, no show.       |              |     |
| 11 | 4156        | /        | Lost   |              |     |
| 12 | 4150        | 10       | Sst, sl arg else as No. 10, no shows.  |              |     |
| 13 | 4147        | /        | Lost   |              |     |
| 14 | 4143        | 20       | Sst, pred f, else as No. 10, no shows.   |              |     |
| 15 | 4140        | /        | Misfire  |              |     |
| 16 | 4139        | /        | Empty  |              |     |
| 17 | 4117        | /        | Lost   |              |     |
| 18 | 4114        | 15       | Sh, mod yel brn, firm, subfis, pr-mod cpctd, f sdy in prs.   |              |     |



tr : trace - M : medium - G : good

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tr : trace - M : medium - G : good

~~W~~ 82036



# Norsk Hydro

|                             |                        |                         |
|-----------------------------|------------------------|-------------------------|
| SIDE WALL CORES DESCRIPTION |                        | SERVICE COMPANY: Schlum |
|                             |                        | ASKED: 30               |
|                             |                        | SHOT: 28                |
|                             |                        | LOST: 7                 |
|                             |                        | EMPTY: 2                |
| WELL: 15/5-2                | RUN N°: 6              | SAMPLES RECOVERED: 19   |
| LICENCE: 048                | PAGE N°: 1 of 2        | Misfires: 2             |
|                             | DATE: 23 November 1978 | GEOLOGIST:              |
|                             |                        |                         |

tr: trace - M: medium - G: good

| N° | DEPTHS<br>m | REC<br>% | LITHOLOGY   | Fluorescence |     |
|----|-------------|----------|---|--------------|-----|
|    |             |          |   |              | CUT |
| 1  | 4288,5      | /        | Lost  |              |     |
| 2  | 4275        | 20       | Sst, arg grdg to v.f Sst, gy grnish strongly mic in pt.                                     |              |     |
| 3  | 4263,5      | /        | Lost  |              |     |
| 4  | 4243        | 20       | Sst, f, subrnd, v fri, wh to pink, no show.   |              |     |
| 5  | 4212,5      | /        | Lost  |              |     |
| 6  | 4183        | /        | Lost  |              |     |
| 7  | 4156,5      | /        | Lost  |              |     |
| 8  | 4148,5      | 30       | Sst, f-m, heterogeneous, fri, subang, sl arg and mic, no show.                              |              |     |
| 9  | 4150        | 30       | Sst, f-m, heterogeneous, fri, subang, sl arg and mic. Thin layers of Sh, pale grn, no show. |              |     |
| 10 | 4147        | /        | Lost  |              |     |
| 11 | 4076        | /        | Empty   |              |     |
| 12 | 4047,5      | 30       | Sst, dk brn, f, fairly well consolidated, sl mic, no show.                                  |              |     |
| 13 | 4014        | 30       | Sst, arg, gy dk brn, sl mic, thin coal layers and vns.                                      |              |     |
| 14 | 3984        | /        | Misfire   |              |     |
| 15 | 3970        | 20       | Sst, grdg to v.f Sst, brn, sl mic w thin coal vns.  |              |     |
| 16 | 3955        | 50       | Sh, v sl slty, dk brn.  |              |     |
| 17 | 3946,5      | /        | Empty   |              |     |
| 18 | 3935        | 60       | Sh, sl slty, blk gy, ind.   |              |     |





tr : trace - M : medium - G : good

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# Norsk Hydro

|                             |                        |  |                         |  |
|-----------------------------|------------------------|--|-------------------------|--|
| SIDE WALL CORES DESCRIPTION |                        |  | SERVICE COMPANY: Schlum |  |
|                             |                        |  | ASKED: 30               |  |
|                             |                        |  | SHOT: 30                |  |
|                             |                        |  | LOST: 6                 |  |
|                             |                        |  | EMPTY: 3                |  |
|                             |                        |  | SAMPLES RECOVERED: 21   |  |
|                             |                        |  | GEOLOGIST: A. Davies    |  |
| WELL: 15/5-2                | RUN N°: 7              |  |                         |  |
| LICENCE: 048                | PAGE N°: 1 of 2        |  |                         |  |
|                             | DATE: 27 November 1978 |  |                         |  |

tr: trace - M: medium - G: good

| N° | DEPTHS<br>m | REC<br>% | LITHOLOGY  | Fluorescence |  | CUT |
|----|-------------|----------|--|--------------|--|-----|
|    |             |          |  |              |  |     |
| 1  | 4147        | 15       | Sst. gyish brn. vf-f. subrnd- subang. qtz sm red. hematite strn firm- mod hd. mod fri. v sl calc. cmr. sl arg. mod por. no show. |              |  |     |
| 2  | 4146        | 15       | Sst. wh. lt gy. f. occ m. ang-sub ang. firm. fri. calc cmr. sl arg. mod srted. pr por. no show.                                  |              |  |     |
| 3  | 4145        | 20       | Sst. v lt brn gy. vf. ang-subang. firm. fri. clr. red. grn. qtz v well srted. cln. calc cmr. mod por. no show.                   |              |  |     |
| 4  | 4144        | 30       | Sst. lt brn. vf-f. as no. 3 mod well srted. mod por. no show.  |              |  |     |
| 5  | 4142        | 20       | Sst. as no. 3 no show.   |              |  |     |
| 6  | 4140        | /        | Empty  |              |  |     |
| 7  | 4139        | 30       | Sh. gy red. sft. cly. pr-mod cpct. blk. v. sl. calc. no show.  |              |  |     |
| 8  | 4117        | 30       | Sh. gy red. sft as no. 7 w intercal slty + f sdy. sl calc no show.   |              |  |     |
| 9  | 4112.5      | 30       | Cly. mod lt gy. sft. pr cpctd. tr f. clr ang qtz. non calc. no show.   |              |  |     |
| 10 | 4096        | /        | Lost   |              |  |     |
| 11 | 4077        | 30       | Sh. m dk gy. mod hd. mod cpctd. subfis-fis. tr f diss pyr. cal. no show.   |              |  |     |
| 12 | 4072        | 15       | Sh. m dk gy- brn gy. hd. well cpct. blk. sl calc. no show.   |              |  |     |
| 13 | 4063        | /        | Lost   |              |  |     |
| 14 | 4030        | 40       | Sh. m dkgy as no. 13. subfis. non calc. no show.   |              |  |     |
| 15 | 4008        | 10       | Sh. m gy. hd. well cpct. blk. non calc.  |              |  |     |
| 16 | 3994        | 20       | Sh. brn gy. mod hd-hd. well cpctd. blk-subfis. sl earthy. slty. sl calc. no flu. <u>weak lt yel crush cut</u>                    |              |  |     |
| 17 | 3987        | 25       | Sh. as no. 16 no flu. <u>weak lt yel crush cut</u>   |              |  |     |
| 18 | 3981        | 30       | Sh. as no. 17 firm- mod hd. tr pyr. v sl calc. no flu. <u>weak lt yel crush cut</u>  |              |  |     |



tr : trace - M : medium - G : good

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# Norsk Hydro

|                             |                        |                         |
|-----------------------------|------------------------|-------------------------|
| SIDE WALL CORES DESCRIPTION |                        | SERVICE COMPANY: Schlum |
|                             |                        | ASKED: 30               |
|                             |                        | SHOT: 30                |
|                             |                        | LOST: 3                 |
|                             |                        | EMPTY: 10               |
| WELL: 15/5-2                | RUN N°: 8              | SAMPLES RECOVERED: 17   |
| LICENCE: 048                | PAGE N°: 1 of 2        |                         |
|                             | DATE: 28 November 1978 | GEOLOGIST: A. Davies    |

tr: trace - M: medium - G: good

| N° | DEPTHS<br>m | REC<br>% | LITHOLOGY   | Fluorescence |     |
|----|-------------|----------|---|--------------|-----|
|    |             |          |   | TRANS        | CUT |
| 1  | 3992        | 30       | Sltst, dk yel brn, firm, fri, pr ind, sft, cly mtx, occ vi ang qtz<br>micro mic, tr carb, low por, no show.                 |              |     |
| 2  | 3990        | 20       | Sst, dk yel brn, vf, occ f, ang-subang, weak calc cmt, slty,<br>mtx, fri pr ind, micro mic, tr pyr, low-mod por, no show.   |              |     |
| 3  | 3985        | /        | Empty   |              |     |
| 4  | 3980        | /        | Empty   |              |     |
| 5  | 3975        | /        | Empty   |              |     |
| 6  | 3972        | /        | Empty   |              |     |
| 7  | 3953        | /        | Empty   |              |     |
| 8  | 3950        | /        | Empty   |              |     |
| 9  | 3943        | 20       | Sltst, dk yel brn as no. 1 v. calc, no flu, no cut,<br>v weak lt yel flu resd.  |              |     |
| 10 | 3935        | 20       | Sh, dusky yel brn, firm, pr cpct, blk, subfis, slty occ f sdy,<br>sl calc, earthy, no flu, v slow, weak dull yel crush cut. |              |     |
| 11 | 3900        | 60       | Sh, dusky yel brn, firm-mod hd, mod cpct, blk, slty, sl earthy,<br>sl calc, no flu, dull yel crush cut                      |              |     |
| 12 | 3890        | 65       | Sh, brn blk, firm, mod cpct, homogenous, occ sl slty, sl calc,<br>blk, no show.   |              |     |
| 13 | 3885        | 15       | Sh, brn blk as no. 12 sub fis, v calc, no show.   |              |     |
| 14 | 3880        | 60       | Sh, brn blk, blk-subfis as no. 13 no show,  |              |     |
| 15 | 3875        | 20       | Sh, brn blk as no. 14 calc,<br>occ slty, no show.   |              |     |
| 16 | 3868        | /        | Empty   |              |     |
| 17 | 3855        | /        | Empty   |              |     |
| 18 | 3837        | 50       | Sh, brn blk-dk gy, firm-mod hd, w cpct, fis, occ splitry,<br>slty in pts, sl calc, v calc, no show.                         |              |     |



tr : trace - M : medium - G : good

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# Norsk Hydro

|                             |  |                         |  |
|-----------------------------|--|-------------------------|--|
|                             |  | SERVICE COMPANY: Schlum |  |
|                             |  | ASKED: 30               |  |
|                             |  | SHOT: 29                |  |
|                             |  | LOST: 14                |  |
|                             |  | EMPTY: 2                |  |
|                             |  | SAMPLES RECOVERED: 13   |  |
|                             |  | Misfire: 1              |  |
|                             |  | GEOLOGIST:              |  |
|                             |  | A. Davies               |  |
| SIDE WALL CORES DESCRIPTION |  |                         |  |
| WELL: 15/5-2                |  | RUN NO: 9               |  |
| LICENCE: 048                |  | PAGE NO: 1 of 2         |  |
|                             |  | DATE: 28 November 1978  |  |

tr: trace - M: medium - G: good

| Nº | DEPTHS<br>m | REC<br>% | LITHOLOGY  | Fluorescence |  |     |
|----|-------------|----------|--|--------------|--|-----|
|    |             |          |  |              |  | CUT |
| 1  | 4140        | 30       | Sltst, gy red, sft-firm, pr-mod cpct, cly, grdg to vf ang Sst, non calc, no shows.                       |              |  |     |
| 2  | 4096        | 20       | Sltst, lt gy-v lt gy, firm as no. 1 no show.   |              |  |     |
| 3  | 4065        | 10       | Cly st, dk yel brn, sft, pr cpct, gummy, slty, sl calc, no show.   |              |  |     |
| 4  | 4063        | /        | Empty  |              |  |     |
| 5  | 4027        | /        | Lost   |              |  |     |
| 6  | 3985        | /        | Lost   |              |  |     |
| 7  | 3980        | /        | Lost   |              |  |     |
| 8  | 3975        | 30       | Mrl, lt brn, sft, pr cpct, sticky, gummy, slty, sl calc.   |              |  |     |
| 9  | 3972        | /        | Lost   |              |  |     |
| 10 | 3968        | /        | Empty  |              |  |     |
| 11 | 3966        | 30       | Coal, blk, hd, brit, dull, sl arg, low rank, thin shiney vit lam, no flu, v weak, slow lt vel crush cut. |              |  |     |
| 12 | 3964        | /        | Lost   |              |  |     |
| 13 | 3953        | /        | Lost   |              |  |     |
| 14 | 3950        | /        | Lost   |              |  |     |
| 15 | 3936        | /        | Lost   |              |  |     |
| 16 | 3935        | 15       | Lat, dk gy, hd, mod dns, well ind, micro-f xln, arg, no vis por, no show.                                |              |  |     |
| 17 | 3932        | /        | Lost   |              |  |     |
| 18 | 3927        | /        | Lost   |              |  |     |



tr : trace - M : medium - G : good

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APPENDIX 3

WELL SUMMARY



## WELL SUMMARY

| Coord: 58°38'36,7"N, 01°36'16,5"E<br>Line: 508 - 190 SP: 106<br>Depths datum: R.K.B.<br>Rig: TREASURE SEEKER<br>Water depth: 120,5 m RKB.elev: 25 m<br>Stopped in: TRIASSIC(?)   |                        |        |                              | Spudded: AUGUST 16. 1978<br>Started drilling: AUGUST 16. 1978<br>At T.D.: NOVEMBER 14. 1978<br>Completed: DECEMBER 16. 1978<br>Status: Temporarily Suspended<br>T.D. Driller: 4323 m T.D. Logger: 4326m   |   |   |         | Well<br>15/5 - 2<br>Country<br>NORWAY |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|--|------------------------|--------|------------------------------|---|---|---|---------|---------------------------------------|--|------------------------|--------|---------|---------------------------|--|------------------------|--------|--|-------|----------------------------|--|--|---------|------|--------|----------------------------|--|--------|---------------|----|-----------------|------------------------|---|---|---------------|----------------|--------|------------------------|--------------|---|--|---|-----------------|--------------------------|---|---------------|---|--|---|------------------------|---|-----|------------|---|---|-------------------------|---------------|---|-----|---------------|---|---|---|---------------|---|-----|--------|--------------------------|---|---|-----------------|---|---|---------------------------|---|---|-----------|--------------|---|------------|-----------------|---|--|---|-----------------|--------------------------|---|--------|---|--|---|-----------------|---|---|--------|---|---|--------------------------|---------------|----|---|----------|---|---|---|-----------------|----|---|----------|--------------------------|---|------------|-----------------|---|---|----------|---|---|-----|---------------|---|---------------------------|--|--|--|---|-------------------|---------|--|--|--|--|--|--------------------------|--|--|--|--|--|--------|--|--|--|--|--|---------------------------|--|--|--|--|--|-------------------------|--|--|--|--|--|------------------------------|--|--|--|--|--|--|--|--|
| OPERATOR: NORSK HYDRO PRODUKSJON A/S   |                        |        |                              | LICENCE: 048  |   |   |         | OWNED BY: STATOIL/PETRONORD           |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| TARGETS:<br>UPPER / MIDDLE JURASSIC SANDSTONES   |                        |        |                              | RESULTS:<br>EARLY - MIDDLE BATHONIAN <u>SST</u> : 4035-4055 m<br>GROSS PAY: 20 m NET PAY: 7,3 m<br>AVERAGE $\phi$ : 14,3 % AVERAGE $S_w$ : 41,7 %<br>TRIASSIC (?) <u>SST</u> : 4141,3-4158,1 m<br>GROSS PAY: 16,8 m NET PAY: 12,8 m<br>AVERAGE $\phi$ : 14,6 % AVERAGE $S_w$ : 43,0 % |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| <table border="1"> <thead> <tr> <th colspan="3">CASINGS</th> <th colspan="3">SHOWS</th> </tr> </thead> <tbody> <tr> <td>30"</td> <td>AT</td> <td>194 m</td> <td colspan="3">194 - 310 m: 0,1-4,0% C1.</td> </tr> <tr> <td>20"</td> <td>AT</td> <td>454 m</td> <td colspan="3">310 - 1300 m: 0,5-1,0% C1.</td> </tr> <tr> <td>13 3/8"</td> <td>AT</td> <td>1598 m</td> <td colspan="3">occ C2, 520-570 m peak 12%</td> </tr> <tr> <td>9 5/8"</td> <td>AT</td> <td>3696 m</td> <td colspan="3">1300-2278 m: &lt;0,4% C1,</td> </tr> <tr> <td>7" LINER</td> <td>AT</td> <td>4300 m</td> <td colspan="3">tr C2, C3 from 2268 m.</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">2278 - 2789 m: &lt;0,2% C1,</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">tr C2, C3 from 2510 m.</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">2789 - 2793 m: C1 - nC4</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">peak of 6,0 %.</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">2793 - 3005 m: 0,2-2,0 %</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">C1, C2, occ C3 peak 4,0 %</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">at 2829 m.</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">3005 - 3702 m: 0,1-0,6 %</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">C1, occ C2, C3.</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">3702 - 3956 m: 0,1-1,0 %</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">C1-C3, occ iC4 and nC4.</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">3956 - 3990 m: 0,1-3,0 %</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">C1-C3.</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">3990 - 4050 m: 0,4-40,0 %</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">C1-nC4.</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">4050 - 4130 m: 0,1-3,0 %</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">C1-C3.</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">4130 - 4270 m: 0,3-32,0 %</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">C1-C3, occ iC4 and nC4.</td> </tr> <tr> <td colspan="3"></td> <td colspan="3">4270 - 4323 m: &lt;0,2% C1, C2.</td> </tr> </tbody> </table> |                        |        |                              | CASINGS   |   |   | SHOWS   |                                       |  | 30"                    | AT     | 194 m   | 194 - 310 m: 0,1-4,0% C1. |  |                        | 20"    | AT   | 454 m | 310 - 1300 m: 0,5-1,0% C1. |  |  | 13 3/8" | AT   | 1598 m | occ C2, 520-570 m peak 12% |  |        | 9 5/8"        | AT | 3696 m          | 1300-2278 m: <0,4% C1, |   |   | 7" LINER      | AT             | 4300 m | tr C2, C3 from 2268 m. |              |   |  |   |                 | 2278 - 2789 m: <0,2% C1, |   |               |   |  |   | tr C2, C3 from 2510 m. |   |     |            |   |   | 2789 - 2793 m: C1 - nC4 |               |   |     |               |   | peak of 6,0 %.  |   |               |   |     |        | 2793 - 3005 m: 0,2-2,0 % |   |   |                 |   |   | C1, C2, occ C3 peak 4,0 % |   |   |           |              |   | at 2829 m. |                 |   |  |   |                 | 3005 - 3702 m: 0,1-0,6 % |   |        |   |  |   | C1, occ C2, C3. |   |   |        |   |   | 3702 - 3956 m: 0,1-1,0 % |               |    |   |          |   | C1-C3, occ iC4 and nC4.   |   |                 |    |   |          | 3956 - 3990 m: 0,1-3,0 % |   |            |                 |   |   | C1-C3.   |   |   |     |               |   | 3990 - 4050 m: 0,4-40,0 % |  |  |  |   |                   | C1-nC4. |  |  |  |  |  | 4050 - 4130 m: 0,1-3,0 % |  |  |  |  |  | C1-C3. |  |  |  |  |  | 4130 - 4270 m: 0,3-32,0 % |  |  |  |  |  | C1-C3, occ iC4 and nC4. |  |  |  |  |  | 4270 - 4323 m: <0,2% C1, C2. |  |  |  |  |  |  |  |  |
| CASINGS  |                        |        | SHOWS                        |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| 30"  | AT                     | 194 m  | 194 - 310 m: 0,1-4,0% C1.    |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| 20"  | AT                     | 454 m  | 310 - 1300 m: 0,5-1,0% C1.   |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| 13 3/8"  | AT                     | 1598 m | occ C2, 520-570 m peak 12%   |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| 9 5/8"   | AT                     | 3696 m | 1300-2278 m: <0,4% C1,       |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| 7" LINER   | AT                     | 4300 m | tr C2, C3 from 2268 m.       |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | 2278 - 2789 m: <0,2% C1,     |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | tr C2, C3 from 2510 m.       |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | 2789 - 2793 m: C1 - nC4      |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | peak of 6,0 %.               |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | 2793 - 3005 m: 0,2-2,0 %     |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | C1, C2, occ C3 peak 4,0 %    |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | at 2829 m.                   |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | 3005 - 3702 m: 0,1-0,6 %     |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | C1, occ C2, C3.              |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | 3702 - 3956 m: 0,1-1,0 %     |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | C1-C3, occ iC4 and nC4.      |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | 3956 - 3990 m: 0,1-3,0 %     |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | C1-C3.                       |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | 3990 - 4050 m: 0,4-40,0 %    |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | C1-nC4.                      |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | 4050 - 4130 m: 0,1-3,0 %     |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | C1-C3.                       |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | 4130 - 4270 m: 0,3-32,0 %    |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | C1-C3, occ iC4 and nC4.      |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        | 4270 - 4323 m: <0,2% C1, C2. |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| <table border="1"> <thead> <tr> <th colspan="3">CORES</th> </tr> </thead> <tbody> <tr> <td rowspan="2">CORE #1</td> <td>CUT: 4013,6 - 4020,6 m</td> <td></td> </tr> <tr> <td>REC: 4013,6 - 4018,7 m</td> <td>72,8 %</td> </tr> <tr> <td rowspan="2">CORE #2</td> <td>CUT: 4032,5 - 4043 m</td> <td></td> </tr> <tr> <td>REC: 4032,5 - 4042,3 m</td> <td>93,3 %</td> </tr> </tbody> </table>  |                        |        |                              | CORES   |   |   | CORE #1 | CUT: 4013,6 - 4020,6 m                |  | REC: 4013,6 - 4018,7 m | 72,8 % | CORE #2 | CUT: 4032,5 - 4043 m      |  | REC: 4032,5 - 4042,3 m | 93,3 % | <table border="1"> <thead> <tr> <th colspan="2">LOGS</th> <th colspan="2">SHOWS</th> </tr> </thead> <tbody> <tr> <td>BHC-GR</td> <td>192 - 464,5 m</td> <td>1</td> <td>VELOCITY SURVEY</td> <td>500 - 4323 m</td> <td>1</td> <td>In <u>Lst</u> 2792 m: tr of slow pale yel-blue crush cut.</td> </tr> <tr> <td>ISF / SONICGR</td> <td>455 - 1621,5 m</td> <td>2</td> <td>HRT</td> <td>541 - 1589 m</td> <td>1</td> <td>In <u>Lst</u> 2828 m: tr of slow pale yel crush cut.</td> </tr> <tr> <td>"</td> <td>1366 - 1620,5 m</td> <td>2a</td> <td>"</td> <td>2655 - 3652 m</td> <td>2</td> <td>In <u>Lst</u> 3488 - 3515 m: pale yel - yel wh flu, wh - pale blue, slow-fast strmg flu cut.</td> </tr> <tr> <td>"</td> <td>1593 - 3610 m</td> <td>3</td> <td>CCL</td> <td>0 - 3696 m</td> <td>1</td> <td>In <u>Lst</u> 3565 - 3582 m: pale yel - yel wh flu, wh - pale blue, non-slow strmg flu cut.</td> </tr> <tr> <td>"</td> <td>3500 - 3715 m</td> <td>4</td> <td>CPI</td> <td>4005 - 4295 m</td> <td>1</td> <td>In <u>Lst</u> 3707 - 3723 m: wh - yel wh flu, wh - blue wh, fast - instant strmg flu cut.</td> </tr> <tr> <td>"</td> <td>3691 - 4134 m</td> <td>5</td> <td>RFT</td> <td>MISRUN</td> <td>1</td> <td>In <u>Sh</u> 3757 m: tr lt yel, slow, weak crush cut.</td> </tr> <tr> <td>"</td> <td>4000 - 4326,5 m</td> <td>6</td> <td>"</td> <td>4148,5 m</td> <td>2</td> <td>In <u>Sh</u> 3783 - 3785 m: pale yel, slow, weak crush cut.</td> </tr> <tr> <td>FDC / CNL</td> <td>455 - 1612 m</td> <td>1</td> <td>"</td> <td>3990,5 - 4292 m</td> <td>3</td> <td>In <u>Sh</u> 3833 m: tr of lt yel, v weak, slow strmg and crush cut.</td> </tr> <tr> <td>"</td> <td>1593 - 3713,5 m</td> <td>2</td> <td>"</td> <td>4053 m</td> <td>4</td> <td>In <u>Sh</u> 3860 m: lt yel, v weak, slow crush cut.</td> </tr> <tr> <td>"</td> <td>3689 - 4134 m</td> <td>3</td> <td>"</td> <td>4053 m</td> <td>5</td> <td>In <u>Sst</u> 4002 - 4015 m: abn pale blue flu, slow but extensive bluish wh cut.</td> </tr> <tr> <td>"</td> <td>3691 - 4326 m</td> <td>4a</td> <td>"</td> <td>4157,5 m</td> <td>6</td> <td>In <u>Sst</u> 4025 - 4035 m: abn pale yel flu, pale yel - wh, slow strmg cut, 80 % pale brn hydrocarbon stain</td> </tr> <tr> <td>"</td> <td>4000 - 4325,5 m</td> <td>4b</td> <td>"</td> <td>4157,5 m</td> <td>7</td> <td>In <u>Sst</u> 4036 - 4055 m: dull orange flu, yel - wh, fast strmg cut, hydrocarbon stain on clear qtz.</td> </tr> <tr> <td>DLL / MSFL</td> <td>4000 - 4324,5 m</td> <td>1</td> <td>"</td> <td>4157,5 m</td> <td>8</td> <td>In <u>Lst</u> 4190 m: wh - yel flu, wh, fast strmg cut.</td> </tr> <tr> <td>HDT</td> <td>1593 - 3712 m</td> <td>1</td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>"</td> <td>3690,5 - 4323,5 m</td> <td>2</td> <td></td> <td></td> <td></td> <td></td> </tr> </tbody> </table> |       |                            |  |  |         | LOGS |        | SHOWS                      |  | BHC-GR | 192 - 464,5 m | 1  | VELOCITY SURVEY | 500 - 4323 m           | 1 | In <u>Lst</u> 2792 m: tr of slow pale yel-blue crush cut. | ISF / SONICGR | 455 - 1621,5 m | 2      | HRT                    | 541 - 1589 m | 1 | In <u>Lst</u> 2828 m: tr of slow pale yel crush cut. | " | 1366 - 1620,5 m | 2a                       | " | 2655 - 3652 m | 2 | In <u>Lst</u> 3488 - 3515 m: pale yel - yel wh flu, wh - pale blue, slow-fast strmg flu cut. | " | 1593 - 3610 m          | 3 | CCL | 0 - 3696 m | 1 | In <u>Lst</u> 3565 - 3582 m: pale yel - yel wh flu, wh - pale blue, non-slow strmg flu cut. | "                       | 3500 - 3715 m | 4 | CPI | 4005 - 4295 m | 1 | In <u>Lst</u> 3707 - 3723 m: wh - yel wh flu, wh - blue wh, fast - instant strmg flu cut. | " | 3691 - 4134 m | 5 | RFT | MISRUN | 1                        | In <u>Sh</u> 3757 m: tr lt yel, slow, weak crush cut. | " | 4000 - 4326,5 m | 6 | " | 4148,5 m                  | 2 | In <u>Sh</u> 3783 - 3785 m: pale yel, slow, weak crush cut. | FDC / CNL | 455 - 1612 m | 1 | "          | 3990,5 - 4292 m | 3 | In <u>Sh</u> 3833 m: tr of lt yel, v weak, slow strmg and crush cut. | " | 1593 - 3713,5 m | 2                        | " | 4053 m | 4 | In <u>Sh</u> 3860 m: lt yel, v weak, slow crush cut. | " | 3689 - 4134 m   | 3 | " | 4053 m | 5 | In <u>Sst</u> 4002 - 4015 m: abn pale blue flu, slow but extensive bluish wh cut. | "                        | 3691 - 4326 m | 4a | " | 4157,5 m | 6 | In <u>Sst</u> 4025 - 4035 m: abn pale yel flu, pale yel - wh, slow strmg cut, 80 % pale brn hydrocarbon stain | " | 4000 - 4325,5 m | 4b | " | 4157,5 m | 7                        | In <u>Sst</u> 4036 - 4055 m: dull orange flu, yel - wh, fast strmg cut, hydrocarbon stain on clear qtz. | DLL / MSFL | 4000 - 4324,5 m | 1 | " | 4157,5 m | 8 | In <u>Lst</u> 4190 m: wh - yel flu, wh, fast strmg cut. | HDT | 1593 - 3712 m | 1 |                           |  |  |  | " | 3690,5 - 4323,5 m | 2       |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| CORES  |                        |        |                              |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| CORE #1  | CUT: 4013,6 - 4020,6 m |        |                              |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  | REC: 4013,6 - 4018,7 m | 72,8 % |                              |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| CORE #2  | CUT: 4032,5 - 4043 m   |        |                              |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  | REC: 4032,5 - 4042,3 m | 93,3 % |                              |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| LOGS   |                        | SHOWS  |                              |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| BHC-GR   | 192 - 464,5 m          | 1      | VELOCITY SURVEY              | 500 - 4323 m  | 1 | In <u>Lst</u> 2792 m: tr of slow pale yel-blue crush cut.   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| ISF / SONICGR  | 455 - 1621,5 m         | 2      | HRT                          | 541 - 1589 m  | 1 | In <u>Lst</u> 2828 m: tr of slow pale yel crush cut.  |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| "  | 1366 - 1620,5 m        | 2a     | "                            | 2655 - 3652 m   | 2 | In <u>Lst</u> 3488 - 3515 m: pale yel - yel wh flu, wh - pale blue, slow-fast strmg flu cut.                  |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| "  | 1593 - 3610 m          | 3      | CCL                          | 0 - 3696 m  | 1 | In <u>Lst</u> 3565 - 3582 m: pale yel - yel wh flu, wh - pale blue, non-slow strmg flu cut.                   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| "  | 3500 - 3715 m          | 4      | CPI                          | 4005 - 4295 m   | 1 | In <u>Lst</u> 3707 - 3723 m: wh - yel wh flu, wh - blue wh, fast - instant strmg flu cut.                     |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| "  | 3691 - 4134 m          | 5      | RFT                          | MISRUN  | 1 | In <u>Sh</u> 3757 m: tr lt yel, slow, weak crush cut.   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| "  | 4000 - 4326,5 m        | 6      | "                            | 4148,5 m  | 2 | In <u>Sh</u> 3783 - 3785 m: pale yel, slow, weak crush cut.   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| FDC / CNL  | 455 - 1612 m           | 1      | "                            | 3990,5 - 4292 m   | 3 | In <u>Sh</u> 3833 m: tr of lt yel, v weak, slow strmg and crush cut.  |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| "  | 1593 - 3713,5 m        | 2      | "                            | 4053 m  | 4 | In <u>Sh</u> 3860 m: lt yel, v weak, slow crush cut.  |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| "  | 3689 - 4134 m          | 3      | "                            | 4053 m  | 5 | In <u>Sst</u> 4002 - 4015 m: abn pale blue flu, slow but extensive bluish wh cut.                             |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| "  | 3691 - 4326 m          | 4a     | "                            | 4157,5 m  | 6 | In <u>Sst</u> 4025 - 4035 m: abn pale yel flu, pale yel - wh, slow strmg cut, 80 % pale brn hydrocarbon stain |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| "  | 4000 - 4325,5 m        | 4b     | "                            | 4157,5 m  | 7 | In <u>Sst</u> 4036 - 4055 m: dull orange flu, yel - wh, fast strmg cut, hydrocarbon stain on clear qtz.       |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| DLL / MSFL   | 4000 - 4324,5 m        | 1      | "                            | 4157,5 m  | 8 | In <u>Lst</u> 4190 m: wh - yel flu, wh, fast strmg cut.   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| HDT  | 1593 - 3712 m          | 1      |                              |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
| "  | 3690,5 - 4323,5 m      | 2      |                              |   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |
|  |                        |        |                              | Checked: S.I. Leivestad<br>Date: 8.6.79   |   |   |         |                                       |  |                        |        |         |                           |  |                        |        |  |       |                            |  |  |         |      |        |                            |  |        |               |    |                 |                        |   |   |               |                |        |                        |              |   |  |   |                 |                          |   |               |   |  |   |                        |   |     |            |   |   |                         |               |   |     |               |   |   |   |               |   |     |        |                          |   |   |                 |   |   |                           |   |   |           |              |   |            |                 |   |  |   |                 |                          |   |        |   |  |   |                 |   |   |        |   |   |                          |               |    |   |          |   |   |   |                 |    |   |          |                          |   |            |                 |   |   |          |   |   |     |               |   |                           |  |  |  |   |                   |         |  |  |  |  |  |                          |  |  |  |  |  |        |  |  |  |  |  |                           |  |  |  |  |  |                         |  |  |  |  |  |                              |  |  |  |  |  |  |  |  |

