

**CORE LABORATORIES UK LTD.**

*Petroleum Reservoir Engineering*

**ABERDEEN, SCOTLAND**

**Reservoir Fluid Study**

**for**

**STATOIL**

**Well: 34/10-1 DST 2**

**Flow 2**

**North Sea**

**Norway**

CORE LABORATORIES UK LTD.

*Petroleum Reservoir Engineering*

ABERDEEN, SCOTLAND

4 th December, 1978.

Statoil,  
Lagardsveien 78,  
P.O. Box 300,  
4001, Stavanger,  
Norway.

Attention: Mr. Per Thomassan.

Subject: Reservoir Fluid Analysis  
Well: 34/10-1 DST No. 2  
Flow 2.  
North Sea, Norway.  
Our File Number: RFLA-78059

Gentlemen:

on August 24th 1978, a subsurface sample was collected from the subject well and forwarded to our Aberdeen laboratory. This report presents the results of analyses performed on this sample

A portion of the reservoir fluid was placed in a high pressure visual cell and thermally expanded to the reservoir temperature of 161°F. At this temperature a constant composition expansion was conducted during which a bubble point pressure of 3644 psig was observed. The fluid was then subjected to a differential vaporization, which resulted in the total liberation of 567 cubic feet of gas at 14.73 psia and 60°F. per barrel of residual oil at 60°F., with an associated relative oil volume of 1.256 barrels of saturated oil per barrel of residual oil. In addition at several pressure levels below the observed saturation pressure, oil densities, gas deviation factors, and gas gravities were measured. These data are tabulated on pages two through four and graphically represented on pages five and six.

The viscosity of the reservoir fluid was measured over a wide range of pressures at 161°F., in a rolling ball viscosimeter. The viscosity of the fluid was found to vary from a minimum of 1.08 centipoise at the saturation pressure to a maximum of 3.71 centipoise at atmospheric pressure. The results of the viscosity measurements are tabulated on page seven.

A two-stage flash separation was conducted in the laboratory at the following conditions: 460 psia at 72°F., 15 psia at 60°F. The ratios and factors derived from this test are presented on page nine. Also, gas samples evolved at each stage of separation were collected in the laboratory and analyzed for hydrocarbon composition. These compositions are listed on page ten. In addition, the stock tank oil was collected and analyzed for hydrocarbon composition, using low temperature fractional distillation apparatus. The results of this test are presented on page eleven.

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Statoil.

Page Two.

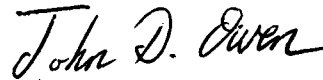
Well: 34/10-1 DST No. 2 Flow 2

Using the experimentally determined compositions of the separator gas and stock tank oil, in conjunction with the factors and ratios derived from the flash separation, we were able to calculate a well stream composition. The resulting calculated well stream composition is given on page twelve.

Thank you for the opportunity to perform this fluid study. It is always a pleasure to be of service to Statoil, and should you have any questions or if we may be of further assistance, please do not hesitate to contact us.

Very truly yours

Core Laboratories U.K. Limited.



JDO/rmb:  
7cc/Addressee:

John D. Owen.  
Supervisor.

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Company STATOIL Date Sampled 24th August, 1978.  
 Well 34/10-1 DST 2 Flow 2 County NORTH SEA  
 Field ..... State NORWAY.

**FORMATION CHARACTERISTICS**

Formation Name .....  
 Date First Well Completed ..... 19.....  
 Original Reservoir Pressure ..... PSIG @ .....Ft.  
 Original Produced Gas-Liquid Ratio ..... SCF/Bbl  
     Production Rate ..... Bbl/Day  
     Separator Pressure and Temperature ..... PSIG..... ° F.  
     Oil Gravity at 60°F. .... ° API  
 Datum ..... Ft. Subsea  
 Original Gas Cap .....

