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25 FEB. 1980

**REGNSKJERT
OLJEDELELSE INNATE**

PETROPHYSICAL EVALUATION

WELL 34/10-3

BY: PETROLEUM ENGINEERING
PETROPHYSICAL GROUP
NOV 1979

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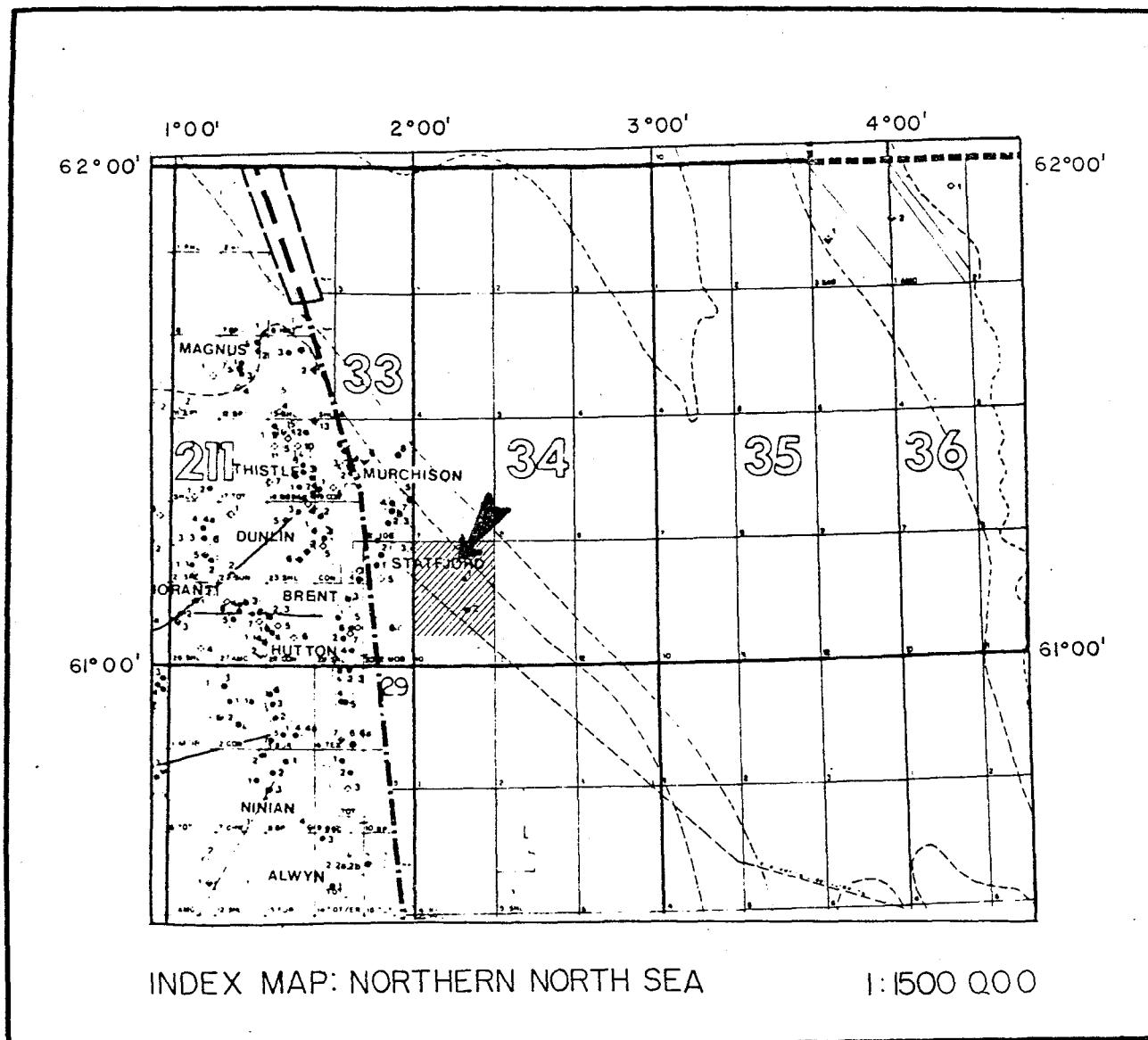
CONTENTS

| | PAGE |
|--------------------------------------|------|
| General well data | 1 |
| Introduction | 2 |
| Summary | 2 |
| Lithology | 2 |
| Log quality | 3 |
| Input parameters | 3 |
| Formation water salinity | 3 |
| Formation temperature | 3 |
| Mud properties | 4 |
| Hydrocarbon density | 4 |
| Resistivity | 4 |
| Shale parameters | 5 |
| Computations | 5 |
| Shale volume | 5 |
| Porosity | 6 |
| Formation factor | 6 |
| Saturation exponent | 6 |
| Watersaturation | 7 |
| Coring summary | 8 |
| Comparison between core and log data | 9 |
| Permeability | 9 |
| Testing summary | 10 |
| Results table | 11 |
| Appendix | |

GENERAL WELL DATA

Norway offshore

Licence : 050
Wildcat well : 34/10-3
Location : $61^{\circ}12'49.5''N$
 $02^{\circ}11'55.1''E$
Spudded : 14 March 1979
Rig Released : 8 june 1979
KB-elevation : 25 m
Water depth : 179 m
Total depth : 2802 m
Objective : Jurassic sandstone
Operator : Statoil
Partners : Norsk Hydro, Saga Petroleum
Status : Plugged and abandonned



INTRODUCTION

This is the second well drilled on the delta-structure in block 34/10. The main objective was to test the Jurassic sandstone formations for hydrocarbon accumulations. The purpose of this report is to evaluate the petrophysical parameters of these formations using electrical logs core and test data.

SUMMARY

Only Brent formation (1892 - 2092 m) encountered hydrocarbons in 34/10-3. Statfjord formation (2495 - 2715 m) is waterbearing.

Oil water contact is at \pm 1971.5 m. Brent encounters 35.75 m. Net sand. Average porosity in 29.6 % and average watersaturation in the oil zone is 38.5 %.

Statfjord formation encounters 100.25 m of net sand with an average porosity of 18.9 %.

LITHOLOGY

The reservoir zones have been divided into the following units:

NESS (1892 - 1979) : Delta plain. Interbedded shale, sand, coal.

ETIVE (1979 - 2002) : Delta front. Clean sandstone.

RANNOCH (2002 - 2084) : Shore face. Fining downwards sequence. Some tight carbonate, cemented zones.

STATFJORD FM
(2495 - 2715) : Interbedded shale and sandstone.

LOG QUALITY

The logs are generally of good quality. In Statfjord formation, the sonic transit time has been taken out of BHC-G, run 1. The sonic on ISF/BHC-G run 6 is not acceptable.

INPUT PARAMETERS

Input parameters to the calculations have been picked from cross-plots, measured data and empirical relations.

FORMATION WATER SALINITY

DST No. 1 produced formation water with a salinity of 433200 ppm NaCl. Log analysis indicates the salinity to be the same in Statfjord and Brent formation. The following values have been used for formation water resistivity under reservoir conditions.

Brent fm : 0.073 Ω m at 160 $^{\circ}$ F

Statfjord fm : 0.062 Ω m at 185 $^{\circ}$ F

FORMATION TEMPERATURE

A constant temperature have been used in the computations for each zone:

Brent : 160 $^{\circ}$ F

Statfjord : 185 $^{\circ}$ F

MUD PROPERTIES

| | At 48° F | At reservoir cond. |
|-------|-------------------------|--------------------|
| | $R_{mf} = .39 \Omega m$ | .13 Ωm |
| Brent | $R_m = .554 "$ | .18 " |
| | $R_{mc} = 1.60$ | .52 " |
| | *23000 ppm NaCl | |

| | At 55° F | At reservoir cond. |
|---------|-------------------------------|--------------------|
| | $R_{mf} = .323^{**} \Omega m$ | 0.105 Ωm |
| Statfj. | $R_m = .495 "$ | 0.150 " |
| | $R_{mc} = 1.15$ | 0.340 " |
| | **24000 ppm NaCl | |

HYDROCARBON DENSITY

The hydrocarbon density have been picked from RFT-pressure plots. A value of 0.785 gm/cc has been used.

RESISTIVITY

Brent formation:

RLLD has been used uncorrected (chart Rint - 9, Schlumberger).

R_{MSFL} has been used for RXO corrected for mudcake effect (chart RXO - 2, Schlumberger).

Corrections on R_{MSFL} :

- Hydrocarbon zone $RXO = 0.88 R_{MSFL}$
- Water zone $RXO = 0.80 R_{MSFL}$

Statfjord formation:

R_{ILD} (6FF40) has been used as R_T . No RXO tool available ($SXO = 1$)

SHALE PARAMETERS

Shale parameters have been selected from crossplots and visual inspection of the logs. High content of K-feldspar and mica increases the GR-reading. This makes it necessary to adjust GR min values in Rannoch. The table below lists the parameters used zone by zone.

| ZONE | ØNSH | ρBSH | ΔtsH | RSH | GR min | GR max |
|-----------|------|------|------|-----|--------|--------|
| NESS | .45 | 2.35 | 120 | 1.5 | 30 | 73 |
| ETIVE | .45 | 2.35 | 120 | 1.5 | 30 | 73 |
| RANNOCH | .45 | 2.35 | 120 | 1.5 | 42 | 73 |
| STATFJORD | .45 | 2.45 | 100 | 2.0 | 30 | 90 |

COMPUTATIONS

SHALE VOLUME

Gamma Ray and FDC/CNL crossplots have been used for Vsh calculations. Where both indicators have been used, the minimum value have been picked as Vsh. Below is listed for which intervals the two indicators have been used:

| Interval | Indicaor |
|-------------|------------|
| 1885 - 1892 | FDC/CNL |
| 1892 - 2100 | FDC/CNL,GR |
| 2490 - 2725 | FDC/CNL,GR |

POROSITY

The porosity has been calculated with a complex lithology method using density and neutron logs with the following matrix parameters:

| | FDC | CNL |
|---------------|------|--------|
| Quartz | 2.65 | -0.035 |
| Heavy mineral | 2.9 | .25 |
| Fluid | 1.0 | 1.0 |

FORMATION FACTOR

Measurements performed on cores in Brent formation indicates that the following relationship can be used for formation factor:

$$F = \Phi^{-2}$$

In Statfjord formation, Humble's relationship has been used:

$$F = 0.62 \Phi^{-2.15}$$

SATURATION EXPONENT

Core measured data give an average value of 1.95 in Brent formation. In Statfjord formation, a value of 2 has been used.

WATERSAURATION

The Nigeria-equation (Schlumberger) has been used for calculations of the water saturation.

Nigeria Equation:

$$\frac{1}{R_T} = \frac{(V_{clay})^C S_w}{R_{clay}} + \frac{\emptyset^m S_w^n}{a R_w}$$

where:

- R_T = Resistivity of virgin zone
- S_w = Watersaturation
- R_{clay} = Resistivity of clay (Rsh)
- C = Vclay-exponent (1.6 used)
- \emptyset = Porosity
- a = Lithology factor
- R_w = Formation water resistivity
- m = Cementation exponent
- n = Saturation exponent

CORING SUMMARY

Eight cores were out in Brent formation. The core-depths have been correllated to the CPI-depths based on description and petrophysical parametres.

Core # 1 1904 - 1919.4 rec.: 95.5 %
Log depth (Cpi) : 1902.5 - 1918.4

Core # 2 1919.4 - 1930.9 rec.: 90.4 %
Log depth (Cpi) : 1918.4 - 1929.9

Core # 3 1930.9 - 1936.1 rec.: 48 %

Core # 4 1936.1 - 1953.2 rec.: 68 %
Log depth (cpi) : 1934.1 - 1951.2

Core # 5 1953.2 - 1971.1 rec.: 88 %
Log depth (cpi) : 1951.2 - 1968.1

Core # 6 1971.1 - 1989.2 rec.: 100 %
Log depth (cpi) : 1968.1 - 1986.2

Core # 7 1989.2 - 2007.3 rec.: 95 %
Log depth (cpi) : 1986.2 - 2004.3

Core # 8 2007.3 - 2025.3 rec.: 100 %
Log depth (cpi) : 2004.3 - 2022.3

COMPARISON BETWEEN CORE AND LOG DATA

Log porosity and grain density have been compared with core data (GECO) in the interval 1979.5 - 2023 (cpi). The results are listed in the table below:

| | LOG | CORE | LOG/CORE |
|-----------------------|-------|-------|----------|
| Average Porosity | 31.90 | 33.45 | 0.954 |
| Average grain density | 2.71 | 2.672 | . |

Data on 34/10-1-core indicates that the porosity at net-confining pressure should be 96-98 % of the porosity measured at atmospheric pressure; hence the log porosity is within acceptable limits. Histograms and crossplots of log and core porosity are enclosed in appendix.

PERMEABILITY

Horizontal permeability has been plotted against helium porosity for each lithologic unit on enclosed graphs in the appendix. There are two distinct trends; for Rannoch and Etive. The data in Ness are too scattered to make a good trend. The trends in Etive and Rannoch agrees with the relationship found in 34/10-1 which was:

$$\begin{aligned} \text{ETIVE} &: \phi = .1 + .068 \log k \\ \text{RANNOCH} &: \phi = .15 + .07 \log k \\ \text{where} &: \phi = \text{porosity in fractions} \\ &: k = \text{permeability in mD} \end{aligned}$$

TESTING SUMMARY

Three DST's were performed. Here is listed a summary of the main results of these tests:

DST # 1 : Interval : 1990 - 1995
Choke : 20/64 "
Production : 2600 STB/d (water)

DST # 2 : Interval : 1935 - 1940
Choke : (29 + 14)/64"
Production : 2850 STB/d oil
 $1167 \cdot 10^3$ scf/d

DST # 3 : Interval : 1895 - 1900
Choke : 10/64"
Production : 650 STB/d oil
 Sand plugging

34/10-3 RESULTS TABLE OF PETROPHYSICAL PARAMETERS

| FORMATION | INTERVAL RKB (m) | NET SAND (m) | AVERAGE POROSITY (%) | AVERAGE WATER- SATURATION (%) | NET/ GROSS RATIO |
|-------------|---------------------|-----------------|----------------------------|-------------------------------------|------------------------|
| NESS | 1892-1979 | 35.75 | 27.3 | 38.5 | 0.411 |
| | | 37.25 | 26.8 | 42.8 | 0.428 |
| ETIVE | 1979-2002 | 22.25 | 32.4 | 100 | 0.967 |
| RANNOCH | 2002-2084 | 72.25 | 30.3 | 100 | 0.881 |
| TOTAL BRENT | 1892-2092 | 35.75 | 27.3 | 38.5 | 0.179 |
| | | 131.75 | 29.6 | 0.879 | .659 |
| STATFJORD | 2495-2715 | 100.25 | 18.9 | 100 | 0.456 |

CUT-OFF CRITERION:

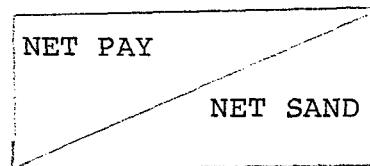
VSH > 40%

PHIF < 12%

SW > 65%

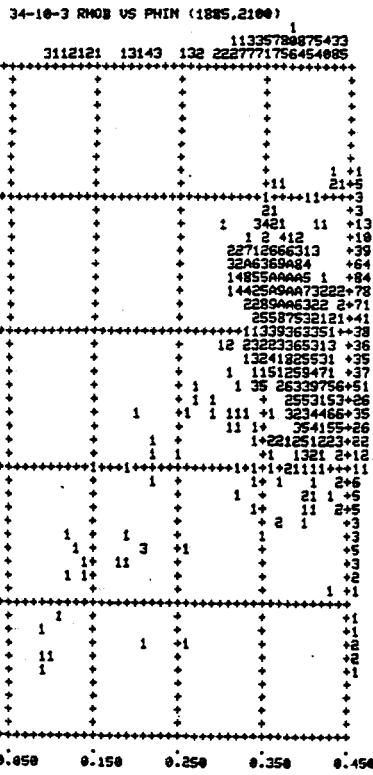
Bed thickness < 1 m (Brent fm)

Net sand = Net pay above O/W contact

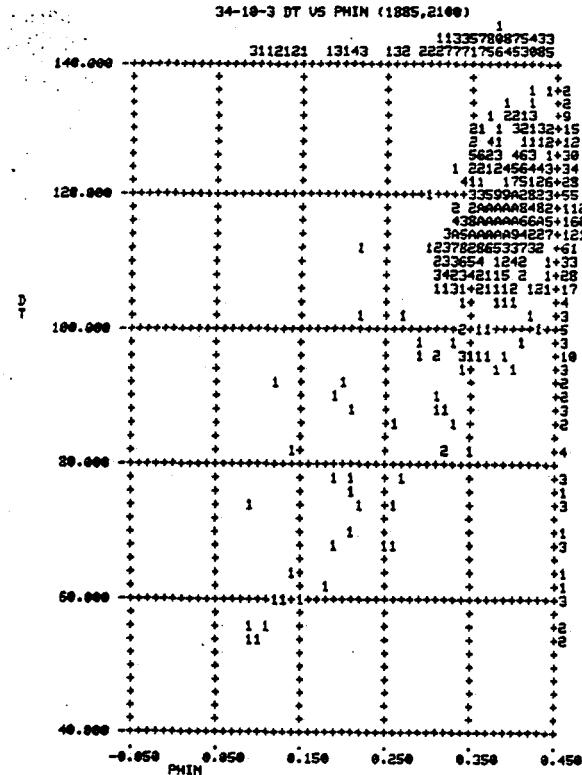


APPENDIX

- Crossplots log vs log
 - permeability vs porosity
 - log vs core
- Summary log
- CPI
- Listing