## RFT RESULTS

Well:

15/5-2

## RFT RESULTS

| RUN 1        |                    | RUN 3      |                    | RUN 5      |                    |
|--------------|--------------------|------------|--------------------|------------|--------------------|
| DEPTH (KB)   | FORMATION PRESSURE | DEPTH (KB) | FORMATION PRESSURE | DEPTH (KB) | FORMATION PRESSURE |
| TOOL FAILURE |                    | ① 4150 m   | 10455 PSIG         | ① 4053 m   | 10229 PSIG         |
| RUN 2        |                    | ② 4148,5 m | 10455 PSIG         | RUN 6      |                    |
| DEPTH (KB)   | FORMATION PRESSURE | ③ 4145 m   | 10460 PSIG         | DEPTH (KB) | FORMATION PRESSURE |
| ① 4148,5 m   | 10560 PSIG         | ④ 4143,5 m | 10460 PSIG         | ① 4157,5 m | 10516 PSIG         |
| RUN 3        |                    | ⑤ 4055 m   | 10231 PSIG         | RUN 7      |                    |
| DEPTH (KB)   | FORMATION PRESSURE | ⑥ 4053 m   | 10227 PSIG         | DEPTH (KB) | FORMATION PRESSURE |
| ① 4292 m     | 10682 PSIG         | ⑦ 4051,5 m | 10227 PSIG         | ① 4157,5 m | 10471 PSIG         |
| ② 4271,5 m   | TIGHT              | ⑧ 4049 m   | 10225 PSIG         | ② 4157,5 m | 10482 PSIG         |
| ③ 4259 m     | 10610 PSIG         | ⑨ 4045,2 m | SEAL FAILURE       | RUN 8      |                    |
| ④ 4227 m     | 10562 PSIG         | ⑩ 4045,5 m | SEAL FAILURE       | DEPTH (KB) | FORMATION PRESSURE |
| ⑤ 4210 m     | 10538 PSIG         | ⑪ 4046 m   | SEAL FAILURE       | ① 4157,5 m | 10456 PSIG         |
| ⑥ 4195,5 m   | 10528 PSIG         | ⑫ 3991 m   | SEAL FAILURE       | RUN 4      |                    |
| ⑦ 4186 m     | SEAL FAILURE       | ⑬ 3990,5 m | SEAL FAILURE       | DEPTH (KB) | FORMATION PRESSURE |
| ⑧ 4157 m     | 10456 PSIG         | RUN 4      |                    | ① 4053 m   | 10229 PSIG         |
| ⑨ 4155,5 m   | 10457 PSIG         | DEPTH (KB) | FORMATION PRESSURE |            |                    |
| ⑩ 4151,5 m   | TIGHT              | ① 4053 m   | 10229 PSIG         |            |                    |

Segregated sampling was performed as follows:

Run 1 Tool failed

Run 2 at 4148,5 m { Recovery 1 gal. mud filtrate  
2 3/4 gal. mud filtrate

Run 3 at 4145 m { Recovery 1 gal. mud filtrate  
2 3/4 gal. mud filtrate

Run 4 at 4053 m Sampling failed

Run 5 at 4053 m { Recovery 1 gal. mud filtrate  
2 3/4 gal. mud filtrate

Run 6 at 4157,5 m { Recovery 1 gal. failed  
6 gal. mud filtrate

Run 7 at 4157,5 m No recovery, tool malfunction

Run 8 at 4157,5 m { Recovery 1 gal. mud filtrate  
6 gal. mud filtrate

Checked: S. Leivestad

Date: 8.6.79

## 1

| LOCATED ON LINE : 508-190 |                  |        |        |       | WELL  |  |
|---------------------------|------------------|--------|--------|-------|---|--|
| N 58°38'36.7"             |                  |        |        |       | S P 106   |  |
| E 01°35'16.5"             |                  |        |        |       | 01°35'16.5"   |  |
| WATER DEPTH 120 m         |                  |        |        |       | 15/5-2  |  |
| DEPTHS<br>m<br>KB         | LITHO<br>SECTION | SYSTEM | SERIES | SHOWS | DESCRIPTIONS. OBS   |  |
| 50                        |                  |        |        |       | 25 m SEA LEVEL  |  |
| 100                       |                  |        |        |       |   |  |
| 150                       |                  |        |        |       | 145.5 m SEA BOTTOM<br>Drilled with return to seabed.  |  |
| 200                       |                  |        |        |       | 194<br><u>Cly</u> , m-m dk gy olvg, sft-firm,<br>silty, sl stky, sl-mod calc.   |  |
| 250                       |                  |        |        |       | Occ intbds of <u>Sd</u> :<br>qtz, clr, occ fros, vf-crs,<br>occ v crs, ang-subrnd, pr<br>srted, w/dk gy-dk g-n-<br>blk lithic frags.  |  |
| 300                       |                  |        |        |       | Tr <u>Lst</u> , wh, hd, cnky.   |  |
| 350                       |                  |        |        |       | Tr shell frags and <u>Pyr</u> .   |  |
| 400                       |                  |        |        |       | 480   |  |
| 450                       |                  |        |        |       | Abn shell frags,<br>Tr <u>Glau</u> and <u>Lig</u> .   |  |
| 500                       |                  |        |        |       | 700   |  |
| 550                       |                  |        |        |       | 758<br><u>Sd</u> , clr, lse, vf-f, ang-<br>subrnd, mod well srted,<br>w/occ layers of <u>Cly</u> , a/a.<br>Tr shell frags, <u>Pyr</u> ,<br><u>Glau</u> and <u>Mica</u> .              |  |
| 600                       |                  |        |        |       | 910<br><u>Cly</u> , olv gy-olv grn, sft, sl<br>calc, silty.<br>Tr <u>Sd</u> , clr, vf-f, subang<br>mod srted.<br>Tr shell frags, <u>Mica</u> , <u>Glau</u> .                          |  |
| 650                       |                  |        |        |       | 1060<br><u>Sd</u> , clr, vf-m, occ crs, ang-<br>subang, pr srted, w/lithic<br>frags.<br>Below 1250 m lam of<br><u>Sst</u> , mgy, brn-gy, brn-grn,<br>firm, micro mic, v arg, mod calc |  |
| 700                       |                  |        |        |       |   |  |
| 750                       |                  |        |        |       |   |  |
| 800                       |                  |        |        |       |   |  |
| 850                       |                  |        |        |       |   |  |
| 900                       |                  |        |        |       |   |  |
| 950                       |                  |        |        |       |   |  |
| 1000                      |                  |        |        |       |   |  |
| 1050                      |                  |        |        |       |   |  |
| 1100                      |                  |        |        |       |   |  |
| 1150                      |                  |        |        |       |   |  |
| 1200                      |                  |        |        |       |   |  |
| 1250                      |                  |        |        |       |   |  |

# GEOLOGICAL WELL SUMMARY

2

| DEPTH<br>E<br>KB | LITHO<br>SECTION | SYSTEM/<br>SERIES | STAGES<br>SHOWS  | DESCRIPTIONS OBS   | LOCATED ON LINE |             | WELL  |
|------------------|------------------|-------------------|------------------|--|-----------------|-------------|---|
|                  |                  |                   |                  |  | SP              | WATER DEPTH |   |
|                  |                  |                   |                  |  |                 | 120 m       | 15/5 - 2  |
| 2500             |                  | TERTIARY          | DANIAN PALEOCENE | Sh, a/a, incr in <u>Cl</u> ,<br>m gy-brn gy, sft, non calc.  |                 |             | 3711  |
| 2550             |                  |                   |                  | 2506<br><u>Cl</u> , a/a w/ minor <u>Sh</u> a/a.  |                 |             | 3759 (M2)   |
| 2600             |                  |                   |                  | 2650   |                 |             | 3774 <u>Sh</u> , dk brn, brn blk, sft -<br>firm, earthy, silty, carb, n-si calc,<br>pyl.  |
| 2650             |                  |                   |                  | 2705<br><u>Lst</u> , wh, crm, mod hd, micro-<br>xin and lt gy, sft, arg, grdg<br>to <u>Mrst</u> and tr of <u>Sh</u> , m dk<br>gy-blk, firm, occ silty, calc.                                     |                 |             | 3814  |
| 2700             |                  |                   |                  | 2782<br><u>Lst</u> , a/a but pred cln, occ<br>chky, occ grdg to <u>Mrst</u> , lt-m<br>gy, sft-firm.  |                 |             | 3831 <u>Sh</u> , dk brn-dk gy, firm-mod<br>hd, blk-fis, occ earthy,<br>silty, carb, si-mod calc   |
| 2750             |                  |                   |                  | Minor thin intbds of<br><u>Sh</u> , lt-dk gy, w/ blk lam,<br>firm-hd, subfis, calc.  |                 |             | 3694 intbd w/strgs of <u>Lst</u> ,<br>m - dk-brn, micro-xin, arg<br>and <u>Dol</u> , dk brn, hd - v hc.   |
| 2800             |                  |                   |                  | Tr <u>Gla</u> , <u>Pyr</u> .   |                 |             | 3960 <u>Sh</u> , a/a intbd w/Coal.  |
| 2850             |                  |                   |                  | 2967<br><u>Mrst</u> , lt-m rd brn, minor<br>lt gy, hd, v arg, intbd w/<br><u>Lst</u> , wh, crm, lt brn rd, firm,<br>crypto xin, often arg, grdg to<br><u>Mrst</u> , a/a.                         |                 |             | 4037 <u>Sst</u> , wh-lt brn, vf-f, occ m<br>and crs-vcrs, ang-subrnd,<br>fri-hd, calc, occ silic cmtd,<br>mod-well srted, pr-mod por.   |
| 2900             |                  |                   |                  | 3060<br><u>Mrst</u> , pred lt-m gy, minor<br>rd brn a/a, firm, v arg, occ<br>grdg to <u>Sh</u> . Occ intbds of<br><u>Lst</u> , crm, wh, hd, micro-<br>crypto xin, cln and arg, occ<br>si dol.    |                 |             | 4113 <u>Sst</u> , pale yelsh brn, yelsh<br>gy, occ grnsh gy, occ rd<br>stained, vf-m, in pt silty,<br>ang-subrnd, lse-fri,<br>silic and calc cmt, occ mic,<br>pr-weil srt, pr-fair por. |
| 2950             |                  |                   |                  | 3293<br><u>Mrst</u> , lt-m gy, minor lt brn<br>and rd brn, grdg downwards<br>to <u>Lst</u> , wh, lt gy, sft and hd<br>Tr <u>Sh</u> , dk gy, rd brn, occ<br>silty, tr carb, calc and non<br>calc. |                 |             | Intbds of <u>Sh</u> , brnsh gy,<br>gysh rd, dusk brn, lt-dk<br>gy, micro-mic, si-non calc   |
| 3000             |                  | UPPER CRETACEOUS  | SANTON - CAMPAN  | 3507<br><u>Mrst</u> , lt-m gy, chky, calcilutite,<br>and micro-xin, occ arg.   |                 |             | In places grdg to <u>Sist</u> ,<br>gysh rd, fri-hd, non calc.   |
| 3050             |                  |                   |                  | 3588 <u>Mrst</u> , lt-m gy, sft-firm,<br>intbd w/ <u>Lst</u> , wh lt gy, sft -<br>hd, micro-xin, chky, in pts<br>grdg to <u>Mrst</u> , a/a. Tr <u>Sh</u> , a/a.                                  |                 |             | Tr of <u>Lst</u> and <u>Dol</u> .   |
| 3100             |                  |                   |                  | 3637   |                 |             |   |
| 3150             |                  |                   |                  | 3689 <u>Sh</u> , lt-dk gy, lt gy grn,<br>3701 rd brn, micro-mic, non-<br>v calc, in pt grdg to <u>Mrst</u> .<br>strgs of <u>Lst</u> and tr <u>Sst</u> .  |                 |             |   |
| 3200             |                  |                   |                  |  |                 |             |   |
| 3250             |                  |                   |                  |  |                 |             |   |
| 3300             |                  |                   |                  |  |                 |             |   |
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| 3500             |                  | UPPER CRETACEOUS  | SANTON - CAMPAN  |  |                 |             |   |
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|                  |                  | UPPER CRETACEOUS  | SANTON - CAMPAN  |  |                 |             |   |
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SECTION B  
OPERATIONS

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# 1. LOCATION SURVEY

From June 5 through June 16, 1978 the vessel M/S "Bommeløy" performed a site survey in the area for the planned well 15/5-2, which was given as:-

58° 38' 34.85" N

01° 36' 17.27" E

The survey area was a rectangle of approximately 5.0 by 4.6 kilometers. The survey equipment used was echo sounder for bathymetric mapping, dual channel side scan sonar, boomer and high and low energy sparker. 5 Gravity cores were also obtained.

The gravity cores showed that the sea bed consisted of fine sand which made the penetration for the gravity corer difficult. The length of the samples achieved varied from a few centimeter to 1.3 m.

The seismic data indicated that the uppermost 30 m of the sediments consisted of soft sand. Between 30 and 140 m below the sea bed a zone probably consisting of morainic deposits was identified.

No shallow gas zones were observed in the upper layers around the given drilling location. No obstructions were found within the survey area, which could be interpreted to create any problems for the drilling operation.

The water depth at the proposed location was found to be 121.3 m, referred to Mean Sea Level.



## 2. POSITIONING AND ANCHORING OF THE RIG

The location for the well 15/5-2 was defined as shotpoint 106 on seismic line 508-190 shot by Western in 1976, with the use of Decca Hifix and Sat.nav. as navigation systems. The well should be spudded within a radius of 70 m from this position.

The equipment on board the rig for positioning was Pulse/8 and Sat.nav. No problems were encountered during the moving of the rig, and on August 15. at 15.30 hrs. the rig arrived on the location. At 22.30 hrs. all eight anchors were set with piggy-backs on No. 1,3,5 and 7, as shown in Fig. A-1.

Prior to spudding on August 16 the anchors were pretensioned to:-

|              |        |
|--------------|--------|
| Chain No. 1: | 820 kN |
| " " 2:       | 780 "  |
| " " 3:       | 910 "  |
| " " 4:       | 730 "  |
| " " 5:       | 930 "  |
| " " 6:       | 930 "  |
| " " 7:       | 870 "  |
| " " 8:       | 1000 " |

Before drilling out of the 30" casing all anchors were tested to minimum 1110 kN.

The final position of well 15/5-2 was established on August 18 at 09.00 GMT. (referred to the European Datum 1950):

58° 38' 36.7" N  
01° 36' 16.5" E

This is 60 m in a 348 degrees direction from the planned location.

### 3. OPERATION RESUME

#### 3.1 Summary

Treasure Seeker was taken over from Statoil August 15, at 07.35 hrs. and moved to the well 15/5-2 location. It was ready to spud after 40 hrs. of anchor handling.

The 36" hole was drilled to 194.5 m RKB and the 30" casing was set at 194 m and cemented back to the sea floor. The riser was run and a 17½" pilot hole was drilled to 469 m with returns to the surface. The hole was logged prior to under-reaming to 26". The 20" casing was run to 454 m and cemented back to the sea floor.

After having run and tested the BOP stack to full working pressure the 20" casing shoe was drilled out and a formation integrity test was run at 474 m giving 1.47 rd.

The drilling of the 17½" hole continued to 1267 m without stabilizers in the drill string. While running in the hole after having installed the stabilizers, a tight hole section was encountered, and while working the drill string through this section, the string unscrewed 185 m above the bit. The fish was recovered on the first attempt, and the drilling of the 17½" hole continued down to 1615 m. The hole was logged, and the 13-3/8" casing was run with the casing shoe at 1598 m RKB. The casing was cemented back to 1150 m before the casing was tested to 207 bar.

The 12-1/4" hole was drilled down to 1635 m, where a formation integrity test was performed, giving 1.68 rd.

When drilling from 1884 m to 2069 m torque problems were encountered and the near bit stabilizer was found to be worn 1/4" on the diameter of the blades. Below 2069 m no severe problems were encountered and the drilling continued down to 2293 m.

When pulling out for bit change the string got stuck at 1928 m and the drill string was backed off at 1723 m. After jarring on the fish without any success the string was backed off at 1839 m, leaving nine joints of 8" drill collars, three stabilizers, one bit sub, one junk basket and the bit in the hole.

A cement plug was set twice above the fish for side tracking before the operation successfully continued by drilling the 12-1/4" side tracked hole.

When drilling at 1879 m the operation was shut down for 48 hrs. due to heavy weather conditions.

The drilling of the 12-1/4" hole continued down to 3606 m without any major problems. At this depth an intermediate ISF/sonic log was run to confirm the geological prognosis. After having drilled to 3714 m, logs were run before two cones lost in the hole were fished out.