**WELL CHARACTERISTICS**

Elevation ..... Ft.  
 Total Depth ..... Ft.  
 Producing Interval 1839-1844 ..... M  
 Tubing Size and Depth 3½ In. to 1835 ..... M  
 Productivity Index ..... Bbl/D/PSI @ ..... Bbl/Day  
 Last Reservoir Pressure ..... PSIG @ .....Ft.  
     Date ..... 19.....  
     Reservoir Temperature ..... ° F. @ ..... Ft.  
     Status of Well .....  
     Pressure Gauge .....  
 Normal Production Rate ..... Bbl/Day  
     Gas-Oil Ratio ..... SCF/Bbl  
     Separator Pressure and Temperature ..... PSIG..... ° F.  
     Base Pressure ..... PSIA  
 Well Making Water ..... % Cut

**SAMPLING CONDITIONS**

Sampled at 1530 ..... M  
 Status of Well .....  
     Gas-Oil Ratio ..... SCF/Bbl  
     Separator Pressure and Temperature ..... PSIG..... ° F.  
     Tubing Pressure ..... PSIG  
     Casing Pressure ..... PSIG  
 Sampled by FLOPETROL .....  
 Type Sampler .....

**REMARKS :**

Received cylinder 20475-99  
 Ambient bubble point is 3268 psig at 66°F.

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Well 34/10-1 DST 2 .....

Flow 2

**VOLUMETRIC DATA OF ..... Reservoir Fluid SAMPLE**

1. Saturation pressure (bubble-point pressure) ..... 3644 PSIG @ ..... 161 °F.
2. Specific volume at saturation pressure : ft<sup>3</sup>/lb ..... 0.02082 ..... @ ..... 161 °F.
3. Thermal expansion of saturated oil @ ..... 5000 ..... PSI =  $\frac{V @ 161 \text{ °F}}{V @ 67 \text{ °F}} = 1.03837$
4. Compressibility of saturated oil @ reservoir temperature : Vol/Vol/PSI :
  - From ..... 5000 ..... PSI to ..... 4600 ..... PSI = .....  $7.87 \times 10^{-6}$  .....
  - From ..... 4600 ..... PSI to ..... 4200 ..... PSI = .....  $7.90 \times 10^{-6}$  .....
  - From ..... 4200 ..... PSI to ..... 3644 ..... PSI = .....  $8.15 \times 10^{-6}$  .....

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Well ...34/10-1 DST 2 Flow 2.....

Pressure-Volume Relations at ...161... °F.

Pressure PSIG	Relative Volume (1)	Y Function (2)
5000	344.73	0.9892
4800	330.94	0.9907
4600	317.16	0.9923
4400	303.37	0.9939
4200	289.58	0.9955
4100	282.69	0.9963
4000	275.79	0.9971
3900	268.89	0.9979
3800		0.9987
3700	255.11	0.9996
3644		1.0000
3620		1.0012
3561		1.0041
3448		1.0107
3290		1.0208
3019		1.0413
2713		1.0723
2412		1.1141
2092		1.1771
1795		1.2615
1496		1.3887
1235		1.5587
1019		1.7716
760		2.2010
552		2.8412
395		3.9115

(1) Relative Volume :  $V/V_{sat}$  is barrels at indicated pressure per barrel at saturation pressure.

$$(2) \text{ Y Function} = \frac{(P_{sat}-P)}{(P_{abs})(V/V_{sat}-1)}$$

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 Well ..... 34/10-1 DST 2 Flow 2 .....

Differential Vaporization at 161 °F.