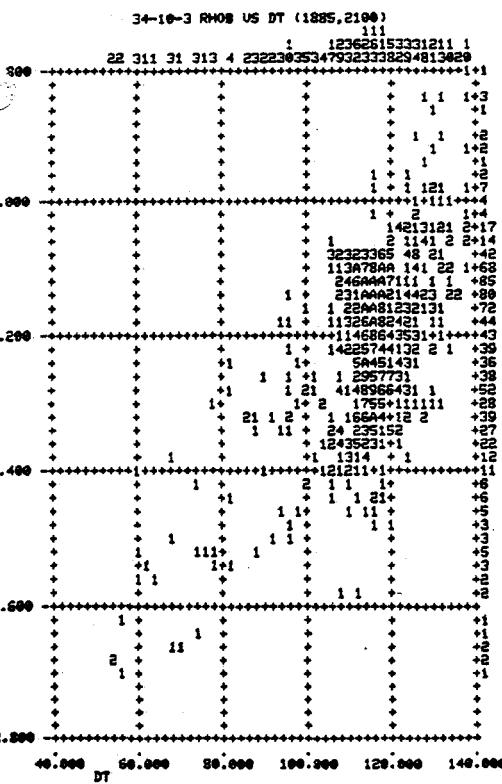
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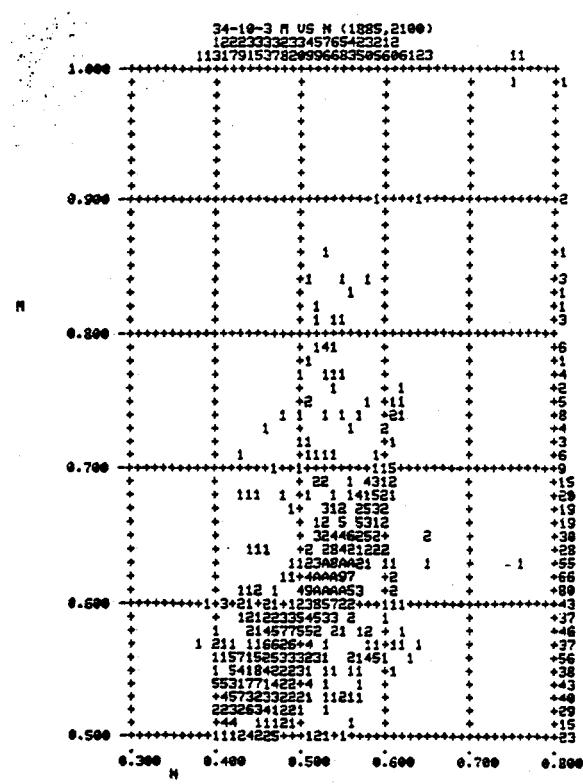
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BRENT (1885 - 2100)

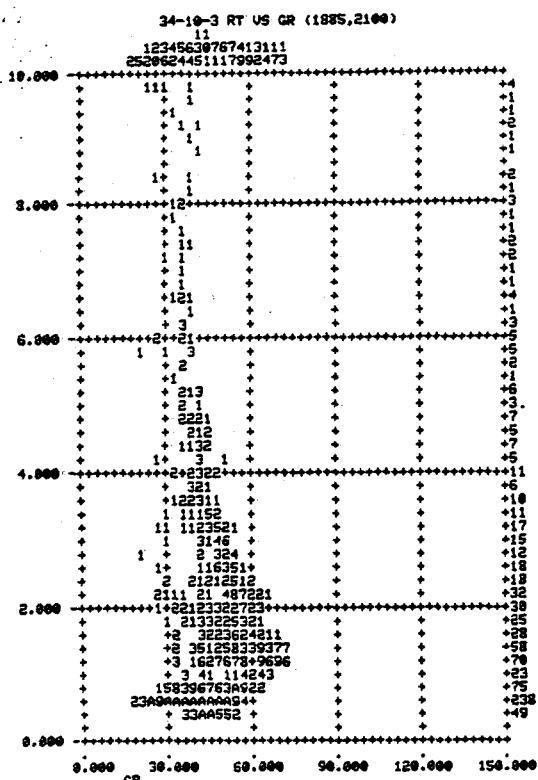
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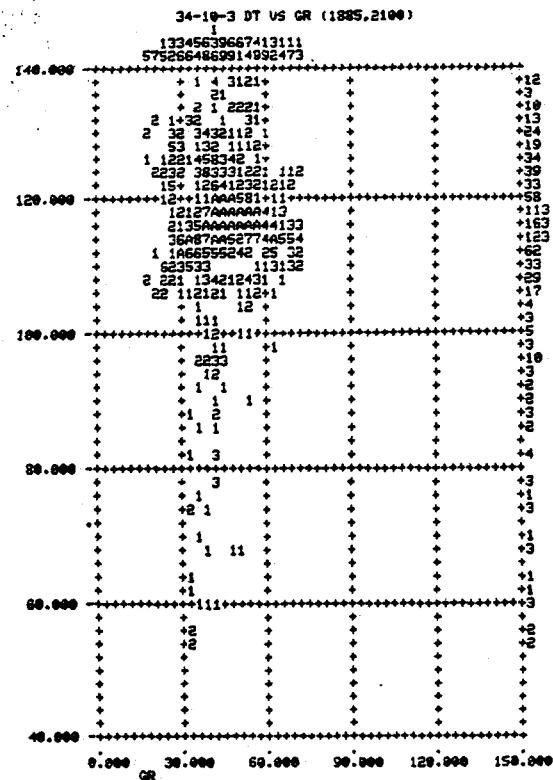
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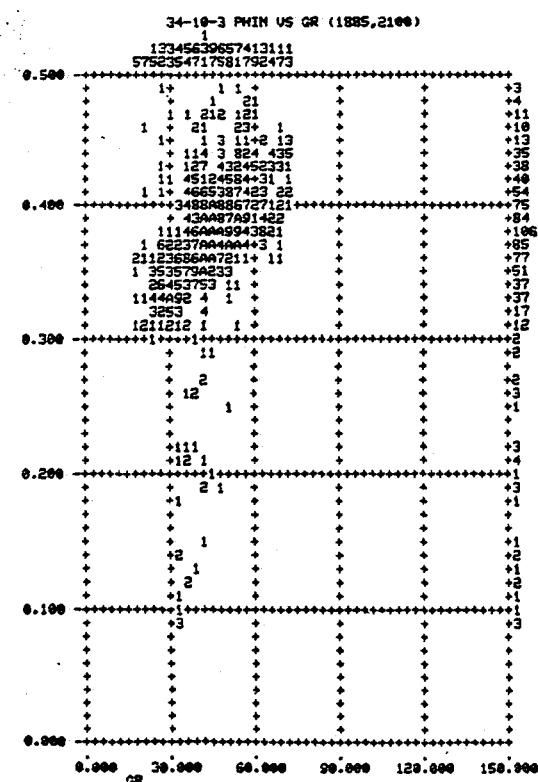
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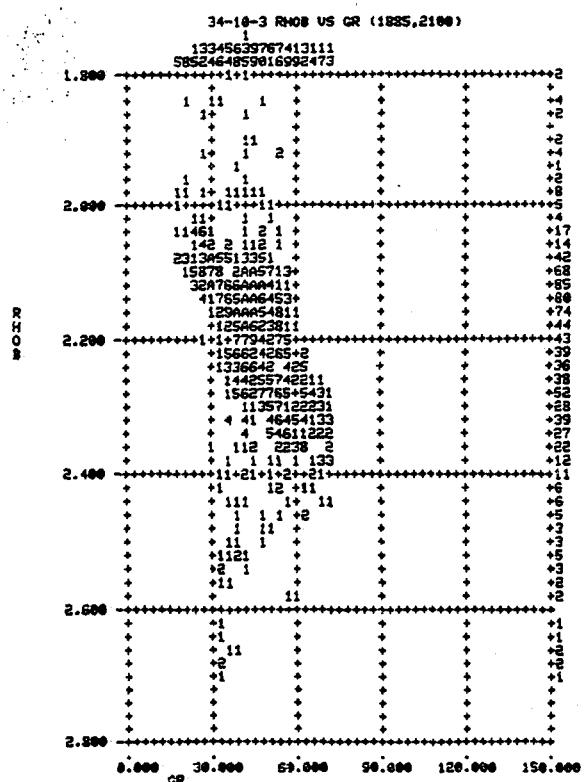
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BRENT (1885 - 2100)

CROSSPLOTS : RT/GR, DT/GR, PHIN/GR, RHOB/GR

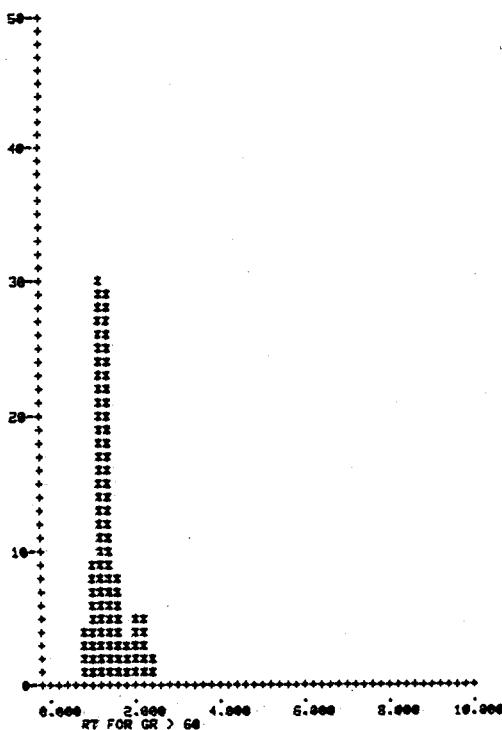


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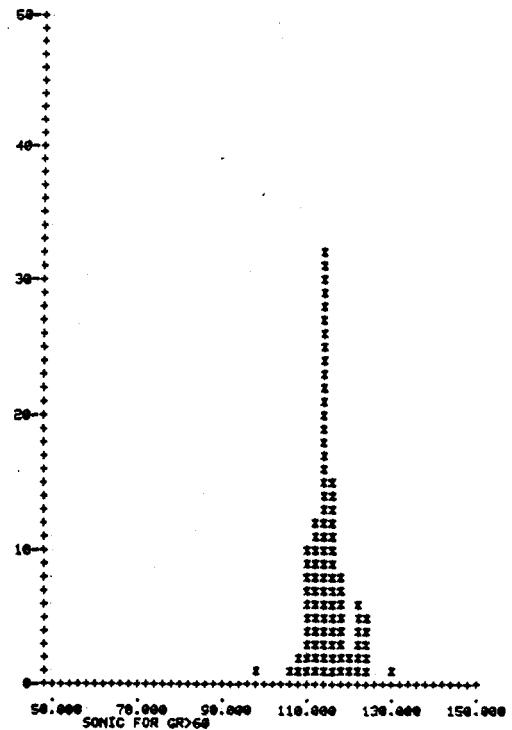


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FREQUENCY PLOT



FREQUENCY PLOT



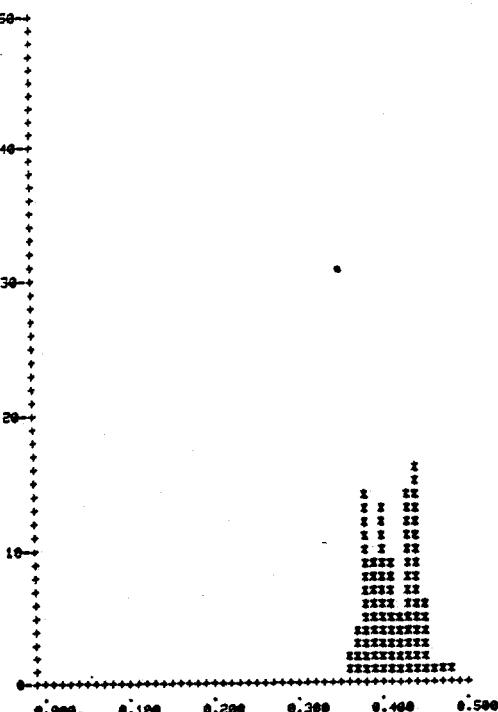
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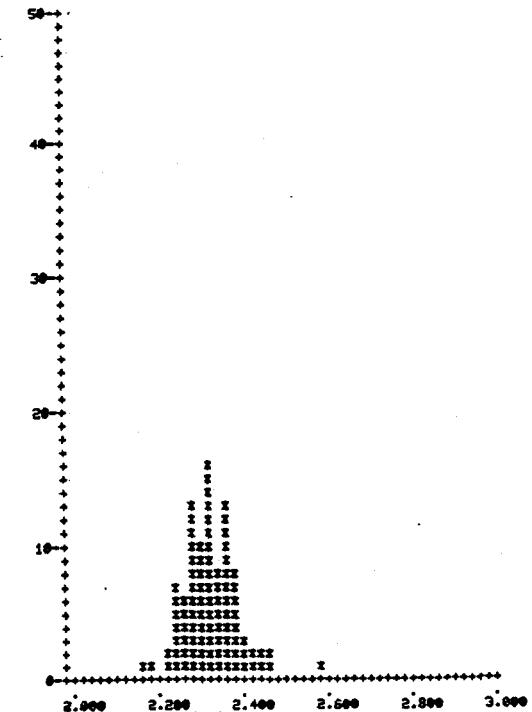
BRENT (1885 - 2100)

HISTOGRAMS FOR GR>60: RT, DT, PHIN, RHOB

FREQUENCY PLOT

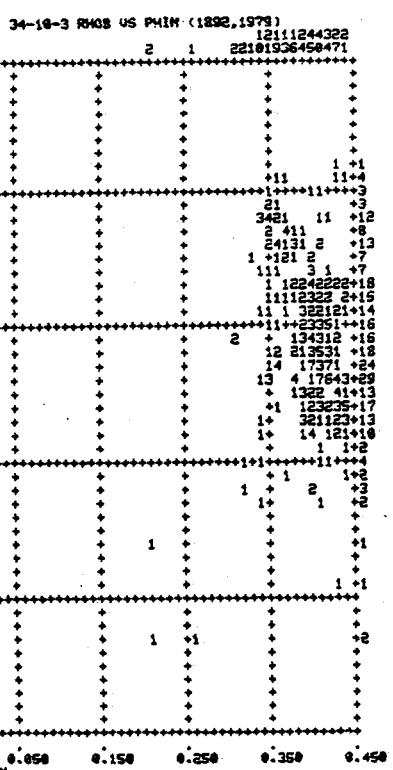


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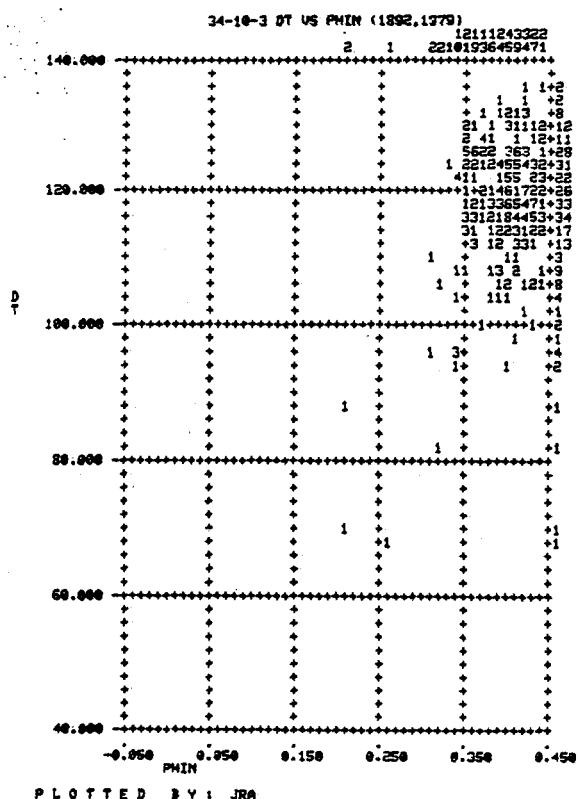


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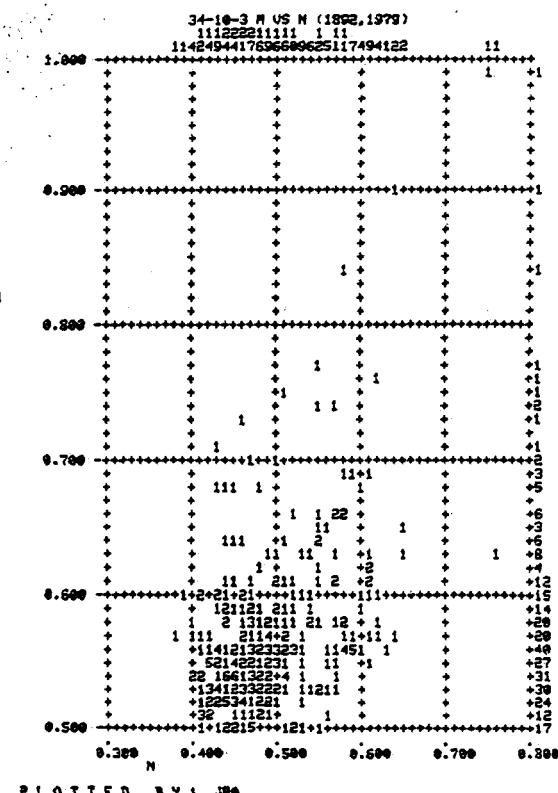
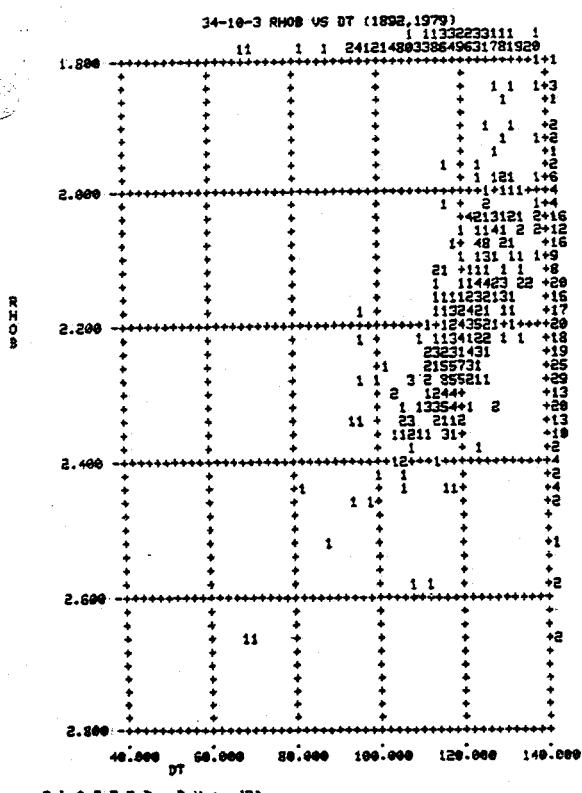
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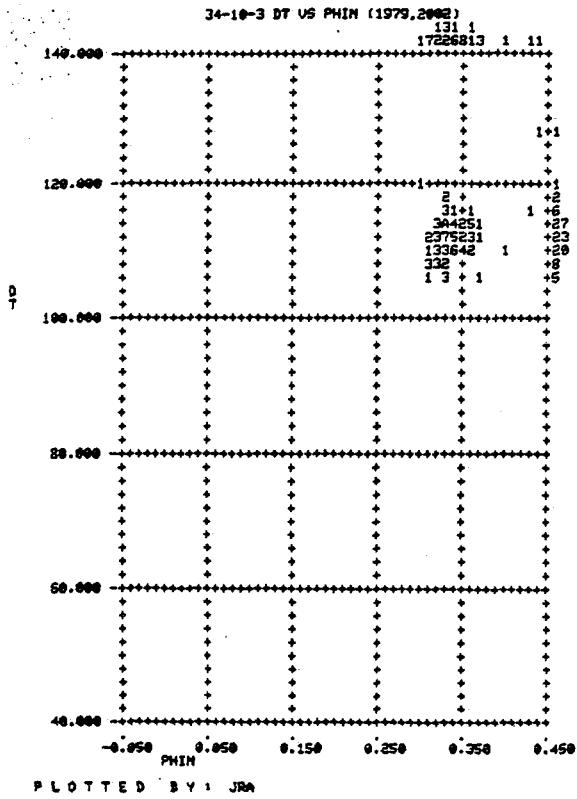
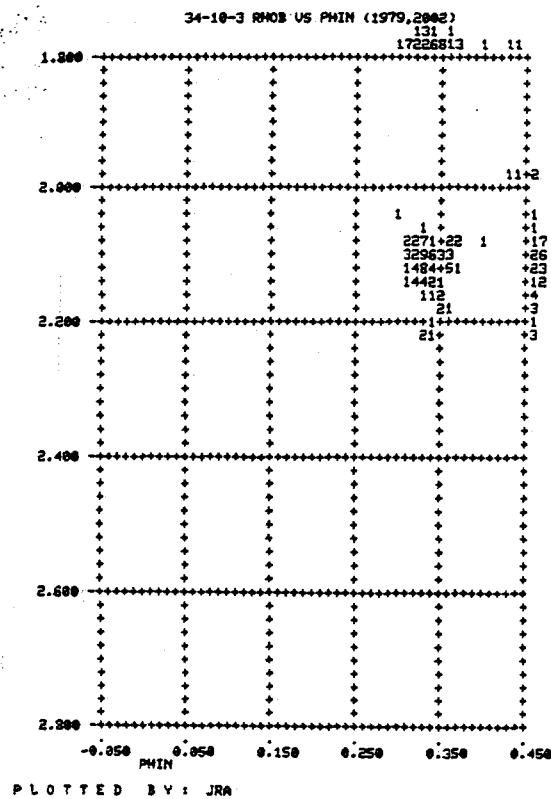
NESS (1892 - 1979)