The 9-5/8" casing was run with the casing shoe at 3696 m RKB. The cement was brought back in the annulus to 3200 m, and the casing was tested to 345 bar. A formation integrity test was performed at 3719 m, giving 2.07 rd.

The drilling of the 8-3/8" hole continued down to 4013 m, where the mud density had to be increased from 1.46 rd to 1.63 rd due to gas cut mud. Two cores were cut, one from 4013 m to 4020 m, and one from 4032 m to 4044. At 4130 m two intermediate logs consisting of ISF/sonic and FDC/CNL were run before the drilling of 8-3/8" hole continued down to 4322 m, using a 1.90 rd mud.

Due to heavy weather on November 14 the riser was disconnected, and in the same period one anchor chain broke. A total of 4.5 days were lost before the broken chain could be repaired and the riser connected.

The final logging in the 8-3/8" hole took place over a period of 11 days. Problems encountered during this period were malfunctioning of the RFT and CST tools, sticking of HDT tool and in the attempts to obtain formation fluid samples by the RFT. Only mud filtrate samples were obtained from the RFT sampling.

After discussion with the partners it was decided to temporary abandon the well, and a 7" liner was run with the shoe set at 4300 m.

While cementing the liner one cement line plugged, causing the cement to be brought back in the annulus only to 3780 m. 5.3 m<sup>3</sup> cement were spotted on top of the liner hanger, of which 2.9 m<sup>3</sup> were squeezed into the formation, leaving a 60 m plug on top of the liner, which was successfully tested to 140 bar.

The well was temporary abandoned, and the last anchor was retrieved on December 16, after waiting on weather for approximately 10 days.

## Weekly drilling report

- 6 -

|                        |                |                        |           |    |
|------------------------|----------------|------------------------|-----------|----|
| Week<br>14/8-20/8-1978 | Weeks Progress | Report no.<br>1        | Page<br>1 | of |
| Area<br>North Sea      | Well<br>15/5-2 | Rig<br>TREASURE SEEKER |           |    |

|        |                   |     |  |  |  |  |  |
|--------|-------------------|-----|--|--|--|--|--|
| Casing | Size              | 30" |  |  |  |  |  |
|        | Setting depth (m) | 194 |  |  |  |  |  |

| Date | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation  |
|------|---------------------------|---------------------------|-------------------------|---|
| 15/8 | -                         | -                         | -                       | Treasure Seeker was taken over from Statoil at 07.35 hrs. Moved the rig from 24/12-1 to 15/5-2. The anchors were run with 4 piggybacks. Started to ballast the rig.   |
| 15/8 | 192                       | 1.07                      | 1.30                    | Ballasted the rig. Ran a 26" bit and a 36" hole opener. The measured depth to sea bed was 145.5 m. RKB. Drilled 36" hole from 145.5 m to 192 m.   |
| 17/8 | 194.5                     | 1.07                      | 1.08                    | Drilled from 192 m to 194.5 m. Made a short trip and started to run the 30" casing. Was not able to get below 182.5 m. Pulled out the 30" casing and ran in the hole with the 36" hole-opener again. Reamed from 175 m to 194.5 m. Ran and landed the 30" casing at 194 m. Cemented the same with full returns to seabed. |
| 18/8 | 202                       | 1.07                      | 1.08                    | Ran the 30" hydraulic latch on the 21" riser. Installed the diverter and tested same. Ran in the hole with 17½" bit to drill the pilot hole. Tagged cement at 190 m. Drilled from 194.5 m to 202 m.   |
| 19/8 | 469                       | 1.07                      | 1.14                    | Drilled 17½" hole from 202 m to 469 m. Ran sonic log but the tool would not go below 282 m. Reamed with the 17½" bit to bottom and raised the mud weight to 1.14 rd.  |
| 20/8 | 469                       | 1.07                      | 1.16                    | Conditioned the mud prior to logging. Ran sonic log. Opened the 17½" hole to 26" by using an underreamer.   |

|                        |                |                        |           |    |
|------------------------|----------------|------------------------|-----------|----|
| Week<br>21/8-27/8-1978 | Weeks Progress | Report no.<br>2        | Page<br>2 | of |
| Area<br>North Sea      | Well<br>15/5-2 | Rig<br>TREASURE SEEKER |           |    |

|        |                   |     |     |  |  |  |  |
|--------|-------------------|-----|-----|--|--|--|--|
| Casing | Size              | 30" | 20" |  |  |  |  |
|        | Setting depth (m) | 194 | 454 |  |  |  |  |

| Date | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation  |
|------|---------------------------|---------------------------|-------------------------|---|
| 21/8 | 469                       | 1.07                      | 1.16                    | Pulled the 21" riser. Made wiper trip with the 26" bit.<br>Started to run the 20" casing.   |
| 22/8 | 469                       | 1.07                      | 1.16                    | Ran the 20" casing with the shoe at 454 m. Tested the casing to 69 bar for 15 min. Prepared to run the BOP and the riser.   |
| 23/8 | 469                       | 1.07                      | 1.16                    | When function testing the BOP the lower annular preventer would not open fully. Dressed and serviced the same and changed out spm and shuttle valves for the upper outer choke valve. Ran the 21" riser and the BOP and latched the BOP to the wellhead. Tested the BOP to the full working pressure.                 |
| 24/8 | 559                       | 1.07                      | 1.16                    | Finished testing the BOP. Drilled 17½" hole to 474 m. Ran leak-off test, giving 1.47 rd. equivalent mud density. Drilled 17½" hole from 474 m to 559 m.   |
| 25/8 | 966                       | 1.07                      | 1.13                    | Drilled 17½" hole from 559 m to 966 m.  |
| 26/8 | 1267                      | 1.07                      | 1.14                    | Drilled 17½" hole from 966 m to 1267 m. Pulled out for bit change. Ran in with new bit and 2 string stabilizers.  |
| 27/8 | 1267                      | 1.07                      | 1.16                    | Ran in the hole. Hit tight spots at 760 m and 1124 m. Lost 333 kN of the string weight when attempted to pass 1124 m. Pulled out and found the drill string had unscrewed 2 singles above the drill collars. Ran in with an overshot, latched to the fish and pulled out. Ran in the hole and reamed all tight spots. |

|                       |                |                        |           |    |
|-----------------------|----------------|------------------------|-----------|----|
| Week<br>28/8-3/9-1978 | Weeks Progress | Report no.<br>3        | Page<br>3 | of |
| Area<br>North Sea     | Well<br>15/5-2 | Rig<br>TREASURE SEEKER |           |    |

|        |                   |     |     |        |  |  |  |
|--------|-------------------|-----|-----|--------|--|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 |  |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   |  |  |  |

| Date | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|------|---------------------------|---------------------------|-------------------------|--|
| 28/8 | 1416                      | 1.07                      | 1.16                    | Reamed to bottom. Drilled 17½" hole from 1267 m to 1416 m.   |
| 29/8 | 1615                      | 1.07                      | 1.17                    | Drilled 17½" hole from 1416 m to 1615 m. Conditioned mud prior to logging.   |
| 30/8 | 1615                      | 1.07                      | 1.20                    | Made wiper trip to the 20" casing shoe. Pulled out for logging. Schlumberger was not able to get below 990 m. Ran in with the bit and raised the mud density to 1.20 rd and reduced the water loss to 6 cc.  |
| 31/8 | 1615                      | 1.07                      | 1.20                    | Ran ISF-sonic-GR log. The sonice tool did not work in the lower 200 m, had to relog the bottom section.<br>Ran the FDC-GR log. The caliper arm would not work. Repaired cable failure.<br>Ran the FDC-GR for 2. time, but the tool did not operate properly. Pulled out and checked the tool.<br>Ran FDC-GR for the 3. time. |
| 1/9  | 1615                      | 1.07                      | -                       | Finished running FDC-GR log. RIH with 17½" bit. Had to break all connections to check made up torque.  |
| 2/9  | 1615                      | 1.07                      | -                       | Ran and cemented the 13-3/8" casing with the shoe at 1598 m.   |
| 3/9  | 1615                      | 1.07                      | -                       | Tested the casing to 207 bar for 15 min. Ran temperature log which indicated the top of the cement to be at 1150 m. Tested the BOP and the surface equipment to 345 bar.   |

|      |               |                |            |      |                 |
|------|---------------|----------------|------------|------|-----------------|
| Week | 4/9-10/9-1978 | Weeks Progress | Report no. | Page | of              |
|      |               |                | 4          | 4    |                 |
| Area | North Sea     | Well           | 15/5-2     | Rig  | Treasure Seeker |

|        |                   |     |     |        |  |  |  |
|--------|-------------------|-----|-----|--------|--|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 |  |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   |  |  |  |

| Date | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation  |
|------|---------------------------|---------------------------|-------------------------|---|
| 4/9  | 1802                      | 1.07                      | 1.20                    | Ran in with 12-1/4" bit. Tagged the cement at 1573 m. Drilled cement, collar and shoe and continued to drill 12-1/4" hole to 1635 m.<br>Ran leak-off test, giving 1.68 rd equivalent mud density. Drilled 12-1/4" hole from 1635 m to 1802 m.   |
| 5/9  | 1884                      | 1.07                      | 1.20                    | Pulled out to install stabilizers in the string.<br>Drilled 12-1/4" hole from 1802 m to 1884 m. Bit torqued up.<br>Pulled out and had 400 kN overpull at 1800 m.  |
| 6/9  | 1903                      | 1.07                      | 1.20                    | The bit and the stabilizers were badly balled up and the inner teeth on the bit were broken. Ran in the hole and drilled from 1884 m to 1903 m. The rotary stalled due to high torque.<br>Pulled out. Found that the near bit stabilizer was 1/4" worn down. Ran in the hole without the near bit stabilizer.                                     |
| 7/9  | 2149                      | 1.07                      | 1.20                    | Drilled 12-1/4" hole from 1903 m to 2069 m. Had torque problems when the 3 stabilizers in the string passed 1901 m.   |
| 8/9  | 2293                      | 1.07                      | 1.22                    | Drilled 12-1/4" hole from 2069 m to 2293 m. Pulled out for bit change. Got stuck 3 times on the way out. Managed to work the pipe free by circulating. The depths were 2106 m, 1963 m and 1944 m. When reaching 1928 m the pipe got stuck again and the circulation was lost. Pulled with max. 890 kN overpull without managing to free the pipe. |



|                       |                |                        |           |
|-----------------------|----------------|------------------------|-----------|
| Week<br>4/9-10/9-1978 | Weeks Progress | Report no.<br>4        | Page<br>5 |
| Area<br>North Sea     | Well<br>15/5-2 | Rig<br>Treasure Seeker |           |

|        |                   |     |     |        |  |  |  |
|--------|-------------------|-----|-----|--------|--|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 |  |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   |  |  |  |

| Date | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|------|---------------------------|---------------------------|-------------------------|--|
| 9/9  | 2293                      | 1.07                      | 1.22                    | <p>Attempted to free the string by pulling 979 kN overpull without success. Ran free point indicator which indicated that the string was free down to the drill collars.</p> <p>Schlumberger ran string shot in an and attempt to back off at 1723 m. No success. Ran 2. string shot and managed to back off. When the pipe backed off the Schlumberger cable broke on surface and was dropped inside the drill pipe.</p> <p>Started to build fishing spear for the cable.</p> |
| 10/9 | 2293                      | 1.07                      | 1.22                    | <p>Schlumberger ran the CCl-log and tagged the top of wire at 265 m. RIH with the rig made fishing spear and fished for the cable. No success.</p> <p>Cemented a 50 m cement plug from 1190 m to 1240 m inside the drill pipe.</p> <p>After waiting on cement, pulled out with the string and the wire.</p>  |

|                        |                |                        |           |    |
|------------------------|----------------|------------------------|-----------|----|
| Week<br>11/9-17/9-1978 | Weeks Progress | Report no.<br>5        | Page<br>6 | of |
| Area<br>North Sea      | Well<br>15/5-2 | Rig<br>Treasure Seeker |           |    |

|        |                   |     |     |        |  |  |  |
|--------|-------------------|-----|-----|--------|--|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 |  |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   |  |  |  |

| Date | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|------|---------------------------|---------------------------|-------------------------|--|
| 11/9 | 2293                      | 1.07                      | 1.22                    | Retrieved the Schlumberger wire.<br>Ran CCL-log to check the 13-3/8" casing.<br>Found everything ok.<br>Ran in the hole with a jar in the string<br>and screwed into the fish. Jared both<br>ways but were unable to free the fish.                                |
| 12/9 | 2293                      | 1.07                      | 1.22                    | Backed off at 1839 m after 2 attempts.<br>Retrieved 12 joints of 8" drill collars.<br>Ran in the hole and set a cement plug from<br>the top of fish at 1839 m to 1779 m.<br>Tested the BOP.  |
| 13/9 | 1827                      | 1.07                      | 1.22                    | Finished testing the BOP.<br>Ran in the hole with a new bottom hole<br>assembly for sidetracking.<br>Drilled 12-1/4" hole from 1775 m to 1827 m.   |
| 14/9 | 1740                      | 1.07                      | 1.22                    | Drilled 12-1/4" hole from 1827 m to 1840 m<br>where the top of the fish was tagged.<br>Pulled out of the hole and set a new<br>cement plug from 1840 m to 1740 m.  |
| 15/9 | 1829                      | 1.07                      | 1.22                    | Drilled 12-1/4" hole from 1781 m to 1829 m.<br>The angle was build up to 5-3/4°.<br>Pulled out to change bottom hole<br>assemblies.  |
| 16/9 | 1874                      | 1.07                      | 1.22                    | Drilled 12-1/4" hole from 1829 m to 1879 m.<br>The angle dropped to 5°.<br>Due to hurricane forecast pulled into<br>13-3/8" casing shoe and prepared to hang<br>off. Waited on weather from 16.00 hrs.<br>Hung off at 18.30 hrs. and disconnected<br>at 23.00 hrs. |
| 17/9 | 1874                      | 1.07                      | 1.22                    | Waited on weather.   |

|      |                |                |            |   |      |                 |    |  |
|------|----------------|----------------|------------|---|------|-----------------|----|--|
| Week | 18/9-24/9-1978 | Weeks Progress | Report no. | 6 | Page | 7               | of |  |
| Area | North Sea      | Well           | 15/5-2     |   | Rig  | Treasure Seeker |    |  |

|        |                   |     |     |        |   |  |  |
|--------|-------------------|-----|-----|--------|---|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 | . |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   |   |  |  |

| Date | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation  |
|------|---------------------------|---------------------------|-------------------------|---|
| 18/9 | 1945                      | 1.07                      | 1.20                    | Waited on weather until 10.00 hrs.<br>Latched on to the BOP and drilled 12-1/4" hole from 1874 m to 1945 m.   |
| 19/9 | 2127                      | 1.07                      | 1.20                    | Drilled 12-1/4" hole from 1945 m to 2127 m.   |
| 20/9 | 2232                      | 1.07                      | 1.26                    | Drilled 12-1/4" hole from 2127 m to 2232 m.<br>Pulled out of hole for bit change. Got stuck at 1939 m but managed to free the string by jarring down. Added 1% diesel to the mud, lowered the water loss and raised the mud density to 1.26 rd. Worked the string in singles through the tight section. |
| 21/9 | 2232                      | 1.07                      | 1.26                    | Pulled out of the hole.<br>Tested the BOP.<br>Ran in the hole with a new bit.   |
| 22/9 | 2351                      | 1.07                      | 1.26                    | Reamed from 1991 m to 2048 m and from 2147 m to 2232 m.<br>Drilled 12-1/4" hole from 2232 m to 2351 m.<br>From 09.00 to 15.00 hrs. rig personnel were on strike.  |
| 23/9 | 2456                      | 1.07                      | 1.26                    | Drilled 12-1/4" hole from 2351 m to 2355 m.<br>Pulled out of the hole for bit change.<br>Drilled 12-1/4" hole from 2355 m to 2456 m.  |
| 24/9 | 2613                      | 1.10                      | 1.26                    | Drilled 12-1/4" hole from 2456 m to 2488 m.<br>Pulled out for bit change and continued drilling to 2613 m.  |

|                        |                |                        |           |    |
|------------------------|----------------|------------------------|-----------|----|
| Week<br>25/9-1/10-1978 | Weeks Progress | Report no.<br>7        | Page<br>8 | of |
| Area<br>North Sea      | Well<br>15/5-2 | Rig<br>Treasure Seeker |           |    |

|        |                   |     |     |        |  |  |  |
|--------|-------------------|-----|-----|--------|--|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 |  |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   |  |  |  |

| Date | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation  |
|------|---------------------------|---------------------------|-------------------------|---|
| 25/9 | 2711                      | 1.17                      | 1.26                    | Drilled 12-1/4" hole from 2613 m to 2639 m. Pulled out for bit change and continued drilling to 2711 m.                           |
| 26/9 | 2737                      | 1.17                      | 1.27                    | Drilled 12-1/4" hole from 2711 m to 2731 m. Made a bit change and drilled to 2737 m.  |
| 27/9 | 2826                      | 1.17                      | 1.27                    | Drilled 12-1/4" hole from 2737 m to 2826 m. Pulled out for bit change.  |
| 28/9 | 2826                      | 1.17                      | 1.27                    | Tested the BOP. Made up the turbine and diamond bit and ran in the hole. Had to ream through tight sections at 2034 m and 2321 m. |
| 29/9 | 2842                      | 1.17                      | 1.27                    | Reamed 12-1/4" hole from 2341 m to 2742 m and from 2799 m to 2826 m. Drilled 12-1/4" hole from 2826 m to 2842 m.                  |
| 30/9 | 2929                      | 1.17                      | 1.27                    | Drilled 12-1/4" hole from 2842 m to 2929 m. Made short trip to 2400 m.  |
| 1/10 | 3007                      | 1.17                      | 1.27                    | Drilled 12-1/4" hole from 2929 m to 3007m.  |

|      |                |                |            |   |      |                 |    |  |
|------|----------------|----------------|------------|---|------|-----------------|----|--|
| Week | 2/10-8/10-1978 | Weeks Progress | Report no. | 8 | Page | 9               | of |  |
| Area | North Sea      | Well           | 15/5-2     |   | Rig  | Treasure Seeker |    |  |

|        |                   |     |     |        |  |  |  |
|--------|-------------------|-----|-----|--------|--|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 |  |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   |  |  |  |

| Date | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|------|---------------------------|---------------------------|-------------------------|--|
| 2/10 | 3075                      | 1.17                      | 1.27                    | Drilled 12- 1/4" hole from 3007 m to 3075 m.   |
| 3/10 | 3147                      | 1.17                      | 1.27                    | Drilled 12-1/4" hole from 3075 m to 3147 m.  |
| 4/10 | 3213                      | 1.17                      | 1.27                    | Drilled 12-1/4" hole from 3147 m to 3213 m.  |
| 5/10 | 3279                      | 1.18                      | 1.27                    | Drilled 12-1/4" hole from 3213 m to 3279 m.  |
| 6/10 | 3340                      | 1.18                      | 1.27                    | Drilled 12-1/4" hole from 3279 m to 3340 m.  |
| 7/10 | 3359                      | 1.18                      | 1.27                    | Drilled 12-1/4" hole from 3340 m to 3359 m.<br>Had to pull out due to one pump motor<br>burned down. Tight hole was encountered<br>at 2210 m and 1857 m. |
| 8/10 | 3369                      | 1.18                      | 1.27                    | Tested the BOP and surface equipment and<br>ran in the hole with conventional rock bit.<br>Drilled 12-1/4" hole from 3359 m to 3369 m.                   |

|                         |                |                        |            |
|-------------------------|----------------|------------------------|------------|
| Week<br>9/10-15/10-1978 | Weeks Progress | Report no.<br>9        | Page<br>10 |
| Area<br>North Sea       | Well<br>15/5-2 | Rig<br>Treasure Seeker |            |

|        |                   |     |     |        |  |  |  |
|--------|-------------------|-----|-----|--------|--|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 |  |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   |  |  |  |

| Date  | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|-------|---------------------------|---------------------------|-------------------------|--|
| 9/10  | 3411                      | 1.17-1.22                 | 1.30                    | Drilled 12-1/4" hole from 3369 m to 3411 m.  |
| 10/10 | 3435                      | 1.17-1.22                 | 1.30                    | Drilled 12-1/4" hole from 3411 m to 3425 m. Pulled out for bit change. Continued drilling to 3435 m.   |
| 11/11 | 3486                      | 1.17-1.22                 | 1.30                    | Drilled 12-1/4" hole from 3435 m to 3486 m. Started to pull out for bit change.  |
| 12/10 | 3504                      | 1.17-1.22                 | 1.30                    | Changed the bit and continued drilling 12-1/4" hole from 3486 m to 3504 m. Had drop in pump pressure. Searched for leaks in the surface equipment, but no leaks were detected. Pulled out. Found crack in the crossover between the hw. drill pipe and the drill collar. |
| 13/10 | 3544                      | 1.17-1.22                 | 1.30                    | Changed the bit and the crossover and ran in the hole. Drilled 12-1/4" hole from 3504 m to 3544 m.   |
| 14/10 | 3599                      | 1.17-1.22                 | 1.30                    | Drilled 12-1/4" hole from 3544 m to 3599 m.  |
| 15/10 | 3606                      | 1.17-1.22                 | 1.30                    | Drilled 12-1/4" hole from 3599 m to 3606 m. Pulled out of the hole for bit change. Ran ISF/sonic/GR log as intermediate log run. Tested the BOP and the surface equipment.   |

|                       |                |                        |            |    |
|-----------------------|----------------|------------------------|------------|----|
| Week<br>16/10 - 22/10 | Weeks Progress | Report no.<br>10       | Page<br>11 | of |
| Area<br>North Sea     | Well<br>15/5-2 | Rig<br>Treasure Seeker |            |    |

|        |                   |     |     |        |  |  |  |
|--------|-------------------|-----|-----|--------|--|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 |  |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   |  |  |  |

| Date  | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation  |
|-------|---------------------------|---------------------------|-------------------------|---|
| 16/10 | 3626                      | 1.22                      | 1.30                    | Finished testing the surface equipment. Ran in the hole with the two cone bit, type A1. Hit bridge at 3593 m and had to jar to free the string. Reamed from 3593 m to 3606 m. Drilled 12-1/4" hole from 3606 m to 3626 m. |
| 17/10 | 3681                      | 1.22                      | 1.30                    | Drilled 12-1/4" hole from 3626 m to 3681 m.   |
| 18/10 | 3712                      | 1.27                      | 1.34                    | Drilled 12-1/4" hole from 3681 m to 3712 m. Circulated and raised the mud density to 1.34 rd. Pulled out of the hole for logging.   |
| 19/10 | 3712                      | 1.27                      | 1.34                    | Finished pulling out. Found both cones lost. Ran 3 log runs.<br>Run No. 1: ISF/sonic/gr/sp<br>Run No. 2: fdc/cnl/cal/gr<br>Run No. 3: hdt<br>Started to ran in the hole with a magnet.                                    |
| 20/10 | 3712                      | 1.27                      | 1.34                    | Recovered only small fragments with the magnet. Finished logging by running 2 runs with cst log. Ran in the hole with a reverse circulating junk basket with a finger shoe.   |
| 21/10 | 3712                      | 1.27                      | 1.34                    | Pulled out of hole with the reverse circulating junk basket but recovered only lost bullets from the cst log. Ran in the hole with a hard formation bit and drilled on the junk. Pulled out of the hole.                  |
| 22/10 | 3714                      | 1.27                      | 1.34                    | Ran in the hole with a convential junk basket. Recovered both lost cones. Made a wiper trip prior to running the 9-5/8" casing. Drilled 2 m of new hole to ensure that all the junk was recovered.                        |

|                       |                |                        |               |
|-----------------------|----------------|------------------------|---------------|
| Week<br>23/10 - 29/10 | Weeks Progress | Report no.<br>11       | Page<br>12 of |
| Area<br>North Sea     | Well<br>15/5-2 | Rig<br>Treasure Seeker |               |

|        |                   |     |     |        |       |  |  |
|--------|-------------------|-----|-----|--------|-------|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 | 9-5/8 |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   | 3696  |  |  |