Pressure PSIG	Solution Gas/Oil Ratio (1)	Relative Oil Volume (2)	Relative Total Volume (3)	Oil Density gm/cc	Deviation Factor Z	Gas Formation Volume Factor (4)	Incremental Gas Gravity
3644 251.2	567 100.8	1.256	1.256	0.7694			
3300 227.53	514 91.38	1.235	1.281	0.7762	0.906	0.00481	0.631
2900 199.95	453 80.53	1.213	1.321	0.7839	0.882	0.00532	0.629
2500 172.37	393 69.87	1.190	1.379	0.7922	0.874	0.00611	0.628
2100 144.79	332 59.02	1.168	1.473	0.8000	0.877	0.00729	0.628
1700 117.21	274 48.71	1.147	1.623	0.8075	0.890	0.00913	0.629
1300 89.63	212 37.69	1.123	1.891	0.8171	0.908	0.01215	0.630
900 62.05	152 27.02	1.101	2.424	0.8254	0.931	0.01790	0.641
500 34.47	92 16.36	1.079	3.850	0.8336	0.959	0.03276	0.662
153 10.55	33 5.87	1.058	10.887	0.8421	0.987	0.10335	0.738
0	0	1.044		0.8463			1.009

At 60 °F = 1.000

over liberated.  $B_{oil} = B_{oid} \cdot \frac{V}{V_{oil}}$   
 $P [bar]$

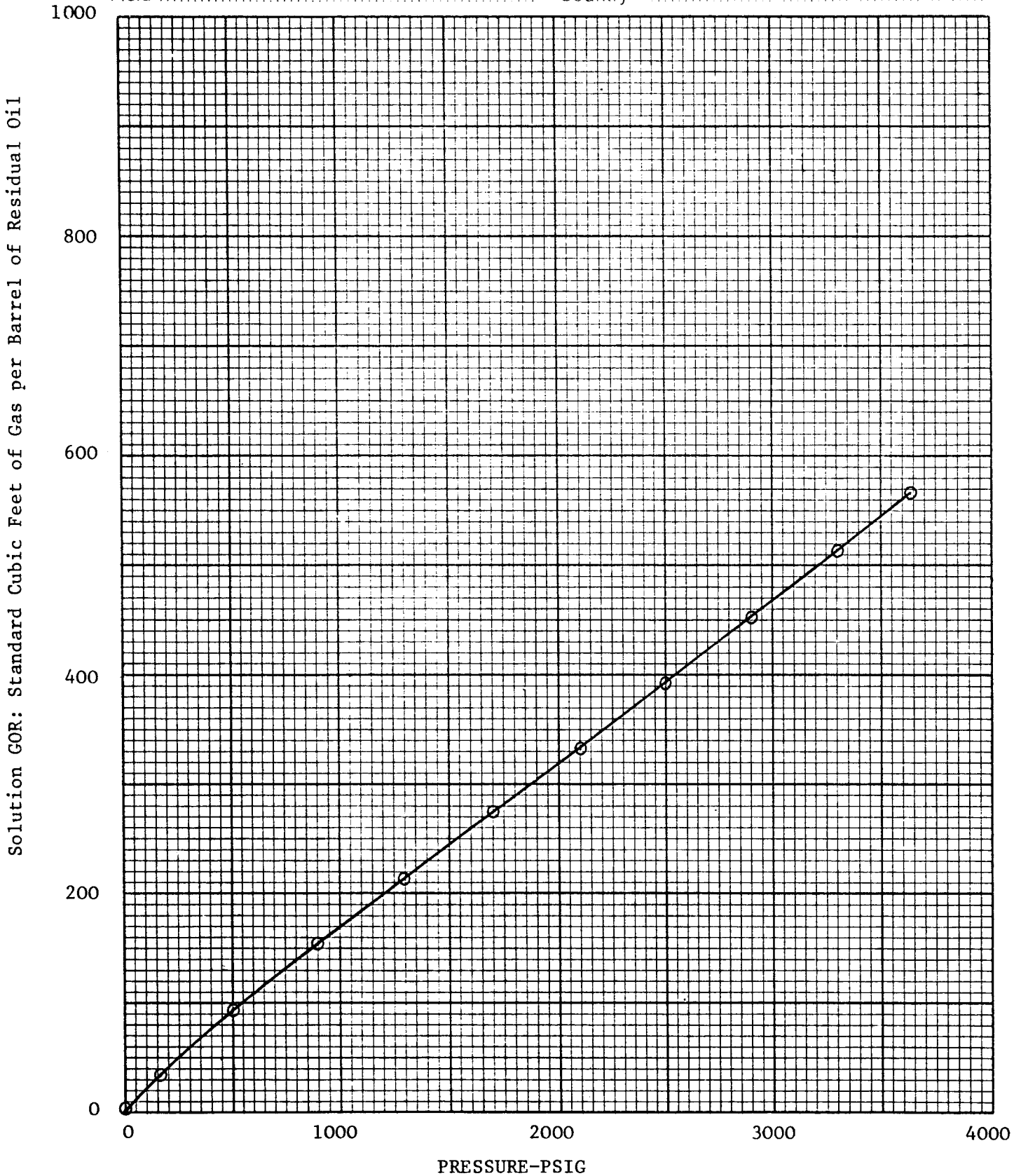
Gravity of residual oil = ..... 28.5 ..... ° API @ 60°F.