CROSSPLOTS : RHOB/PHIN, DT/RHOB, DT/PHIN, M/N



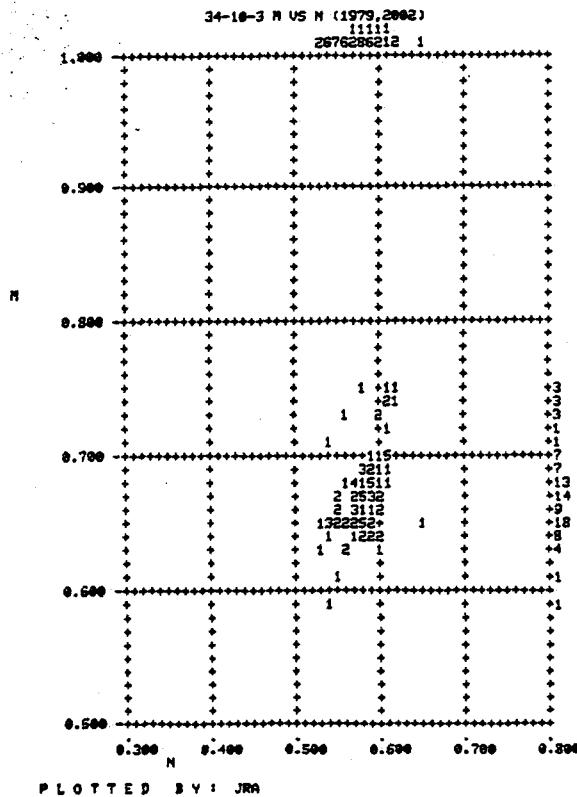
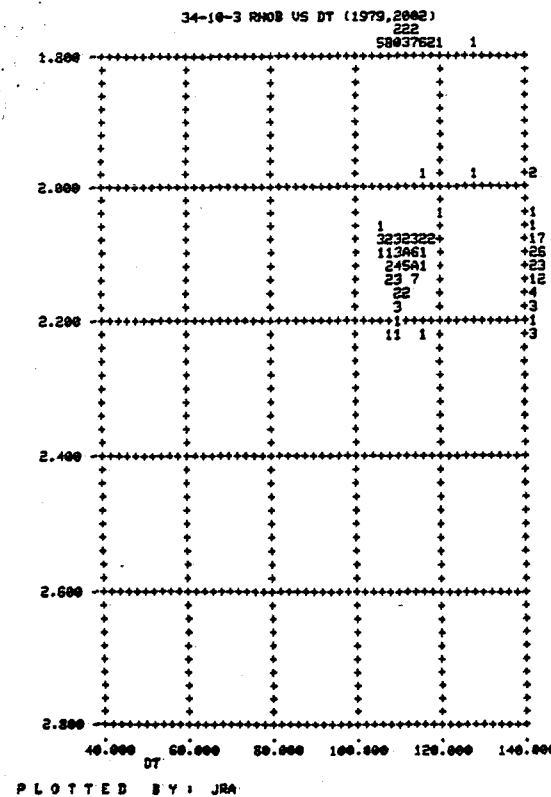
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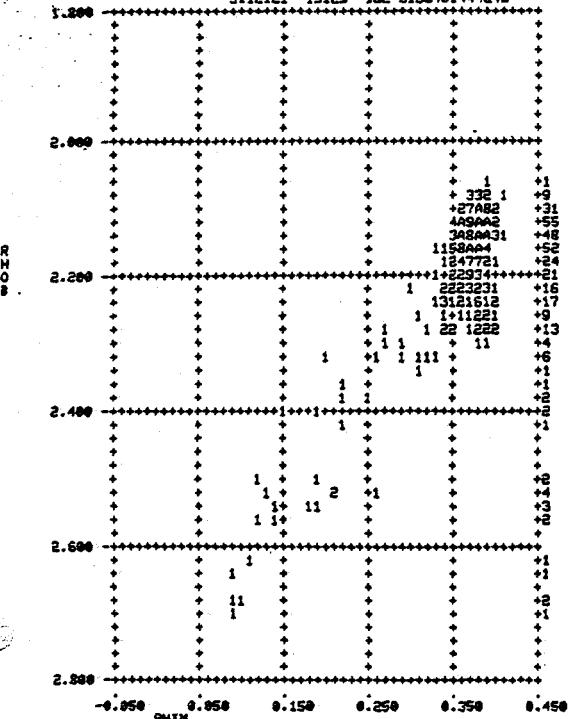


ETIVE (1979 - 2002)

CROSSPLOTS : RHOB/PHIN, DT/RHOB, DT/PHIN, M/N

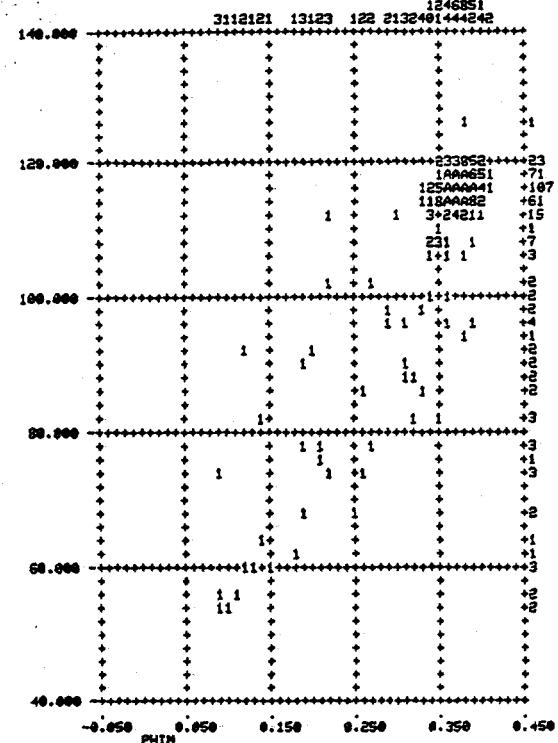


34-10-3 RHOB VS PHIN (2002,2084)
1246851
3112121 13123 122 2132461444242



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34-10-3 DT VS PHIN (2002,2084)

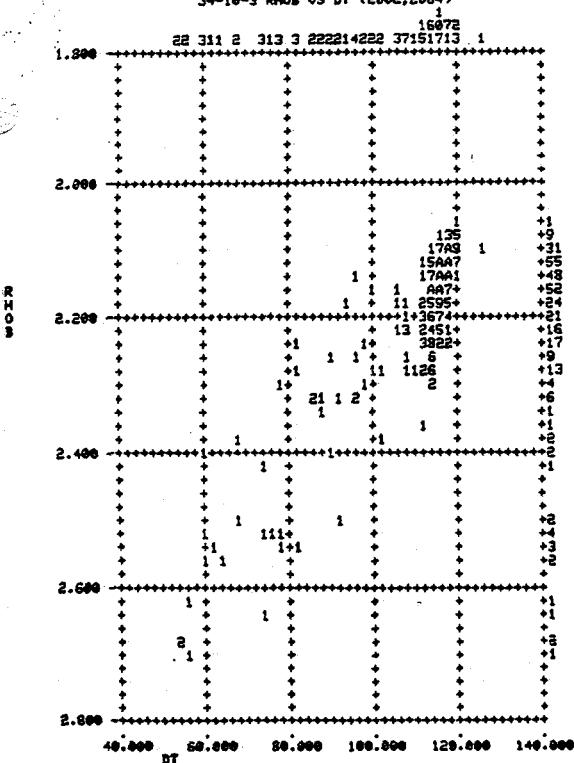


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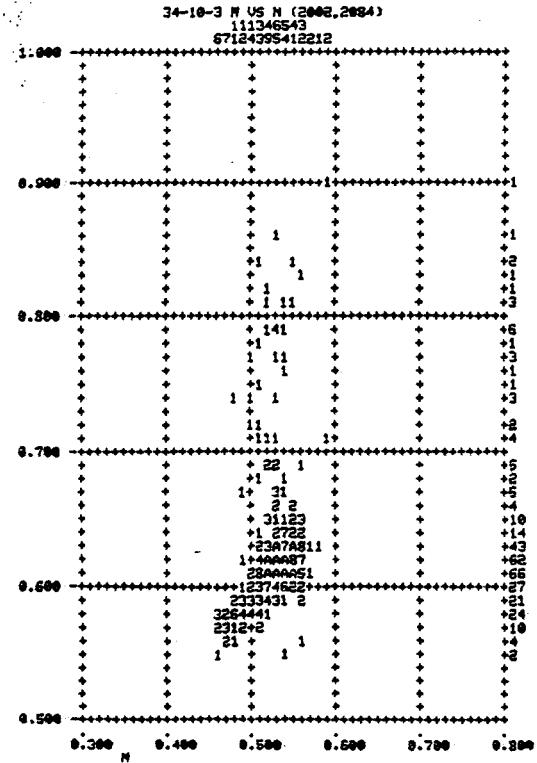
RANNOCH (2002 - 2084)

CROSSPLOTS : RHOB/PHIN, DT/RHOB, DT/PHIN, M/N

34-10-3 RHOB VS DT (2002,2084)

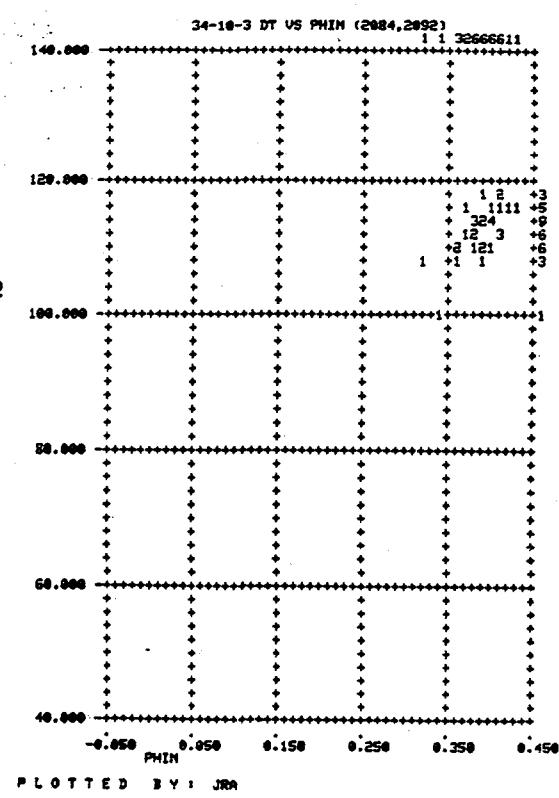
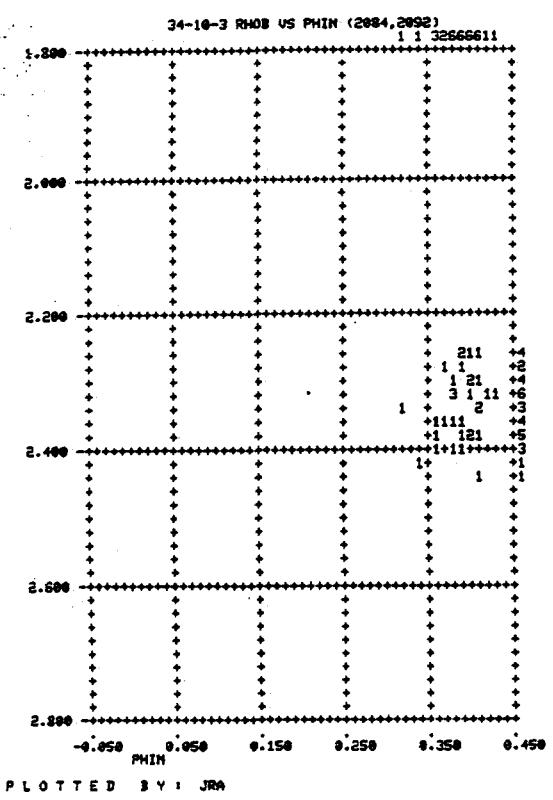


34-10-3 N VS M (2002,2084)



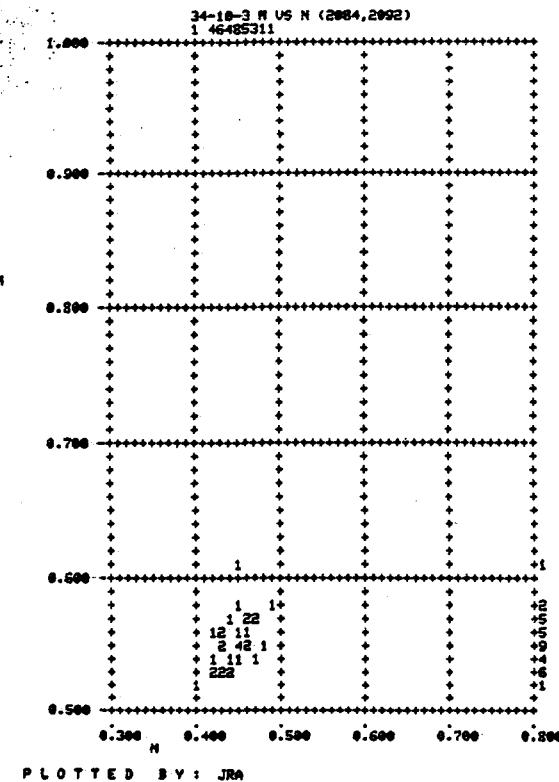
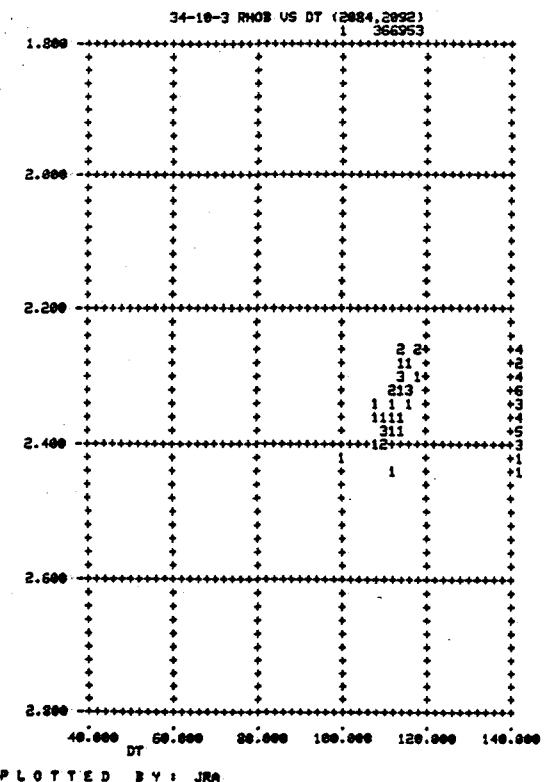
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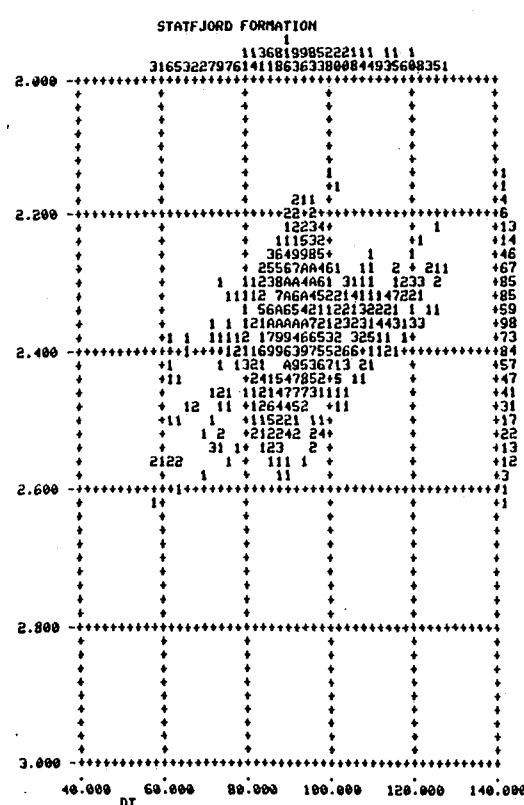
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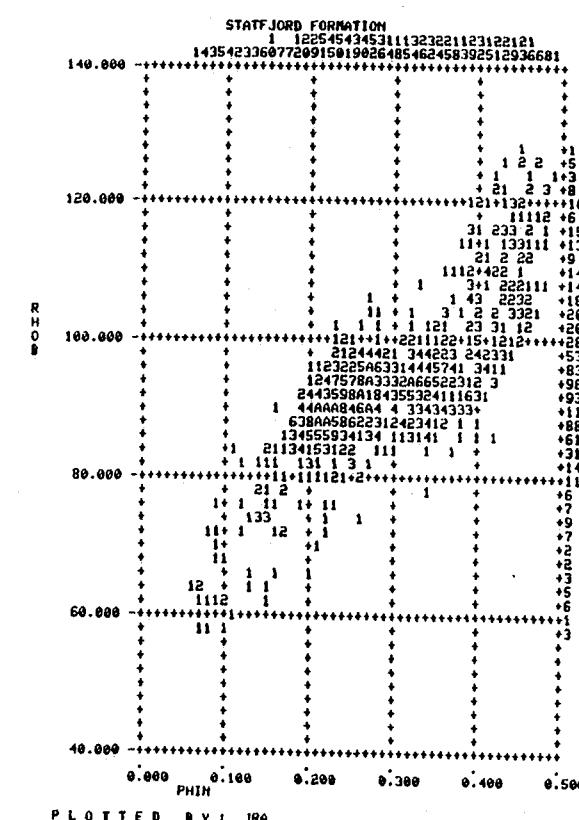
BROOM (2084 - 2092)