| Date  | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|-------|---------------------------|---------------------------|-------------------------|--|
| 23/10 | 3714                      | 1.27                      | 1.34                    | Ran the 9-5/8" casing. Rigged up for cementing. The casing shoe set at 3696 m.   |
| 24/10 | 3714                      | 1.27                      | 1.34                    | Cemented the 9-5/8" casing back to 3200 m. Torqued up the seal assembly to 19000 Nm and tested the same to 69 bar. Pulled out and layed down the running string. Ran down with the 18-3/4" seal assembly retrieving and reinstallation tool on 8" drill collars. Torqued up the seal assembly to 34000 Nm. Ran the temperature log. Located top of the cement at 3200 m. Started to test the BOP.  |
| 25/10 | 3714                      | 1.27                      | 1.34                    | Continued testing the BOP. Had 14 bar in pressure drop on all 690 bar tests. The tests on the annulars to 240 bar were ok. Tested the kelly hose, kelly valves and stabbing valve to 345 bar. Ran down with the test plug and a circulating sub. Attempted to pressure test the seal assembly against closed lower pipe ram but chicksans on the drill floor were leaking. Repaired the chicksans and tested the seal assembly to 690 bar for 15 min. Continued testing the BOP to 690 bar on the rams and valves. Located the leak to be in the coflexip house on the kill side. Made up bit No. 25 and new bottom hole assembly. |
| 26/10 | 3725                      | 1.27                      | 1.40                    | Tagged the cement at 3646 m. Tested the casing to 345 bar for 15 min. Drilled the float collar, cement and float shoe. Drilled 8-3/8" hole from 3714 m to 3719 m. Ran a leak-off test, giving leak-off pressure equivalent to 2.07 rd mud. Drilled 8-3/8" hole from 3719 m to 3725 m.  |
| 27/10 | 3765                      | 1.33                      | 1.40                    | Drilled 8-3/8" hole from 3725 m to 3743 m. Pulled out of the hole for bit change. Installed the stabilizers in the string and ran in the hole with bit No. 26. Drilled 8-3/8" hole from 3725 m to 3765 m.  |



|                       |                |                        |            |    |
|-----------------------|----------------|------------------------|------------|----|
| Week<br>23/10 - 29/10 | Weeks Progress | Report no.<br>11       | Page<br>13 | of |
| Area<br>North Sea     | Well<br>15/5-2 | Rig<br>Treasure Seeker |            |    |

|        |                   |     |     |        |       |  |  |
|--------|-------------------|-----|-----|--------|-------|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 | 9-5/8 |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   | 3696  |  |  |

| Date  | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|-------|---------------------------|---------------------------|-------------------------|--|
| 28/10 | 3808                      | 1.33                      | 1.40                    | Drilled 8-3/8" hole from 3765 m to 3808 m. Pulled out of the hole for bit change. Ran bit No. 27. Had 3-3/4 hrs. rig repairing on the block retractor.           |
| 29/10 | 3865                      | 1.37                      | 1.44                    | Finished repairing the block retractor. Drilled 8-3/8" hole from 3808 m to 3825 m. Raised the mud density to 1.44 rd. Drilled 8-3/8" hole from 3825 m to 3865 m. |

|      |              |                |            |    |      |                 |    |
|------|--------------|----------------|------------|----|------|-----------------|----|
| Week | 30/10 - 5/11 | Weeks Progress | Report no. | 12 | Page | 14              | of |
| Area | North Sea    | Well           | 15/5-2     |    | Rig  | Treasure Seeker |    |

|        |                   |     |     |        |       |  |  |
|--------|-------------------|-----|-----|--------|-------|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 | 9-5/8 |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   | 3696  |  |  |

| Date  | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|-------|---------------------------|---------------------------|-------------------------|--|
| 30/10 | 3913                      | 1.39                      | 1.44                    | Drilled 8-3/8" hole from 3865 m to 3871 m. Pulled out of the hole for bit change. Drilled 8-3/8" hole from 3871 m to 3913 m.   |
| 31/10 | 3941                      | 1.39                      | 1.44                    | Drilled 8-3/8" hole from 3913 m to 3941 m. Made wiper trip to 3859 m. Pulled out of the hole for bit change. Had 6-1/4 hrs. rig repair on the block retractor.   |
| 1/11  | 4001                      | 1.40                      | 1.44                    | Drilled 8-3/8" hole from 3941 m to 3994 m. Circulated up formation sample. Drilled 8-3/8" hole from 3994 m to 4001 m.  |
| 2/11  | 4013                      | 1.45                      | 1.59                    | Drilled 8-3/8" hole from 4001 m to 4013 m. Made a flow check, no flow. Worked the pipe without pumping and circulated a full circulation. Maximum gas reading was 1020 units. Raised the mud density in steps to 1.52 rd. Was not able to obtain more than 1.48 rd. on the mud density out. Raised the mud density to 1.59 rd. |
| 3/11  | 4013                      | 1.45                      | 1.59                    | Pulled out of the hole for bit change. Retrieved the wear bushing and tested the BOP.  |
| 4/11  | 4020                      | 1.60                      | 1.63                    | Ran in the hole with the core barrel and circulated a full circulation. Had maximum gas reading on 2000 units. Raised the mud density to 1.63 rd. Cored 8-3/8" hole from 4013 m to 4020 m. Pulled out with the core barrel.  |
| 5/11  | 4030                      | 1.74                      | 1.80                    | Recovered 5 m with core. Ran in the hole with bit No. 30. Circulated and conditioned the mud. Had maximum gas reading of 1440 units. Drilled 8-3/8" hole from 4020 m to 4030 m. Had drilling break up to 20 m/hr at 4026 m. Checked for flow - well stabile. Raised the mud density in steps to 1.80 rd.                       |

|      |              |                |            |    |      |                 |    |
|------|--------------|----------------|------------|----|------|-----------------|----|
| Week | 6/11 - 12/11 | Weeks Progress | Report no. | 13 | Page | 15              | of |
| Area | North Sea    | Well           | 15/5-2     |    | Rig  | Treasure Seeker |    |

|        |                   |     |     |        |       |  |  |
|--------|-------------------|-----|-----|--------|-------|--|--|
| Casing | Size              | 30  | 20  | 13-3/8 | 9-5/8 |  |  |
|        | Setting depth (m) | 194 | 454 | 1598   | 3696  |  |  |

| Date  | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|-------|---------------------------|---------------------------|-------------------------|--|
| 6/11  | 4032                      | 1.74                      | 1.80                    | Circulated and raised the mud density to 1.80 rd. Pulled out for coring.   |
| 7/11  | 4059                      | 1.74                      | 1.82                    | Cored 8-3/8" hole from 4032 m to 4044 m. Pulled out of the hole and recovered 94%. Made up bit No. 31 and ran in the hole. Circulated and conditioned the mud, trip gas 1870 units. Drilled 8-3/8" hole from 4044 m to 4059 m. Made flow checks at 4044 m, 4053 m and 4059 m - no flow. Raised the mud density to 1.82 rd. |
| 8/11  | 4111                      | 1.74                      | 1.82                    | Drilled 8-3/8" hole from 4059 m to 4111 m.   |
| 9/11  | 4130                      | 1.74                      | 1.82                    | Drilled 8-3/8" hole from 4111 m to 4130 m. Circulated and conditioned the mud, and pulled out for bit change and logging. Rigged up Schlumberger and ran the ISF/sonic/gr log.   |
| 10/11 | 4150                      | 1.70                      | 1.82                    | Ran the FDC/CNL log. Ran in the hole with a diamond bit. Drilled 8-3/8" hole from 4129 m to 4150 m.  |
| 11/11 | 4192                      | 1.80                      | 1.90                    | Drilled 8-3/8" hole from 4150 m to 4183 m. Circulated a full circulation after drilling break at 4183 m. Maximum gas reading was 1600 units. Drilled 8-3/8" hole from 4183 m to 4185 m. Raised the mud density to 1.90 rd. Drilled 8-3/8" hole from 4185 m to 4192 m.  |
| 12/11 | 4271                      | 1.80                      | 1.90                    | Drilled 8-3/8" hole from 4192 m to 4271 m. Circulated and conditioned the mud due to high viscosity out.   |

## Weekly drilling report

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|      |               |                |            |    |      |                 |    |
|------|---------------|----------------|------------|----|------|-----------------|----|
| Week | 13/11 - 19/11 | Weeks Progress | Report no. | 14 | Page | 16              | of |
| Area | North Sea     | Well           | 15/5-2     |    | Rig  | Treasure Seeker |    |

|        |                   |     |     |         |        |  |  |
|--------|-------------------|-----|-----|---------|--------|--|--|
| Casing | Size              | 30  | 20  | 13-3/8" | 9-5/8" |  |  |
|        | Setting depth (m) | 194 | 454 | 1598    | 3696   |  |  |

| Date  | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|-------|---------------------------|---------------------------|-------------------------|--|
| 13/11 | 4271                      | 1.80                      | 1.90                    | Due to excess pump pressure across the diamond bit this was pulled out of the hole. The bit was found 100% worn. Tested the BOP.<br>Ran in with bit No. 33.  |
| 14/11 | 4322                      | 1.80                      | 1.90                    | Circulated a full circulation and drilled 8-3/8" hole from 4271 m to 4322 m. Due to heavy weather the bit was pulled into the 9-5/8" casing shoe and the string was hung off on the upper pipe ram. At 18.30 hrs. anchor chain No. 8 parted after having a tension peak up to 2669 kN.   |
| 15/11 | 4322                      | 1.80                      | 1.90                    | Waited on weather  |
| 16/11 | 4322                      | 1.80                      | 1.90                    | Waited on weather  |
| 17/11 | 4322                      | 1.80                      | 1.90                    | Waited on weather.<br>Deballasted the rig to transfer draft and managed to transfer the chain end from the rig to the supply-boat.   |
| 18/11 | 4322                      | 1.80                      | 1.90                    | Ballasted the rig to 60 ft draft. Run out and set anchor No. 8. Tensioned up to 800 kN. Ballasted the rig to 70 ft draft and connected the riser to the BOP. Checked for any pressure build-up before opening the shear ram. Retrieved the hang-off tool and ran to bottom. Circulated a full circulation. Maximum gas reading was 1650 units. Pulled out of the hole. |
| 19/11 | 4322                      | 1.80                      | 1.90                    | Ran ISF/Sonic/GR log.<br>Ran FDC/CNL/GR log. The tool was sticking between 3714 m to 3928 m and between 4306 m and 4125 m. Misrun. Ran DLL/MSFL log. The tool was sticking at 3707 m. Misrun. Ran in the hole for wiper trip.  |

|                       |                |                        |               |
|-----------------------|----------------|------------------------|---------------|
| Week<br>20/11 - 26/11 | Weeks Progress | Report no.<br>16       | Page<br>17 of |
| Area<br>North Sea     | Well<br>15/5-2 | Rig<br>Treasure Seeker |               |

| Casing | Size              | 30  | 20  | 13-3/8 | 9-5/8 |  |  |
|--------|-------------------|-----|-----|--------|-------|--|--|
|        | Setting depth (m) | 194 | 454 | 1598   | 3696  |  |  |

| Date  | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|-------|---------------------------|---------------------------|-------------------------|--|
| 20/11 | 4322                      | 1.80                      | 1.90                    | Circulated and conditioned the mud.<br>Pulled out of the hole.<br>Ran FDC/CNL log.<br>Prepared to run the velocity survey.   |
| 21/11 | 4322                      | 1.80                      | 1.90                    | Ran the velocity survey. Ran in the hole for wiper trip before running the RFT No. 1.  |
| 22/11 | 4322                      | 1.80                      | 1.90                    | Ran the RFT No. 1. The tool got stuck at 3706 m. Got free, but the tool did not function properly. Rigged up and ran the HDT log. The tool hung up several places between 4000 m and the 9-5/8" casing shoe.<br>Ran the CST No. 1 and 2.                 |
| 23/11 | 4322                      | 1.80                      | 1.90                    | Ran the CST No. 3 and 4. Ran in the hole for wiper trip.   |
| 24/11 | 4322                      | 1.80                      | 1.90                    | Conditioned the mud and pulled out of the hole.<br>Ran the RFT No. 2 and 3.  |
| 25/11 | 4322                      | 1.80                      | 1.90                    | Ran the RFT No. 4. Misrun due to blocking of the flow line to the sample chamber.<br>Ran the RFT No. 5.<br>Ran the HDT No. 2. The tool got stuck at 3724 m. Started to run in the hole, with the drill pipe while stripping over the Schlumberger cable. |
| 26/11 | 4322                      | 1.80                      | 1.90                    | Continued to run in the hole while stripping over the cable. Recovered the fish and pulled out.<br>Ran in the hole for wiper trip.<br>Circulated and conditioned the mud.  |

|      |              |                |            |    |      |                 |    |
|------|--------------|----------------|------------|----|------|-----------------|----|
| Week | 27/11 - 3/12 | Weeks Progress | Report no. | 17 | Page | 18              | o' |
| Area | North Sea    | Well           | 15/5-2     |    | Rig  | Treasure Seeker |    |

|        |                   |     |     |        |       |         |  |
|--------|-------------------|-----|-----|--------|-------|---------|--|
| Casing | Size              | 30  | 20  | 13-3/8 | 9-5/8 | 7 liner |  |
|        | Setting depth (m) | 194 | 454 | 1598   | 3696  | 4300    |  |

| Date  | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation   |
|-------|---------------------------|---------------------------|-------------------------|--|
| 27/11 | 4322                      | 1.80                      | 1.90                    | Made a short trip into the 9-5/8" casing shoe and ran to bottom again. Circulated a full circulation before pulling out. Waited 2-1/4 hrs. before a new Schlumberger cable was installed. Ran the CST No. 5.   |
| 28/11 | 4322                      | 1.80                      | 1.90                    | Ran the CST No. 6 and 7. Ran in the hole for wiper trip.   |
| 29/11 | 4322                      | 1.80                      | 1.90                    | Ran the RFT No. 6. Had installed a 2-3/4 gal and a 6 gal chamber, but the 2-3/4 gal would not open. Ran the RFT No. 7. The 6 gal chamber would not open. Ran the RFT No. 8. Recovered mud filtrate sample.   |
| 30/11 | 4322                      | 1.80                      | 1.90                    | Tested the BOP and ran in the hole for wiper trip.   |
| 1/12  | 4322                      | 1.80                      | 1.90                    | Prepared to run the 7" liner. Ran 67 joints 7" liner, 29 lbs/ft on drill pipe.   |
| 2/12  | 4322                      | 1.80                      | 1.90                    | Hung off the liner at 3494 m with the shoe at 4300 m. Started to cement the liner. After having mixed 24.4 m <sup>3</sup> out of total 31.3 m <sup>3</sup> the cement liner plugged up. Released the plug and displaced the cement. Pressured up to 138 bar when the plug landed, but the pressure bled off. Pulled out of the hole and layed down the running string. Ran down and attempted to pressure test the liner hanger to 110 bar. The pressure bled back to 89 bar. Established a injectivity rate of 0.24 m <sup>3</sup> /min at 110 bar. Spotted 5.2 m <sup>3</sup> cement on top of the liner and squeezed 2.9 m <sup>3</sup> around the liner hanger. The final squeeze pressure was 110 bar. Held 96 bar on the cement for 4 hrs. |

|                      |                |                        |            |    |
|----------------------|----------------|------------------------|------------|----|
| Week<br>27/11 - 3/12 | Weeks Progress | Report no.<br>17       | Page<br>19 | of |
| Area<br>North Sea    | Well<br>15/5-2 | Rig<br>Treasure Seeker |            |    |

|        |                   |     |     |        |       |         |  |
|--------|-------------------|-----|-----|--------|-------|---------|--|
| Casing | Size              | 30  | 20  | 13-3/8 | 9-5/8 | 7 liner |  |
|        | Setting depth (m) | 194 | 454 | 1598   | 3696  | 4300    |  |

| Date | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation  |
|------|---------------------------|---------------------------|-------------------------|---|
| 3/12 | PBTD:<br>3434 m           | 1.80                      | 1.90                    | Bled off the pressure and pulled out. Pressure tested the first cement plug on top of the liner hanger to 138 bar for 15 min. Set a 30 m balanced cement plug from 445 m to 415 m. Pulled out and ran a bridge plug on wire line down to 305 m. Pressure tested the bridge plug to 69 bar for 15 min. Retrieved the wear bushing. |

|                      |                |                        |            |    |
|----------------------|----------------|------------------------|------------|----|
| Week<br>4/12 - 10/12 | Weeks Progress | Report no.<br>18       | Page<br>20 | of |
| Area<br>North Sea    | Well<br>15/5-2 | Rig<br>Treasure Seeker |            |    |

|        |                   |     |     |        |       |         |  |
|--------|-------------------|-----|-----|--------|-------|---------|--|
| Casing | Size              | 30  | 25  | 13-3/8 | 9-5/8 | 7 liner |  |
|        | Setting depth (m) | 194 | 454 | 1598   | 3696  | 4300    |  |

| Date | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation  |
|------|---------------------------|---------------------------|-------------------------|---|
| 4/12 | PBTD:<br>305              | 1.80                      | 1.90                    | Prepared to pull the riser and BOP. Waited on weather from 02:30 hrs. Disconnected the riser due to one broken tension wire.  |
| 5/12 | PBTD:<br>305              | 1.80                      | 1.90                    | Waited on weather to 19.00 hrs. Connected the riser to the BOP and pulled the BOP and the riser.  |
| 6/12 | PBTD:<br>305              | 1.80                      | 1.90                    | Finished pulling the BOP and prepared to run the corrosion cap. Had to modify the running tool. Ran the corrosion cap and cut guide lines No. 2, 3 and 4 by using the hydraulic cutter. The knife broke and the divers had to be used to cut guide line No. 1. Deballasted the rig to 60 ft. draft. Retrieved the piggy-back anchor No. 1 and 3. Had to shut down operation due to the weather. |
| 7/12 | -                         | -                         | -                       | Waited on weather   |
| 8/12 | -                         | -                         | -                       | Waited on weather   |
| 9/12 | -                         | -                         | -                       | Waited on weather   |
| 10/2 | -                         | -                         | -                       | Pulled anchor No. 2, 7 and the piggy-back anchor No.5. Attempted to retrieve piggy-back No. 7, but the pennant line broke and the anchor was lost overboard. Waited on weather.   |



|      |               |                |            |    |      |                 |    |  |
|------|---------------|----------------|------------|----|------|-----------------|----|--|
| Week | 11/12 - 17/12 | Weeks Progress | Report no. | 19 | Page | 21              | of |  |
| Area | North Sea     | Well           | 15/5-2     |    | Rig  | Treasure Seeker |    |  |

|        |                   |     |     |        |       |         |  |
|--------|-------------------|-----|-----|--------|-------|---------|--|
| Casing | Size              | 30  | 20  | 13-3/8 | 9-5/8 | 7 Liner |  |
|        | Setting depth (m) | 194 | 454 | 1598   | 3696  | 4300    |  |

| Date  | Depth (m)<br>Progress (m) | Pore Press<br>grad (r.d.) | Mud Dens<br>grad (r.d.) | Detailed operation  |
|-------|---------------------------|---------------------------|-------------------------|---|
| 11/12 | -                         | -                         | -                       | Waited on weather   |
| 12/12 | -                         | -                         | -                       | Waited on weather   |
| 13/12 | -                         | -                         | -                       | Waited on weather   |
| 14/12 | -                         | -                         | -                       | Waited on weather   |
| 15/12 | -                         | -                         | -                       | Waited on weather for 4 hours.<br>Deballasted the rig and started to pull the anchors. Anchor chain No. 4 broke on the wildcat and shortly after the tail chain on the anchor broke and the anchor was dropped.<br>Managed to retrieve anchor No. 4 after 2 hrs. grappling. Continued picking up the remaining anchors. |
| 16/12 | -                         | -                         | -                       | Last anchor was bolstered at 02.30 hrs.   |

### 3.3 Time Distribution

The total time used to move the rig to the location, to drill and temporary plug and abandon the well 15/5-2 was 122.8 days. The time distribution is shown in Table A.1 and Fig. A.2.

The operation can be divided into five main groups:

1. Underway and position the rig; 1,7 days
2. Drilling of the well to TD; 98,5 days
3. Final logging; 11,0 days
4. Plug and abandon the well; 1,6 days
5. Waiting on weather before moving; 10 days

A total of 7,3 days were lost when the pipe got stuck at 1930 m and the hole had to be sidetracked.

2 days were lost due to waiting on weather on September 17 and 18.

Close to two days were lost due to the fishing for the two cones that were lost in the hole.

4,5 days were lost due to waiting on weather from November 15 to 18.

The long time spent on the final logging was caused by several factors:

- a. Malfunctions of the RFT-tool
- b. Several attempts to obtain formation fluid sample.
- c. Malfunctions of the CST gun
- d. Stuck HDT. Had to fish the tool out by stripping over the cable.

A total of 10 days were lost waiting on weather after the well was plugged prior to any anchor handling could take place.

TABLE A.1  
TIME DISTRIBUTION

| OPERATION                                      | HOURS  | PERCENTAGE<br>OF TOTAL TIME |
|--|--------|-----------------------------|
| 1. Under way                                   | 8      | 0,3                         |
| 2. Positioning and mooring                     | 32,75  | 1,1                         |
| 3. Drilling                                    | 814,5  | 27,6                        |
| 4. Tripping                                    | 262,5  | 9,0                         |
| 5. Surveying                                   | 42     | 1,4                         |
| 6. Circ. and conditioning the mud              | 71,5   | 2,4                         |
| 7. Reaming                                     | 25     | 0,9                         |
| 8. Slipping and cutting the drlg. line         | 20,75  | 0,7                         |
| 9. Subsea equipment handling                   | 30,5   | 1,0                         |
| 10. Testing of equipment                       | 102,5  | 3,5                         |
| 11. Running and cementing casing               | 236,75 | 8,0                         |
| 12. Formation evaluation                       |        |                             |
| a. Logging, leak-off tests<br>circ. bottoms up | 385,5  | 13,1                        |
| b. Coring                                      | 51,25  | 1,7                         |
| 13. Lost time drlg. equipment                  | 63,25  | 2,2                         |
| 14. Lost time subsea equipment                 | 12,25  | 0,4                         |
| 15. Lost time fishing                          | 148,25 | 5,0                         |
| 16. Lost time hole problems                    | 159,5  | 5,4                         |
| 17. Lost time mooring                          | 11,25  | 0,4                         |
| 18. Lost time waiting on weather               | 395,5  | 13,4                        |
| 19. Lost time waiting on equipment             | 2      | 0,1                         |
| 20. Plugging and abandonment                   | 38     | 1,3                         |
| 21. Misc.                                      | 33,5   | 1,1                         |
| SUM TOTAL                                      | 2947   | 100%                        |
| = 122,8 days                                   |        |                             |

TABLE A.2

HOLE DEVIATION - 15/5-2

| Depth<br>(m)        | Inclination<br>(degrees) | Direction<br>(degrees) |
|---------------------|--------------------------|------------------------|
| 194.5               | 1.50                     | -                      |
| 297                 | 0.50                     | 310                    |
| 402                 | 0.25                     | 200                    |
| 469                 | 0.25                     | 212                    |
| 560                 | 0.13                     | 115                    |
| 722                 | 0.25                     | 310                    |
| 815                 | 0.13                     | 290                    |
| 919                 | 0.50                     | 355                    |
| 1007                | 0.13                     | 315                    |
| 1101                | 0.13                     | 263                    |
| 1195                | 0.63                     | 48                     |
| 1284                | 0.25                     | 65                     |
| 1390                | 0.25                     | 80                     |
| 1495                | 0.25                     | 160                    |
| 1600                | 0.75                     | 5                      |
| 1697                | 1.00                     | 124                    |
| 1802                | 0.75                     | 30                     |
| 1884                | 1.00                     | 15                     |
| 1983                | 1.00                     | 335                    |
| 2069                | 0.75                     | 315                    |
| 2154                | 0.75                     | 0                      |
| 2260                | 1.00                     | 0                      |
| 1796 (1. sidetrack) | 1.38                     | 20                     |
| 1815 ( " )          | 1.75                     | 10                     |
| 1834 ( " )          | 2.00                     | 9                      |
| 1800 (2. sidetrack) | 2.50                     | 102                    |
| 1819 ( " )          | 4.75                     | 110                    |

TABLE A.2 Cont.

| Depth<br>(m) |                | Inclination<br>(degrees) | Direction<br>(degrees) |
|--------------|----------------|--------------------------|------------------------|
| 1828         | (2. sidetrack) | 5.75                     | 111                    |
| 1859         | ( " )          | 5.00                     | 107                    |
| 1888         | ( " )          | 4.25                     | 107                    |
| 1917         | ( " )          | 4.00                     | 113                    |
| 1945         | ( " )          | 3.50                     | 119                    |
| 1973         | ( " )          | 2.75                     | 122                    |
| 2031         | ( " )          | 2.75                     | 144                    |
| 2127         | ( " )          | 1.75                     | 135                    |
| 2232         | ( " )          | 1.25                     | 185                    |
| 2326         |                | 0.75                     | 200                    |
| 2432         |                | 1.13                     | 190                    |
| 2488         |                | 1.00                     | 180                    |
| 2639         |                | 0.75                     | 175                    |
| 2731         |                | 0.50                     | 143                    |
| 2826         |                | 1.25                     | 228                    |
| 2929         |                | 1.00                     | 225                    |
| 3076         |                | 1.25                     | 203                    |
| 3256         |                | 2.50                     | 186                    |
| 3333         |                | 2.50                     | 200                    |
| 3425         |                | 2.00                     | 190                    |
| 3486         |                | 2.25                     | 196                    |
| 3712         |                | 2.50                     | 195                    |
| 4130         |                | 1.75                     | 195                    |

4. TEMPORARY ABANDONMENT OF THE WELL

The approved abandonment program is shown in Fig. A-3 and it was carried out as follows:

1. A 60 m cement plug from 3494 m to 3434 m was set on top of the liner hanger.
2. A 30 m cement plug was set from 445 m to 415 m.
3. A bridge plug was set at 305 m.
4. A corrosion cap was mounted on the wellhead.
5. The wellhead location was marked with 3 buoys shown in Fig. A-4.

