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FORMATION FACTOR TESTS
STATOIL PETROPHYSICS LAB.

STATOIL WELL ██████████
REPORT DATE: 30/5-77.

OBJECT

To find a relationship of the kind. $F = a\phi^{-m}$ from physical measurements of plug samples of varying ϕ .

INTRODUCTION

From plugs with a wide range of porosity, Formation Factor (F) tests were done while the plugs were saturated in brine, equivalent to well 15/9-1 formation water concentration.

By using certain useful cross-plot techniques to eliminate spurious effects, a line of the equation

$$F = \phi^{-1.75} \text{ (LAB.CONDITIONS)}$$

was curve - fitted to the points.

A discussion on various cross-plots follows, and a comparison of independent (STATEX) ϕ and Grain Density measurements is made.

EXPERIMENTAL PROCEDURE

After cleaning and extraction of 53 plugs, permeabilities in air, and porosities according to Boyle's Law method ($\phi_{B.L.}$) were found.

From these, 23 plugs with a wide range in $\phi_{B.L.}$ were selected for Formation Factor tests, measured with a brine solution of 90,000 ppm. RaCl, approximately equivalent to formation water concentration, which had been permeating the plugs after vacuum extraction, and held for 24 hours under 1000 psi. pressure.

ϕ saturation was measured as a confirmation of $\phi_{B.L.}$, and the Formation Factor tests were checked successfully for repeatability.

RESULTS

$\phi_{B.L.}$ vs. F was plotted for all 23 plugs (fig 1). Much scatter was observed, but, on further investigation with $\phi_{B.L.}$ vs. f_B LAB cross-plot (fig 2), could be attributed to points which contain amounts of Dolomite.

If these points are eliminated from fig 1, we obtain the resultant plot, fig 3, which, using curve - fitting technique, gives an equation

$$F = \phi^{-1.75}$$

with coefficient of determination $r^2 = 0.99$

The F reading is affected by the dolomite content of the sandstone plug, and gives an irrational reading for highly dolomitic sandstones.

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Grain Density ($=\rho_{ma}$ LAB) and Equivalent Bulk Density in situ ($=\rho_B$ LAB) calculations.

$$\rho_{ma} \text{ LAB} = W/V_g$$

$$\rho_B \text{ LAB} = \frac{(V_B - V_g) \rho_{mf} + W}{V_B}$$

where W = Dry weight of plug (g)

V_g = Grain volume from $\phi_{B.L.}$ (cc)

V_B = Bulk Volume (cc)

ρ_{mf} = density of mud filtrate, (g/cc) assumed to be the predominant fluid in the invaded zone, where the log value of ρ_B is measured.

These values were calculated, and (fig 4) $\rho_B \text{ Log vs } \rho_B \text{ LAB}$ was plotted with $\phi_{B.L.}$ vs $\rho_B \text{ LAB}$ (Fig 2)

Fig 2. illustrates that most of the points fall near the sandstone line, and the limestone and Dolomite points plot to the north-east (N-E) in increasing dolomite content; shale tends to pull the points slightly to the N-E direction off the clean sandstone line, most of the shale points having heavier minerals than basic shale which has a density of 2.52 - 2.55 g/cc. for 15/9-1.

Fig. 4 is useful in identifying the hydrocarbon effect on the ρ_B LOG values. The higher density dolomite points show deviation from the 45° line, due to the depth-shifting process limits of accuracy. This plot is also illustrated in figs 5, 6, & 7.

NB Matching of logs and cores was done by relating a 1/200 core description log with the neutron-density log, and finding obvious shale and coal correlation points - good correlation was found throughout, considering that the log was from a sidetracked hole about 10 m. away horizontally from the original cored hole.

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$\phi_{B.L}$ vs ϕ_{SAT} (Fig 8) on 24 points was drawn using formula

$$\phi_{SAT} = \frac{W_{wet} - W_{dry} \times 100}{SAT \text{ FLUID} \times VB}$$

The cleanest points plotted on the 45° line, and we obtain an idea of clay-swelling properties referring to the points to the N-W of the clean line.

FIG. 9 is a plot of DRY CORE ϕ (ie, $\phi_{B.L.}$) against ϕ EFFECTIVE LOG (ie, the ϕ value from the GOLOG program with the shale and hydrocarbon effect taken off.

Generally the trend is for the more shaley cores to plot to the N.W. of the 45° LINE.

This suggests that there is a tendency for the drying process involed in the core porosity analysis to increase the ϕ value due to the drying out of the water absorbed to the surface of the clays.

FIG. 8, $\phi_{DRY \text{ CORE}}$ vs ϕ_{SAT} , shows a similar effect.

This exageration of the Dry Core ϕ should be taken into account in Formation Factor versus porosity tests, and also in Capillary Pressure experim~~ents~~ts.

The need for humidity - controlled ϕ measurements, and exact correlation between log and lab. work is emphasised here.