CROSSPLOTS : RHOB/PHIN, DT/RHOB, DT/PHIN, M/N

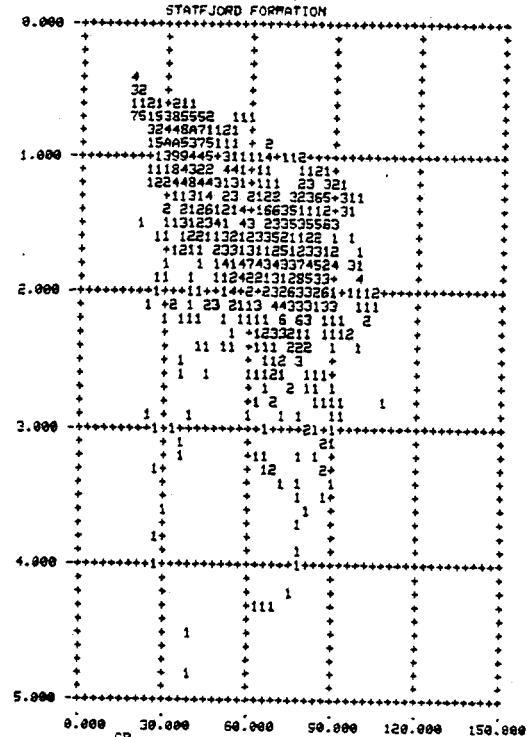
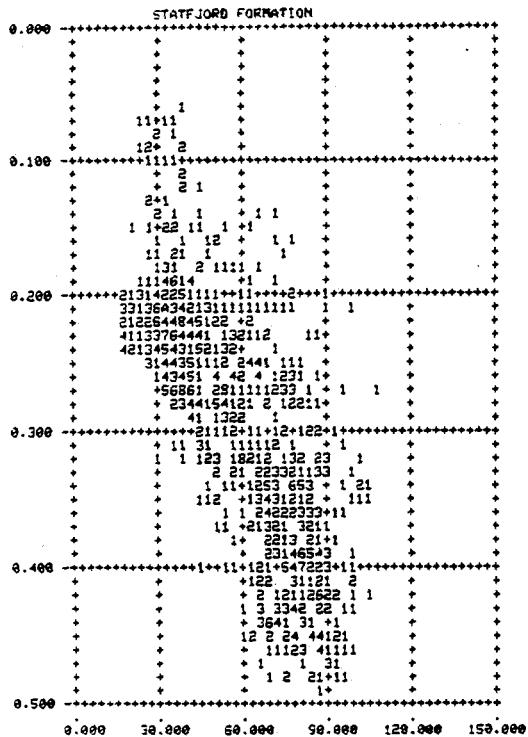




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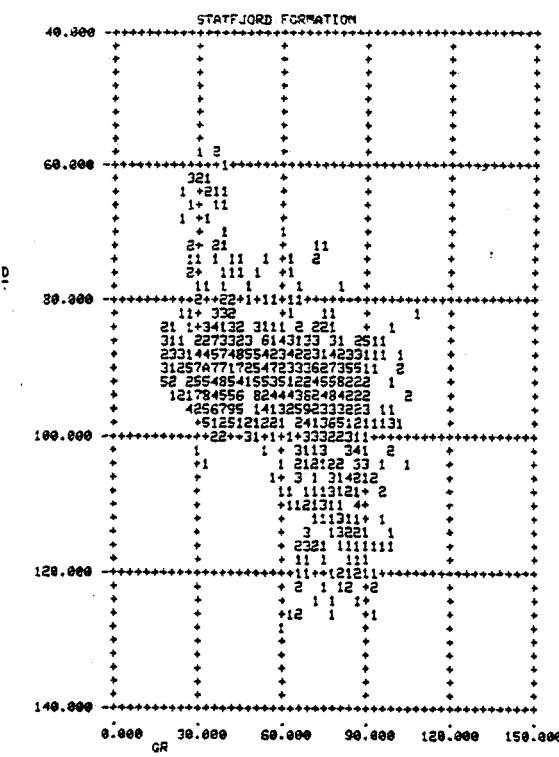
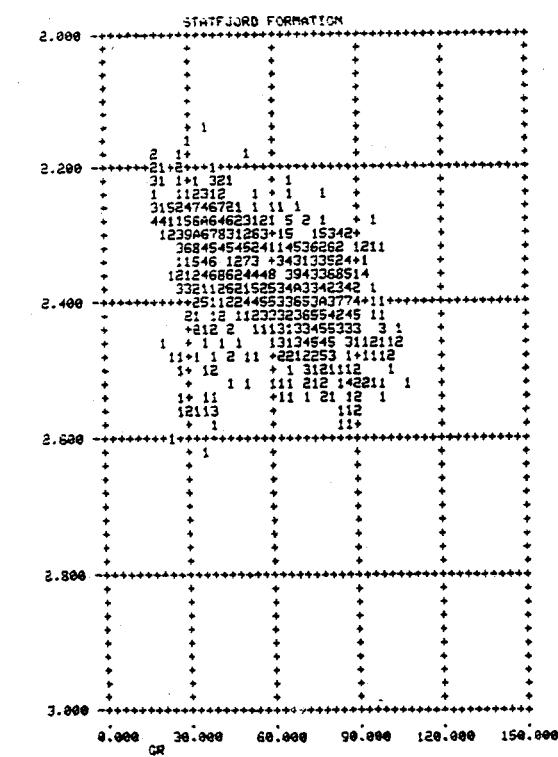


STATFJORD FORMATION : CROSSPLOTS RHOB/DT, RHOB/PHIN
(2495 - 2715)



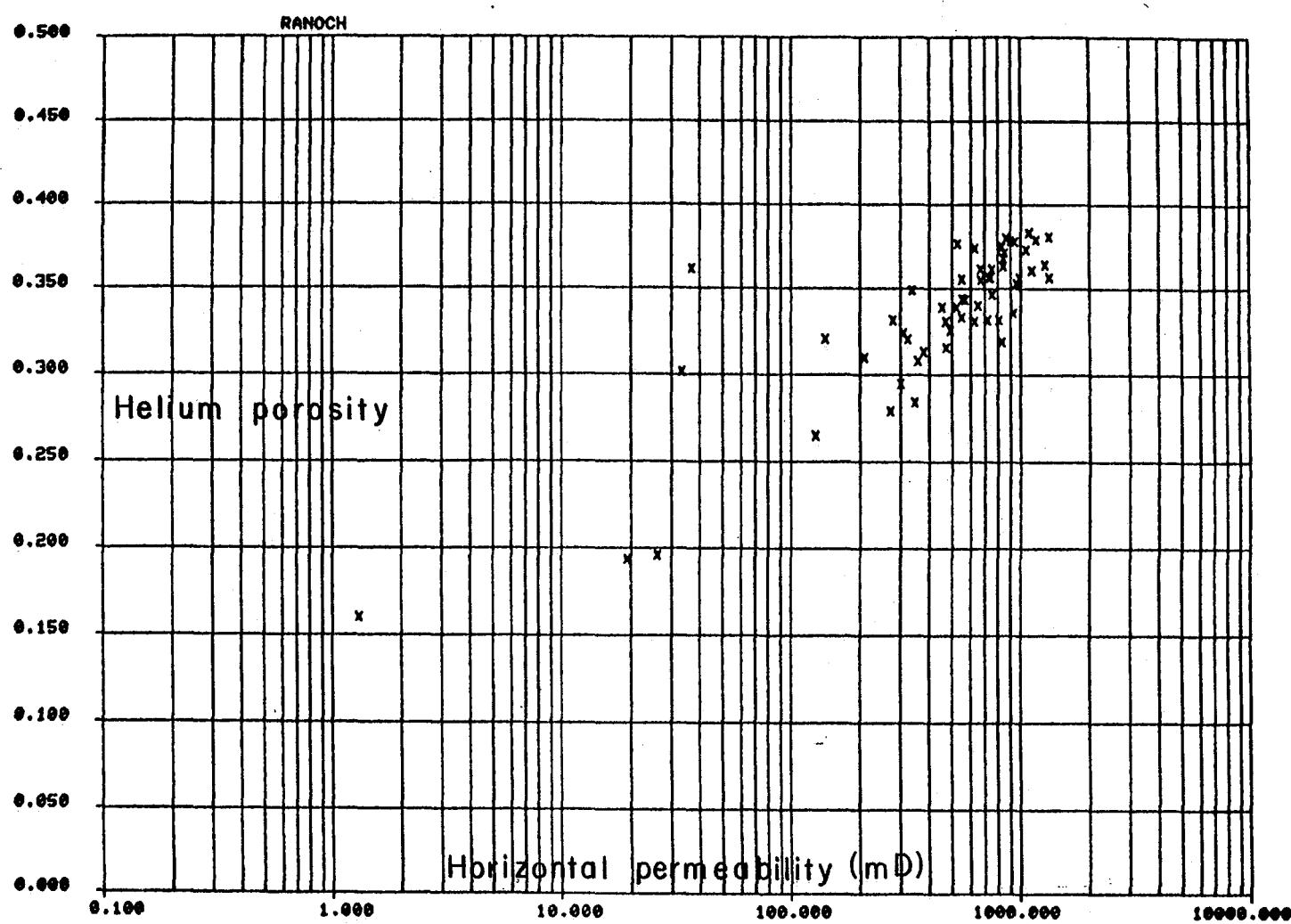
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STATFJORD FORMATION : CROSSPLOTS GR versus PHIN, RHOB, RT, DT
(2495 - 2715)



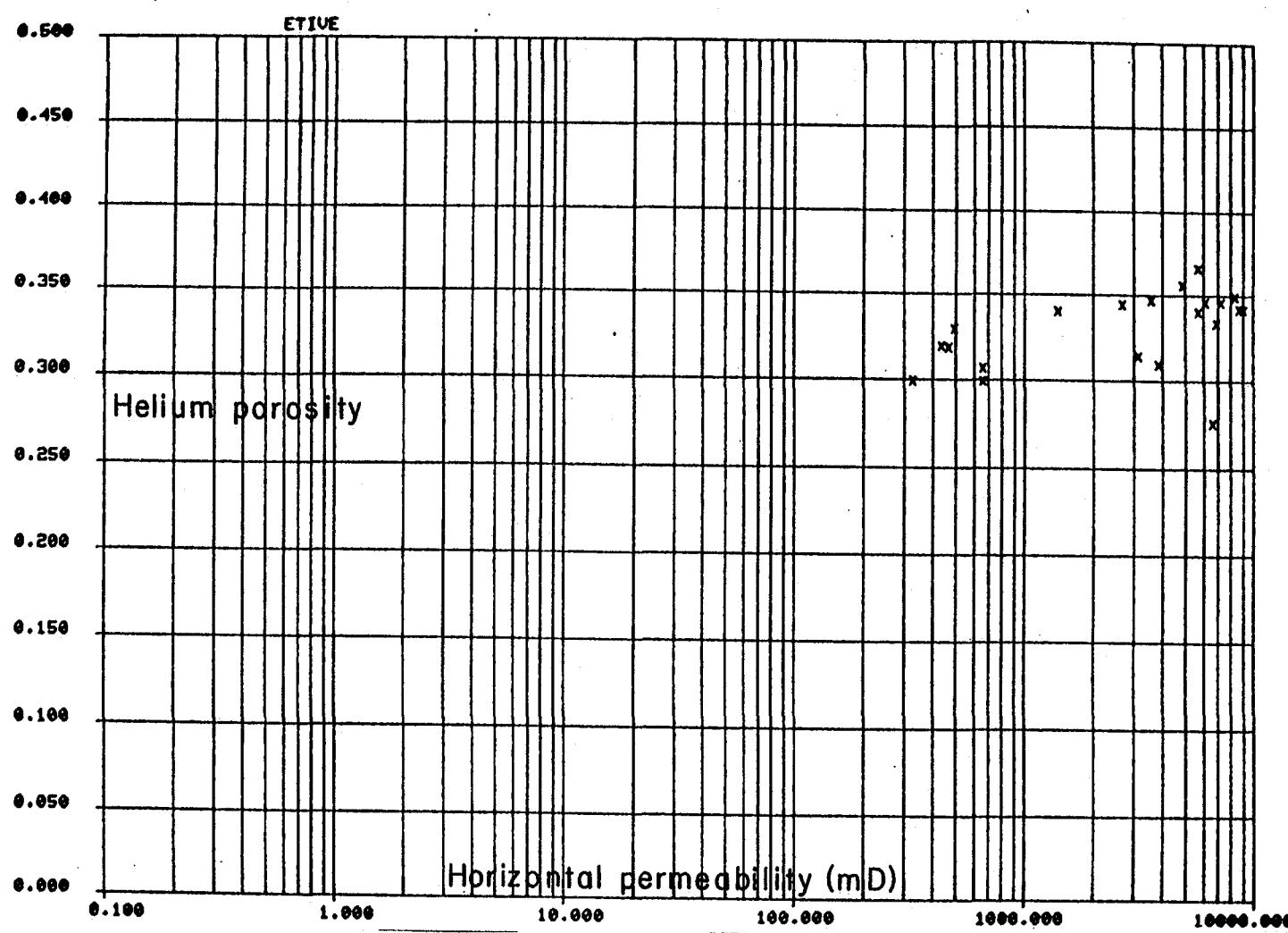
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RANOCH



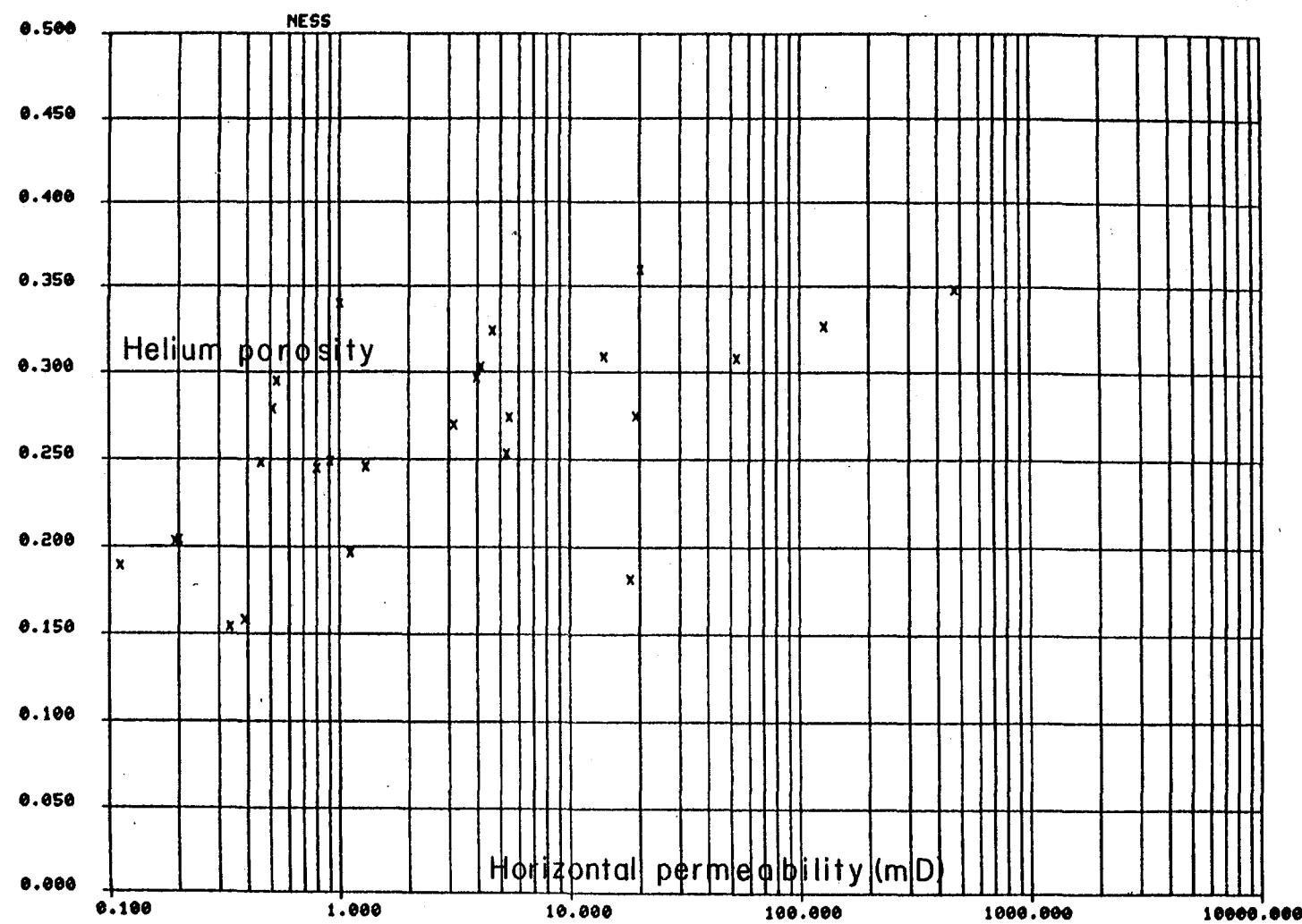
34/10-3 Helium porosity vs. horizontal permeability