Due to the temporary abandonment, no inspection of the sea bed was done prior to abandoning the well.

The following items are reported lost on 15/5-2 Phase I.

1. Drain pipe from shaker and shaker tank 16 m long, OD = 24". Direction:  $360^{\circ}$ , 15 m from the wellhead.
2. One 15 ton piggy-back anchor with 2 x 152 m pennant lines. Direction:  $216^{\circ}$ , 914 m from the wellhead.
3. Crane wire, 129 m, OD = 38 mm. Direction:  $180^{\circ}$ , 40 m from the wellhead.

## 5. PORE PRESSURE AND FORMATION INTEGRITY

### 5.1 Pore Pressure

The pore pressure detection started at appr. 2000 m and was performed to total depth of 4313 m. Drilling parameters and electric logs were used in this work. The results are given in the following table.

| <u>Depth</u> | <u>dc-exp.</u> | <u>Sonic log</u> | <u>Predicted</u> |
|--------------|----------------|------------------|------------------|
| 2600         | 1.07           | 1.07             | 1.07             |
| 2690         | 1.18           | "                | "                |
| 2700         | "              | "                | "                |
| 2800         | "              | "                | 1.15             |
| 2900         | "              | "                | "                |
| 2980         | "              | 1.23             | "                |
| 3000         | "              | "                | "                |
| 3100         | "              | "                | "                |
| 3200         | "              | "                | "                |
| 3250         | "              | 1.31             | "                |
| 3300         | "              | "                | "                |
| 3350         | "              | 1.42             | "                |
| 3400         | "              | "                | "                |
| 3425         | 1.22           | "                | "                |
| 3500         | "              | "                | "                |
| 3520         | "              | 1.44             | "                |
| 3600         | "              | "                | "                |

| <u>Depth</u> | <u>dc-exp.</u> | <u>Sonic log</u> | <u>Predicted</u> |
|--------------|----------------|------------------|------------------|
| 3700         | 1.27           | 1.60             | 1.20             |
| 3760         | 1.43 *         | "                | 1.25             |
| 3800         | " *            | "                | 1.27             |
| 3820         | 1.43 *         | 1.80             | 1.29             |
| 3900         | " *            | "                | 1.38             |
| 3960         | 1.57           | "                | 1.43             |
| 4000         |                | "                | 1.50             |
| 4050         |                | 1.75             | 1.57             |

\*) Calculated after the well was drilled.

The result from RFT taken at 4049 m showed a pressure of 1.77 rd.

## 5.2 Formation Integrity

The following table shows the formation integrity tests .

|               |   |          |         |
|---------------|---|----------|---------|
| 20" csg.      | : | 454 m ,  | 1.47 rd |
| 13 3/8" csg.: |   | 1598 m , | 1.68 rd |
| 9 5/8" csg.:  |   | 3696 m , | 2.07 rd |



## 6. MATERIALS REPORT

### 6.1 Casing and Wellhead

A Vetco SG-5 1000 bar wellhead system was used. This would made it possible to use the 1000 bar BOP stack if higher formation pressures were encountered.

The 36" hole was spudded and drilled without any guidance system. The 30" casing was run with the 30" wellhead housing locked into the permanent guide structure. The extended posts would have facilitated guidance if the 1000 bar BOP stack had to be used.

The riser was run prior to drilling of the 17½" pilot hole and underreaming to 26" hole. The 20" casing was run with the 18-3/4" wellhead housing and landed in the 30" wellhead.

The 17½" hole was drilled with the 690 bar BOP stack installed. The 13-3/8" casing was run, landed in the 18-3/4" housing and cemented.

The 12-1/4" hole was drilled and the 9-5/8" casing was run, and cemented.

The 8-3/8" hole was drilled to TD at 4322 m. The 7" liner was run and hung off inside the 9-5/8" casing by using a Brown Oil Tool hydraulic liner hanger.

The well was temporary plugged and abandoned.

The following types of casing were run:

| Size     | Grade | Weight<br>lbs/ft | Length<br>m | Threads  | Setting depth<br>m |
|----------|-------|------------------|-------------|----------|--------------------|
| 30"      | B     | 310              | 38.1        | S.J.     |                    |
|          | B     | 457              | 13.5        | S.J.     | 194                |
| 20"      | K-55  | 133              | 286.2       | But.     |                    |
|          | K-55  | 133              | 12.3        | But/Lx   |                    |
|          | K-55  | 133              | 13.1        | Vetco/Lx | 454                |
| 13-3/8"  | K-55  | 68               | 34.4        | But.     |                    |
|          | N-80  | 72               | 1420.8      | But.     | 1598               |
| 9-5/8"   | N-80  | 47               | 514.4       | But.     |                    |
|          | P-110 | 47               | 1838.9      | But.     |                    |
|          | P-110 | 53.5             | 1200.3      | VAM      | 3696               |
| 7" liner | N-80  | 29               | 798.8       | But.     | 4300 m             |

6.2 Drill Bit Record

| Size    | Amount | IADC Code    |
|---------|--------|--------------|
| 26"     | 1      | 111          |
| 17½"    | 2      | 111          |
|         | 1      | 124          |
| 12-1/4" | 1      | 114          |
|         | 11     | 135          |
|         | 4      | 215          |
|         | 1      | 527          |
|         | 1      | 517          |
|         | 1      | 325          |
|         | 1      | LX16 diamond |
| 8-3/8"  | 3      | 134          |
|         | 2      | 135          |
|         | 1      | 136          |
|         | 1      | 214          |
|         | 2      | 527          |
|         | 1      | Core head    |
|         | 1      | S-IR diamond |

TABLE A.3

## BIT RECORD

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|   |  |             |  |                      |  |                                |  |              |  |            |  |          |  |                 |  |
|---|--|-------------|--|----------------------|--|--------------------------------|--|--------------|--|------------|--|----------|--|-----------------|--|
| COUNTY<br><b>NORWAY</b>                 |  | FIELD       |  | STATE                |  | SECTION                        |  | TOWNSHIP     |  | RANGE      |  | LOCATION |  | WELL NO.        |  |
| CONTRACTOR<br><b>WILHELM WILHELMSEN</b> |  |             |  | RIG NO.<br><b>TS</b> |  | OPERATOR<br><b>NORSK HYDRO</b> |  |              |  | TOOLPUSHER |  |          |  | SALESMAN        |  |
| SPUD                                    |  | UNDER SURF. |  | UNDER INTER.         |  | SET SAND ST.                   |  | REACHED T.D. |  | PUMP NO. 1 |  | LINER    |  | PUMP NO. 2      |  |
| DRILL PIPE                              |  | TOOL JOINTS |  | SIZE                 |  | TYPE                           |  | O.D.         |  | NUMBER     |  | O.D.     |  | I.D.            |  |
|   |  |             |  |                      |  |                                |  |              |  |            |  |          |  | LENGTH          |  |
|   |  |             |  |                      |  |                                |  |              |  |            |  |          |  | DRAWWORKS POWER |  |

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| NO. | SIZE           | MAKE           | TYPE                     | JET 32ND IN      | SERIAL | DEPTH OUT (M) | (H)   | HOURS  | m/hr | ACCUM. DRILL. MTS. | WT. 1000 N | R P M  | VERT. DEV. | PUMP PRESS. BAR | PUMP OPERATION | S P M |     | MUD  |      |      | DULL. COND. |   |       |       | FORMATION REMARKS |
|-----|----------------|----------------|--------------------------|------------------|--------|---------------|-------|--------|------|--------------------|------------|--------|------------|-----------------|----------------|-------|-----|------|------|------|-------------|---|-------|-------|-------------------|
|     |                |                |                          |                  |        |               |       |        |      |                    |            |        |            |                 |                | 1     | 2   | WT.  | VIS. | W.L. | 7           | 8 | 9     | OTHER |                   |
| 1   | 26"/36"        | HUGHES SERVO   | OSC - 3AJ                | 3 x 22           |        | 194.5         | 49    | 13     | 3.77 | 13                 | 75         | 60     | 1 1/2      | 40              | P 7"           | 80    | 80  | 1.08 | 12   | -    | 2           | 2 | 1     |       |                   |
| 1   | RERUN          | FOR REAMING    |                          |                  |        |               |       |        |      |                    |            |        |            |                 |                |       |     |      |      |      |             |   |       |       |                   |
| 2   | 17 1/2"        | REED           | Y 11 J                   | 3 x 20           |        | 469           | 274.5 | 10 3/4 | 25.5 | 23 3/4             | 44         | 150    |            | 138             | P 7"           | 90    | 90  | 1.14 | 6    | -    | 1           | 2 | 1     |       |                   |
| 2   | RERUN          | FOR REAMING    |                          |                  |        |               |       |        |      |                    |            |        |            |                 |                |       |     |      |      |      |             |   |       |       |                   |
|     | 26"            | SERVO          | UNDERREAMING             |                  |        |               |       |        |      |                    |            |        |            |                 |                |       |     |      |      |      |             |   |       |       |                   |
| 1   | RERUN          | CIRCULATING    |                          |                  |        |               |       |        |      |                    |            |        |            |                 |                |       |     |      |      |      |             |   |       |       |                   |
| 3   | 17 1/2"        | SMITH          | DSJ                      | 3 x 18           |        | 1267          | 834   | 40.5   | 20.6 | 64 1/4             | 100        | 100/50 |            | 190             | P 7"           | 100   | 100 | 1.06 | 4-8  | -    | 6           | 4 | 1     |       |                   |
| 4   | 17 1/2"        | SMITH          | SDT                      | 3 x 18           | WA 799 | 1615          | 348   | 38 3/4 | 9    | 103                | 220        | 150    | 1/4        | 220             | P 7"           | 86    | 86  | 1.16 |      |      | 4           | 2 | 1     |       |                   |
| RRV | FOR COND. HOLE | FOR LOG        |                          |                  |        |               |       |        |      |                    |            |        |            |                 |                |       |     |      |      |      |             |   |       |       |                   |
| RRV | FOR COND. HOLE | FOR 13 3/8 CSG |                          |                  |        |               |       |        |      |                    |            |        |            |                 |                |       |     |      |      |      |             |   |       |       |                   |
| 5   | 12 1/4         | SMITH          | SDGH                     | 1 x 14<br>2 x 15 | WC 607 | 1802          | 187   | 13 3/4 | 13.6 | 126.7              | 60         | 50/150 |            | 207             | P 7"           | 60    | 60  | 1.20 |      |      | 4           | 4 | 1     |       | CMT. CLAY         |
| 6   | 12 1/4         | SMITH          | SDS EN-CJ                | 4 x 12           | WA 843 | 1884          | 82    | 4      | 20.5 | 130.7              | 110        | 178    |            | 206             | P 7"           | 55    | 55  | 1.20 |      |      | 5           | 2 | 1     |       |                   |
| 7   | 12 1/4         | SMITH          | SDGH                     | 1 x 14<br>2 x 15 | WC 585 | 1993          | 19    | 3 1/2  | 5.4  | 134 1/2            | 120        | 25/200 |            | 210             | P 7"           | 60    | 60  | 1.20 |      |      | 1           | 2 | 1/8   |       |                   |
| 8   | 12 1/4         | SMITH          | SDGH                     | 1 x 14<br>2 x 15 | VP 113 | 2293          | 390   | 31 1/4 | 12.5 | 165 1/2            | 178        | 110    | 1°         | 193             | P 7"           | 55    | 55  | 1.20 |      |      | -           | - | -     |       | LOST IN HOLE      |
|     |                |                | PLUGGED BACK W/CEMENT TO |                  |        | 1775 M        |       |        |      |                    |            |        |            |                 |                |       |     |      |      |      |             |   |       |       |                   |
| 9   | 12 1/4         | SMITH          | SDGH                     | 3 x 15           | WC 605 | 1840          | 65    | 2 3/4  | 23.6 | 168 1/4            | 110        | 50     |            | 140/80          | S 7"           | 100   | 60  | 1.20 |      |      | 1           | 1 | 1     |       |                   |
|     |                |                | PLUGGED BACK W/CEMENT TO |                  |        | 1781 M        |       |        |      |                    |            |        |            |                 |                |       |     |      |      |      |             |   |       |       |                   |
| 10  | 12 1/4         | SMITH          | SDGH                     | 3 x 15<br>1 x 14 | VM 658 | 1829          | 48    | 6 1/4  | 7.7  | 174 1/2            | 160        | 100    |            | 90              | S 7"           | 70    |     | 1.22 |      |      | 1           | 1 | 1     |       |                   |
| 11  | 12 1/4         | SMITH          | SDGH                     | 2 x 15<br>2 x 14 | WB 851 | 2232          | 403   | 40 3/4 | 9.9  | 215 1/4            | 150        | 130    |            | 188/207         | P 7"           | 53    | 53  | 1.2  |      |      | 6           | 6 | 1/8   |       |                   |
| 12  | 12 1/4         | SMITH          | SDGH                     | 1 x 13<br>2 x 14 | VM 692 | 2355          | 123   | 9      | 13.7 | 224 1/4            | 133        | 110    |            | 214             | P 7"           | 51    | 51  | 1.26 |      |      | 6           | 7 | 0 1/8 |       |                   |
| 13  | 12 1/4         | SMITH          | SDGH                     | 1 x 13<br>2 x 14 | VM 915 | 2488          | 133   | 17 3/4 | 7.5  | 242 1/2            | 177        | 115    |            | 210             | P 7"           | 51    | 51  | 1.26 |      |      | 8           | 6 | 1/8   |       |                   |
| 14  | 12 1/4         | SMITH          | SDGH                     | 2 x 14<br>1 x 13 | VN 022 | 2639          | 151   | 12 1/2 | 12.1 | 254 1/2            | 150        | 120    |            | 214             | P 7"           | 50    | 50  | 1.26 |      |      | 7           | 5 | 1/8   |       |                   |



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## BIT RECORD

Table A.3 cont.

| COUNTY           |        | FIELD         |         | STATE            |          | SECTION       |     | TOWNSHIP     |      | RANGE              |           | LOCATION |            | WELL NO.       |                  |              |              |            |      |                 |        |             |   |       |                           |                   |
|------------------|--------|---------------|---------|------------------|----------|---------------|-----|--------------|------|--------------------|-----------|----------|------------|----------------|------------------|--------------|--------------|------------|------|-----------------|--------|-------------|---|-------|---------------------------|-------------------|
| NORWAY           |        |               |         |                  |          |               |     |              |      |                    |           |          |            | 15/5 - 2       |                  |              |              |            |      |                 |        |             |   |       |                           |                   |
| CONTRACTOR       |        |               |         | RIG NO.          |          | OPERATOR      |     |              |      | TOOLPUSHER         |           |          |            | SALESMAN       |                  |              |              |            |      |                 |        |             |   |       |                           |                   |
| WILH. WILHELMSEN |        |               |         | TS               |          | NORSK HYDRO   |     |              |      |                    |           |          |            |                |                  |              |              |            |      |                 |        |             |   |       |                           |                   |
| SPUD             |        | UNDER SURF.   |         | UNDER INTER.     |          | SET SAND ST.  |     | REACHED T.D. |      | PUMP NO. 1         |           | LINER    |            | PUMP NO. 2     |                  | LINER        |              | PUMP POWER |      | TYPE MUD        |        |             |   |       |                           |                   |
| DRILL PIPE       |        | TOOL JOINTS   |         | SIZE             |          | TYPE          |     | O.D.         |      | DRILL COLLARS      |           | NUMBER   |            | O.D.           |                  | I.D.         |              | LENGTH     |      | DRAWWORKS POWER |        |             |   |       |                           |                   |
| NO               | SIZE   | MAKE          | TYPE    | JET SEND IN      | SERIAL   | DEPTH OUT (M) | (M) | HOURS        | M/HR | ACCUM. DRILL. HRS. | WT 1000 N | R P M    | VERT. DEV. | PUMP PRESS BAR | PUMP OPER. ATION | S P M        |              |            | MUD  |                 |        | DULL. COND. |   |       |                           | FORMATION REMARKS |
|                  |        |               |         |                  |          |               |     |              |      |                    |           |          |            |                |                  | 1            | 2            | WT         | VIS. | W.L.            | T      | B           | G | OTHER |                           |                   |
| 15               | 12 1/4 | HUGHES        | XDV     | 1 x 13<br>2 x 14 | 596 RK   | 2731          | 92  | 19 1/4       | 4.8  | 273<br>3/4         | 220       | 100      |            | 214            | P-7"             | 50<br>58     | 50<br>57     | 1.26       |      |                 | 5      | 5           | 1 |       | MARL/LIMESTONE            |                   |
| 16               | 12 1/4 | SMITH         | SDGH    | 1 x 13<br>2 x 14 | VN 766   | 2826          | 95  | 24           | 4.0  | 297<br>3/4         | 155       | 120      |            | 214            | P                | 7"<br>7"     | 6"<br>6"     | 1.26       |      |                 | 3      | 6           | 1 |       | LIMESTONE                 |                   |
| 17               | 12 1/4 | DIAMANT BOART | LX 16   | -                | 7600206  | 3359          | 533 | 172          | 3.1  | 469<br>3/4         | 200       | 750      |            | 290            | P                | 75<br>6"     | 75<br>6"     | 1.27       |      |                 | CRACKS |             |   |       | LIMESTONE/MARL            |                   |
| 18               | 12 1/4 | HUGHES        | J 22    | 1 x 12<br>2 x 13 | CH 439   | 3425          | 66  | 38 1/2       | 1.7  | 508<br>1/4         | 245       | 58       |            | 220            | P                | 56<br>6 1/2" | 56<br>6 1/2" | 1.30       |      |                 | 1      | 3           | 1 |       | LIME / MARL               |                   |
| 19               | 12 1/4 | SMITH         | SDGH    | 1 x 12<br>2 x 13 | WC 539   | 3486          | 61  | 25 3/4       | 2.4  | 534<br>1/2         | 245       | 120      |            | 220            | P                | 55<br>6 1/2" | 55<br>6 1/2" | 1.30       |      |                 | 6      | 4           | 1 |       | BROKEN TEETH              |                   |
| 20               | 12 1/4 | HUGHES        | XDV     | 1 x 12<br>2 x 13 | RK 594   | 3504          | 18  | 9 1/2        | 1.9  | 543<br>1/2         | 245       | 80/90    |            | 220            | P 6 1/2"         | 56           | 56           | 1.30       |      |                 | 6      | 7           | 1 |       | "                         |                   |
| 21               | 12 1/4 | HUGHES        | XDV     | 1 x 12<br>2 x 13 | RK 593   | 3606          | 102 | 43           | 2.4  | 596<br>1/2         | 245       | 100      |            | 220            | P 6 1/2"         | 53           | 53           | 1.30       |      |                 | 4      | 8           | 1 |       | "                         |                   |
| 22               | 12 1/4 | SMITH         | A-1     | 1 x 10<br>2 x 13 | 612 SB   | 3712          | 106 | 50 1/4       | 2.1  | 636<br>3/4         |           | 70/90    |            | 227            | P 6 1/2"         | 55           | 55           | 1.30       |      |                 | 8      | 8           | 1 |       | NOZZLES OUT.              |                   |
| 23               | 12 1/4 | HUGHES        | XDR     | 3 x 13           | Q 7056   | 3712          | 0   | 3            | 0    | 636<br>3/4         | 22        | 50       |            | 130            | P 6 1/2"         | 53           | 53           | 1.34       |      |                 | 6      | 2           | 1 |       | CONES OFF MARL/LIMESTONE  |                   |
| 24               | 12 1/4 | HUGHES        | XDV     | 3 x 13<br>2 x 10 | 116 RK   | 3714          | 2   | 1/2          | 4    | 637<br>1/4         | 45        | 50       |            | 130            | P 6 1/2"         | 53           | 53           | 1.34       |      |                 | 1      | 1           | 1 |       | DRILL. JUNK.              |                   |
| 25               | 8 3/8  | SMITH         | SDG     | 1 x 11<br>2 x 10 | 723 FR   | 3743          | 29  | 10 1/2       | 2.8  | 647<br>3/4         | 180       | 85       |            | 170            | S 6 1/2"         | 65           |              | 1.40       |      |                 | 7      | 8           | 1 |       | DRILL. CMT FLOATS, SHALE  |                   |
| 26               | 8 3/8  | SMITH         | SV      | 1 x 11<br>2 x 10 | 958 FT   | 3808          | 65  | 18           | 3.6  | 665<br>3/4         | 151       | 80       |            | 208            | S 6 1/2"         | 65           |              | 1.40       |      |                 | 5      | 7           | 1 |       | SH./LIMIE                 |                   |
| 27               | 8 3/8  | SMITH         | SDG     | 1 x 11<br>2 x 10 | 897 FR   | 3871          | 63  | 20 1/4       | 3.1  | 686<br>3/4         | 133       | 80       |            | 208            | S 6 1/2"         | 68           |              | 1.44       |      |                 | 7      | 8           | 1 |       | SH./LIMIE                 |                   |
| 28               | 8 3/8  | HTC           | J 3     | 1 x 11<br>2 x 10 | JA 70 II | 3941          | 70  | 21 3/4       | 3.2  | 707<br>3/4         | 133       | 80       |            | 208            | S 6 1/2"         | 68           |              | 1.44       |      |                 | 6      | 3           | 1 |       | SH./DOLE                  |                   |
| 29               | 8 3/8  | SMITH         | SDG     | 1 x 11<br>2 x 10 | 389 RR   | 4013          | 72  | 21 1/2       | 3.3  | 729<br>1/4         | 132       | 80       |            | 200            | S 6 1/2"         | 68           |              | 1.44       |      |                 | 6      | 8           | 1 | BT    | SH./SD./COAL              |                   |
| CB 1             | 8 3/8  | HYC           | CMH 1-P | -                | 17078    | 4020          | 7   | 3 1/2        | 2.0  | 732<br>3/4         | 124       | 100      |            | 124<br>137     | S 6 1/2"         | 60           |              | 1.63       |      |                 | 3      | 0           | 0 |       | SH./COAL                  |                   |
| 30               | 8 3/8  | SMITH         | SDGH    | 1 x 11           | 351 RS   | 4032          | 12  | 2 3/4        | 4.4  | 735<br>1/2         | 135       | 80       |            | 230            | S 6 1/2"         | 53           |              | 1.80       |      |                 | 1      | 1           | 1 |       | SH./COAL/SAND             |                   |
| CB 1 RR          | 8 3/8  | HYC           | CMH 1-P | -                | 17078    | 4044          | 12  | 4 3/4        | 2.5  | 740<br>1/4         | 125       | 80       |            | 145            | S 6 1/2"         | 59           |              | 1.82       |      |                 | 20     | 0           | 0 |       | SH./SD./SLST.             |                   |
| 31               | 8 3/8  | SMITH         | F 2     | 3 x 12           | 415 PR   | 4130          | 86  | 40           | 2.2  | 780<br>1/4         | 132       | 50/70    |            | 220            | S 6 1/2"         | 73           |              | 1.82       |      |                 | 2      | 4           | 1 |       | SH./SD./SLST.             |                   |
| 32               | 8 3/8  | HYC           | S-1R    | -                | 17029    | 4271          | 141 | 39 3/4       | 3.5  | 820<br>1/4         | 110<br>66 | 150      |            | 220            | S 6 1/2"         | 68           |              | 1.90       |      |                 | 100    | 0           | 0 |       | SHOWS OF PYR SST/MAR/SLST |                   |
| 33               | 8 3/8  | SMITH         | F-2     | 3 x 12           | 368 PR   | 4322          | 51  | 9 1/2        | 5.4  | 829<br>1/4         | 90        | 50/60    |            | 205            | S 6 1/2"         |              |              |            |      |                 | 1      | 2           | 1 |       | SST POOH TO LOC           |                   |
| 34               | 8 3/8  | SMITH         | SDGH    | -                | 628 PC   | WIPER TRIP    |     |              |      |                    |           |          |            |                |                  |              |              |            |      |                 |        |             |   |       |                           |                   |