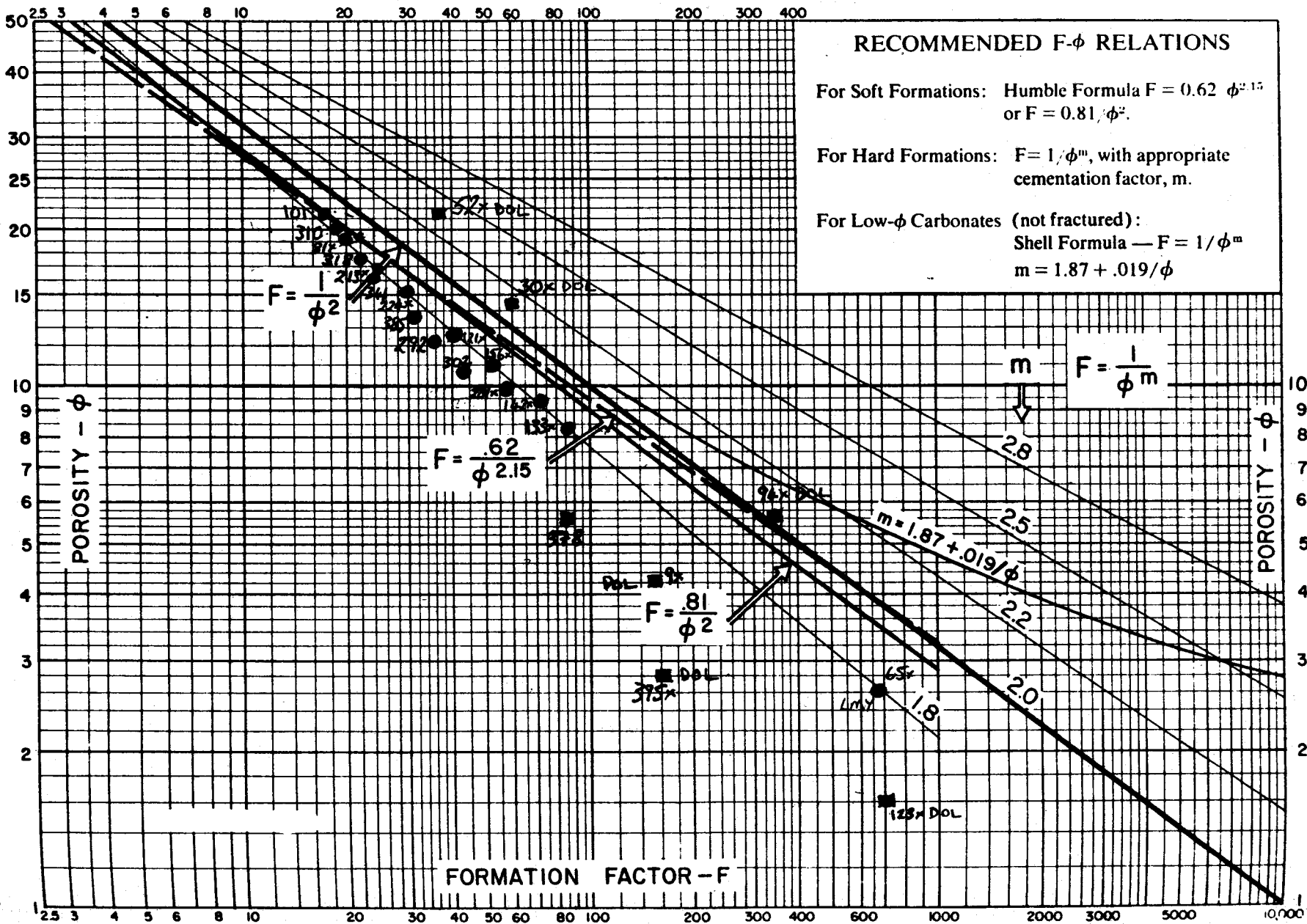
————— • —————
 ϕ 's from STATOIL and STATEX measured on the same 13 plugs, were plotted beside each other (Fig 10), and fair agreement was observed.

————— • —————
 For zones of obvious hydrocarbon content, as selected by CNL/FDC log, the average ρ_{MA} equals 2.65 g/cc with range of points between 2.64 and 2.67 g/cc, apart from one shaley points of 2.69 g/cc (22 plugs).