- (1) Cubic feet of gas at 14.73 psia and 60 °F. per barrel or residual oil at 60°F.
- (2) Barrels of oil at indicated pressure and temperature per barrel of residual oil at 60°F.
- (3) Barrels of oil plus liberated gas at indicated pressure and temperature per barrel of residual oil at 60°F.
- (4) Cubic feet of gas at indicated pressure and temperature per cubic foot at 14.73 psia and 60°F.

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Differential Vaporization of Reservoir Fluid at 161°F.

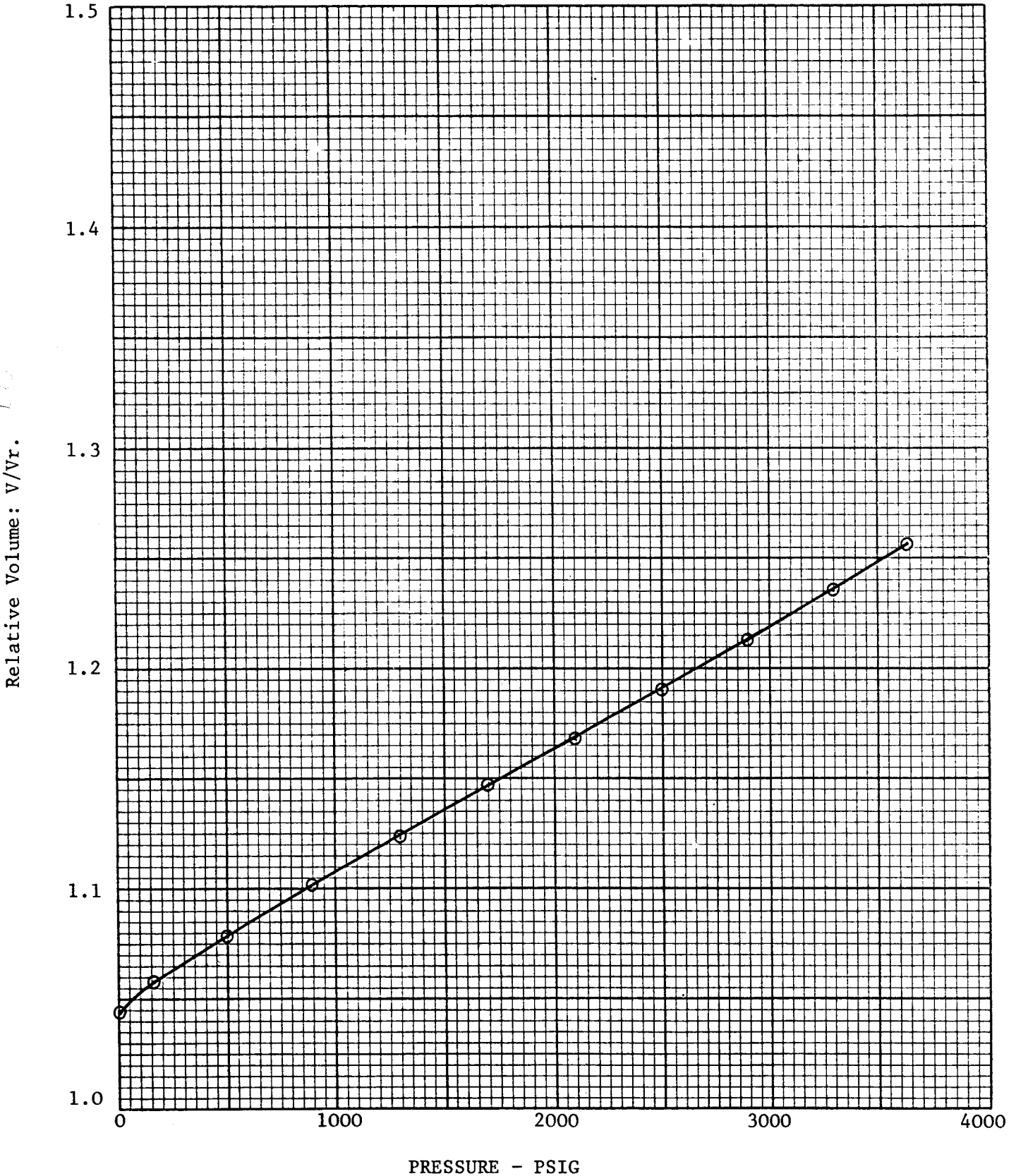
Company	STATOIL	Formation	
Well	34/10-1 DST 2 Flow 2	Province	NORTH SEA
Field		Country	NORWAY