ETIVE

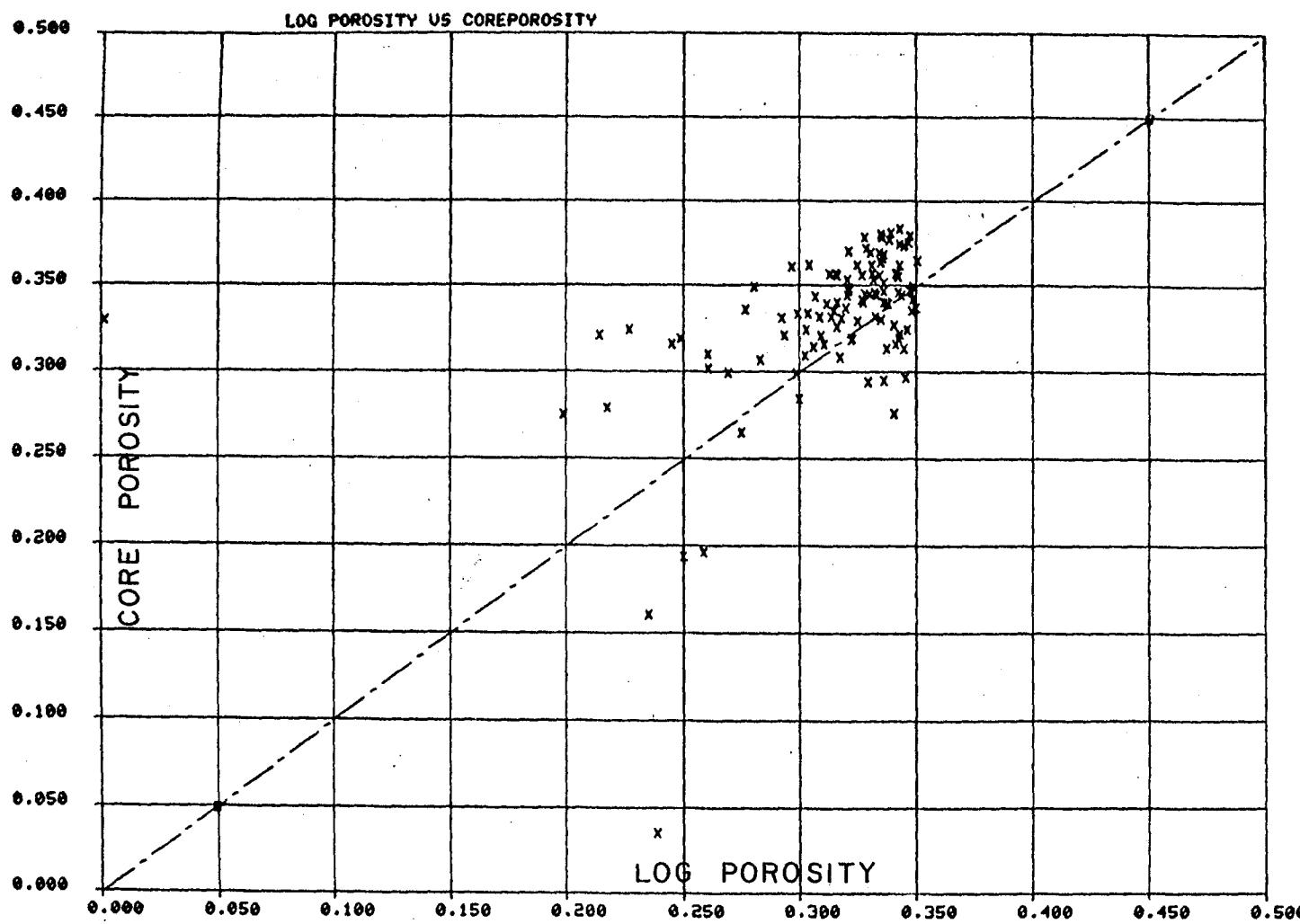


34/10-3 Helium porosity vs. horizontal permeability

NESS



34/10-3 Helium porosity vs. horizontal permeability.



34/10-3 LOG - VS COREPOROSITIES
INTERVAL 1980-2025

WELL: 34-10-3 (1890 - 2100)

DATE: 24OCT79/ILF

| DEPTH | VSH | PHIF | SW |
|---------|-------|-------|-------|
| 1890.00 | 1.000 | 0.001 | 1.000 |
| 1890.25 | 1.000 | 0.001 | 1.000 |
| 1890.50 | 0.972 | 0.001 | 1.001 |
| 1890.75 | 0.709 | 0.124 | 0.891 |
| 1891.00 | 0.521 | 0.232 | 0.714 |
| 1891.25 | 0.605 | 0.211 | 0.627 |
| 1891.50 | 0.863 | 0.091 | 0.683 |
| 1891.75 | 0.716 | 0.129 | 0.693 |
| 1892.00 | 0.722 | 0.140 | 0.664 |
| 1892.25 | 1.000 | 0.001 | 1.000 |
| 1892.50 | 1.000 | 0.001 | 1.000 |
| 1892.75 | 1.000 | 0.001 | 1.000 |
| 1893.00 | 1.000 | 0.001 | 1.000 |
| 1893.25 | 1.000 | 0.001 | 1.000 |
| 1893.50 | 1.000 | 0.001 | 1.000 |
| 1893.75 | 0.299 | 0.242 | 0.438 |
| 1894.00 | 0.286 | 0.246 | 0.420 |
| 1894.25 | 0.257 | 0.245 | 0.398 |
| 1894.50 | 0.229 | 0.244 | 0.386 |
| 1894.75 | 0.229 | 0.240 | 0.373 |
| 1895.00 | 0.228 | 0.238 | 0.359 |
| 1895.25 | 0.246 | 0.246 | 0.329 |
| 1895.50 | 0.274 | 0.257 | 0.296 |
| 1895.75 | 0.218 | 0.266 | 0.280 |
| 1896.00 | 0.226 | 0.273 | 0.279 |
| 1896.25 | 0.244 | 0.274 | 0.281 |
| 1896.50 | 0.262 | 0.266 | 0.293 |
| 1896.75 | 0.308 | 0.254 | 0.305 |
| 1897.00 | 0.289 | 0.257 | 0.311 |
| 1897.25 | 0.252 | 0.257 | 0.325 |
| 1897.50 | 0.205 | 0.251 | 0.346 |
| 1897.75 | 0.177 | 0.249 | 0.362 |
| 1898.00 | 0.148 | 0.248 | 0.375 |
| 1898.25 | 0.194 | 0.246 | 0.386 |
| 1898.50 | 0.240 | 0.261 | 0.371 |
| 1898.75 | 0.212 | 0.259 | 0.421 |
| 1899.00 | 0.188 | 0.252 | 0.415 |
| 1899.25 | 0.165 | 0.214 | 0.468 |
| 1899.50 | 0.197 | 0.175 | 0.571 |
| 1899.75 | 0.226 | 0.164 | 0.607 |
| 1900.00 | 0.256 | 0.232 | 0.431 |
| 1900.25 | 0.311 | 0.217 | 0.464 |
| 1900.50 | 0.375 | 0.198 | 0.502 |
| 1900.75 | 0.384 | 0.197 | 0.522 |
| 1901.00 | 0.365 | 0.191 | 0.538 |
| 1901.25 | 0.309 | 0.210 | 0.510 |
| 1901.50 | 0.244 | 0.232 | 0.480 |
| 1901.75 | 0.234 | 0.229 | 0.483 |
| 1902.00 | 0.331 | 0.204 | 0.547 |
| 1902.25 | 0.427 | 0.191 | 0.543 |

WELL: 34-10-3 (1890 - 2100)

DATE: 24OCT79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-------|-------|-------|
| 1902.50 | 0.483 | 0.176 | 0.560 |
| 1902.75 | 0.510 | 0.139 | 0.631 |
| 1903.00 | 0.537 | 0.111 | 0.824 |
| 1903.25 | 0.588 | 0.086 | 0.976 |
| 1903.50 | 0.566 | 0.120 | 0.900 |
| 1903.75 | 0.545 | 0.124 | 0.931 |
| 1904.00 | 0.554 | 0.139 | 0.882 |
| 1904.25 | 0.581 | 0.133 | 0.923 |
| 1904.50 | 1.000 | 0.001 | 1.000 |
| 1904.75 | 1.000 | 0.001 | 1.000 |
| 1905.00 | 1.000 | 0.001 | 1.000 |
| 1905.25 | 1.000 | 0.001 | 1.000 |
| 1905.50 | 1.000 | 0.001 | 1.000 |
| 1905.75 | 1.000 | 0.001 | 1.000 |
| 1906.00 | 1.000 | 0.001 | 1.000 |
| 1906.25 | 1.000 | 0.001 | 1.000 |
| 1906.50 | 1.000 | 0.001 | 1.000 |
| 1906.75 | 1.000 | 0.001 | 1.000 |
| 1907.00 | 1.000 | 0.001 | 1.000 |
| 1907.25 | 1.000 | 0.001 | 1.000 |
| 1907.50 | 1.000 | 0.001 | 1.000 |
| 1907.75 | 0.482 | 0.176 | 0.770 |
| 1908.00 | 0.602 | 0.127 | 0.843 |
| 1908.25 | 0.648 | 0.094 | 0.934 |
| 1908.50 | 0.647 | 0.062 | 1.141 |
| 1908.75 | 0.619 | 0.129 | 0.794 |
| 1909.00 | 0.498 | 0.170 | 0.875 |
| 1909.25 | 1.000 | 0.001 | 1.000 |
| 1909.50 | 1.000 | 0.001 | 1.000 |
| 1909.75 | 1.000 | 0.001 | 1.000 |
| 1910.00 | 0.338 | 0.257 | 0.663 |
| 1910.25 | 0.320 | 0.217 | 0.658 |
| 1910.50 | 0.338 | 0.207 | 0.655 |
| 1910.75 | 1.000 | 0.001 | 1.000 |
| 1911.00 | 1.000 | 0.001 | 1.000 |
| 1911.25 | 1.000 | 0.001 | 1.000 |
| 1911.50 | 0.428 | 0.183 | 0.647 |
| 1911.75 | 0.447 | 0.172 | 0.647 |
| 1912.00 | 0.483 | 0.162 | 0.661 |
| 1912.25 | 0.520 | 0.146 | 0.696 |
| 1912.50 | 0.621 | 0.122 | 0.781 |
| 1912.75 | 0.607 | 0.125 | 0.817 |
| 1913.00 | 0.592 | 0.122 | 0.884 |
| 1913.25 | 0.573 | 0.119 | 0.918 |
| 1913.50 | 0.573 | 0.119 | 0.922 |
| 1913.75 | 0.572 | 0.132 | 0.870 |
| 1914.00 | 0.544 | 0.136 | 0.839 |
| 1914.25 | 0.516 | 0.151 | 0.773 |
| 1914.50 | 0.460 | 0.149 | 0.790 |
| 1914.75 | 0.469 | 0.151 | 0.800 |

WELL: 34-10-3 (1890 - 2100)

DATE: 24 OCT 79 / ILP

| DEPTH | VSH | PHIF | SW |
|---------|-------|-------|-------|
| 1915.00 | 0.477 | 0.196 | 0.650 |
| 1915.25 | 1.000 | 0.001 | 1.000 |
| 1915.50 | 1.000 | 0.001 | 1.000 |
| 1915.75 | 1.000 | 0.001 | 1.000 |
| 1916.00 | 1.000 | 0.001 | 1.000 |
| 1916.25 | 1.000 | 0.001 | 1.000 |
| 1916.50 | 1.000 | 0.001 | 1.000 |
| 1916.75 | 0.477 | 0.226 | 0.755 |
| 1917.00 | 0.332 | 0.256 | 0.759 |
| 1917.25 | 0.186 | 0.235 | 0.600 |
| 1917.50 | 0.102 | 0.248 | 0.400 |
| 1917.75 | 0.157 | 0.232 | 0.483 |
| 1918.00 | 0.305 | 0.182 | 0.626 |
| 1918.25 | 0.453 | 0.155 | 0.707 |
| 1918.50 | 0.600 | 0.116 | 0.829 |
| 1918.75 | 0.553 | 0.123 | 0.861 |
| 1919.00 | 0.507 | 0.128 | 0.906 |
| 1919.25 | 0.298 | 0.195 | 0.685 |
| 1919.50 | 0.089 | 0.267 | 0.517 |
| 1919.75 | 0.129 | 0.280 | 0.461 |
| 1920.00 | 0.168 | 0.272 | 0.484 |
| 1920.25 | 0.208 | 0.270 | 0.495 |
| 1920.50 | 0.256 | 0.226 | 0.557 |
| 1920.75 | 0.527 | 0.135 | 0.858 |
| 1921.00 | 0.562 | 0.130 | 0.976 |
| 1921.25 | 0.597 | 0.139 | 0.928 |
| 1921.50 | 1.000 | 0.001 | 1.000 |
| 1921.75 | 1.000 | 0.001 | 1.000 |
| 1922.00 | 1.000 | 0.001 | 1.000 |
| 1922.25 | 1.000 | 0.001 | 1.000 |
| 1922.50 | 0.593 | 0.166 | 0.906 |
| 1922.75 | 1.000 | 0.001 | 1.000 |
| 1923.00 | 1.000 | 0.001 | 1.000 |
| 1923.25 | 1.000 | 0.001 | 1.000 |
| 1923.50 | 1.000 | 0.001 | 1.000 |
| 1923.75 | 1.000 | 0.001 | 1.000 |
| 1924.00 | 0.395 | 0.214 | 0.743 |
| 1924.25 | 0.423 | 0.203 | 0.763 |
| 1924.50 | 0.607 | 0.121 | 0.932 |
| 1924.75 | 0.616 | 0.083 | 1.020 |
| 1925.00 | 0.625 | 0.045 | 1.170 |
| 1925.25 | 0.589 | 0.076 | 0.987 |
| 1925.50 | 0.511 | 0.127 | 0.806 |
| 1925.75 | 0.478 | 0.143 | 0.766 |
| 1926.00 | 0.521 | 0.135 | 0.762 |
| 1926.25 | 0.446 | 0.153 | 0.738 |
| 1926.50 | 0.441 | 0.152 | 0.739 |
| 1926.75 | 0.436 | 0.163 | 0.717 |
| 1927.00 | 0.389 | 0.177 | 0.650 |
| 1927.25 | 0.338 | 0.216 | 0.463 |

WELL: 34-10-3 (1890 - 2100)

DATE: 24OCT79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-----------|-------|-------|
| 1927.50 | 0.287 | 0.238 | 0.474 |
| 1927.75 | 0.277 | 0.252 | 0.487 |
| 1928.00 | 0.258 | 0.252 | 0.530 |
| 1928.25 | 0.301 | 0.208 | 0.581 |
| 1928.50 | 0.343 | 0.148 | 0.754 |
| 1928.75 | 0.229 | 0.243 | 0.520 |
| 1929.00 | 0.386 | 0.227 | 0.488 |
| 1929.25 | 0.163 | 0.294 | 0.405 |
| 1929.50 | 0.162 | 0.302 | 0.382 |
| 1929.75 | 0.162 | 0.316 | 0.351 |
| 1930.00 | 0.157 | 0.313 | 0.301 |
| 1930.25 | 0.152 | 0.312 | 0.314 |
| 1930.50 | 0.198 | 0.292 | 0.360 |
| 1930.75 | 0.253 | 0.253 | 0.459 |
| 1931.00 | 0.259 | 0.224 | 0.549 |
| 1931.25 | 0.212 | 0.231 | 0.538 |
| 1931.50 | 0.066 | 0.235 | 0.461 |
| 1931.75 | 00000.000 | 0.309 | 0.290 |
| 1932.00 | 00000.000 | 0.368 | 0.199 |
| 1932.25 | 00000.000 | 0.366 | 0.145 |
| 1932.50 | 00000.000 | 0.371 | 0.103 |
| 1932.75 | 00000.000 | 0.371 | 0.107 |
| 1933.00 | 00000.000 | 0.360 | 0.178 |
| 1933.25 | 00000.000 | 0.352 | 0.197 |
| 1933.50 | 00000.000 | 0.335 | 0.224 |
| 1933.75 | 00000.000 | 0.411 | 0.260 |
| 1934.00 | 1.000 | 0.001 | 1.000 |
| 1934.25 | 1.000 | 0.001 | 1.000 |
| 1934.50 | 1.000 | 0.001 | 1.000 |
| 1934.75 | 1.000 | 0.001 | 1.000 |
| 1935.00 | 00000.000 | 0.322 | 0.171 |
| 1935.25 | 00000.000 | 0.345 | 0.166 |
| 1935.50 | 00000.000 | 0.352 | 0.188 |
| 1935.75 | 00000.000 | 0.351 | 0.218 |
| 1936.00 | 00000.000 | 0.352 | 0.201 |
| 1936.25 | 00000.000 | 0.350 | 0.176 |
| 1936.50 | 00000.000 | 0.357 | 0.184 |
| 1936.75 | 00000.000 | 0.353 | 0.199 |
| 1937.00 | 00000.000 | 0.348 | 0.219 |
| 1937.25 | 00000.000 | 0.349 | 0.237 |
| 1937.50 | 00000.000 | 0.348 | 0.238 |
| 1937.75 | 00000.000 | 0.347 | 0.191 |
| 1938.00 | 00000.000 | 0.346 | 0.153 |
| 1938.25 | 00000.000 | 0.354 | 0.173 |
| 1938.50 | 00000.000 | 0.356 | 0.200 |
| 1938.75 | 0.006 | 0.358 | 0.231 |
| 1939.00 | 0.049 | 0.346 | 0.278 |
| 1939.25 | 0.093 | 0.326 | 0.340 |
| 1939.50 | 0.152 | 0.296 | 0.375 |
| 1939.75 | 0.189 | 0.280 | 0.397 |

WELL: 34-10-3 (1890 - 2100)