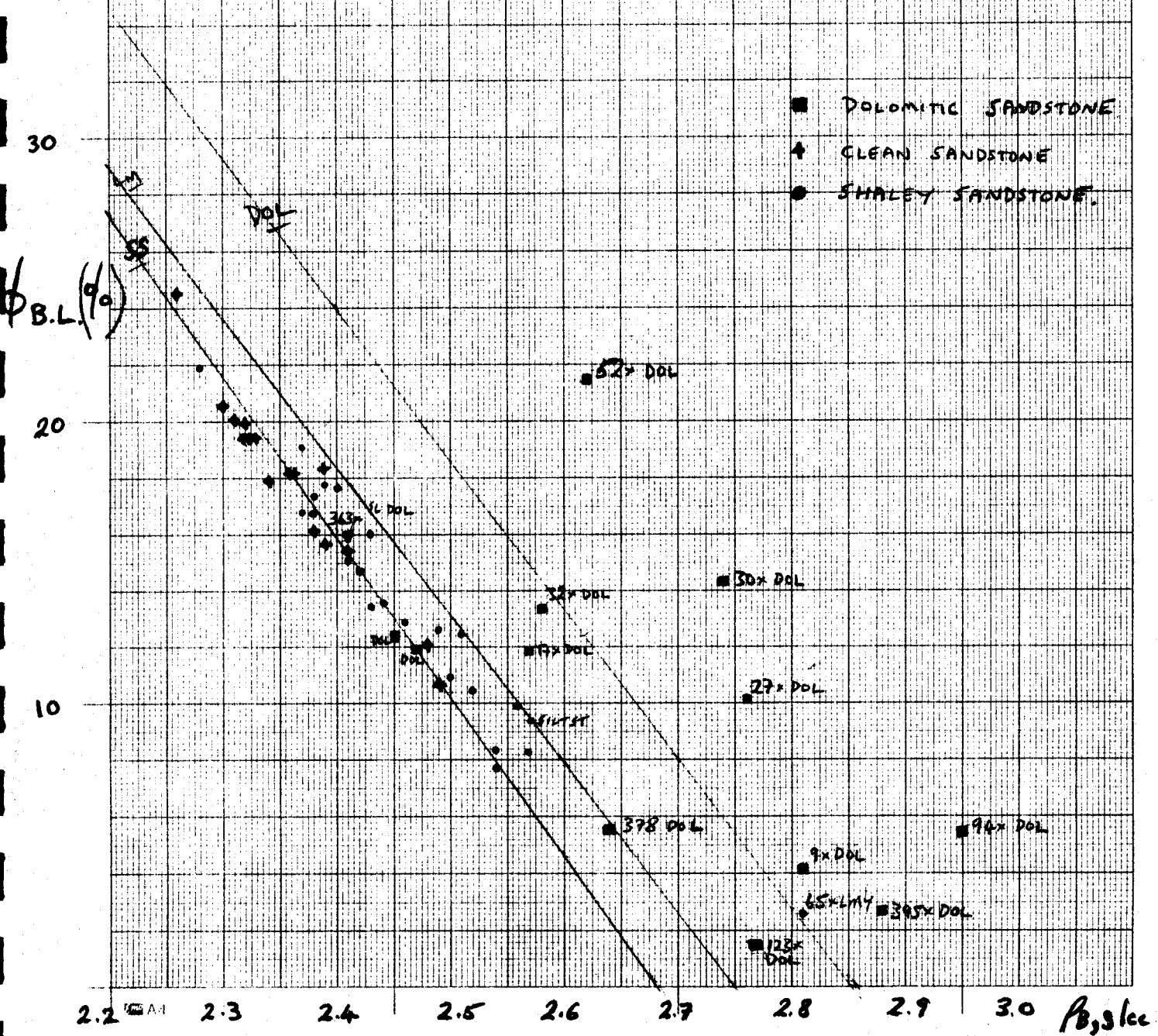
For the 13 plugs analysed by STATEX and STATOIL, the variation of ρ_{MA} from equality (fig 11) was a function of the slight differences in measured ϕ .

- DOLOMITIC POINTS
- SANDSTONE POINTS

FORMATION FACTOR VERSUS POROSITY [Fig 1] [23 plugs]



$\phi_{B.L.}$ vs ρ_B LAB [53 plugs] (fig 2)