Differential Vaporization of Reservoir Fluid at 161°F.

Company	STATOIL	Formation	
Well	34/10-1 DST 2 Flow 2	Province	NORTH SEA
Field		Country	NORWAY



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Well ..... 34/10-1 DST 2 Flow 2 .....

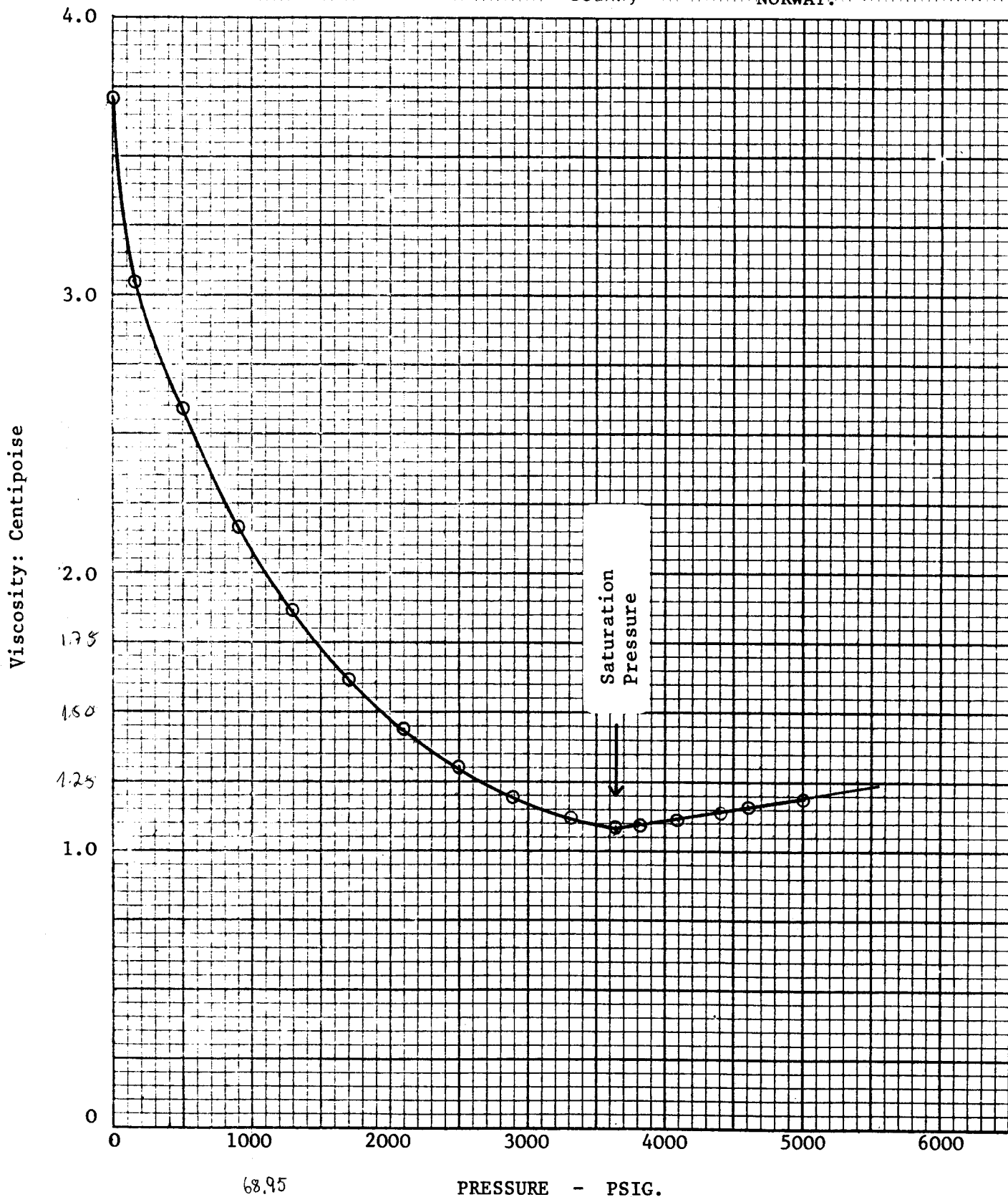
Viscosity Data at 161 °F.