### 6.3 Bottom Hole Assemblies

| Bit No. | Bit size       | Bottom Hole Assembly  |
|---------|----------------|---|
| 1       | 26"            | bit - 36" hole opener - 1 x 9½" monel - 8-9½" DC - XO - 3 x HWDP                                    |
| 2       | 17 1/2"        | bit - bit sub - 1 x 9½" monel - 8 x 9½" DC - XO - 15 x HWDP   |
| RR2     | 17 1/2"        | bit - 26" UR - bit sub - 1 x 9½" monel - 8 x 9½" DC - XO - 15 HWDP                                  |
| 3       | 17 1/2"        | bit - bit sub - 1 x 9½" monel - 14 x 9½" DC - XO - 15 HWDP  |
| 4       | 17 1/2"        | bit - NB stab - 1 x 9½" monel - stab.- 2 x 9½" DC - stab - 12 x 9½" DC - XO - 15 HWDP               |
| 5       | 12 1/4"        | bit - bit sub - 1 x 8" monel - 20 x 8" DC - XO - 15 HWDP  |
| 6       | 12 1/4"        | bit - NB stab - 1 x 8" monel - stab - 2 x 8" DC - stab - 3 x 8" DC stab.- 15 x 8" DC - XO - 15 HWDP |
| 7       | 12 1/4"        | As bit no. 6  |
| 8       | 12 1/4"        | bit - junk sub - bit sub - 1 x 8" monel - stab - 2 x 8" DC - stab - 3 x 8" DC - stab - XO - 15 HWDP |
|         | Fishing string | XO - jar - 11 x 8" DC - 1 x bumper sub - XO - 15 HWDP   |
| 9       | 12 1/4"        | bit - bit sub - XO - 1 x 6½" monel - 5 x 6½" DC - XO - stab - 9 x 8" DC - XO - 15 HWDP              |
| 10      | 12 1/4"        | Bit - NB stab - XO - 1 x 6½" monel - 5 x 6½" DC - XO - XO - 9 x 8" DC - XO - 15 HWDP                |

| Bit No. | Bit size | Bottom Hole Assembly  |
|---------|----------|---|
| 11      | 12 1/4"  | bit - bit sub - 1 x 8" monel - stab - 1 x 8" DC - stab - 3 x 8" DC - slip on centr. - 7 x 8" DC - jar - 3 x 8" DC - XO - 15 HWDP              |
| 12      | 12 1/4"  | bit - NB stab - 1 x 8" monel - stab - 2 x 8" DC - 3 x 8" DC - slip on centr. - 9 x 8" DC - jar - 3 x 8" DC - XD - 15 HWDP                     |
| 13      | 12 1/4"  | As bit no. 12   |
| 14      | 12 1/4"  | As bit no. 12   |
| 15      | 12 1/4"  | As bit no. 12   |
| 16      | 12 1/4"  | bit - junk sub - bit sub - 1 x 8" monel - stab - 2 x 8" DC - stab - 3 x 8" DC - slip on centr. - 9 x 8" DC - jar - 3 x 8" DC - XO - 15 HWDP   |
| 17      | 12 1/4"  | bit - turbine - XO - stab - 1 x 8" monel - stab - 2 x 8" DC - stab - 3 x 8" DC - slip on centr. - 12 x 8" DC - jar - 3 x 8" DC - XO - 15 HWDP |
| 18      | 12 1/4"  | bit - NB stab. - 1 x 8" monel - stab. - 2 x 8" DC - stab. - 3 x 8" DC - slip on centr. - 12 x 8" DC - jar - 3 x 8" DC - XD - 15 HWDP          |
| 19      | 12 1/4"  | As bit no. 18   |
| 20      | 12 1/4"  | As bit no. 18   |
| 21      | 12 1/4"  | As bit no. 18   |

| Bit No. | Bit Size       | Bottom Hole Assembly   |
|---------|----------------|--|
| 22      | 12 1/4"        | bit - NB stab - 1 x 8" monel - stab - 2 x 8" DC - stab - 3 x 8" DC - stab - 12 x 8" DC - jar - 3 x 8"DC - XO - 15 HWDP                             |
|         | Fishing string | Magnet - junk sub - NB stab - 1 x 8" monel - stab - 2 x 8" DC - stab - 3 x 8"DC - stab - 12 x DC - jar - 3 x 8"DC - XD - 15 HWDP.                  |
|         | Fishing string | Reverse circ.junk basket - stab - 1 x 8" monel - stab - 2 x 8"DC - stab - stab - 15 x 8"DC - jar - 3 x 8"DC - XO - 15 HWDP.                        |
| 23      | 12 1/4"        | bit - bit sub - 1 x 8" monel - 17 x 8"DC - jar - 3 x 8"DC - XO - 15 HWDP.  |
| 24      | 12 1/4"        | As bit no. 23.   |
| 25      | 8 3/8"         | bit - bit sub - 1 x 6½" monel - 22 x 6½" DC - XO - jar - XO - 3 x 6½" DC - XO - 15 HWDP.   |
| 26      | 8 3/8"         | bit - junk sub - NB stab - 1 x 6½" monel - stab - 2 x 6½" DC - stab - 3 x 6½" DC - stab - 17 x 6½" DC - XO - jar - XO - 3 x 6½" DC - XO - 15 HWDP. |
| 27      | 8 3/8"         | As bit no.26 except for the junk sub.  |
| 28      | 8 3/8"         | As bit no.27.  |
| 29      | 8 3/8"         | As bit no.26.  |



| Bit No.           | Bit Size | Bottom Hole Assembly  |
|-------------------|----------|---|
| Core bit no.1.    | 8 3/8"   | bit - core bbl - XO - stab - 2 x 6½" DC - stab - 3 x 6½" DC - stab - 17 x 6½" DC - XO - jar - XO 3 x 6½" DC - XO - 15 HWDP. |
| 30                | 8 3/8"   | As bit no.27.   |
| RR Core bit no.1. | 8 3/8"   | As core bit no.1.   |
| 31                | 8 3/8"   | As bit no.27.   |
| 32                | 8 3/8"   | bit - NB stab - 1 x 6½" monel - stab - 2 x 6½" DC - stab - 3 x 6½" DC - stab - 20 x 6½" DC - XO - 15 HWDP.                  |
| 33                | 8 3/8"   | As bit no.27.   |
| 34                | 8 3/8"   | As bit no.27.   |

#### 6.4 Mud Report

36" hole, 30" csg.: The 36" hole was drilled with sea water with returns to the sea bed. 45 m<sup>3</sup> mud with 1.04 rd was mixed and spotted on connections and 50 m<sup>3</sup> mud with 1.20 rd was mixed which was displaced in the hole prior to running casing.

26" hole, 20" csg.: The riser was run before the 17½" pilot hole was drilled. A 1.08 rd sea water mud mixed with gel, spersene, caustic soda, drilling detergent, magconol and soda ash was used. The mud density was raised to 1.14 rd and YP to 11 before logging.

Increased the mud density to 1.16 rd while underreaming the hole to 26".

17½" hole, 13-3/8" csg.: Drilled out of the 20" csg. shoe with 1.13 rd. Lost 80 m<sup>3</sup> mud due to an open dump valve. Started to control the fluid loss at 1250 m; but problems was encountered due to continuously adding of water. At 1462 m the water loss was 9 cc. Prior to running of the logs the water loss was reduced to 6 cc and the mud density increased to 1.20 rd. Materials used in this interval were barite, gel, caustic soda, spersene, XP-20, CMC, lime, soda ash and tannathin. Chloride content varied from 20 000 to 14 000 ppm.

12-1/4" hole, 9-5/8" csg.: Drilled out with the mud density of 1.20 rd. The water loss was 6.0 cc down to 2172 m at which depth this was reduced to 4.0 cc. Problems were encountered in keeping the viscosity down while drilling the sidetracked hole at 1966 m. Added mud consisting of

prehydrated bentonite, spersene and XP-20. Had to slow down the pumps to 1000 gal/min due to capacity limitations in the mud treatment system. Had tight hole when pulling out from 2232 m. and bit lube and diesel was added to the mud. The water loss was reduced to less than 3 cc and at the same time the mud density was increased to 1.26 rd. When drilling below 2345 m continued to add bit lube, sollex and diesel (4%) to reduce the torque. Increased the mud density to 1.30 rd from 3415 m and down to 3682 m. At this depth the density was increased to 1.34 rd. Chloride content was reduced from 14 000 ppm in the top of the 17½" hole to 5000 ppm at 2172 m. Below 2172 m the chloride content varied between 6000 ppm and 4600 ppm. Materials used in this interval were barite, gel spersene, XP-20, caustic soda, CMC, bit lube, drilling detergent, lime, drispac, magconol, soda ash, soltex, and resinex.

8-3/8" hole, 7" liner: Drilled out of the 9-5/8" casing with the mud density of 1.40 rd. At 3873 this was increased to 1.43 rd and at 4013 m to 1.59 rd. The mud density was continuously increased to 1.90 rd at 4200 m. This mud density was necessary to control the increased amount of gas. The water loss was kept to approximately 3.0 cc in this hole section. Materials used in this interval were barite, gel, spersene, caustic soda, XP-20, CMC, bit lube, lime, drispac, soda ash and resinex.

## WELL DATA SHEET

TABLE A.4

MAG-949-A

|                           |  |                    |  |                             |  |                 |  |                     |  |
|---------------------------|--|--------------------|--|-----------------------------|--|-----------------|--|---------------------|--|
| OPERATOR<br>Norsk Hydro   |  | SURVEY SEC.<br>T R |  | CASING SIZE<br>20" 454      |  | DRLG. DAYS<br>6 |  | BIT SIZE<br>26"     |  |
| WELL<br>15/5-2            |  | FIELD<br>15        |  | SURFACE<br>20" 454          |  | DRLG. DAYS<br>6 |  | BIT SIZE<br>26"     |  |
| CONTRACTOR<br>Wilhelmsen, |  | COUNTY             |  | INTERMEDIATE<br>13 5/8 1598 |  | DRLG. DAYS<br>6 |  | BIT SIZE<br>17 1/2" |  |
| ENGINEER                  |  | STATE              |  | COUNTRY<br>Norway           |  | PRODUCTION      |  |                     |  |

| Aug78 | DEPTH | Sp Gr | VISCOSITY |      | CORR. 115°F |      | GELS |      | pH   | FLUID LOSS  |                      | CL<br>CACL<br>NACL | ALKALINITY |     |     | CA ppm | Mg ppn | RETORT |       |         | ACTIVITY |    | RATIO |     | # Bbl   | C     |     |
|-------|-------|-------|-----------|------|-------------|------|------|------|------|-------------|----------------------|--------------------|------------|-----|-----|--------|--------|--------|-------|---------|----------|----|-------|-----|---------|-------|-----|
|       |       |       | SEC.      | CPS. | PV          | YP   | 0    | 10   |      | 100 PSI API | 500 PSI 300 °F HT-HP |                    | PF         | PM  | MF  |        |        | % OIL  | % SOL | % WATER | As       | Am | OIL   | H2O |         |       | CEC |
|       |       |       |           |      |             |      |      |      |      |             |                      |                    |            |     |     |        |        |        |       |         |          |    |       |     |         |       |     |
| DATE  | WT.   |       |           |      |             |      |      |      |      |             |                      |                    |            |     |     |        |        |        |       |         |          |    |       |     |         |       |     |
| 8-17  | 0     | 1040  | 100       | -    | 10          | 25   | 7    | 13   | 9.5  | n/c         |                      | 2,500              | .5         |     |     | 18     |        | 0      | 3     | 97      |          |    |       | 32  |         |       |     |
| 18    | 194.5 | 1050  | 48        | -    | 8           | 11   | 6    | 15   | 10.0 | n/c         |                      | 3,000              | .2         |     |     | 160    |        | 0      | 3     | 97      |          |    |       | 22  | Run 30  |       |     |
| 19    | 297   | 1080  | 42        | -    | 4           | 8    | 2    | 9    | 9.5  | n/c         |                      | 14,000             | .2         |     |     | 240    |        | 0      | 3.5   | 96.5    |          |    |       | 18  | Dr1g    |       |     |
| 20    | 469   | 1140  | 35        | -    | 6           | 11   | 3    | 15   | 10.0 | n/c         |                      | 15,000             | .4         |     |     | 320    |        | 0      | 5     | 95      |          |    |       | 21  | Dr1g    |       |     |
| 21    | 469   | 1160  | 40        | -    | 7           | 12   | 2    | 14   | 10.0 | n/c         |                      | 15,000             | .3         |     |     | 250    |        | 0      | 7     | 93      |          |    |       | 24  | Ind. re |       |     |
| 22    | 469   | 1160  | 40        | -    | 7           | 15   | 3    | 15   | 10.0 | n/c         |                      | 16,000             | .3         |     |     | 400    |        | 0      | 6     | 94      |          |    |       | 22  | 20"     |       |     |
| 23    | 469   | 1030  | 50        | -    | 7           | 20   | 4    | 20   | 9.5  | n/c         |                      | 500                | .2         |     |     | 160    |        | 0      | 3     | 97      |          |    |       | 21  | Prehy.  |       |     |
| 24    | 608   | 1129  | 34        | 15.5 | 3           | 9    | 6    | 20   | 9.5  | n/c         |                      | 20,000             | .2         | .6  | 0   | 1800   |        | 0      | 3     | 97      |          |    |       | 19  |         |       |     |
| 25    | 1016  | 1129  | 34        | 30   | 8           | 14   | 6    | 20   | 9.5  | n/c         |                      | 20,000             | .2         | .6  | 0   | 1200   |        | 0      | 6     | 94      |          |    |       | 20  |         |       |     |
| 26    | 1267  | 1168  | 43        | 34   | 10          | 14   | 3    | 16   | 9.5  | n/c         |                      | 18,000             | .2         | .4  | 0   | 1000   |        | 0      | 7     | 93      |          |    |       | 28  |         |       |     |
| 27    | 1462  | 1164  | 65        | 32   | 9           | 14   | 3    | 10   | 9.5  | 9           |                      | 16,500             | .2         | .3  | 0   | 400    |        | 0      | 8     | 92      |          |    |       | 40  |         |       |     |
| 28    | 1462  | 1164  | 65        | 32   | 9           | 14   | 3    | 10   | 9.5  | 9           |                      | 16,500             | .2         | .3  | 0   | 400    |        | 0      | 8     | 92      |          |    |       | 40  |         |       |     |
| 29    | 1616  | 1177  | 50        | 24   | 8           | 8    | 2    | 9    | 9.5  | 9           |                      | 19,000             | .1         | .2  | 0   | 700    |        | 0      | 10    | 90      |          |    |       | 40  |         |       |     |
| 30    | 1616  | 1200  | 49        | 27   | 9           | 9    | 2    | 7    | 10.5 | 6.5         |                      | 15,000             | .2         | .4  | 10  | 360    |        | 0      | 11    | 89      |          |    |       | 40  |         |       |     |
| 31    | 1616  | 1200  | 48        | 26   | 8           | 10   | 2    | 9    | 9.5  | 5.0         |                      | 15,000             | .1         | .4  | 0   | 360    |        | 0      | 11    | 89      |          |    |       | 40  | Logs    |       |     |
| 1     | 1616  | 1200  | 72        |      | 12          | 11   | 14   | 58   | 10.5 | 6.3         |                      | 14,000             | .25        | .45 | 0   | 360    |        | 0      | 12    | 88      |          |    |       |     |         | Circ  |     |
| 2     | 1616  | 1200  | 68        |      | 11          | 12   | 6.7  | 41.2 | 10.0 | 6.2         |                      | 14,000             | .3         | .2  | 0   | 360    |        | 0      | 12    | 88      |          |    |       |     |         | 3 3/8 |     |
| 3     | 1598  | 1200  | 68        |      | 12.5        | 11.5 | 7.6  | 18.2 | 9.5  | 6.6         |                      | 14,000             | .2         | -   | 0   | 460    |        |        | -     | -       |          |    |       |     |         | BOA   |     |
| 4     | 1802  | 1200  | 75        |      | 15          | 12   | 4    | 6    | 11.0 | 5.8         |                      | 13,000             | .2         | 7   | 0   | 400    |        |        | 10    | 90      |          |    |       |     |         | Drill |     |
| 5     | 1884  | 1200  | 47        |      | 9           | 11   | 3    | 20   | 10.5 | 5.7         |                      | 11,000             | .7         | 1.2 | 1.9 | 360    |        |        | 11    | 89      |          |    |       | 32  | Drill   |       |     |
| 6     | 1912  | 1210  | 44        |      | 11          | 9    | 3    | 21   | 11.5 | 5.8         |                      | 12,000             | .8         | 1.8 | 2.6 | 350    |        |        | 10    | 90      |          |    |       | 40  | Drill   |       |     |
| 7     |       |       |           |      |             |      |      |      |      |             |                      |                    |            |     |     |        |        |        |       |         |          |    |       |     |         |       |     |
| 8     | 2199  | 1200  | 51        | 30   | 10          | 10   | 3    | 8    | 10.5 | 5.4         |                      | 8,000              | 1.0        | 1.9 | 1.3 | 200    |        | 0      | 11    | 89      |          |    |       | 28  | Drill   |       |     |
| 9     | 2294  | 1220  | 48        | 20   | 6           | 8    | 2    | 5    | 10.5 | 6.0         |                      | 8,000              | .8         | 1.4 | 1.9 | 200    |        | 0      | 10    | 90      |          |    |       | 26  | Stuck   |       |     |
| 10    | 2294  | 1220  | 46        | 19   | 5           | 7    | 2    | 4    | 10.0 | 6.0         |                      | 7,800              | .5         | .9  | .8  | 200    |        | 0      | 9     | 91      |          |    |       | 25  | Stuck   |       |     |
| 11    | 2294  | 1220  | 46        | 19   | 5           | 7    | 2    | 4    | 9.5  | 6.5         |                      | 7,800              | .3         | .6  | .5  | 200    |        | 0      | 9     | 91      |          |    |       | 25  | Stuck   |       |     |
| 12    | 2294  | 1220  | 47        | 16   | 5           | 6    | 2    | 4    | 8.5  | 6.0         |                      | 7,500              | .1         | .3  | .2  | 180    |        | 0      | 9     | 91      |          |    |       | 26  | Stuck   |       |     |

DATE SPUD:

16/8/78

DATE T.D.:

15.11.78

B.H.T.

COMPLETION FLUID TYPE: None

PACKER MUD TYPE: Active mud

COST: 0

COST: 0

C1

## WELL DATA SHEET

TABLE A.4 cont.

MAQ-948-A

| OPERATOR   |       | Norsk Hydro |           | SURVEY SEC. |           | T         |      | R       |      | CASING SIZE  |                      | DEPTH      |            | DRLG. DAYS |     | BIT SIZE |      |        |      |      |                |                |       |                  |       |
|------------|-------|-------------|-----------|-------------|-----------|-----------|------|---------|------|--------------|----------------------|------------|------------|------------|-----|----------|------|--------|------|------|----------------|----------------|-------|------------------|-------|
| WELL       |       | 15/         |           | FIELD       |           | 15        |      |         |      | SURFACE      |                      | 20         |            | 454        |     | 6        |      |        |      |      |                |                |       |                  |       |
| CONTRACTOR |       | Wilhelmson  |           | COUNTY      |           |           |      |         |      | INTERMEDIATE |                      | 13 3/8     |            | 1598       |     | 17 1/2"  |      |        |      |      |                |                |       |                  |       |
| ENGINEER   |       |             |           | STATE       |           | North Sea |      | COUNTRY |      | Norway       |                      | PRODUCTION |            | 9 5/8"     |     | 3696     |      |        |      |      |                |                |       |                  |       |
|            |       |             |           |             |           |           |      |         |      |              |                      |            |            |            |     |          |      |        |      |      |                |                |       |                  |       |
| DATE       | DEPTH | SpGr        | VISCOSITY |             | CORR. USE |           | GELS |         | pH   | FLUID LOSS   |                      | CL         | ALKALINITY |            |     | CA       | Mg   | RETORT |      |      | ACTIVITY       |                | RATIO |                  | # Bbl |
|            |       |             | SEC.      | CPS.        | PV        | YP        | 0    | 10      |      | 100 PSI API  | 500 PSI 300 °F HT-HP |            | PF         | PM         | MF  |          |      | %      | %    | %    | A <sub>o</sub> | A <sub>m</sub> | OIL   | H <sub>2</sub> O |       |
| Sept 13    | 1780  | 1220        | 48        | 16          | 5         | 6         | 2    | 3       | 9.5  | 7.0          |                      | 8000       | .2         | .5         | .4  | 200      |      |        | 9    | 91   |                |                |       |                  | 25    |
| 14         | 1840  | 1220        | 46        | 15          | 5         | 5         | 2    | 4       | 11.5 | 6.8          |                      | 6000       | .9         | 2.8        | 1.7 | 500      |      |        | 9    | 91   |                |                |       |                  | 30    |
| 15         | 1740  | 1220        | 44        | 14          | 4         | 6         | 2    | 4       | 11.0 | 6.2          |                      | 6500       | .8         | 1.6        | 2.3 | 500      | 1500 |        | 8    | 92   |                |                |       |                  | 30    |
| 16         | 1829  | 1220        | 46        | 21          | 7         | 7         | 6    | 27      | 10.0 | 6.1          |                      | 7500       | 3.1        | 4.2        | 3.8 | 560      | 1640 |        | 10   | 90   |                |                |       |                  | 29    |
| 17         | 1874  | 1220        | 46        | 18          | 6         | 6         | 2    | 22      | 10.5 | 6.0          |                      | 6000       | 1.1        | 2.6        |     | 300      | 1100 |        | 8    | 92   |                |                |       |                  | 31    |
| 18         | 1874  | 1220        | 41        | 18          | 6         | 6         | 2    | 22      | 9.5  | 6.2          |                      | 6000       | 2.1        |            | 2.8 | 300      | 1100 |        | 9    | 91   |                |                |       |                  |       |
| 19         | 1966  | 1210        | 44        | 11          | 5         | 6         | 2    | 20      | 11.0 | 5.8          |                      | 6000       | 1.3        |            | 2.4 | 330      | 1070 |        | 8    | 92   |                |                |       |                  | 31    |
| 20         | 2172  | 1210        | 48        | 19          | 9.5       | 5.5       | 4    | 26      | 11.0 | 6.0          |                      | 5000       | 1.1        |            | 2.2 | 330      | 970  | 3      | 9    | 88   |                |                |       |                  | 28    |
| 21         | 2232  | 1260        | 54        | 23          | 10        |           | 7    | 26      | 11.0 | 4.6          |                      | 5000       | .9         | 1.2        | 2.1 | 350      |      | 4      | 12   | 84   |                |                |       |                  | 28    |
| 22         | 7000  | 1260        | 62        | 29          | 9         | 10        | 4    | 6       | 10.2 | 4.1          |                      | 5000       | .6         | 2.1        | 1.4 | 260      | 98   | 4      | 11   | 85   |                |                |       |                  | 30    |
| 23         | 2345  | 1270        | 52        | 25          | 8         | 9         | 3    | 6       | 11.0 | 4.0          | 10                   | 5000       | 1.2        | 2.6        | 1.9 | 400      | 95   | 4      | 11   | 85   |                |                |       |                  | 29    |
| 24         |       | 1260        | 49        | 23          | 8         | 7         | 2    | 5       | 9.9  | 3.4          | 10                   | 5000       | .4         | 1.8        | .9  | 160      | 73   | 4      | 9    | 87   |                |                |       |                  | 25    |
| 25         | 2639  | 1260        | 60        | 36          | 14        | 8         | 4    | 9       | 10.4 | 2.8          | 10                   | 5000       | 1.1        | 2.5        | 1.3 | 200      | 80   | 4      | 10   | 86   |                |                |       |                  | 20    |
| 26         | 2723  | 1260        | 51        | 33          | 12        | 9         | 2    | 6       | 10.7 | 2.8          |                      | 5000       | .4         | 2.6        | 1.1 | 160      | 145  | 4      | 9    | 87   |                |                |       |                  | 25    |
| 27         | 2754  | 1270        | 52        | 30          | 11        | 8         | 2    | 6       | 10.4 | 3.0          |                      | 5000       | .6         | 1.9        | 1.8 | 320      | 290  | 4      | 9    | 87   |                |                |       |                  | 25    |
| 28         | 2826  | 1270        | 46        | 23          | 9         | 5         | 2    | 4       | 11.5 | 3.2          |                      | 5000       | 1.2        | 2.4        | 1.9 | 450      | 260  | 4      | 9    | 87   |                |                |       |                  | 23    |
| 29         | 2826  | 1260        | 55        | 30          | 9         | 7         | 3    | 7       | 10.0 | 3.4          | 10.5                 | 4800       | .8         | 1.5        | 1.3 | 500      | 300  | 4      | 9    | 87   |                |                |       |                  | 23    |
| 30         | 2855  | 1260        | 48        | 30          | 9         | 7         | 3    | 6       | 10.9 | 3.2          | 12.0                 | 6000       | .7         | 2.5        | 1.6 | 150      | 50   | 4      | 8    | 88   |                |                |       |                  | 27    |
| Oct 1      | 2938  | 1270        | 45        | 25          | 10        | 5         | 2    | 4       | 10.2 | 3.6          | 13                   | 6500       | .6         | 2.3        | 1.6 | 160      | 210  | 4      | 9    | 87   |                |                |       |                  | 23    |
| 2          | 3016  | 1270        | 50        | 36          | 14        | 8         | 3    | 7       | 11.0 | 3.6          | 12                   | 4800       | 1.2        | 3.0        | 2.0 | 160      | 146  | 4      | 10   | 87   |                |                |       |                  | 30    |
| 3          | 3081  | 1270        | 48        | 34          | 12        | 10        | 2    | 8       | 10.3 | 3.6          | 8                    | 5000       | .8         | 2.2        | 2.3 | 180      | 140  |        |      |      |                |                |       |                  |       |
| 4          | 3156  | 1270        | 52        | 38          | 13        | 7         | 4    | 7       | 10.0 | 3.8          | 11.0                 | 4600       | .5         | 2.6        |     | 80       |      | 4      | 12.5 | 83.5 |                |                |       |                  | 30    |
| 5          | 3223  | 1270        | 47        | 29          | 5.5       | 5.5       | 2    | 9       | 9.5  | 4.0          | 15.0                 | 5000       | .5         | 2.0        |     | 160      |      | 3      | 15   | 82   |                |                |       |                  |       |
| 6          | 3285  | 1270        | 51        | 37          | 20        | 7.5       | 3    | 6       | 10.5 | 4.4          | 8.0                  | 5000       | 1.2        | 3.0        | 3.8 | 200      |      | 3      | 16   | 81   |                |                |       |                  | 28    |
| 7          | 3359  | 1270        | 46        | 27          | 16        | 7.5       | 3    | 16      | 9.5  | 4.4          | 9.0                  | 5000       | .8         |            | 2.4 | 160      | 140  | 3      | 14   | 83   |                |                |       |                  | 28    |

DATE SHUT:

16/8/79

DATE T.O.:

15/11/78

B.H.T.