DATE: 24 OCT 79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-------|-------|-------|
| 1940.00 | 0.281 | 0.246 | 0.438 |
| 1940.25 | 0.290 | 0.232 | 0.467 |
| 1940.50 | 0.299 | 0.222 | 0.498 |
| 1940.75 | 0.280 | 0.214 | 0.537 |
| 1941.00 | 0.363 | 0.184 | 0.638 |
| 1941.25 | 0.455 | 0.160 | 0.700 |
| 1941.50 | 0.482 | 0.156 | 0.719 |
| 1941.75 | 0.500 | 0.150 | 0.747 |
| 1942.00 | 0.556 | 0.134 | 0.788 |
| 1942.25 | 0.611 | 0.115 | 0.849 |
| 1942.50 | 0.700 | 0.065 | 1.031 |
| 1942.75 | 0.795 | 0.036 | 1.101 |
| 1943.00 | 0.808 | 0.033 | 1.133 |
| 1943.25 | 0.748 | 0.063 | 1.143 |
| 1943.50 | 0.701 | 0.070 | 1.153 |
| 1943.75 | 0.626 | 0.112 | 0.999 |
| 1944.00 | 0.445 | 0.182 | 0.849 |
| 1944.25 | 0.264 | 0.231 | 0.537 |
| 1944.50 | 0.083 | 0.196 | 0.473 |
| 1944.75 | 0.105 | 0.103 | 0.750 |
| 1945.00 | 0.151 | 0.036 | 2.143 |
| 1945.25 | 0.243 | 0.028 | 2.356 |
| 1945.50 | 0.345 | 0.105 | 0.922 |
| 1945.75 | 0.358 | 0.201 | 0.626 |
| 1946.00 | 0.372 | 0.195 | 0.647 |
| 1946.25 | 0.445 | 0.167 | 0.708 |
| 1946.50 | 0.456 | 0.159 | 0.742 |
| 1946.75 | 0.468 | 0.154 | 0.768 |
| 1947.00 | 0.518 | 0.138 | 0.792 |
| 1947.25 | 0.592 | 0.107 | 0.860 |
| 1947.50 | 0.638 | 0.088 | 0.931 |
| 1947.75 | 0.684 | 0.069 | 1.015 |
| 1948.00 | 0.695 | 0.061 | 1.110 |
| 1948.25 | 0.706 | 0.083 | 1.018 |
| 1948.50 | 0.599 | 0.119 | 1.023 |
| 1948.75 | 0.612 | 0.170 | 0.790 |
| 1949.00 | 0.607 | 0.183 | 0.741 |
| 1949.25 | 0.474 | 0.215 | 0.595 |
| 1949.50 | 0.340 | 0.243 | 0.477 |
| 1949.75 | 0.207 | 0.274 | 0.371 |
| 1950.00 | 0.170 | 0.238 | 0.425 |
| 1950.25 | 0.169 | 0.211 | 0.461 |
| 1950.50 | 0.169 | 0.175 | 0.535 |
| 1950.75 | 0.242 | 0.132 | 0.616 |
| 1951.00 | 0.316 | 0.177 | 0.672 |
| 1951.25 | 0.408 | 0.185 | 0.615 |
| 1951.50 | 0.408 | 0.202 | 0.584 |
| 1951.75 | 0.486 | 0.176 | 0.621 |
| 1952.00 | 0.522 | 0.161 | 0.651 |
| 1952.25 | 0.508 | 0.162 | 0.665 |

WELL: 34-10-3 (1890 - 2100)

DATE: 24OCT79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-----------|-----------|-------|
| 1952.50 | 0.498 | 0.154 | 0.705 |
| 1952.75 | 0.489 | 0.139 | 0.779 |
| 1953.00 | 0.627 | 0.089 | 0.920 |
| 1953.25 | 0.766 | 0.062 | 0.914 |
| 1953.50 | 0.835 | 0.049 | 0.919 |
| 1953.75 | 0.718 | 0.080 | 0.947 |
| 1954.00 | 0.755 | 0.077 | 0.945 |
| 1954.25 | 0.792 | 0.066 | 0.986 |
| 1954.50 | 0.726 | 0.082 | 0.983 |
| 1954.75 | 0.610 | 0.114 | 0.868 |
| 1955.00 | 0.494 | 0.134 | 0.838 |
| 1955.25 | 0.609 | 0.075 | 1.044 |
| 1955.50 | 0.724 | 0.067 | 0.943 |
| 1955.75 | 0.839 | 0.059 | 0.856 |
| 1956.00 | 0.758 | 0.081 | 0.875 |
| 1956.25 | 0.677 | 0.099 | 0.900 |
| 1956.50 | 0.639 | 0.112 | 0.902 |
| 1956.75 | 0.648 | 0.115 | 0.875 |
| 1957.00 | 0.652 | 0.116 | 0.853 |
| 1957.25 | 0.656 | 0.090 | 0.961 |
| 1957.50 | 0.688 | 0.050 | 1.153 |
| 1957.75 | 0.812 | 00000.000 | 1.311 |
| 1958.00 | 0.796 | 0.047 | 1.063 |
| 1958.25 | 0.779 | 0.103 | 0.879 |
| 1958.50 | 0.738 | 0.143 | 0.777 |
| 1958.75 | 0.697 | 0.127 | 0.864 |
| 1959.00 | 0.656 | 0.110 | 0.925 |
| 1959.25 | 0.615 | 0.114 | 0.899 |
| 1959.50 | 0.494 | 0.140 | 0.894 |
| 1959.75 | 0.325 | 0.204 | 0.757 |
| 1960.00 | 0.157 | 0.269 | 0.498 |
| 1960.25 | 00000.000 | 0.313 | 0.338 |
| 1960.50 | 0.023 | 0.335 | 0.244 |
| 1960.75 | 0.104 | 0.318 | 0.322 |
| 1961.00 | 0.184 | 0.303 | 0.418 |
| 1961.25 | 0.313 | 0.266 | 0.479 |
| 1961.50 | 0.362 | 0.246 | 0.500 |
| 1961.75 | 0.402 | 0.229 | 0.518 |
| 1962.00 | 0.397 | 0.212 | 0.553 |
| 1962.25 | 0.304 | 0.244 | 0.509 |
| 1962.50 | 0.340 | 0.244 | 0.521 |
| 1962.75 | 0.312 | 0.254 | 0.535 |
| 1963.00 | 0.237 | 0.275 | 0.465 |
| 1963.25 | 0.235 | 0.276 | 0.445 |
| 1963.50 | 0.137 | 0.290 | 0.423 |
| 1963.75 | 0.259 | 0.239 | 0.544 |
| 1964.00 | 0.361 | 0.217 | 0.588 |
| 1964.25 | 0.339 | 0.247 | 0.563 |
| 1964.50 | 0.361 | 0.239 | 0.608 |
| 1964.75 | 0.414 | 0.218 | 0.652 |

WELL: 34-10-3 C 1890 - 2100 0

DATE: 24 OCT 79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-----------|-----------|-------|
| 1965.00 | 0.515 | 0.178 | 0.731 |
| 1965.25 | 0.587 | 0.154 | 0.787 |
| 1965.50 | 0.571 | 0.170 | 0.808 |
| 1965.75 | 0.597 | 0.160 | 0.890 |
| 1966.00 | 0.617 | 0.151 | 0.981 |
| 1966.25 | 0.644 | 0.121 | 0.994 |
| 1966.50 | 0.511 | 0.161 | 0.859 |
| 1966.75 | 0.378 | 0.246 | 0.665 |
| 1967.00 | 1.000 | 0.001 | 1.000 |
| 1967.25 | 1.000 | 0.001 | 1.000 |
| 1967.50 | 1.000 | 0.001 | 1.000 |
| 1967.75 | 1.000 | 0.001 | 1.000 |
| 1968.00 | 00000.000 | 0.343 | 0.515 |
| 1968.25 | 00000.000 | 0.347 | 0.464 |
| 1968.50 | 00000.000 | 0.347 | 0.368 |
| 1968.75 | 00000.000 | 0.337 | 0.429 |
| 1969.00 | 0.003 | 0.342 | 0.431 |
| 1969.25 | 0.012 | 0.340 | 0.442 |
| 1969.50 | 0.054 | 0.281 | 0.517 |
| 1969.75 | 0.072 | 0.330 | 0.528 |
| 1970.00 | 0.107 | 0.319 | 0.552 |
| 1970.25 | 0.180 | 0.300 | 0.585 |
| 1970.50 | 0.313 | 0.247 | 0.676 |
| 1970.75 | 0.488 | 0.174 | 0.814 |
| 1971.00 | 0.611 | 0.122 | 0.934 |
| 1971.25 | 0.611 | 0.136 | 0.894 |
| 1971.50 | 0.488 | 0.183 | 0.832 |
| 1971.75 | 0.364 | 0.222 | 0.802 |
| 1972.00 | 0.241 | 0.231 | 0.859 |
| 1972.25 | 0.118 | 0.273 | 0.790 |
| 1972.50 | 0.124 | 0.286 | 0.777 |
| 1972.75 | 0.129 | 0.293 | 0.779 |
| 1973.00 | 0.135 | 0.301 | 0.779 |
| 1973.25 | 1.000 | 0.001 | 1.000 |
| 1973.50 | 1.000 | 0.001 | 1.000 |
| 1973.75 | 1.000 | 0.001 | 1.000 |
| 1974.00 | 1.000 | 0.001 | 1.000 |
| 1974.25 | 1.000 | 0.001 | 1.000 |
| 1974.50 | 1.000 | 0.001 | 1.000 |
| 1974.75 | 1.000 | 0.001 | 1.000 |
| 1975.00 | 0.613 | 0.199 | 0.820 |
| 1975.25 | 0.677 | 0.120 | 1.077 |
| 1975.50 | 0.649 | 0.067 | 1.503 |
| 1975.75 | 0.676 | 0.001 | 1.944 |
| 1976.00 | 0.722 | 00000.000 | 1.814 |
| 1976.25 | 0.754 | 0.122 | 0.852 |
| 1976.50 | 0.698 | 0.166 | 0.777 |
| 1976.75 | 1.000 | 0.001 | 1.000 |
| 1977.00 | 1.000 | 0.001 | 1.000 |
| 1977.25 | 1.000 | 0.001 | 1.000 |

WELL: 34-10-3 (1890 - 2100)

DATE: 24OCT79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-----------|-------|-------|
| 1977.50 | 1.000 | 0.001 | 1.000 |
| 1977.75 | 0.283 | 0.324 | 0.665 |
| 1978.00 | 0.334 | 0.239 | 0.864 |
| 1978.25 | 0.341 | 0.215 | 0.952 |
| 1978.50 | 1.000 | 0.001 | 1.000 |
| 1978.75 | 1.000 | 0.001 | 1.000 |
| 1979.00 | 1.000 | 0.001 | 1.000 |
| 1979.25 | 00000.000 | 0.356 | 0.916 |
| 1979.50 | 00000.000 | 0.335 | 1.013 |
| 1979.75 | 00000.000 | 0.338 | 1.000 |
| 1980.00 | 00000.000 | 0.330 | 1.018 |
| 1980.25 | 00000.000 | 0.332 | 1.003 |
| 1980.50 | 00000.000 | 0.342 | 0.968 |
| 1980.75 | 00000.000 | 0.344 | 0.957 |
| 1981.00 | 00000.000 | 0.342 | 0.957 |
| 1981.25 | 00000.000 | 0.341 | 0.952 |
| 1981.50 | 00000.000 | 0.348 | 0.924 |
| 1981.75 | 00000.000 | 0.350 | 0.926 |
| 1982.00 | 00000.000 | 0.346 | 0.943 |
| 1982.25 | 00000.000 | 0.348 | 0.954 |
| 1982.50 | 00000.000 | 0.336 | 1.004 |
| 1982.75 | 0.014 | 0.343 | 0.879 |
| 1983.00 | 1.000 | 0.001 | 1.000 |
| 1983.25 | 1.000 | 0.001 | 1.000 |
| 1983.50 | 0.289 | 0.215 | 1.037 |
| 1983.75 | 0.189 | 0.243 | 1.006 |
| 1984.00 | 0.067 | 0.301 | 0.913 |
| 1984.25 | 0.076 | 0.322 | 0.893 |
| 1984.50 | 0.085 | 0.327 | 0.895 |
| 1984.75 | 0.094 | 0.327 | 0.914 |
| 1985.00 | 0.112 | 0.324 | 0.941 |
| 1985.25 | 0.112 | 0.328 | 0.955 |
| 1985.50 | 0.065 | 0.335 | 0.940 |
| 1985.75 | 0.069 | 0.329 | 0.954 |
| 1986.00 | 0.082 | 0.322 | 0.964 |
| 1986.25 | 0.123 | 0.299 | 1.082 |
| 1986.50 | 0.128 | 0.288 | 1.041 |
| 1986.75 | 0.102 | 0.303 | 0.987 |
| 1987.00 | 0.108 | 0.299 | 0.996 |
| 1987.25 | 0.089 | 0.303 | 0.968 |
| 1987.50 | 0.029 | 0.321 | 0.906 |
| 1987.75 | 0.005 | 0.325 | 0.902 |
| 1988.00 | 0.078 | 0.307 | 0.952 |
| 1988.25 | 0.143 | 0.283 | 1.018 |
| 1988.50 | 0.161 | 0.270 | 1.025 |
| 1988.75 | 0.230 | 0.250 | 1.052 |
| 1989.00 | 0.271 | 0.227 | 1.109 |
| 1989.25 | 0.173 | 0.245 | 1.093 |
| 1989.50 | 0.076 | 0.301 | 0.928 |
| 1989.75 | 0.001 | 0.343 | 0.896 |

WELL: 34-10-3 (1890 - 2100)

DATE: 24OCT79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-----------|-------|-------|
| 1990.00 | 00000.000 | 0.347 | 0.929 |
| 1990.25 | 00000.000 | 0.345 | 0.940 |
| 1990.50 | 00000.000 | 0.339 | 0.963 |
| 1990.75 | 00000.000 | 0.333 | 0.964 |
| 1991.00 | 00000.000 | 0.321 | 0.984 |
| 1991.25 | 00000.000 | 0.321 | 1.007 |
| 1991.50 | 00000.000 | 0.320 | 1.016 |
| 1991.75 | 00000.000 | 0.330 | 0.991 |
| 1992.00 | 00000.000 | 0.344 | 0.942 |
| 1992.25 | 00000.000 | 0.349 | 0.940 |
| 1992.50 | 00000.000 | 0.349 | 0.932 |
| 1992.75 | 00000.000 | 0.336 | 0.960 |
| 1993.00 | 0.009 | 0.334 | 0.941 |
| 1993.25 | 0.050 | 0.321 | 0.967 |
| 1993.50 | 0.051 | 0.327 | 0.943 |
| 1993.75 | 0.088 | 0.316 | 0.989 |
| 1994.00 | 0.058 | 0.325 | 0.966 |
| 1994.25 | 0.039 | 0.332 | 0.945 |
| 1994.50 | 0.020 | 0.339 | 0.927 |
| 1994.75 | 0.040 | 0.333 | 0.945 |
| 1995.00 | 0.036 | 0.330 | 0.939 |
| 1995.25 | 0.020 | 0.336 | 0.910 |
| 1995.50 | 0.004 | 0.341 | 0.868 |
| 1995.75 | 00000.000 | 0.342 | 0.835 |
| 1996.00 | 0.017 | 0.335 | 0.830 |
| 1996.25 | 00000.000 | 0.342 | 0.847 |
| 1996.50 | 00000.000 | 0.348 | 0.906 |
| 1996.75 | 00000.000 | 0.347 | 0.964 |
| 1997.00 | 00000.000 | 0.346 | 0.973 |
| 1997.25 | 00000.000 | 0.341 | 0.993 |
| 1997.50 | 0.005 | 0.336 | 1.010 |
| 1997.75 | 0.051 | 0.319 | 1.041 |
| 1998.00 | 0.059 | 0.316 | 1.045 |
| 1998.25 | 0.078 | 0.303 | 1.067 |
| 1998.50 | 0.060 | 0.306 | 1.051 |
| 1998.75 | 0.030 | 0.319 | 1.020 |
| 1999.00 | 0.002 | 0.333 | 0.983 |
| 1999.25 | 0.020 | 0.328 | 1.008 |
| 1999.50 | 0.057 | 0.315 | 1.060 |
| 1999.75 | 0.088 | 0.314 | 1.058 |
| 2000.00 | 00000.000 | 0.345 | 0.981 |
| 2000.25 | 00000.000 | 0.345 | 0.981 |
| 2000.50 | 00000.000 | 0.343 | 0.962 |
| 2000.75 | 00000.000 | 0.333 | 0.963 |
| 2001.00 | 00000.000 | 0.324 | 0.986 |
| 2001.25 | 00000.000 | 0.318 | 1.003 |
| 2001.50 | 00000.000 | 0.326 | 0.975 |
| 2001.75 | 00000.000 | 0.345 | 0.991 |
| 2002.00 | 00000.000 | 0.345 | 0.946 |
| 2002.25 | 00000.000 | 0.336 | 0.927 |

WELL: 34-10-3 (1090 - 2100)

DATE: 24OCT79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-----------|-------|-------|
| 2002.50 | 0.079 | 0.300 | 0.992 |
| 2002.75 | 0.210 | 0.246 | 1.110 |
| 2003.00 | 0.325 | 0.217 | 1.143 |
| 2003.25 | 0.157 | 0.249 | 1.074 |
| 2003.50 | 00000.000 | 0.278 | 0.978 |
| 2003.75 | 00000.000 | 0.277 | 1.027 |
| 2004.00 | 0.039 | 0.288 | 1.032 |
| 2004.25 | 0.042 | 0.310 | 0.996 |
| 2004.50 | 0.044 | 0.313 | 1.029 |
| 2004.75 | 0.047 | 0.314 | 1.031 |
| 2005.00 | 0.050 | 0.314 | 1.034 |
| 2005.25 | 0.023 | 0.311 | 1.054 |
| 2005.50 | 00000.000 | 0.326 | 1.008 |
| 2005.75 | 00000.000 | 0.333 | 0.993 |
| 2006.00 | 00000.000 | 0.338 | 0.981 |
| 2006.25 | 00000.000 | 0.342 | 0.984 |
| 2006.50 | 00000.000 | 0.343 | 0.998 |
| 2006.75 | 00000.000 | 0.351 | 0.991 |
| 2007.00 | 00000.000 | 0.350 | 0.989 |
| 2007.25 | 00000.000 | 0.344 | 1.006 |
| 2007.50 | 00000.000 | 0.341 | 1.010 |
| 2007.75 | 00000.000 | 0.339 | 1.014 |
| 2008.00 | 00000.000 | 0.337 | 1.004 |
| 2008.25 | 00000.000 | 0.331 | 1.007 |
| 2008.50 | 00000.000 | 0.318 | 1.032 |
| 2008.75 | 00000.000 | 0.304 | 0.991 |
| 2009.00 | 00000.000 | 0.276 | 1.001 |
| 2009.25 | 00000.000 | 0.275 | 0.994 |
| 2009.50 | 00000.000 | 0.317 | 0.997 |
| 2009.75 | 0.037 | 0.316 | 0.961 |
| 2010.00 | 0.124 | 0.297 | 0.959 |
| 2010.25 | 0.180 | 0.261 | 1.019 |
| 2010.50 | 0.202 | 0.249 | 1.099 |
| 2010.75 | 0.188 | 0.261 | 1.102 |
| 2011.00 | 0.143 | 0.280 | 1.086 |
| 2011.25 | 0.020 | 0.309 | 0.966 |
| 2011.50 | 0.007 | 0.309 | 1.027 |
| 2011.75 | 00000.000 | 0.321 | 1.051 |
| 2012.00 | 00000.000 | 0.326 | 1.015 |
| 2012.25 | 0.018 | 0.346 | 0.995 |
| 2012.50 | 0.075 | 0.328 | 1.058 |
| 2012.75 | 0.073 | 0.343 | 1.018 |
| 2013.00 | 0.101 | 0.326 | 1.046 |
| 2013.25 | 0.033 | 0.347 | 0.999 |
| 2013.50 | 00000.000 | 0.351 | 0.968 |
| 2013.75 | 00000.000 | 0.338 | 1.001 |
| 2014.00 | 00000.000 | 0.348 | 0.971 |
| 2014.25 | 0.010 | 0.345 | 0.977 |
| 2014.50 | 00000.000 | 0.340 | 0.991 |
| 2014.75 | 00000.000 | 0.335 | 0.981 |