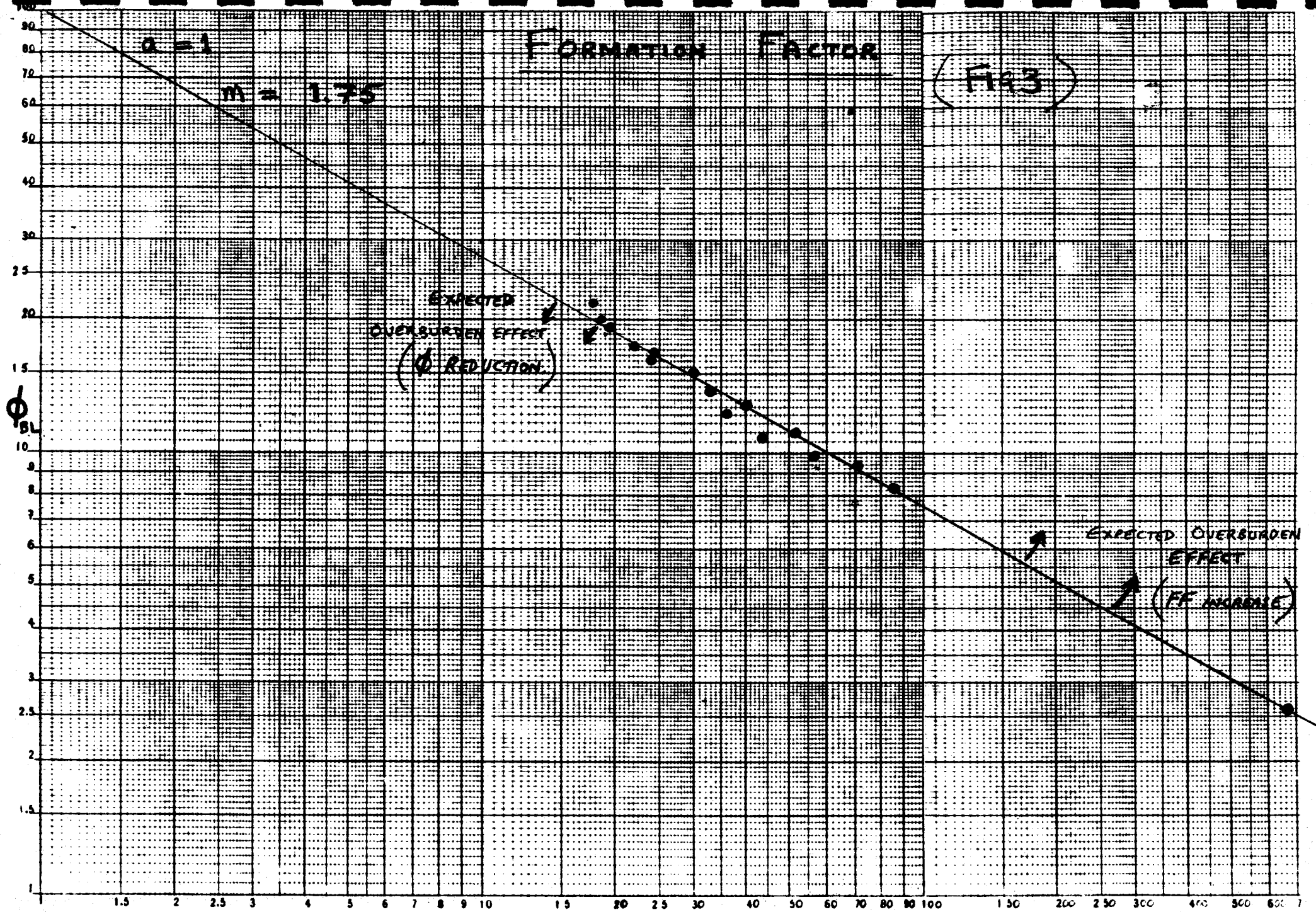


FORMATION FACTOR

$a = 1$

$m = 1.75$

(FF=3)



F.F.

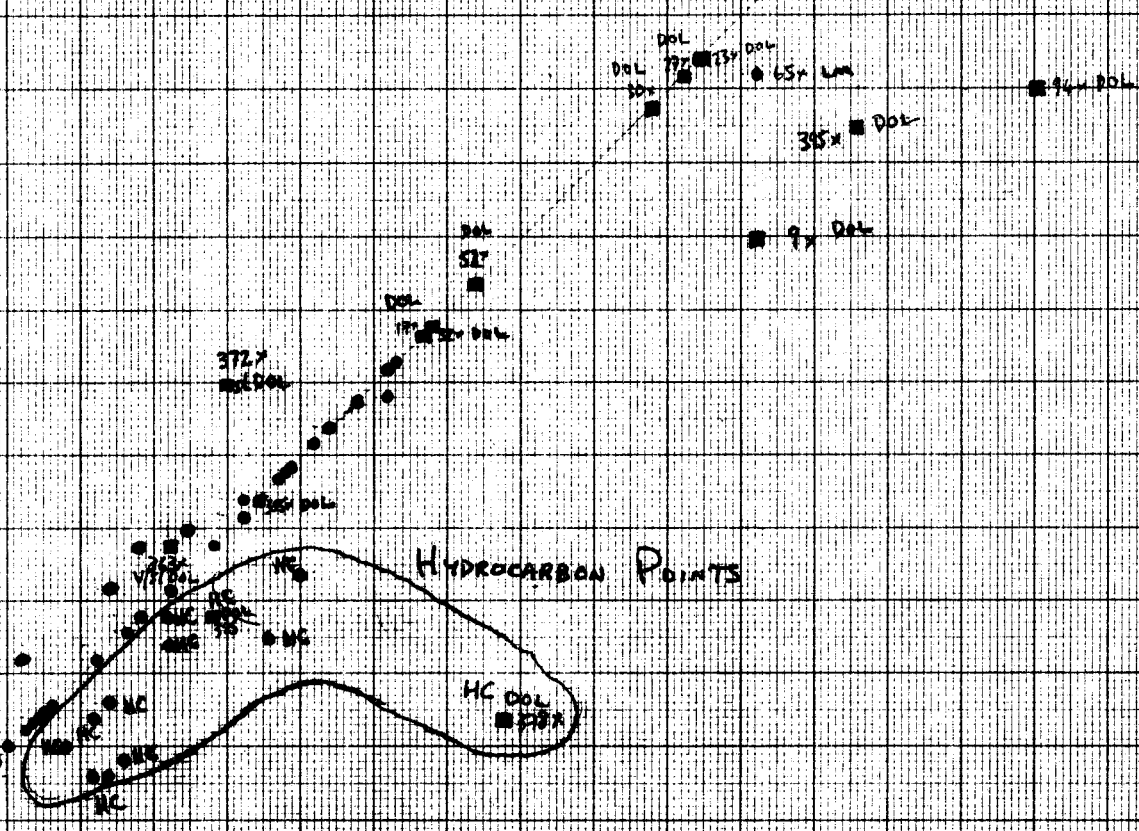
ρ_B LOG vs. ρ_B LAB (fig 4) [53 plugs]

(after depth matching)

- DOLOMITIC POINTS
- SANDSTONE / SHALEY SANDSTONE POINTS

ρ_B LOG
3.0
2.9
2.8
2.7
2.6
2.5
2.4
2.3
2.2

2.2 ρ_B LAB 2.3 2.4 2.5 2.6 2.7 2.8 2.9 3.0



1195

T = 215°F

Rmf = 0.228 @ 55°F, Rm = 0.352 @ 53°F.

