## FORTROLIG i h.t. Besteriteinesinstruksen, jfr. offentlighetslovens §\_\_\_\_\_nr.

STATOIL FINAL REPORT WELL: 34/10-4 CORE NO. 1 - 6

October 1979.

## 26 OKT 1979 REGISTRERT OWEDIREKTORATET



#### **FINAL REPORT**

Well	34/10-4 VellC								No. 6	No. 6		
Field										7		
DEPTH	PERMI	ONTAL EBILITY DARCY	PERME	TICAL ABILITY DARCY	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORES	TURATION ATORAT	GRAIN DENS.	FORMATION DESCRIPTION		
2350.50-66	0.014	0.01			3.8	2.9	0.0	29.6	 2.67	.st.Gy.Fine gr. v.w.cemented w/calcitic		
2350:81-	0.010	0.01			1.8				2.67	A.A		
.23-32	0.124	0.07			5.1				2.67	A.A w/org.matter		
2351.56-74	2080	2020			30.8	21.6	0.0	56.1	2.63	s.st.Gy.Med.gr poor cemented		
2352.10-17	917	877			26.3				2.66	A.A trace of calcite		
2352.63-75	1530	1480		~.	30.0	30.2	0.0	74.7	2.67	A.A		
2353.53-64	5.7	4.3			22.6	29.0	2.5	70.2	2.70	s.st.Gy.Med/Fine gr. w.cemented calcitic		
2353.87-93	8.4	6.5			23.3				2.67	A.A. w/mica trace		
2354.21-27	13	10			21.2			-	2.68	s.st.Gy.Med/Fine gr. w.cemented w/mica		
									• • • • • • • • • • • • • • • • • • •			
			e	nd of	core no	<b>.</b> 6						
-												
-					-							
						· · · · · · · · · · · · · · · ·			·	· · · · · · · · · · · · · · · · · · ·		
-												

----

----

-



#### **FINAL REPORT**

	Company	Statoil	Date	October 1979
t	Well	34/10-4	Core	No. 5
	Field		State	Norway

	DEPTH	PERMI	ONTAL EBILITY DARCY KL	PERME	TICAL ABILITY DARCY KL	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORE-SAT PORESA SO	URATION TORAT STW.	GRAIN DENS.	FORMATION DESCRIPTION
19	07.60-70	4.8	3.6	n.v.p	•p	26.0				2.70	s.st.Gy.Med/Fine gr. w.cemented calcitic w/mica
<b>ا</b>	08.13-20	4.6	3.4	0.88	0.59	26.8				2.63	A.A
1	3.44-53	1.05	0.72	0.58	0.38	19.9	20.9	4.0	72.7	2.95	A.A w/siderite
19	08.85-92	295	275	0.83	0.56	29.3				2.70	s.st.Gy.Med/Fine gr. w.cemented calcitic w/gal
E.											
										-	
					end of	core	no. 5				
<b>.</b>			ţ								
Alter designed in the											
¢.	,										
	<u> </u>					-					
							-				
<b>L_</b>			· · ·								
· · ·											
W. I. C. LLAND											
· · ·					-			_			
[											
	ł		<b>.</b>								L

APPROX Distances

I

COLUMN ST



#### **FINAL REPORT**

Company	Statoil	Date .	October 1979
Well	34/10-4	Core .	No. 5
Field		State	Norway