<u>Pressure PSIG</u>	<u>Oil Viscosity Centipoise</u>	<u>Calculated Gas Viscosity Centipoise</u>	<u>Oil/Gas Viscosity Ratio</u>
5000	344.74	1.19	
4600	317.16	1.16	
4400	303.37	1.14	
4100	282.68	1.11	
3800	262.00	1.09	
3644	251.24	1.08	
3300	227.53	1.11	0.0208
2900	199.95	1.19	0.0196
2500	172.37	1.30	0.0182
2100	144.79	1.44	0.0169
1700	117.21	1.62	0.0157
1300	89.63	1.86	0.0147
900	62.05	2.16	0.0138
500	34.47	2.59	0.0131
160	11.03	3.05	0.0123
0		3.71	

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Viscosity of Reservoir Fluid at 161°F.

Company STATOIL  
Well 34/10-1 DST 2 Flow 2  
Field  
Formation  
Province NORTH SEA  
Country NORWAY.



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Well ...34/10-1 DST 2 Flow 2

**SEPARATOR TESTS OF** Reservoir Fluid ..... **SAMPLE \***

SEPARATOR PRESSURE PSIA	SEPARATOR TEMPERATURE ° F.	GAS/OIL RATIO (1)	GAS/OIL RATIO (2)	STOCK TANK GRAVITY ° API @ 60° F.	FORMATION VOLUME FACTOR (3)	SEPARATOR VOLUME FACTOR (4)	SPECIFIC GRAVITY OF FLASHED GAS
460	72	415	443			1.067	0.626 +
to							
0	60	115 530	115	29.2	1.248	1.000	0.824 +

\* Flow 2 (cylinder 20475-99)

+ Collected and analyzed for hydrocarbons.