8 1/2" G.R. 100 1.95 ————— P_B LOG ————— 2.45 ● = P_B LAB ————— 2.95

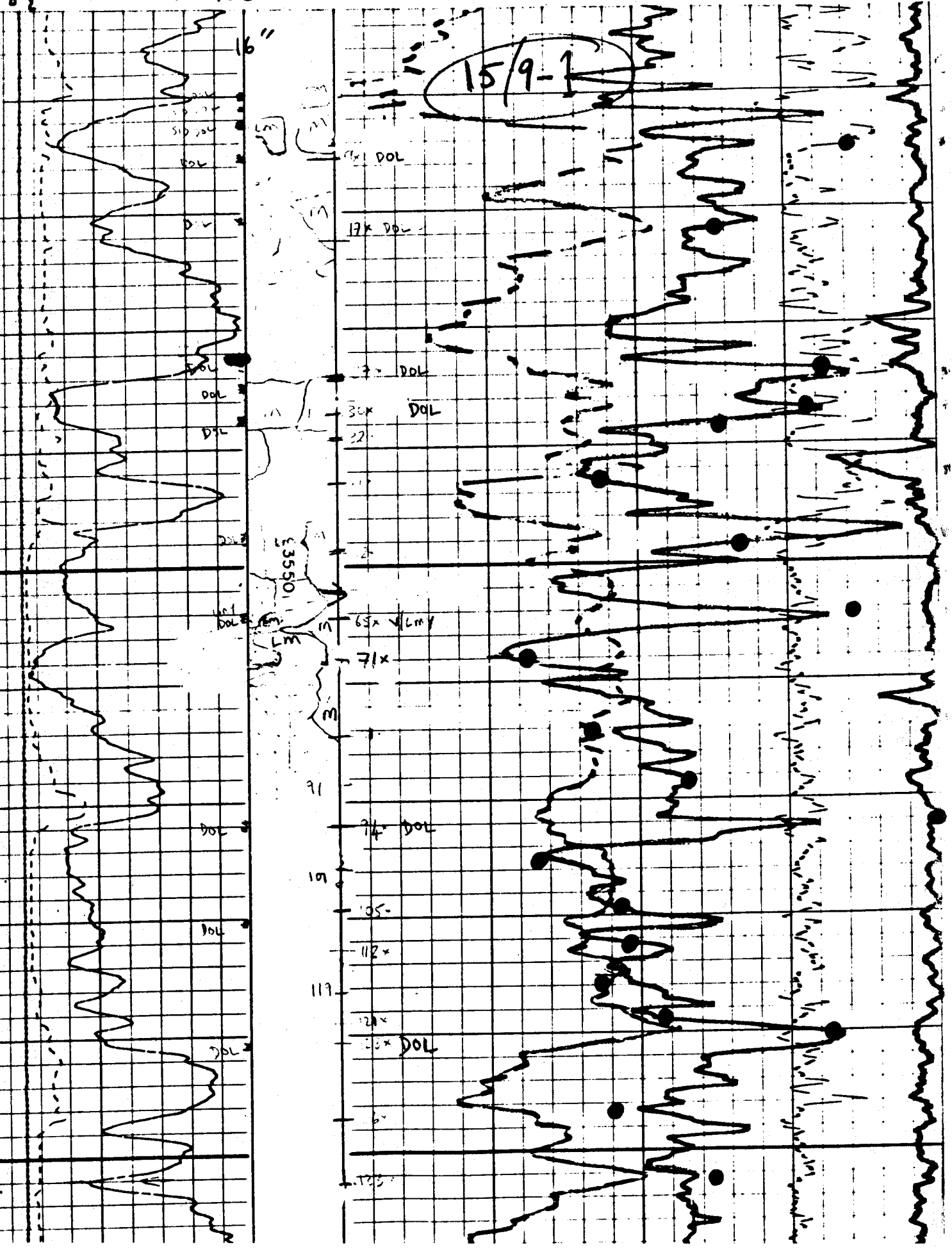


Fig 6