DEPTH	PERME	ONTAL EBILITY DARCY   KL	PERME	TICAL ABILITY DARCY KL	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORE-SAT PORESA SO		GRAIN DENS.	FORMATION DESCRIPTION
1898.90-97	103	91	16	13	28.3				2.70	s.st.Gy.Med/Fine gr. w.cemented calcitic w/mica trace
1899.27-35	27	22	10.6	8.3	27.0	26.9	23.5	48.0	2.73	A.A
1).65-74	38	32	12	10	28.4				2.66	A.A
1900.17-25	6.3	4.7	1.06	0.72	27.4				2.70	A.A. w/coal trace
1900.45-55	95	84	8.1	6.2	30.6	32.1	27.6	42.6	2.68	A.A. without coal
 1901.02-10	127	113	28	24	32.2				2.65	A.A
1901.40-49	4.0	2.9	2.1	1.5	27.3				2.71	A.A
1901.75-85	6.4	4.9	2.6	1.9	29.0	24.8	34.1	41.4	2.68	A.A
1902.18-30	8.3	6.4	2.5	1.8	29.0				2.71	A.A
1902.50-56	11.5	9.1	1.08	0.74	28.4				2.65	A.A
19/02.86-96	26	22	8.2	6.3	30.3	31.1	22.7	45.4	2.68	A.A
<b>-</b> 1903.30-40	57	4.3	0.76	0.51	22.3				2.92	A.A. w/siderite
1903.73-80	18	15	2.9	2.1	29.0				2.71	s.st.Gy.Med/Fine gr. w.cemented calcitic
1904.15-25	4.0	3.0	1.6	1.1	28.6	23.6	26.3	54.8	2.80	A.A. w/siderite
1904.65-78	418	388	N.V.	₽.₽	33.6				2.64	s.st.Gy.Med/Fine gr. poor/w.cemented mica trace
1905.18-24	68	60	9.4	7.3	30.5				2.66	A.A. w/org.matter w/cemented
1905.65-77	191	171	13	10	34.7	26.4	19.8	40.4	2.64	s.st.Gy.Med/Fine gr. w.cemented mica trace
1906.18-28	3.4	2.5	0.86	- 0.58	27.2				2.65	A.A
1906.63-70	3.1	2.3	0.84	0.56	26.8				2.66	A.A. calcitic
1907.10-22	11.2	8.8	N.V.	P.P	25.4	31.9	16.5	55.3	2.67	A.A. w/org.matter

1

L

[ ,

and the second second



#### **FINAL REPORT**

Company	Statoil	DateOctober 1979
Well	34/10-4	No. 5
		State Norway

DEPTH	PERME	ONTAL EBILITY DARCY KL	PERME	FICAL ABILITY DARCY KL	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORE-SAT PORESA SO		GRAIN DENS.	FORMATION DESCRIPTION
1891.10-20	366	336	189	169	34.6	24.2	14.8	29.6	2.65	s.st.Gy.Med/Fine gr. w.cemented w/mica trace
1891.43-50	346	316	252	232	35.2				2.66	A.A
1(	519	489	317	287	35.0				2.65	A.A
1892.20-30	17	14	0.023	0.01	25.1	30.9	26.4	41.5	2.91	s.st.Gy.Fine gr. v.w.cemented W/siderite
1892.53-63	4.7	3.5	21	17	20.5				2.85	A.A
1892.85-93	340	310	149	134	33.7				2.67	s.st.Gy.Fine/med gr. w.cemented calcitic
1893.47-55	357	327	N.V.F	.P	34.8	33.6	28.2	35.3	2.66	A.A
1893.85-95	98	88	44	38	31.4				2.80	A.A
-1894.25-35	54	46	1.9	1.4	30.4				2.65	A.A without calcitic
1894.65-75	22	18	11.6	9.1	30.7	29.7	25.2	41.9	2.72	A.A calcitic org.matter
18-5.02-10	20	17	6.5	5.0	32.1				2.68	A.A w/mica trace
1895.30-37	339	309	144	129	35.8	-			2.64	s.st.Gy.Med/Fine gr. w/cemented w/mica trace
1895.80-90	82	73	17	13	32.8	34.7	23.0	49.0	2.73	A.A
1896.23-30	101	89	4.8	3.6	32.6				2.66	A.A
1896.60-70	54	46	7.8	6.0	30.3				2.67	A.A. calcitic
1896.92- 97.00	33	28	2.7	2.0	24.9	26.3	24.6	47.2	2.77	A.A
1897.31-40	16	13	4.3	3.2	23.3				2.77	A.A
1897.70-79	13	10	2.3	_ 1.7	26.9				2.63	A.A without calcitic org.matter
1898.03-10	422	392	61	53	35.3	32.0	27.3	43.5	2.65	s.st.Gy.Med/Fine gr. w.cemented calcitic w.mica trace
1898.50-60	212	192	49	42	33.6				2.64	A.A without calcitic