118°C

COMPLETION FLUID TYPE: None

PACKER MUD TYPE: Activ. Mud

COST: \$ - 0

COST: \$ - 0

TABLE A.4 cont.

|             |  |  |  |  |  |  |  |  |  |             |  |  |  |  |  |  |  |  |  |              |  |  |  |  |  |  |  |  |  |            |  |  |  |  |  |  |  |  |  |            |  |  |  |  |  |  |  |  |  |          |  |  |  |  |  |  |  |  |  |            |  |  |  |  |  |  |  |  |  |         |  |  |  |  |  |  |  |  |  |            |  |  |  |  |  |  |  |  |  |        |  |  |  |  |  |  |  |  |  |          |  |  |  |  |  |  |  |  |  |         |  |  |  |  |  |  |  |  |  |         |  |  |  |  |  |  |  |  |  |    |  |  |  |  |  |  |  |  |  |    |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                |  |  |  |  |  |  |  |  |  |                |  |  |  |  |  |  |  |  |  |     |  |  |  |  |  |  |  |  |  |                  |  |  |  |  |  |  |  |  |  |     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 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| OPERATOR    |  |  |  |  |  |  |  |  |  | SURVEY SEC. |  |  |  |  |  |  |  |  |  | CASING SIZE  |  |  |  |  |  |  |  |  |  | DEPTH      |  |  |  |  |  |  |  |  |  | DRLG. DAYS |  |  |  |  |  |  |  |  |  | BIT SIZE |  |  |  |  |  |  |  |  |  |            |  |  |  |  |  |  |  |  |  |         |  |  |  |  |  |  |  |  |  |            |  |  |  |  |  |  |  |  |  |        |  |  |  |  |  |  |  |  |  |          |  |  |  |  |  |  |  |  |  |         |  |  |  |  |  |  |  |  |  |         |  |  |  |  |  |  |  |  |  |    |  |  |  |  |  |  |  |  |  |    |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |                |  |  |  |  |  |  |  |  |  |                |  |  |  |  |  |  |  |  |  |     |  |  |  |  |  |  |  |  |  |                  |  |  |  |  |  |  |  |  |  |     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  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 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

TABLE A.4 cont.

## WELL DATA SHEET

MAO-349-A

| OPERATOR    |       | SURVEY SEC. |           | CASING SIZE  |             | DEPTH      |      | DRLG. DAYS |      | BIT SIZE    |                      |   |            |    |     |        |        |        |       |         |                |                |       |                  |       |         |
|-------------|-------|-------------|-----------|--------------|-------------|------------|------|------------|------|-------------|----------------------|---|------------|----|-----|--------|--------|--------|-------|---------|----------------|----------------|-------|------------------|-------|---------|
| WELL        |       | FIELD       |           | SURFACE      |             |            |      |            |      |             |                      |   |            |    |     |        |        |        |       |         |                |                |       |                  |       |         |
| CONTRACTOR  |       | COUNTY      |           | INTERMEDIATE |             |            |      |            |      |             |                      |   |            |    |     |        |        |        |       |         |                |                |       |                  |       |         |
| ENGINEER    |       | STATE       |           | COUNTRY      |             | PRODUCTION |      |            |      |             |                      |   |            |    |     |        |        |        |       |         |                |                |       |                  |       |         |
| Norsk Hydro |       | T R         |           | 13 3/8"      |             | 1598       |      | 6          |      | 17 1/2"     |                      |   |            |    |     |        |        |        |       |         |                |                |       |                  |       |         |
| 15/5-2      |       | 15          |           | 9 5/8"       |             | 3696       |      | 46         |      | 12 1/4"     |                      |   |            |    |     |        |        |        |       |         |                |                |       |                  |       |         |
| Wilhelmson  |       | North Sea   |           | Norway       |             | 4292       |      | 22         |      | 8 3/8"      |                      |   |            |    |     |        |        |        |       |         |                |                |       |                  |       |         |
| DATE        | DEPTH | Sp Gr       | VISCOSITY |              | CORR. 115°F |            | GELS |            | pH   | FLUID LOSS  |                      | CL <input type="checkbox"/><br>CACL <input type="checkbox"/><br>NACL <input type="checkbox"/> | ALKALINITY |    |     | CA ppm | Mg ppm | RETORT |       |         | ACTIVITY       |                | RATIO |                  | # Bbl | CEC     |
|             |       |             | SEC.      | CPS.         | PV          | YP         | 0    | 10         |      | 100 PSI API | 500 PSI 300 °F HT-HP |   | PF         | PM | MF  |        |        | % OIL  | % SOL | % WATER | A <sub>o</sub> | A <sub>m</sub> | OIL   | H <sub>2</sub> O |       |         |
| 4           | 4013  | 1590        | 50        |              | 28          | 14         | 4    | 16         | 10   | 3,5         | 16                   | 4500  | 1.2        |    |     | 160    |        | 2      | 18    | 80      |                |                |       |                  | 30    |         |
| 5           | 4020  | 1630        | 47        |              | 26          | 14         | 4    | 16         | 10   | 3,5         | 14                   | 4000  | 1.8        |    |     | 160    |        | 2      | 19    | 79      |                |                |       |                  | 20    |         |
| 6           | 4030  | 1800        | 48        |              | 35          | 14         | 6    | 16         | 10,5 | 3,5         | 14                   | 4000  | 1.6        |    |     | 160    |        | 2      | 23    | 75      |                |                |       |                  | 20    |         |
| 7           | 4036  | 1800        | 47        |              | 31          | 14         | 4    | 14         | 10,5 | 3,5         | 14                   | 4500  | 1.6        |    |     | 160    |        | 1      | 25    | 74      |                |                |       |                  | 30    |         |
| 8           | 4066  | 1820        | 47        |              | 30          | 12         | 4    | 12         | 11   | 3,5         | 12                   | 4500  | 1.8        |    |     | 160    |        | 1      | 26    | 73      |                |                |       |                  | 30    |         |
| 9           | 4113  | 1820        | 49        |              | 29          | 11         | 4    | 10         | 10,5 | 3,5         | 12                   | 5000  | 1.5        |    |     | 160    |        | 1      | 26    | 73      |                |                |       |                  | 30    |         |
| 10          | 4130  | 1820        | 49        |              | 29          | 11         | 4    | 10         | 10   | 3,5         | -                    | 5000  | 1.5        |    | 3.8 | 160    |        | 1      | 26    | 73      |                |                |       |                  | 30    |         |
| 11          | 4156  | 1820        | 54        |              | 22          | 10         | 5    | 18         | 10   | 4,0         | 13,6                 | 5000  | 1.8        |    | 2.2 | 190    |        | 1      | 23    | 76      |                |                |       |                  | 20    |         |
| 12          | 4200  | 1900        | 54        |              | 24          | 14         | 6    | 26         | 10,5 | 3,8         | 13,2                 | 5000  | 1.5        |    | 1.9 | 160    |        | 1      | 29    | 70      |                |                |       |                  | 26    |         |
| 13          | 4270  | 1900        | 53        |              | 26          | 14         | 7    | 82         | 10,5 | 3,8         | 13,6                 | 5200  | 1.9        |    | 2.6 | 240    |        | TR     | 32    | 68      |                |                |       |                  | 26    |         |
| 14          | 4290  | 1900        | 55        |              | 22          | 14         | 6    | 20         | 11   | 4,0         | 8,6                  | 5000  | 2.4        |    | 3.0 | 230    |        | TR     | 32    | 68      |                |                |       |                  | 26    |         |
| 15          | 4322  | 1900        | 55        |              | 42          | 12         | 9    | 32         | 10   | 3,4         | -                    | 5200  | 2.2        |    | 2.8 | 220    |        | TR     | 33    | 67      |                |                |       |                  | 26    | WOW     |
| 16          | 4322  | 1900        | 55        |              | 42          | 12         | 9    | 32         | 10   | 3,4         | 13                   | 5200  | 2.2        |    | 2.8 | 220    |        | TR     | 33    | 67      |                |                |       |                  | 26    | WOW     |
| 17          | 4322  | 1900        | 55        |              | 42          | 12         | 9    | 32         | 10   | 3,4         | 13                   | 5200  | 2.2        |    | 2.8 | 220    |        | TR     | 33    | 67      |                |                |       |                  | 26    | WOW     |
| 18          | 4322  | 1900        | 55        |              | 42          | 12         | 9    | 32         | 10   | 3,4         | 13                   | 5200  | 2.2        |    | 2.8 | 220    |        | TR     | 33    | 67      |                |                |       |                  | 26    | WOW     |
| 19          | 4322  | 1900        | 45        |              | 30          | 12         | 4    | 14         | 10,5 | 3,2         | 11                   | 5200  | 2.0        |    | 2.6 | 220    |        | TR     | 33    | 67      |                |                |       |                  | 26    | CIRC    |
| 20          | 4322  | 1900        | 43        |              | 27          | 10         | 3    | 12         | 10   | 3,4         | 11                   | 5000  | 1.0        |    |     | 220    |        | TR     | 32    | 68      |                |                |       |                  | 24    | Loggi   |
| 21          | 4322  | 1900        | 43        |              | 27          | 10         | 3    | 12         | 10   | 3,4         | 11                   | 5000  | 1.0        |    |     | 220    |        | TR     | 32    | 68      |                |                |       |                  |       | Log     |
| 22          | 4322  | 1900        | 40        |              | 24          | 8          | 2    | 6          | 10   | 3,0         | 7                    | 4000  | 1.0        |    |     | 160    |        | TR     | 30    | 70      |                |                |       |                  | 22    |         |
| 23          | 4322  | 1900        | 40        |              | 24          | 4          | 2    | 6          | 10   | 3,0         | 7                    | 4000  | 1.0        |    |     | 160    |        | TR     | 30    | 70      |                |                |       |                  | 24    |         |
| 24          | 4322  | 1900        | 56        |              | 18          | 7          | 3    | 8          | 9,5  | 3,2         | -                    | 4000  | 1.0        |    | 2.8 | 160    |        | TR     | 31    | 69      |                |                |       |                  | 24    |         |
| 25          | 4322  | 1900        | 44        |              | 24          | 8          | 2    | 6          | 9,5  | 3,0         | 11,2                 | 4000  | 1.0        |    | -   | 160    |        | TR     | 30    | 70      |                |                |       |                  | 24    |         |
| 26          | 4322  | 1900        | 43        |              | 31          | 15         | 2    | 6          | 9,5  | 3,1         | -                    | 4000  | 1.0        |    | -   | 160    |        | TR     | 30    | 70      |                |                |       |                  | 24    |         |
| 27          | 4322  | 1900        | 54        |              | 16          | 8          | 2    | 8          | 10   | 2,8         | -                    | 4100  | 1.2        |    | 3.1 | 160    |        | TR     | 31    | 69      |                |                |       |                  | 24    | TESTING |
| 28          | 4322  | 1900        | 43        |              | 31          | 15         | 2    | 6          | 10   | 2,8         | 10,2                 | 4000  | 1.0        |    | 3.2 | 160    |        | TR     | 30    | 70      |                |                |       |                  | 24    |         |
| 29          | 4322  | 1900        | 45        |              | 12          | 10         | 4    | 14         | 14   | 3,6         | 10,0                 | 4400  | .9         |    | 2.7 | 160    |        | TR     | 31    | 69      |                |                |       |                  | -     |         |
| 30          | 4322  | 1900        | 47        |              | 25          | 13         | 6    | 16         | 9,3  | 3,4         | 14,0                 | 4400  | .9         |    | 2.8 | 160    |        | TR     | 30    | 70      |                |                |       |                  | 25    |         |

DATE SPUD: 16 August 1978 DATE T.D.: 15 November 1978 B.H.T. 118° COMPLETION FLUID TYPE: None COST: 0  
PACKER MUD TYPE: Active Mud COST: 0

## TABLE A.4 cont.

**MAQ-343.A**46



## 6.5 Cement Report

### 30" Casing

Setting depth was 194 m and it was cemented back to the sea bed.

Lead slurry:

|                   | Composition              | Total used          |
|-------------------|--------------------------|---------------------|
| Class "G" cement: |                          | 13.1 ton            |
| Yield:            | 1.51 m <sup>3</sup> /ton |                     |
| Sea water:        | 1.07 m <sup>3</sup> /ton | 14.0 m <sup>3</sup> |
| Econolite:        | 0.05 m <sup>3</sup> /ton | 0.66 m <sup>3</sup> |
| Density:          | 1.5 rd                   |                     |
| Thickening time:  | 4:00 hrs. at 7°C BHST    |                     |

Tail slurry:

|                     |                          |                     |
|---------------------|--------------------------|---------------------|
| Class "G" cement    |                          | 11.1 ton            |
| Yield:              | 0.84 m <sup>3</sup> /ton |                     |
| Sea water:          | 0.44 m <sup>3</sup> /ton | 4.9 m <sup>3</sup>  |
| CaCl <sub>2</sub> : | 0.07 m <sup>3</sup> /ton | 0.78 m <sup>3</sup> |
| Density:            | 1.87 rd                  |                     |
| Thickening time:    | 3:30 hrs. at 7°C BHST    |                     |

### 20" Casing

Setting depth was 454 m and it was cemented back to the sea bed.

Lead slurry:

|                  |                          |                     |
|------------------|--------------------------|---------------------|
| Class "G" cement |                          | 62.25 ton           |
| Yield:           | 1.51 m <sup>3</sup> /ton |                     |
| Sea water:       | 1.07 m <sup>3</sup> /ton | 66.6 m <sup>3</sup> |
| Econolite:       | 0.05 m <sup>3</sup> /ton | 3.1 m <sup>3</sup>  |
| Density:         | 1.5 rd                   |                     |
| Thickening time: | 6:30 hrs at 28°C BHST    |                     |

Tail slurry:

|                     | Composition              | Total used          |
|---------------------|--------------------------|---------------------|
| Class "G" cement:   |                          | 9.8 ton             |
| Yield:              | 0.79 m <sup>3</sup> /ton |                     |
| Sea water:          | 0.45 m <sup>3</sup> /ton | 4.41 m <sup>3</sup> |
| CaCl <sub>2</sub> : | 0.024 m <sup>3</sup> /   | 0.24 m <sup>3</sup> |
| Density:            | 1.5 rd.                  |                     |
| Thickening time:    | 6:30 hrs. at 28°C BHST   |                     |

13-3/8" Casing

Setting depth was 1598 m and it was cemented back to 1150 m.

Cement slurry:

|                  |                           |                     |
|------------------|---------------------------|---------------------|
| Class "G" cement |                           | 34.5 ton            |
| Yield:           | 0.77 m <sup>3</sup> /ton  |                     |
| Fresh water:     | 0.40 m <sup>3</sup> /ton  | 13.8 m <sup>3</sup> |
| CFR-2L:          | 0.026 m <sup>3</sup> /ton | 0.89 m <sup>3</sup> |
| FL-1:            | 0.036 m <sup>3</sup> /ton | 1.24 m <sup>3</sup> |
| Density:         | 1.89 rd                   |                     |
| Thickening time: | 5:50 hrs. at 42°C BHST    |                     |

9-5/8" Casing

Setting depth was 3696 m and it was cemented back to 3200 m.

Cement slurry:

|                  |                            |                     |
|------------------|----------------------------|---------------------|
| Class "G" cement |                            | 33 ton              |
| Yield:           | 0.77 m <sup>3</sup> /ton   |                     |
| Fresh water:     | 0.40 m <sup>3</sup> /ton   | 13.2 m <sup>3</sup> |
| CFR-2L:          | 0.026 m <sup>3</sup> /ton  | 0.86 m <sup>3</sup> |
| FL-1:            | 0.036 m <sup>3</sup>       | 1.19 m <sup>3</sup> |
| HR-6L:           | 0.0036 m <sup>3</sup> /ton | 0.12 m <sup>3</sup> |
| Density:         | 1.89 rd                    |                     |
| Thickening time: | 5:07 hrs. at 121°C, BHST   |                     |

### 7" Liner

Setting depth was 4300 m and it was cemented back to approximately 3780 m.

#### Cement slurry:

|                  | Composition               | Total used          |
|------------------|---------------------------|---------------------|
| Class "G" cement |                           | 32 ton              |
| Yield:           | 0.76 m <sup>3</sup> /ton  |                     |
| Fresh water:     | 0.447 m <sup>3</sup> /ton | 14.3 m <sup>3</sup> |
| CFR-2L:          | 0.026 m <sup>3</sup> /ton | 0.83 m <sup>3</sup> |
| FL-1:            | 0.067 m <sup>3</sup> /ton | 2.14 m <sup>3</sup> |
| HR-12L:          | 0.012 m <sup>3</sup> /ton | 0.38 m <sup>3</sup> |
| Density:         | 1.92 rd                   |                     |
| Thickening time: | 6:00 hrs. at 138°C BHST   |                     |

### 7" Liner hanger squeeze job

Due to a blocked cement line during the primary cement job the 7" liner hanger had to be squeezed off and a 60 m cement plug was spotted on top of the hanger.

#### Cement slurry:

|                  |                            |                      |
|------------------|----------------------------|----------------------|
| Class "G" cement |                            | 6.7 ton              |
| Yield:           | 0.74 m <sup>3</sup> /ton   |                      |
| Fresh water:     | 0.44 m <sup>3</sup> /ton   | 2.9 ton              |
| CFR-2L:          | 0.013 m <sup>3</sup> /ton  | 0.087 m <sup>3</sup> |
| HR-12L:          | 0.0055 m <sup>3</sup> /ton | 0.037 m <sup>3</sup> |
| FL-1:            | 0.0335 m <sup>3</sup> /ton | 0.224 m <sup>3</sup> |
| Density:         | 1.93 rd                    |                      |

### Cement plug from 415 m to 445 m

|                  |                           |                     |
|------------------|---------------------------|---------------------|
| Class "G" cement |                           | 1.5 ton             |
| Yield:           | 0.74 m <sup>3</sup> /ton  |                     |
| Fresh water:     | 0.424 m <sup>3</sup> /ton | 0.64 m <sup>3</sup> |
| Density:         | 1.93 rd                   |                     |
| Thickening time: | 2.0 hrs.                  |                     |

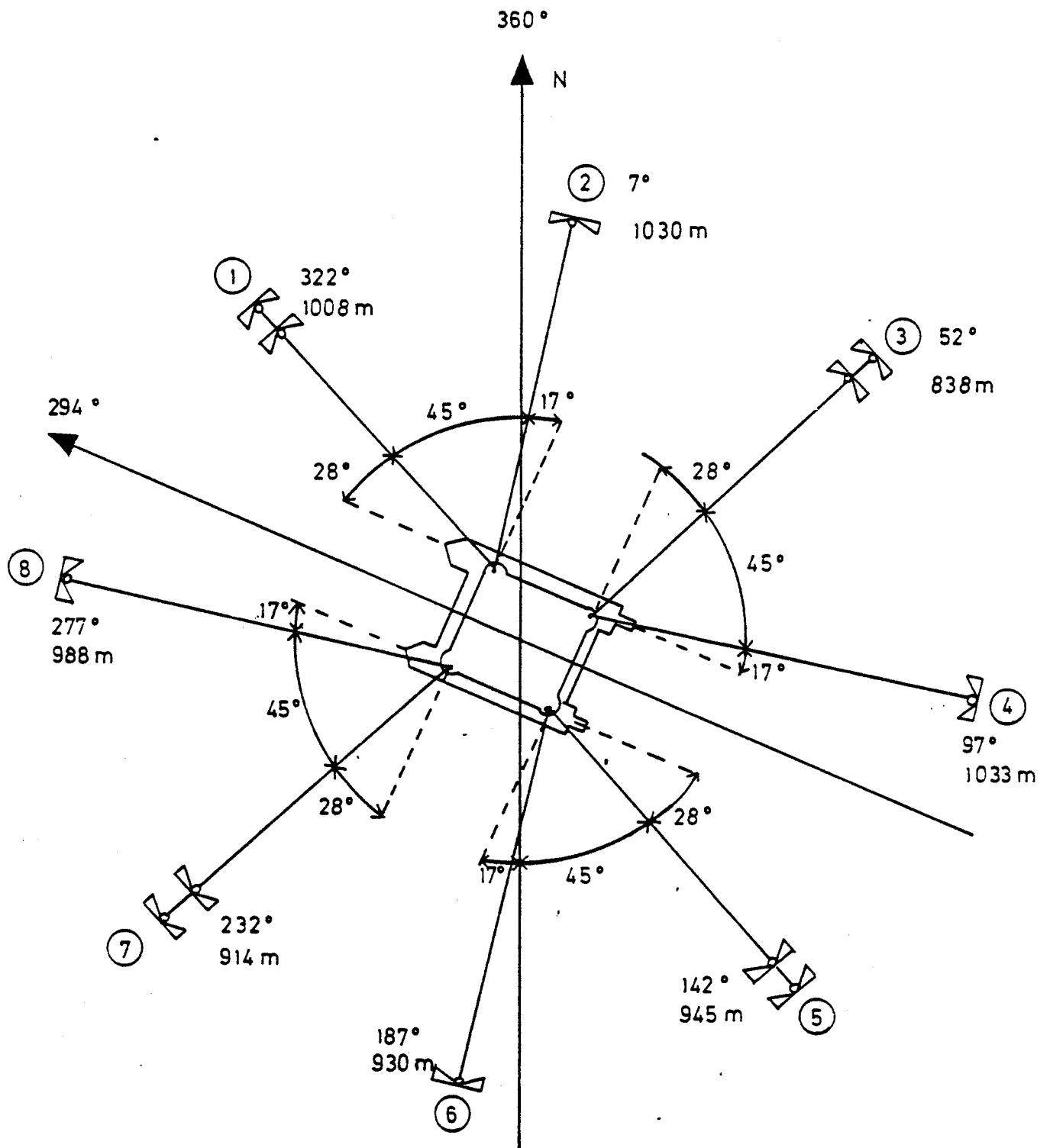
#### 6.6 Lost in the hole

When the pipe got stuck at 1928 m the following equipment had to be left in the hole, see Fig. A-6

- 12-1/4" bit, type SDGH
- Junk sub
- Bit sub
- 3ea 12-3/16" stabilizers
- 1ea 8" monel drill collar
- 8ea 8" drill collars