- (1) Gas/Oil Ratio in cubic feet of gas @ 60° F. and .....14.73..... PSI absolute per barrel of oil @ indicated pressure and temperature.
- (2) Gas/Oil Ratio in cubic feet of gas @ 60° F. and .....14.73..... PSI absolute per barrel of stock tank oil @ 60° F.
- (3) Formation Volume Factor is barrels of saturated oil @ ...3644.. PSI gauge and ....161.... ° F. per barrel of stock tank oil @ 60° F.
- (4) Separator Volume Factor is barrels of oil @ indicated pressure and temperature per barrel of stock tank oil @ 60° F.

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Well ...34/10-1.DST..2.Flow 2

**HYDROCARBON ANALYSIS OF MULTI-STAGE SEPARATOR GASES**

<u>Components:</u>	<u>460 PSIA @ 72 °F</u>		<u>0 PSIA @ 60 °F</u>	
	<u>Mol Percent</u>	<u>GPM</u>	<u>Mol Percent</u>	<u>GPM</u>
Hydrogen Sulfide	NIL		NIL	
Carbon Dioxide	1.58		2.88	
Nitrogen	0.77		0.53	
Methane	91.06		68.13	
Ethane	4.67		17.62	
Propane	0.62	0.171	4.44	1.222
iso-Butane	0.19	0.062	1.93	0.631
n-Butane	0.36	0.114	1.77	0.558
iso-Pentane	0.17	0.062	1.09	0.399
n-Pentane	0.24	0.087	0.71	0.257
Hexanes	0.20	0.082	0.60	0.245
Heptanes plus	0.14	0.064	0.30	0.136
	<u>100.00</u>	<u>0.642</u>	<u>100.00</u>	<u>3.448</u>

Calculated gas gravity(air=1.000)

0.626

0.824

Calculated gross heating value =  
per cubic foot of dry gas at

1072 BTU  
14.73 psia at 60°F.

1353 BTU  
14.73 psia at 60°F.

Collected in the laboratory.

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Company ..... STATOIL ..... Date Sampled ..... 24th August, 1978.....  
 Well ..... 34/10-1 DST 2 Flow 2 ..... County ..... NORTH SEA.....  
 Field ..... State ..... NORWAY.....

**HYDROCARBON ANALYSIS OF ..... Stock Tank Oil ..... SAMPLE**

COMPONENT	MOL PERCENT	WEIGHT PERCENT	DENSITY @ 60° F. GRAMS PER CUBIC CENTIMETER	* API @ 60° F.	MOLECULAR WEIGHT
Hydrogen Sulfide	NIL	NIL			
Carbon Dioxide	0.04	0.01			
Nitrogen	NIL	NIL			
Methane	0.40	0.03			
Ethane	0.65	0.08			
Propane	0.63	0.12			
iso-Butane	0.74	0.18			
n-Butane	0.69	0.17			
iso-Pentane	0.78	0.24			
n-Pentane	0.77	0.24			
Hexanes	1.80	0.66			
Heptanes plus	93.50	98.27	0.8856	28.1	245
	<hr/> 100.00	<hr/> 100.00			

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Well 34/10-1 DST 2 Flow 2

Company STATOIL Formation \_\_\_\_\_  
 Field \_\_\_\_\_ State NORTH SEA- NORWAY

HYDROCARBON ANALYSIS OF Calculated Wellstream

<u>Component</u>	<u>Mol Per Cent</u>
Hydrogen Sulfide	NIL
Carbon Dioxide	0.99
Nitrogen	0.38
Methane	45.57
Ethane	4.18
Propane	0.98
iso-Butane	0.55
n-Butane	0.66
iso-Pentane	0.55
n-Pentane	0.53
Hexanes	1.00
Heptanes plus	44.61
	100.00

Properties of Heptanes Plus:

API gravity at 60°F.	28.2
Specific gravity at 60/60°F.	0.8862
Molecular Weight	243

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**STATOIL:**

**Well: 34/10-1 DST 2 Flow 2.**

Core Laboratories U.K. Limited

Reservoir Fluid Analysis

*John D. Owen*

John D. Owen.  
Supervisor