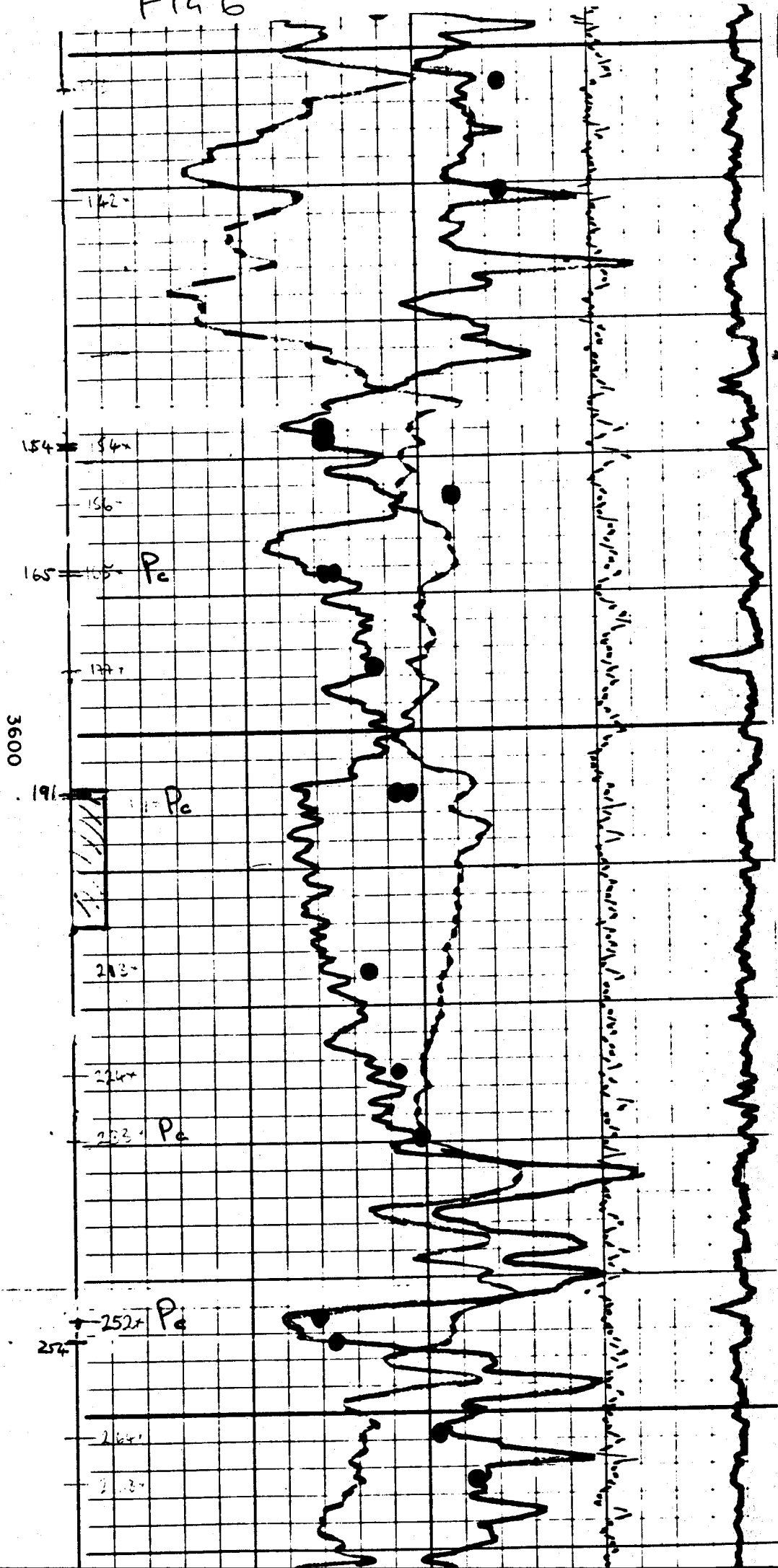
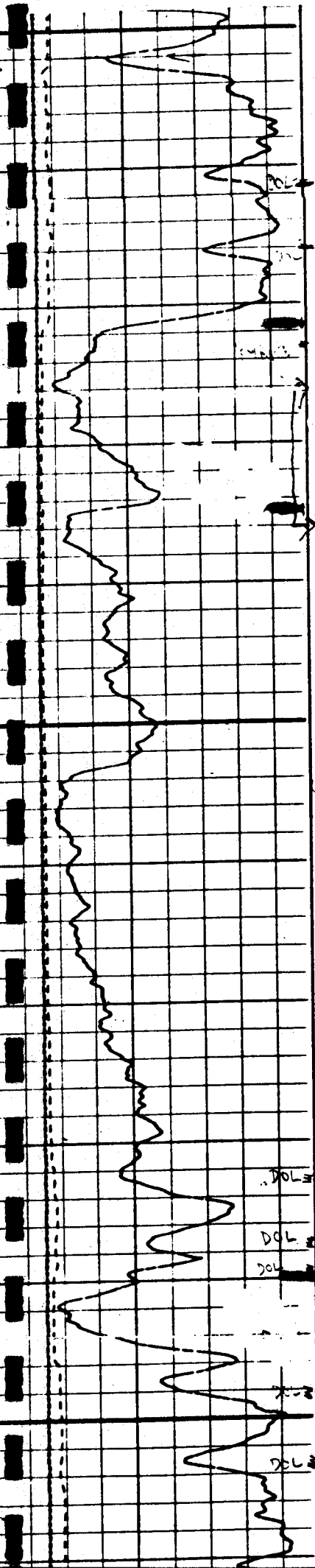
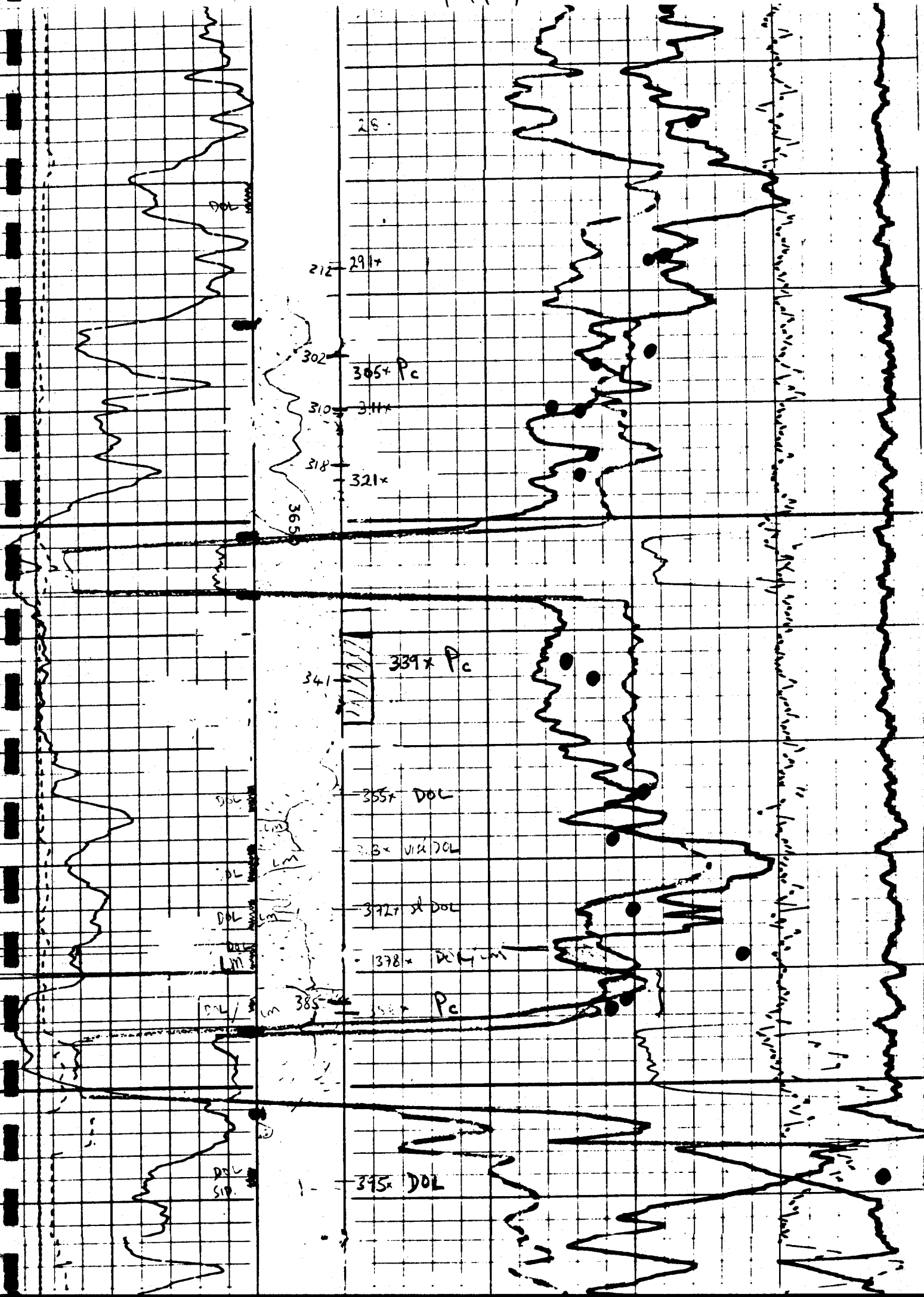