WELL: 34-10-3 (1890 - 2100)

DATE: 24OCT79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-----------|-------|-------|
| 2015.00 | 00000.000 | 0.333 | 0.964 |
| 2015.25 | 00000.000 | 0.342 | 0.949 |
| 2015.50 | 00000.000 | 0.341 | 0.964 |
| 2015.75 | 00000.000 | 0.336 | 0.988 |
| 2016.00 | 0.002 | 0.332 | 1.014 |
| 2016.25 | 0.063 | 0.321 | 1.047 |
| 2016.50 | 0.096 | 0.312 | 1.074 |
| 2016.75 | 0.049 | 0.335 | 0.999 |
| 2017.00 | 0.074 | 0.323 | 1.021 |
| 2017.25 | 0.098 | 0.313 | 1.039 |
| 2017.50 | 0.084 | 0.307 | 1.024 |
| 2017.75 | 0.080 | 0.293 | 1.035 |
| 2018.00 | 00000.000 | 0.303 | 0.903 |
| 2018.25 | 00000.000 | 0.282 | 0.868 |
| 2018.50 | 00000.000 | 0.261 | 0.840 |
| 2018.75 | 00000.000 | 0.250 | 0.807 |
| 2019.00 | 0.077 | 0.235 | 1.125 |
| 2019.25 | 0.114 | 0.259 | 1.287 |
| 2019.50 | 0.114 | 0.294 | 1.137 |
| 2019.75 | 0.113 | 0.316 | 1.059 |
| 2020.00 | 0.048 | 0.335 | 1.017 |
| 2020.25 | 0.064 | 0.330 | 1.030 |
| 2020.50 | 0.045 | 0.334 | 1.024 |
| 2020.75 | 0.033 | 0.336 | 1.024 |
| 2021.00 | 0.095 | 0.325 | 1.050 |
| 2021.25 | 0.084 | 0.329 | 1.044 |
| 2021.50 | 0.044 | 0.341 | 1.018 |
| 2021.75 | 00000.000 | 0.343 | 1.007 |
| 2022.00 | 0.056 | 0.331 | 1.032 |
| 2022.25 | 0.094 | 0.321 | 1.051 |
| 2022.50 | 0.143 | 0.304 | 1.101 |
| 2022.75 | 0.080 | 0.331 | 1.036 |
| 2023.00 | 0.090 | 0.325 | 1.067 |
| 2023.25 | 0.081 | 0.314 | 1.090 |
| 2023.50 | 0.026 | 0.318 | 1.074 |
| 2023.75 | 00000.000 | 0.331 | 1.035 |
| 2024.00 | 0.012 | 0.326 | 1.056 |
| 2024.25 | 00000.000 | 0.333 | 1.045 |
| 2024.50 | 00000.000 | 0.332 | 1.058 |
| 2024.75 | 00000.000 | 0.340 | 1.041 |
| 2025.00 | 00000.000 | 0.335 | 1.055 |
| 2025.25 | 00000.000 | 0.329 | 1.072 |
| 2025.50 | 00000.000 | 0.325 | 1.080 |
| 2025.75 | 0.105 | 0.282 | 1.236 |
| 2026.00 | 0.013 | 0.295 | 1.212 |
| 2026.25 | 00000.000 | 0.206 | 1.768 |
| 2026.50 | 00000.000 | 0.112 | 3.284 |
| 2026.75 | 00000.000 | 0.041 | 1.738 |
| 2027.00 | 00000.000 | 0.017 | 0.800 |
| 2027.25 | 00000.000 | 0.026 | 0.621 |

WELL: 34-10-3 < 1890 - 2100 >

DATE: 24 OCT 79 / ILP

| DEPTH | VSH | FHIF | SW |
|---------|-----------|-------|-------|
| 2027.50 | 00000.000 | 0.034 | 2.192 |
| 2027.75 | 00000.000 | 0.062 | 1.437 |
| 2028.00 | 00000.000 | 0.085 | 2.815 |
| 2028.25 | 00000.000 | 0.107 | 3.621 |
| 2028.50 | 00000.000 | 0.160 | 2.377 |
| 2028.75 | 0.083 | 0.221 | 1.657 |
| 2029.00 | 0.070 | 0.309 | 1.167 |
| 2029.25 | 0.085 | 0.304 | 1.192 |
| 2029.50 | 0.100 | 0.300 | 1.217 |
| 2029.75 | 0.157 | 0.286 | 1.261 |
| 2030.00 | 0.163 | 0.289 | 1.249 |
| 2030.25 | 0.137 | 0.298 | 1.211 |
| 2030.50 | 0.162 | 0.287 | 1.229 |
| 2030.75 | 0.133 | 0.300 | 1.175 |
| 2031.00 | 0.147 | 0.305 | 1.137 |
| 2031.25 | 0.172 | 0.297 | 1.143 |
| 2031.50 | 0.108 | 0.306 | 1.117 |
| 2031.75 | 0.056 | 0.314 | 1.085 |
| 2032.00 | 0.042 | 0.322 | 1.063 |
| 2032.25 | 0.054 | 0.326 | 1.052 |
| 2032.50 | 0.054 | 0.331 | 1.037 |
| 2032.75 | 0.079 | 0.333 | 1.028 |
| 2033.00 | 0.117 | 0.322 | 1.046 |
| 2033.25 | 0.154 | 0.302 | 1.095 |
| 2033.50 | 0.104 | 0.312 | 1.070 |
| 2033.75 | 0.076 | 0.315 | 1.058 |
| 2034.00 | 0.073 | 0.313 | 1.058 |
| 2034.25 | 0.040 | 0.319 | 1.037 |
| 2034.50 | 0.044 | 0.318 | 1.037 |
| 2034.75 | 0.048 | 0.317 | 1.037 |
| 2035.00 | 0.104 | 0.313 | 1.039 |
| 2035.25 | 0.090 | 0.321 | 1.018 |
| 2035.50 | 0.049 | 0.341 | 0.968 |
| 2035.75 | 0.055 | 0.344 | 0.958 |
| 2036.00 | 0.059 | 0.342 | 0.966 |
| 2036.25 | 0.145 | 0.311 | 1.042 |
| 2036.50 | 0.231 | 0.281 | 1.120 |
| 2036.75 | 0.172 | 0.301 | 1.073 |
| 2037.00 | 0.119 | 0.320 | 1.027 |
| 2037.25 | 0.081 | 0.335 | 0.992 |
| 2037.50 | 00000.000 | 0.361 | 0.929 |
| 2037.75 | 0.071 | 0.349 | 0.958 |
| 2038.00 | 0.051 | 0.346 | 0.970 |
| 2038.25 | 0.051 | 0.341 | 0.987 |
| 2038.50 | 0.132 | 0.311 | 1.065 |
| 2038.75 | 0.139 | 0.311 | 1.062 |
| 2039.00 | 0.107 | 0.321 | 1.037 |
| 2039.25 | 0.075 | 0.313 | 1.097 |
| 2039.50 | 0.100 | 0.300 | 1.164 |
| 2039.75 | 0.125 | 0.257 | 1.402 |

WELL: 34-10-9 (1950 - 2100)

DATE: 24OCT79/ILF

| DEPTH | VSH | PHIF | SW |
|---------|-----------|-------|-------|
| 2040.00 | 0.098 | 0.219 | 1.110 |
| 2040.25 | 0.072 | 0.223 | 1.070 |
| 2040.50 | 0.045 | 0.284 | 1.222 |
| 2040.75 | 0.083 | 0.327 | 1.037 |
| 2041.00 | 0.045 | 0.333 | 1.013 |
| 2041.25 | 0.068 | 0.327 | 1.015 |
| 2041.50 | 00000.000 | 0.355 | 0.951 |
| 2041.75 | 0.047 | 0.338 | 1.002 |
| 2042.00 | 0.025 | 0.350 | 0.980 |
| 2042.25 | 00000.000 | 0.356 | 0.973 |
| 2042.50 | 0.040 | 0.325 | 1.096 |
| 2042.75 | 0.059 | 0.301 | 0.988 |
| 2043.00 | 0.042 | 0.276 | 0.906 |
| 2043.25 | 0.025 | 0.258 | 0.815 |
| 2043.50 | 0.050 | 0.276 | 0.983 |
| 2043.75 | 0.101 | 0.313 | 1.115 |
| 2044.00 | 0.110 | 0.317 | 1.094 |
| 2044.25 | 0.032 | 0.345 | 1.016 |
| 2044.50 | 00000.000 | 0.361 | 0.967 |
| 2044.75 | 00000.000 | 0.361 | 0.968 |
| 2045.00 | 00000.000 | 0.360 | 0.969 |
| 2045.25 | 00000.000 | 0.370 | 0.944 |
| 2045.50 | 0.014 | 0.356 | 0.977 |
| 2045.75 | 0.002 | 0.355 | 0.979 |
| 2046.00 | 0.128 | 0.298 | 1.141 |
| 2046.25 | 0.112 | 0.300 | 1.135 |
| 2046.50 | 00000.000 | 0.341 | 1.004 |
| 2046.75 | 0.199 | 0.279 | 1.154 |
| 2047.00 | 0.150 | 0.294 | 1.104 |
| 2047.25 | 0.102 | 0.305 | 1.057 |
| 2047.50 | 0.053 | 0.314 | 1.020 |
| 2047.75 | 0.078 | 0.311 | 1.006 |
| 2048.00 | 0.090 | 0.316 | 1.010 |
| 2048.25 | 0.051 | 0.323 | 1.019 |
| 2048.50 | 0.021 | 0.330 | 0.996 |
| 2048.75 | 00000.000 | 0.335 | 0.979 |
| 2049.00 | 00000.000 | 0.322 | 1.018 |
| 2049.25 | 0.003 | 0.247 | 1.414 |
| 2049.50 | 0.009 | 0.171 | 2.178 |
| 2049.75 | 0.047 | 0.106 | 1.288 |
| 2050.00 | 00000.000 | 0.134 | 0.599 |
| 2050.25 | 00000.000 | 0.133 | 0.907 |
| 2050.50 | 00000.000 | 0.154 | 2.189 |
| 2050.75 | 0.037 | 0.230 | 1.506 |
| 2051.00 | 0.094 | 0.300 | 1.157 |
| 2051.25 | 0.082 | 0.304 | 1.171 |
| 2051.50 | 0.039 | 0.316 | 1.152 |
| 2051.75 | 00000.000 | 0.352 | 1.056 |
| 2052.00 | 00000.000 | 0.353 | 1.058 |
| 2052.25 | 00000.000 | 0.359 | 1.034 |

WELL: 34-10-3 (1250 - 2100)

DATE: 24 OCT 79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-----------|-------|-------|
| 2052.50 | 00000.000 | 0.361 | 1.030 |
| 2052.75 | 0.057 | 0.345 | 1.066 |
| 2053.00 | 00000.000 | 0.366 | 1.009 |
| 2053.25 | 00000.000 | 0.358 | 1.028 |
| 2053.50 | 00000.000 | 0.354 | 1.040 |
| 2053.75 | 0.126 | 0.306 | 1.181 |
| 2054.00 | 0.183 | 0.269 | 1.259 |
| 2054.25 | 0.095 | 0.284 | 1.184 |
| 2054.50 | 0.008 | 0.287 | 1.098 |
| 2054.75 | 00000.000 | 0.283 | 1.078 |
| 2055.00 | 00000.000 | 0.193 | 1.543 |
| 2055.25 | 00000.000 | 0.103 | 1.239 |
| 2055.50 | 00000.000 | 0.099 | 0.954 |
| 2055.75 | 00000.000 | 0.122 | 2.764 |
| 2056.00 | 00000.000 | 0.176 | 1.943 |
| 2056.25 | 00000.000 | 0.230 | 1.512 |
| 2056.50 | 00000.000 | 0.249 | 1.397 |
| 2056.75 | 00000.000 | 0.299 | 1.162 |
| 2057.00 | 0.042 | 0.289 | 1.202 |
| 2057.25 | 0.123 | 0.300 | 1.130 |
| 2057.50 | 0.016 | 0.349 | 0.983 |
| 2057.75 | 0.093 | 0.319 | 1.057 |
| 2058.00 | 00000.000 | 0.343 | 0.978 |
| 2058.25 | 0.035 | 0.327 | 1.008 |
| 2058.50 | 00000.000 | 0.343 | 0.954 |
| 2058.75 | 0.026 | 0.328 | 0.989 |
| 2059.00 | 0.044 | 0.313 | 1.012 |
| 2059.25 | 0.027 | 0.320 | 0.966 |
| 2059.50 | 0.027 | 0.320 | 0.941 |
| 2059.75 | 0.027 | 0.310 | 0.949 |
| 2060.00 | 0.013 | 0.302 | 0.954 |
| 2060.25 | 00000.000 | 0.299 | 0.918 |
| 2060.50 | 0.057 | 0.280 | 1.004 |
| 2060.75 | 0.114 | 0.270 | 1.055 |
| 2061.00 | 0.165 | 0.267 | 1.031 |
| 2061.25 | 0.242 | 0.243 | 1.082 |
| 2061.50 | 0.267 | 0.240 | 1.068 |
| 2061.75 | 0.281 | 0.241 | 1.177 |
| 2062.00 | 0.265 | 0.257 | 1.245 |
| 2062.25 | 0.023 | 0.356 | 0.980 |
| 2062.50 | 00000.000 | 0.359 | 0.978 |
| 2062.75 | 00000.000 | 0.356 | 0.990 |
| 2063.00 | 00000.000 | 0.354 | 1.000 |
| 2063.25 | 0.031 | 0.341 | 1.041 |
| 2063.50 | 00000.000 | 0.339 | 1.092 |
| 2063.75 | 00000.000 | 0.314 | 1.200 |
| 2064.00 | 00000.000 | 0.206 | 1.886 |
| 2064.25 | 0.228 | 0.075 | 1.435 |
| 2064.50 | 0.267 | 0.130 | 1.679 |
| 2064.75 | 0.156 | 0.228 | 1.463 |

WELL: 34-10-3 (1890 - 2100)

DATE: 24 OCT 79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-----------|-------|-------|
| 2065.00 | 0.044 | 0.325 | 1.030 |
| 2065.25 | 00000.000 | 0.339 | 0.982 |
| 2065.50 | 00000.000 | 0.343 | 0.960 |
| 2065.75 | 0.109 | 0.296 | 1.086 |
| 2066.00 | 0.185 | 0.288 | 1.078 |
| 2066.25 | 0.159 | 0.294 | 1.140 |
| 2066.50 | 0.073 | 0.325 | 1.054 |
| 2066.75 | 00000.000 | 0.351 | 0.979 |
| 2067.00 | 00000.000 | 0.358 | 0.954 |
| 2067.25 | 00000.000 | 0.360 | 0.941 |
| 2067.50 | 00000.000 | 0.356 | 0.943 |
| 2067.75 | 0.039 | 0.342 | 0.975 |
| 2068.00 | 0.065 | 0.329 | 1.005 |
| 2068.25 | 0.050 | 0.330 | 0.985 |
| 2068.50 | 0.032 | 0.334 | 0.958 |
| 2068.75 | 0.055 | 0.322 | 0.970 |
| 2069.00 | 0.018 | 0.334 | 0.926 |
| 2069.25 | 0.046 | 0.324 | 0.938 |
| 2069.50 | 0.140 | 0.288 | 1.016 |
| 2069.75 | 0.158 | 0.287 | 0.998 |
| 2070.00 | 0.176 | 0.286 | 0.980 |
| 2070.25 | 0.217 | 0.271 | 1.033 |
| 2070.50 | 0.195 | 0.272 | 1.053 |
| 2070.75 | 0.195 | 0.268 | 1.084 |
| 2071.00 | 0.099 | 0.304 | 1.002 |
| 2071.25 | 0.101 | 0.309 | 1.000 |
| 2071.50 | 0.184 | 0.281 | 1.027 |
| 2071.75 | 0.259 | 0.253 | 1.056 |
| 2072.00 | 0.277 | 0.235 | 1.128 |
| 2072.25 | 0.183 | 0.270 | 1.062 |
| 2072.50 | 0.166 | 0.209 | 1.018 |
| 2072.75 | 0.203 | 0.279 | 1.019 |
| 2073.00 | 0.302 | 0.234 | 1.117 |
| 2073.25 | 0.317 | 0.228 | 1.117 |
| 2073.50 | 0.403 | 0.194 | 1.167 |
| 2073.75 | 0.378 | 0.212 | 1.098 |
| 2074.00 | 0.313 | 0.238 | 1.048 |
| 2074.25 | 0.353 | 0.228 | 1.080 |
| 2074.50 | 0.323 | 0.232 | 1.098 |
| 2074.75 | 0.201 | 0.276 | 1.048 |
| 2075.00 | 0.219 | 0.290 | 1.044 |
| 2075.25 | 0.207 | 0.287 | 1.042 |
| 2075.50 | 0.185 | 0.287 | 1.037 |
| 2075.75 | 0.249 | 0.255 | 1.098 |
| 2076.00 | 0.255 | 0.249 | 1.089 |
| 2076.25 | 0.228 | 0.257 | 1.042 |
| 2076.50 | 0.250 | 0.244 | 1.073 |
| 2076.75 | 0.332 | 0.219 | 1.122 |
| 2077.00 | 0.398 | 0.201 | 1.148 |
| 2077.25 | 0.453 | 0.184 | 1.168 |