7. PRELIMINARY COST REPORT

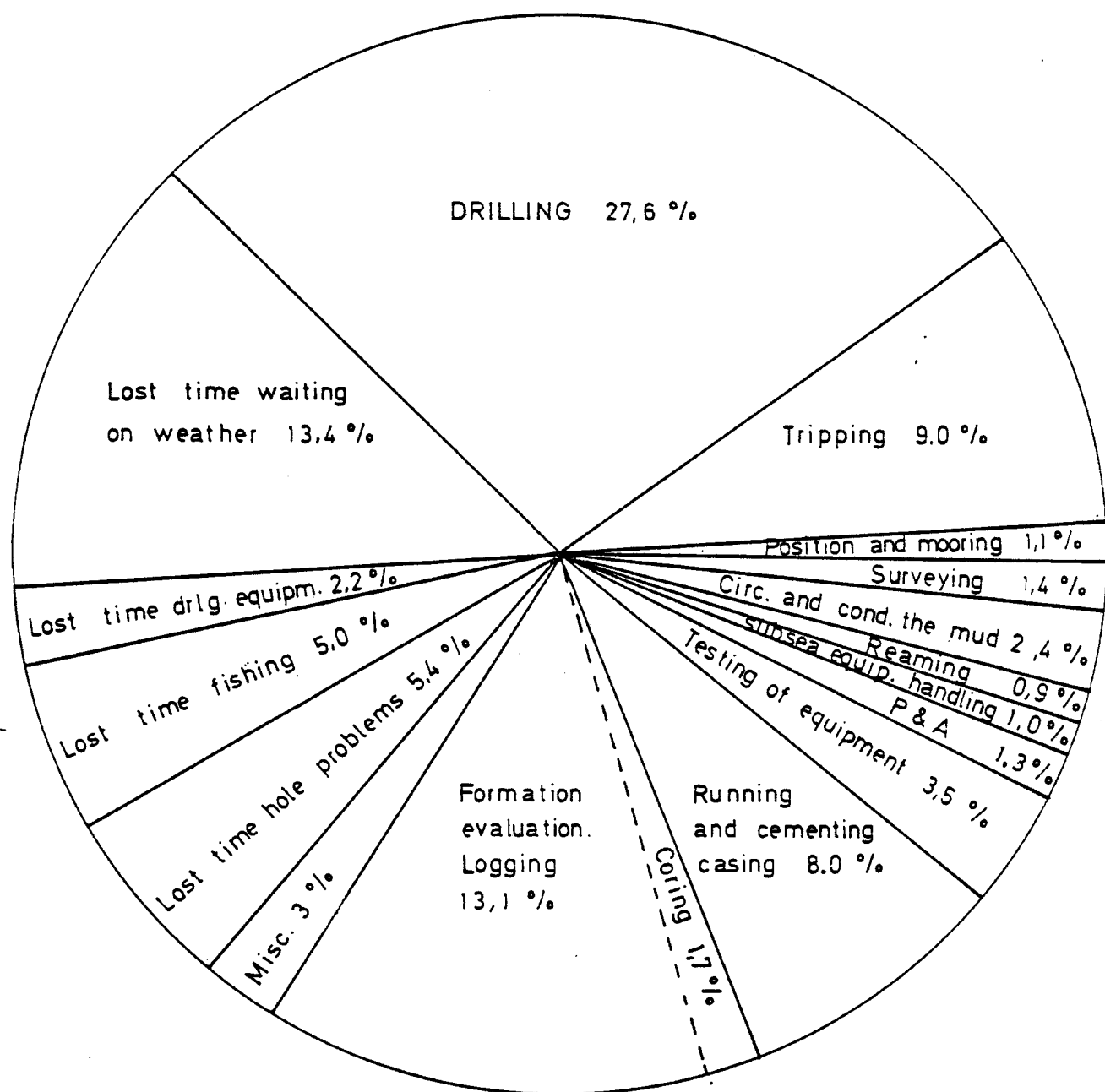
|                    |                              |
|--------------------|------------------------------|
| Site survey, misc. | N.kr. 515.000                |
| Rig contract       | N.kr. 18.090.000             |
| Supplies           | N.kr. 10.816.000             |
| Services           | N.kr. 12.708.000             |
| Operator's cost    | N.kr. 7.894.000              |
| TOTAL              | <hr/> N.kr. 50.023.000 <hr/> |



Heading : 294°

Well coordinates : 50° 38' 36,7" N  
1° 36' 16,5" E

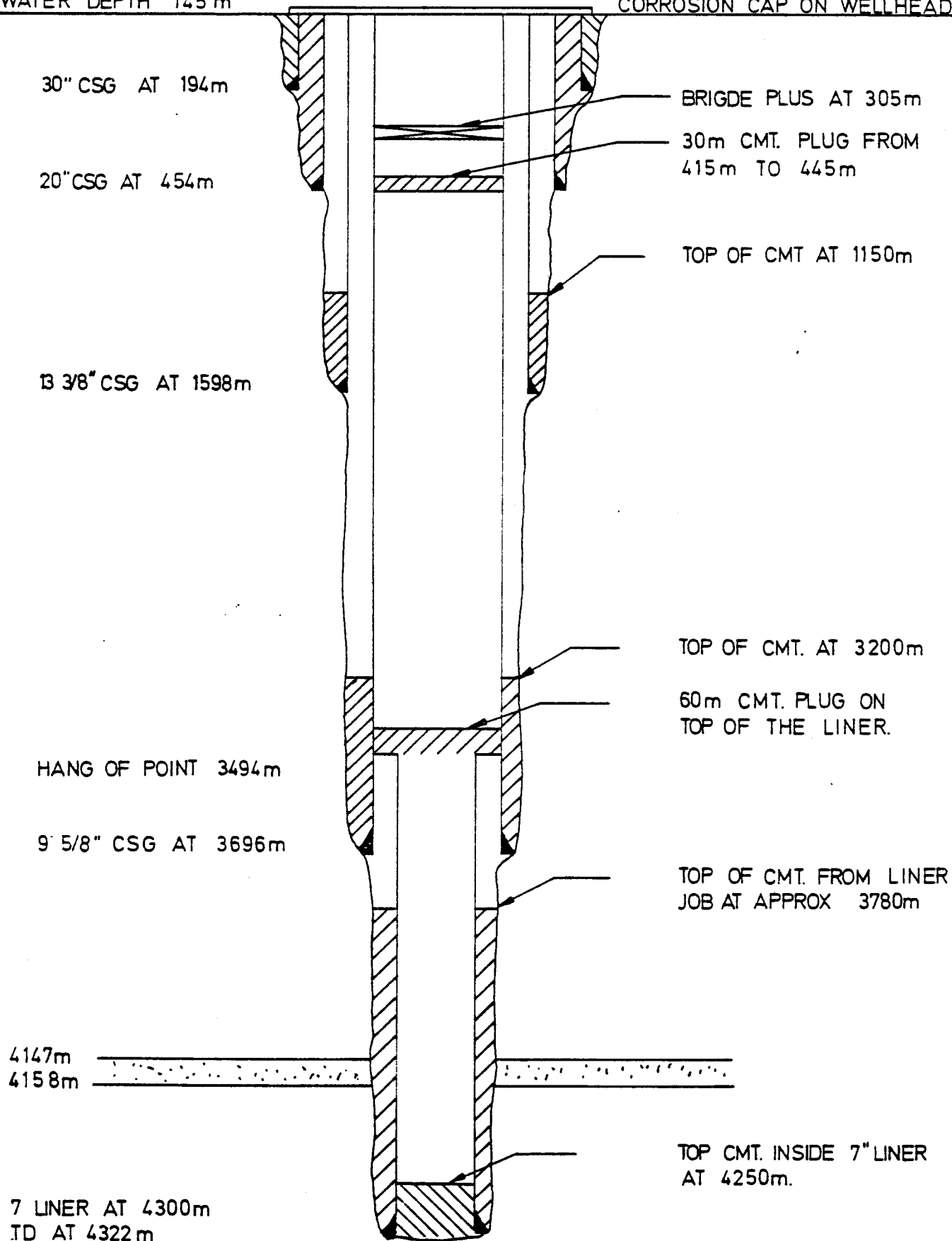
|                               |  |                 |          |
|-------------------------------|--|-----------------|----------|
| Norsk Hydro<br>Drilling Dept. | Mooring line pattern<br>Treasure Seeker<br>Well 15/5-2 | Gr. no.         | Fig.     |
|                               |  | 4               | A 1      |
|                               |  | Date: 22/1-1979 | Dwg. no. |
|                               |  | Sign: TSk/Hes   | 31       |



|                               |   |                 |        |
|-------------------------------|---|-----------------|--------|
| Norsk Hydro<br>Drilling Dept. | Total time distribution.<br>Well 15/5-2 | Gr. no          | Fig.   |
|                               |   | 4               | A 2    |
|                               |   | Date: 22/1-1979 | Dwg no |
|                               |   | Sign: TSk / Hes | 32     |

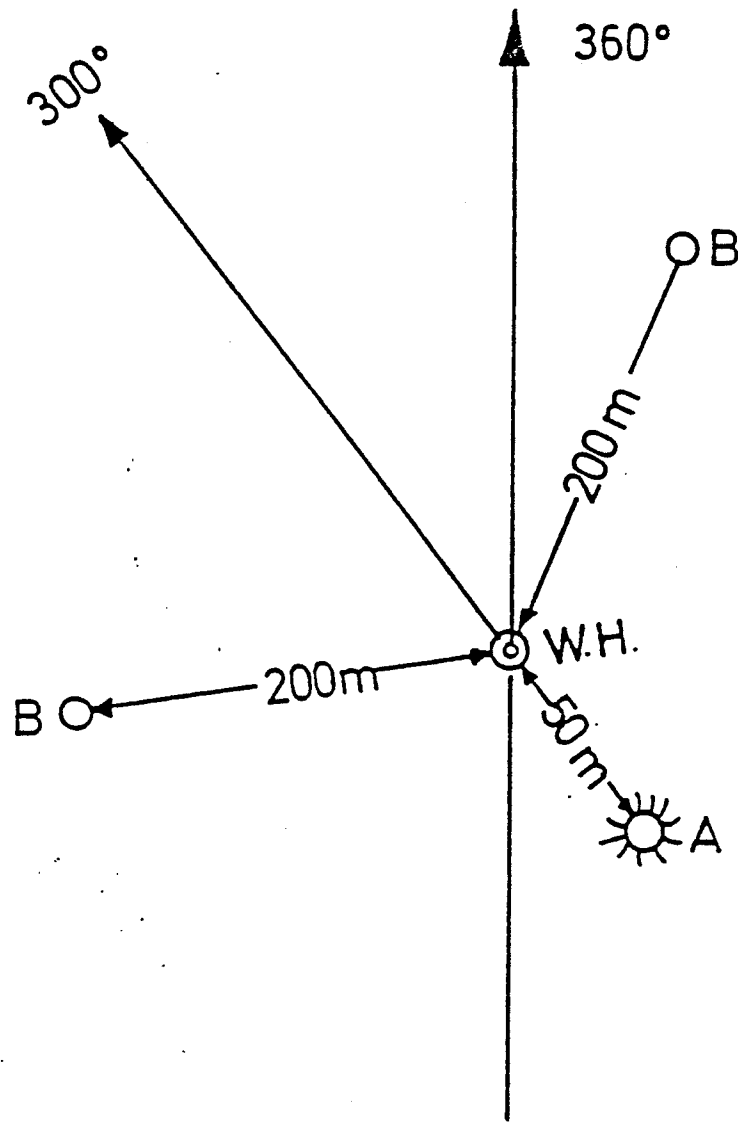
WATER DEPTH 145 m

CORROSION CAP ON WELLHEAD



|                               |   |                              |          |
|-------------------------------|---|------------------------------|----------|
| NORSK HYDRO<br>DRILLING DEPT. | TEMPORARY ABANDONMENT<br>OF WELL 15/5-2 | GR. NO.                      | FIG      |
|                               |   | 4                            | A-3      |
|                               |   | DATE: 21.02.79.<br>SIGN: T.B | DWG. NO. |
|                               |   |                              | 37       |





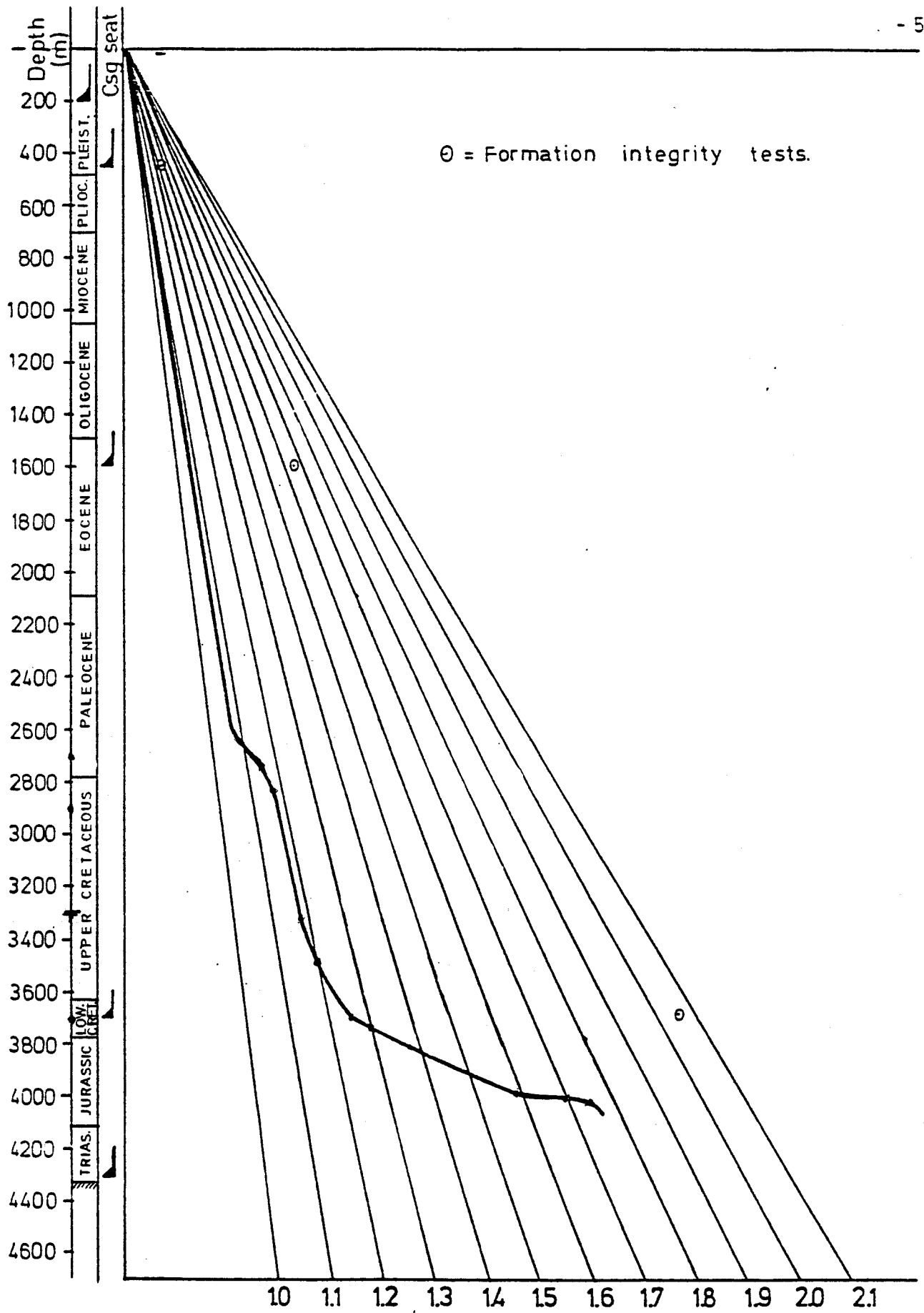
WELLHEAD POSITION :  $58^{\circ} 38' 36.7''$  N  
 $1^{\circ} 36' 16.5''$  E

W.H.: WELLHEAD

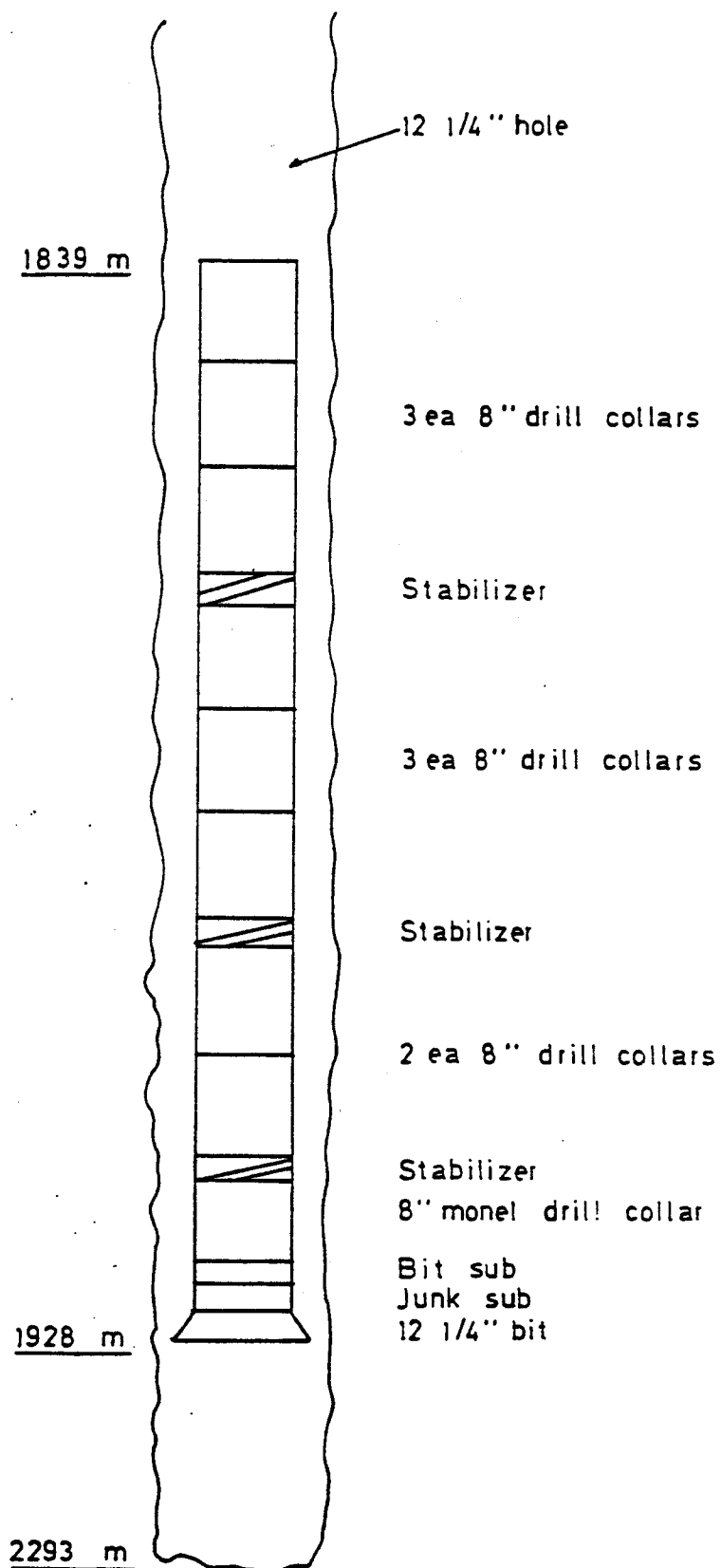
A: 3 WEIGHTS, BUOY W/SIGNAL LIGHTS AND REFLECTOR

B: 3 WEIGHTS, BUOY W/SIGNAL LIGHTS.

|                               |   |                                 |               |
|-------------------------------|---|---------------------------------|---------------|
| NORSK HYDRO<br>DRILLING DEPT. | MARKING BUOY SYSTEM<br>WELL 15/5 - 2<br>(HORIZONTAL VIEW) | GR.NO.<br>4                     | FIG.<br>A-4   |
|                               |   | DATE: 8.3.1979<br>SIGN: TSK/HES | DWG.NO.<br>27 |



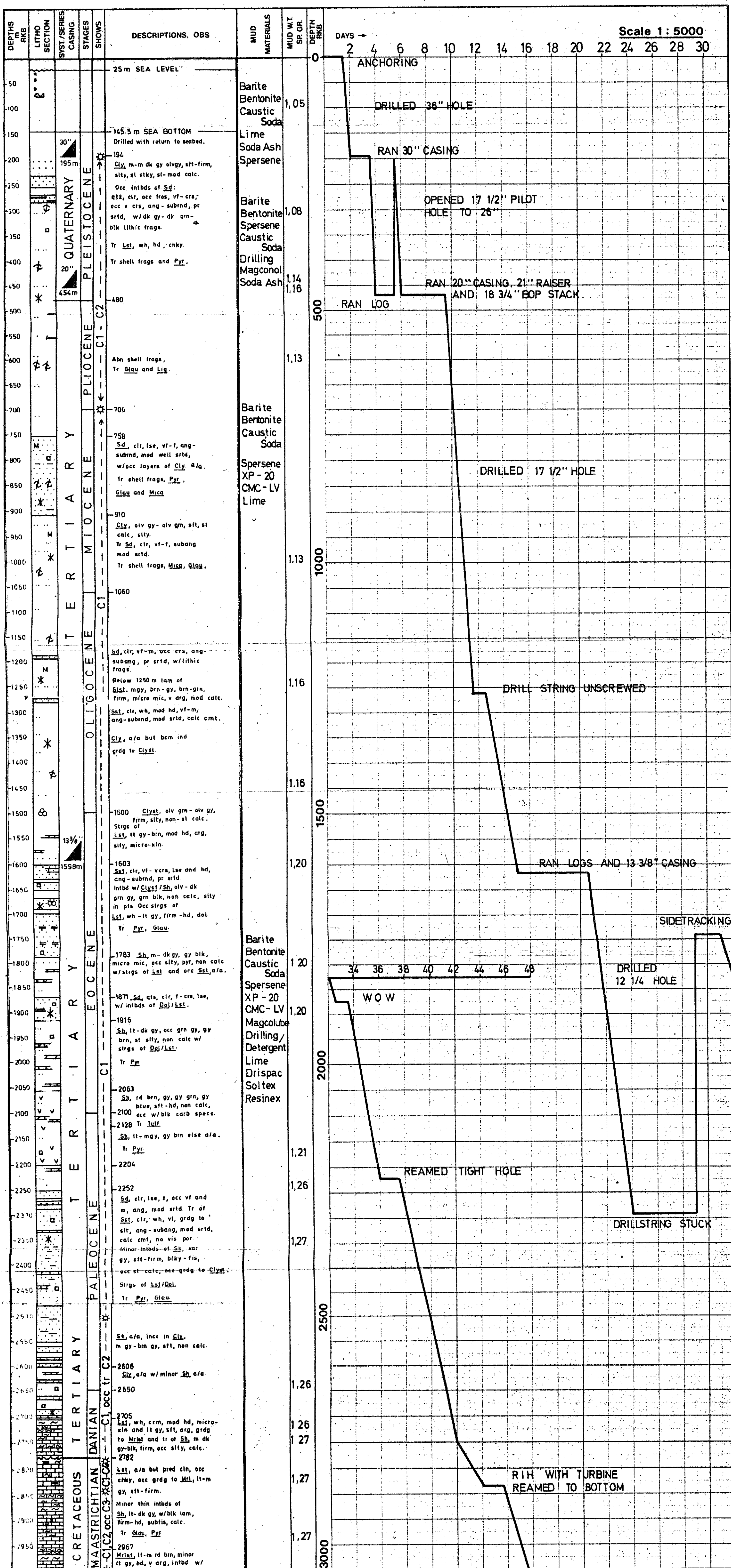
|                                  |  |                                  |                |
|----------------------------------|--|----------------------------------|----------------|
| Norsk Hydro as<br>Drilling Dept. | Pore pressure and for-<br>mation integrity test<br>result on well 15/5-2 | Gr. no.                          | Fig.           |
|                                  |  | 4                                | A-5            |
|                                  |  | Date: 30/1-1979<br>Sign: TSk/Hes | Dwg. no.<br>35 |



|                               |  |                                 |                |
|-------------------------------|--|---------------------------------|----------------|
| Norsk Hydro<br>Drilling Dept. | Fish left in the hole<br>on well 15/5- 2 | Gr. no.                         | Fig.           |
|                               |  | 4                               | A- 6           |
|                               |  | Date: 8/3-1979<br>Sign: TSk/Hes | Dwg. no.<br>36 |

OPERATOR : Norsk Hydro  
 COORDINATES : 58° 38' 36.7" N  
 1° 36' 16.5" E

SPUD IN : August 16, 1978  
 WELL COMPL: December 12, 1978  
 RIG : Treasure Seeker  
 WATER DEPTH : 120.5 m MSL  
 RKB to MSL : 25 m  
 RKB to SEABED: 145.5 m





Norsk Hydro

Oslo - Norway

## DRILLING PROGRESS, WELL: 15/5-2

(CONTINUED)