FIG 4



212

291+

302

305 x Pc

310

311 x

318

321 x

365

341

339 x Pc

355 x DOL

373 x DOL

372 x DOL

378 x DOL

385

387 x Pc

395 x DOL

DOL

LM

DOL

LM

DOL

LM

DOL

LM

DOL

DOL

SIP

SENSITIVITY CHECK ON ϕ (FIG 8)

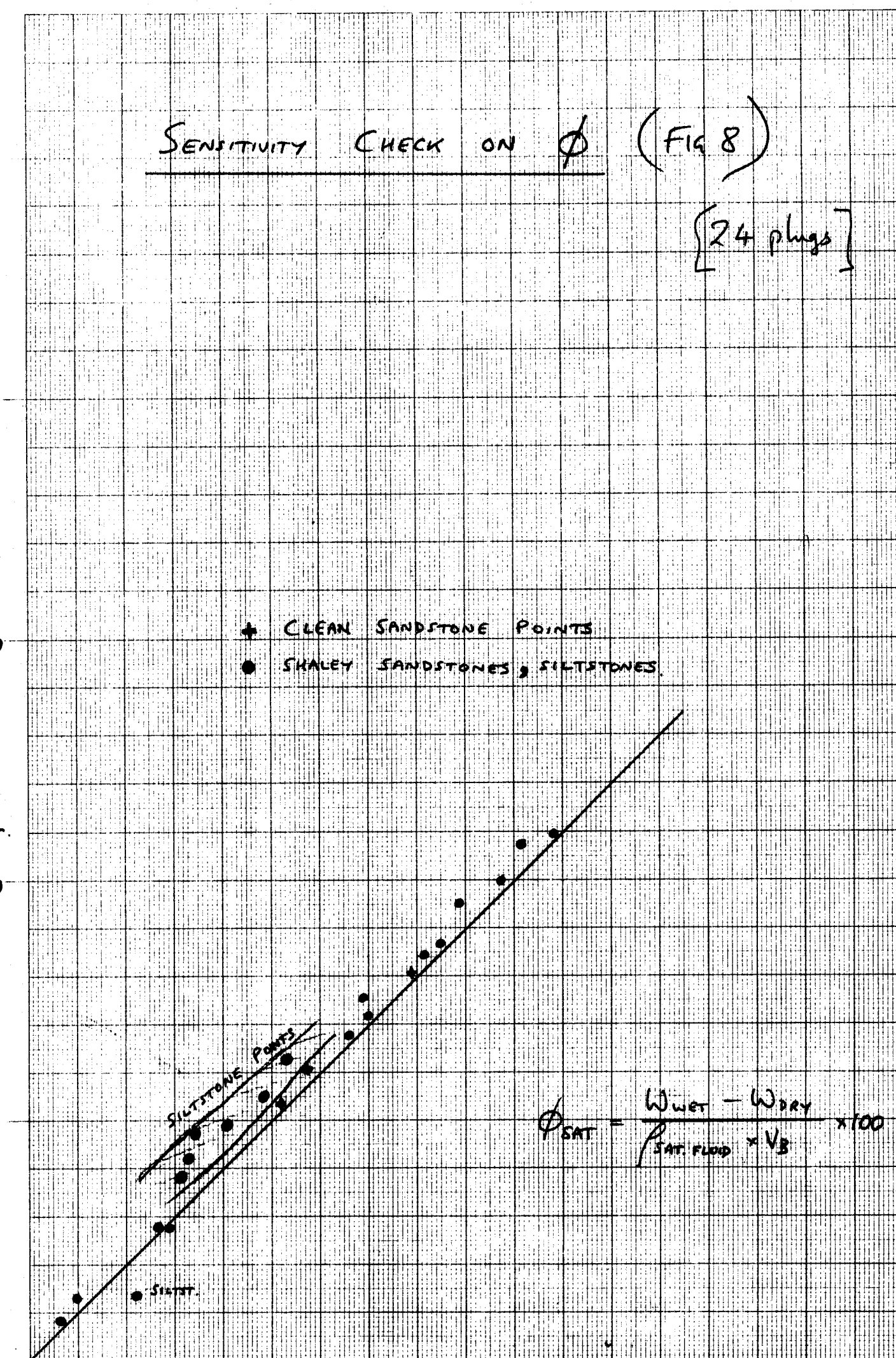
[24 plugs]

- CLEAN SANDSTONE POINTS
- SHALEY SANDSTONES, SILTSTONES

30
B.L.
20
10

SILTSTONE POINTS

$$\phi_{SAT} = \frac{W_{WET} - W_{DRY}}{\rho_{SAT. FLOOD} \times V_B} \times 100$$



(FIG 9.)