WELL: 34-10-3 (1890 - 2100)

DATE: 24 OCT 79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-------|-----------|-------|
| 2077.50 | 0.486 | 0.170 | 1.199 |
| 2077.75 | 0.486 | 0.170 | 1.191 |
| 2078.00 | 0.428 | 0.188 | 1.173 |
| 2078.25 | 0.431 | 0.179 | 1.234 |
| 2078.50 | 0.403 | 0.186 | 1.212 |
| 2078.75 | 0.381 | 0.193 | 1.182 |
| 2079.00 | 0.451 | 0.174 | 1.198 |
| 2079.25 | 0.453 | 0.173 | 1.181 |
| 2079.50 | 0.426 | 0.185 | 1.130 |
| 2079.75 | 0.413 | 0.191 | 1.114 |
| 2080.00 | 0.441 | 0.181 | 1.146 |
| 2080.25 | 0.445 | 0.175 | 1.149 |
| 2080.50 | 0.538 | 0.139 | 1.226 |
| 2080.75 | 0.531 | 0.146 | 1.173 |
| 2081.00 | 0.479 | 0.163 | 1.123 |
| 2081.25 | 0.468 | 0.163 | 1.116 |
| 2081.50 | 0.451 | 0.165 | 1.103 |
| 2081.75 | 0.533 | 0.138 | 1.145 |
| 2082.00 | 0.604 | 0.112 | 1.184 |
| 2082.25 | 0.573 | 0.122 | 1.169 |
| 2082.50 | 0.619 | 0.116 | 1.148 |
| 2082.75 | 0.586 | 0.124 | 1.150 |
| 2083.00 | 0.609 | 0.120 | 1.143 |
| 2083.25 | 0.587 | 0.135 | 1.089 |
| 2083.50 | 0.523 | 0.148 | 1.091 |
| 2083.75 | 0.523 | 0.135 | 1.166 |
| 2084.00 | 0.619 | 0.101 | 1.244 |
| 2084.25 | 0.703 | 0.082 | 1.239 |
| 2084.50 | 0.552 | 0.131 | 1.151 |
| 2084.75 | 0.401 | 0.182 | 1.040 |
| 2085.00 | 0.426 | 0.182 | 1.017 |
| 2085.25 | 0.451 | 0.158 | 1.097 |
| 2085.50 | 0.528 | 0.139 | 1.104 |
| 2085.75 | 0.475 | 0.153 | 1.149 |
| 2086.00 | 0.494 | 0.164 | 1.133 |
| 2086.25 | 0.513 | 0.154 | 1.123 |
| 2086.50 | 0.664 | 0.079 | 1.336 |
| 2086.75 | 0.938 | 00000.000 | 1.397 |
| 2087.00 | 0.986 | 00000.000 | 1.300 |
| 2087.25 | 0.843 | 0.033 | 1.277 |
| 2087.50 | 0.813 | 0.013 | 1.438 |
| 2087.75 | 0.706 | 0.059 | 1.321 |
| 2088.00 | 0.599 | 0.103 | 1.227 |
| 2088.25 | 0.695 | 0.058 | 1.328 |
| 2088.50 | 0.781 | 0.010 | 1.496 |
| 2088.75 | 0.781 | 0.014 | 1.510 |
| 2089.00 | 0.884 | 0.014 | 1.299 |
| 2089.25 | 0.935 | 0.003 | 1.314 |
| 2089.50 | 0.782 | 0.053 | 1.250 |
| 2089.75 | 0.762 | 0.059 | 1.234 |

WELL: 34-10-3 (1890 - 2100)

DATE: 24OCT79/ILP

| DEPTH | VSH | PHIF | SW |
|---------|-------|-----------|-------|
| 2090.00 | 0.581 | 0.124 | 1.098 |
| 2090.25 | 0.089 | 0.260 | 0.843 |
| 2090.50 | 0.076 | 0.220 | 1.000 |
| 2090.75 | 0.299 | 0.135 | 1.456 |
| 2091.00 | 0.522 | 0.097 | 1.480 |
| 2091.25 | 0.654 | 0.086 | 1.375 |
| 2091.50 | 0.732 | 0.045 | 1.399 |
| 2091.75 | 0.873 | 0.008 | 1.392 |
| 2092.00 | 1.000 | 0.001 | 1.000 |
| 2092.25 | 0.994 | 00000.000 | 1.179 |
| 2092.50 | 1.000 | 0.001 | 1.000 |
| 2092.75 | 0.912 | 0.025 | 1.171 |
| 2093.00 | 0.754 | 0.087 | 1.068 |
| 2093.25 | 0.738 | 0.089 | 1.080 |
| 2093.50 | 0.791 | 0.055 | 1.201 |
| 2093.75 | 0.977 | 0.011 | 1.147 |
| 2094.00 | 1.000 | 0.001 | 1.000 |
| 2094.25 | 1.000 | 0.001 | 1.000 |
| 2094.50 | 0.664 | 0.105 | 1.120 |
| 2094.75 | 0.700 | 0.074 | 1.269 |
| 2095.00 | 0.942 | 0.018 | 1.205 |
| 2095.25 | 0.937 | 0.035 | 1.183 |
| 2095.50 | 0.894 | 0.050 | 1.169 |
| 2095.75 | 0.845 | 0.067 | 1.155 |
| 2096.00 | 0.868 | 0.059 | 1.142 |
| 2096.25 | 0.771 | 0.051 | 1.266 |
| 2096.50 | 0.732 | 0.038 | 1.446 |
| 2096.75 | 0.722 | 0.016 | 1.702 |
| 2097.00 | 0.743 | 0.048 | 1.317 |
| 2097.25 | 0.820 | 0.028 | 1.392 |
| 2097.50 | 0.853 | 0.056 | 1.191 |
| 2097.75 | 0.918 | 0.027 | 1.256 |
| 2098.00 | 0.882 | 0.034 | 1.242 |
| 2098.25 | 0.820 | 0.069 | 1.158 |
| 2098.50 | 0.827 | 0.072 | 1.155 |
| 2098.75 | 0.777 | 0.081 | 1.203 |
| 2099.00 | 0.777 | 0.057 | 1.401 |
| 2099.25 | 0.860 | 0.009 | 1.690 |
| 2099.50 | 0.943 | 00000.000 | 1.427 |
| 2099.75 | 0.949 | 0.005 | 1.273 |
| 2100.00 | 0.863 | 0.035 | 1.207 |

COMPUTERIZED LOG INTERPRETATION

statoil
Den norske stats oljeselskap as
PROGRAM: PGH0377 VERSPEC
VERSION: 1 (28PR7D) +
BY: COP/DB-SEKSJONEN

WELL: 34/10-3

FIELD: WILDCAT

ENGINEER: J. RAFDAL

DATE: 22 OCT 1979

DEPTH INTERVAL: 1885 - 2100 (METER)

RKB: 25.0 (METER) SCALE: 1 : 200

PERMANENT DATUM: MSL

DEPTH REFERENCE: ISF/SONIC

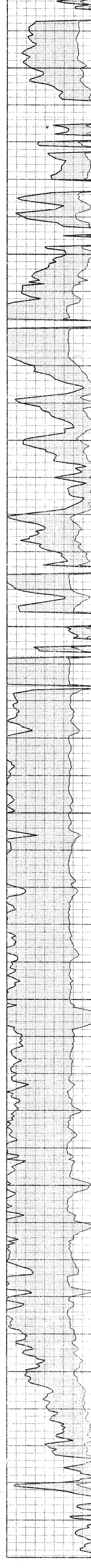
INPUT PARAMETERS:

| DEPTH INTERVAL | RW | RHF | RSH | RHOBSH | PHINSH | DTSH | FORM.TEMP. (DEG. F.) |
|----------------|-------|-------|------|--------|--------|-------|-------------------------|
| 1885 - 2100 | 0.073 | 0.130 | 1.50 | 2.35 | 0.45 | 120.0 | 160 |

BULK VOLUME

SAMPLE VOLUME (%) 100
ROCK VOLUME (%) 100
SANDSTONE

DEPTH
(METER)



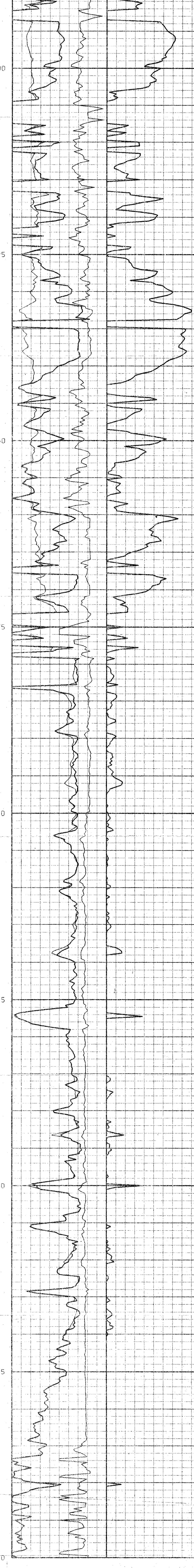
BULK VOLUME

POROSITY (%) 50
POROSITY X WATER SATURATN (%) 50

TOTAL PORE VOL.

WATER SATURATION (%) 0

DRAIN DENSITY
10MM/ML 3.0 3.5



COMPUTERIZED LOG INTERPRETATION

statOil
Den norske stats
oljeselskap a.s.
PROGRAM: PGMO377 VERSATEC
VERSION: 1 (2BPR7B) +
BY: COP/DB-SEKSJONEN

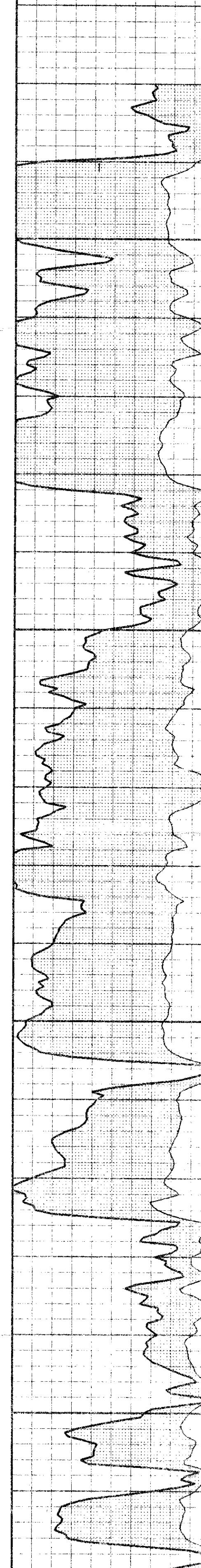
WELL: 34/10-3
FIELD: WILDCAT
ENGINEER: J.RAFDAL
DATE: 22 OCT 1979

DEPTH INTERVAL: 2490 - 2725 (METER)
RKB: 25.0 (METER) SCALE: 1 : 200
PERMANENT DATUM: MSL
DEPTH REFERENCE: ISP/SONIC

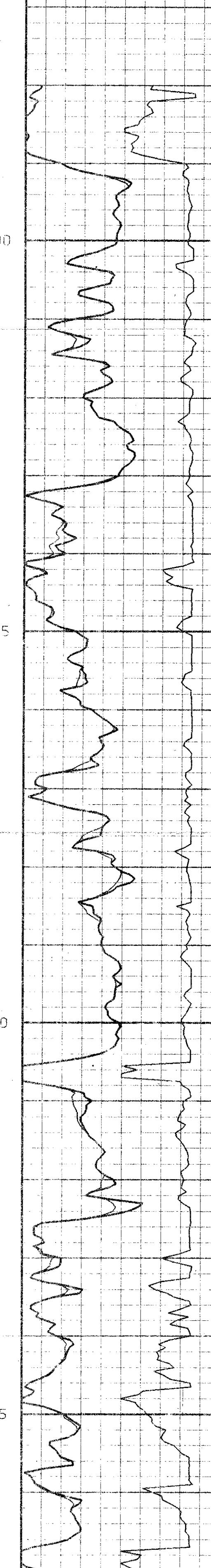
INPUT PARAMETERS:

| DEPTH INTERVAL | RW | RMF | RSH | RHOBSH | PHINSH | DTSH | FORM.TEMP (DEG. F) |
|----------------|-------|-------|------|--------|--------|-------|-----------------------|
| 2490 - 2725 | 0.062 | 0.105 | 2.00 | 2.45 | 0.45 | 100.0 | 185 |

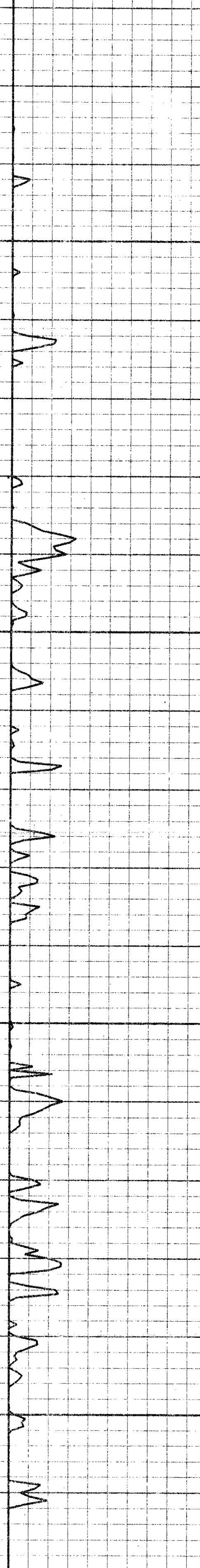
BULK VOLUME



BULK VOLUME



TOTAL PORE VOL.



DEPTH
(METER)

2475

2500

2525

2550

2575

2600

2625

2650

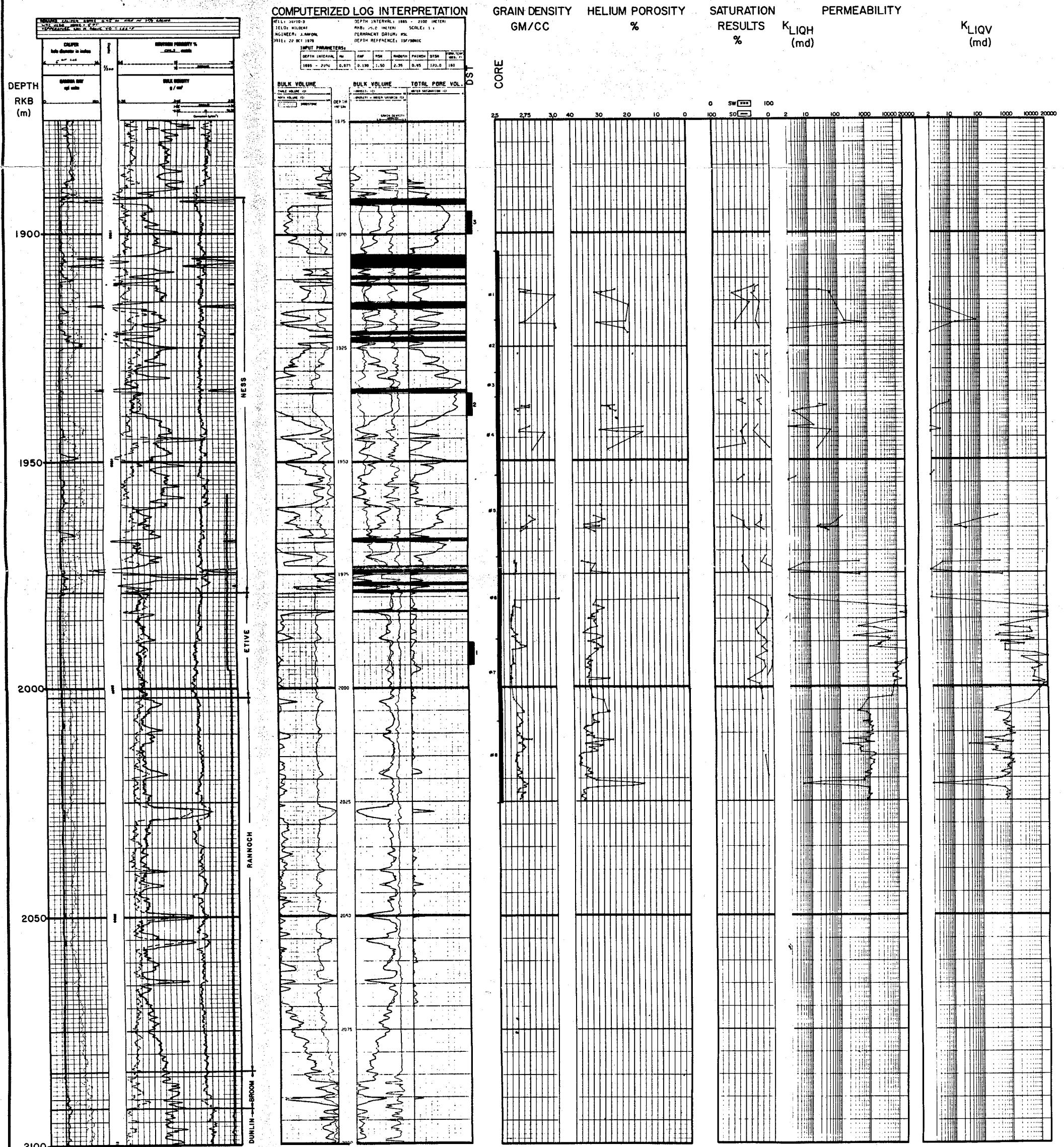
2675

2700

2725

SUMMARY LOG WELL 34/10-3

BRENT FORMATION



DST DATA

DST # 1
Interval : 1990 - 1995
Choke : 20/64"
Production : 2600 STB/D
Water

DST # 2
Interval : 1935 - 1940
Choke : (20+14)/64"
Production: 2850 STB/D (Oil)
 1167×10^3 SCF/D (Gas)

DST # 3
Interval : 1895 - 1900
Choke : 10/64"
Production : 650 STB/D (Oil)
sand plugging

Location
61°12' 49.5" N
02°11' 55.1" E

KBE elevation = 25 m
Water depth=179 m

Spudded:14.March 1979
Rig released:8.Juni 1979
Status:Plugged and abandoned

Oct. : 1979
PE / EVALTEK
JRa/AM