DRY CORE ϕ (W, ϕ B.L. LAB)

USI

ϕ EFF. LOG

(ϕ LOG AFTER SHALE AND
HYDROCARBON EFFECT
SUBTRACTION)

(53 plugs)

30

DRY CORE ϕ (P.U.)

(ϕ B.L.)

45° LINE

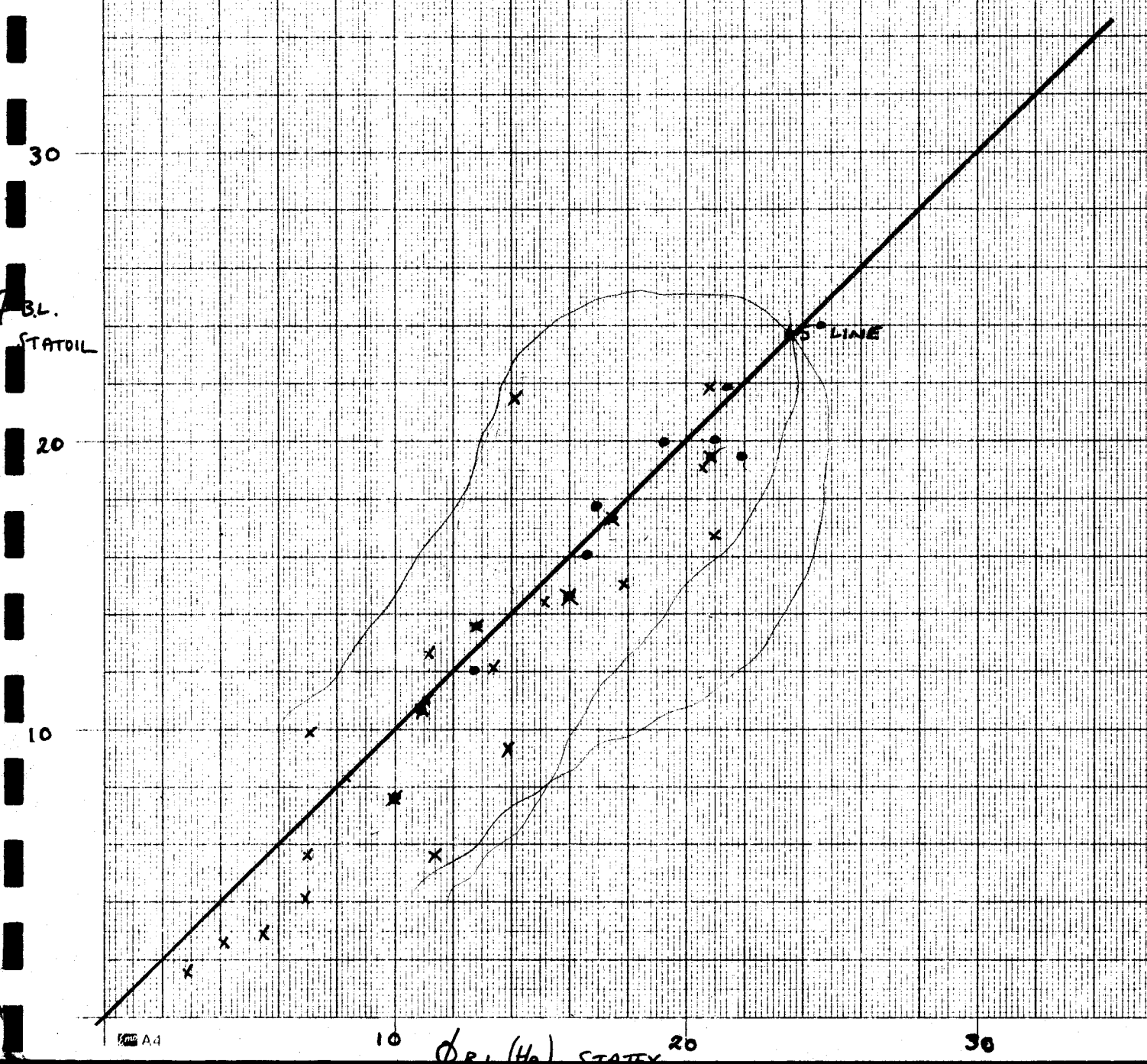
20

10

- + CLEAN SANDSTONE.
- SHALEY SANDSTONE
- DOLOMITIC SANDSTONE

$\phi_{B.L.}$ STATEX VS STATOIL (fig 10)

[13 plugs]



PMA LAB STATOIL VS. PMA LAB. STATEX (FIG 11)

[13 plugs]

PMA LAB
STATOIL

2.7

2.6

2.5

2.4

2.3

2.2

2.2 PMA LAB

2.3

2.4

2.5

2.6

2.7

PMA LAB STATEX