l

L

L



#### **FINAL REPORT**

 Company
 Statoil
 Date
 October 1979

 Well
 34/10-4
 Core
 No. 4

 Field
 State
 Norway

DEPTH	PERM	CONTAL EBILITY DARCY   KL	PERME	TICAL ABILITY DARCY KL	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORE-SAT PORESA SO	URATION TORAT STW.	GRAIN DENS.	FORMAȚION DESCRIPTION
1889.84-95	188	168	129	115	33.8	/0			2.68	s.st.Gy.Med/Fine.gr. w/cemented calcitic w/mica trace
1890.30-38	128	114	86	76	31.9				2.72	A.A
1.56-63	277	257	198	178	34.5	27.2	23.2	27.2	2.66	A.A
			end c	f core	no. 4					· · · · · · · · · · · · · · · · · · ·
							-			
<u> </u>								-		
									18	
L										
<u></u>				-						
									<u></u>	





Company	Statoil	Date .	October 1979
Well	34/10-4	Core .	No. 4
Field		State	Norway

DEPTH	PERM	ONTAL EBILITY DARCY	PERME	TICAL ABILITY DARCY KL	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORE-SAT PORESA SO		GRAIN DENS.	FORMATION DESCRIPTION
1881.40-47	741	701	471	441	36.1	/0	· · · · · · · · · · · · · · · · · · ·		2.66	s.st.Gy.Med/Fine gr. poor/w.cemented calcitic Mica trace
1881.71-80	960	920	754	714	37.5	35.6	31.8	34.7	2.65	A.A
1(	747	707	692	662	37.3				2.67	A.A
1882.46-56	1108	1058	796	756	38.5				2.65	A.A
1883.10-20	951	011	723	683	38.0	35.5	30.9	37.5	2.66	A.A
1883.52-63	1101	1051	706	666	38.3				2.65	A.A
1883.90-97	193	173	84	74	33.2				2.69	A.A. w.cemented
1884.30-40	403	373	256	236	35.4	22.8	22.7	28.3	2.66	A.A
1884.65-70	382	352	205	185	35.3				2.66	A.A
1884.96-	720	680	454	424	37.6				2.65	A.A poor/w.cemented
1805.44-55	681	651	619	589	37.5	22.9	29.8	20.5	2.64	A.A without calcitic
1885.93-	506	476	236	216	36.0				2.65	.A.A calcitic
1886.37-45	364	334	207	187	35.1				2.67	A.A. w.cemented
1886.80-92	483	453	282	262	36.0	34.2	31.1	34.8	2.66	A.A
1887.13-20	717	677	447	417	34.7				2.66	A.A. poor/w.cemented
1887.65-75	300	270	180	160	34.7				2.67	A.A
1888.05-15	295	275	154	139	35.0	25.8	24.1	36.1	2.67	A.A
1888.52-62	232	212	461	431	35.6				2.67	A.A
L889.00- 89.07	372	342	171	154	36.6				2.70	A.A
1889.35-46	677	647	154	138	38.4	32.6	29.2	36.5	2.67	A.A



### **FINAL REPORT**

Company	Statoil	Date October 1979
Well	34/10-4	
Field		State Norway

93 3 .H.P.F 192 3 34 6 21 8	KL 365 363 P 1142 694 881	ка N.V.P 238 439 954 872	218 409 914	% 34.8 35.7 38.8	% 31.9	30.2	38.9	2.76 2.76	s.st.Gy.Med/Fine gr. w.cemented,calcitic w/mica trace A.A
.H.P.I 192 : 34 ( 21 (	P 1142 694	439 954	409 914					2.76	A.A
192 : 34 ( 21 (	1142 694	954	914	38.8					
34 e 21 {	694			38.8					
21 8		872			36.4	30.3	34.3	2.66	s.st.Gy.Med./fine gr. poor cemented trace of calcitic trace of mica
	881		832	37.8				2.68	A.A poor/w.cemented
<u>190</u>		887	847	38.7				2.66	A.A
	1440	1121	1071	39.0	36.1	31.1	37.4	2.64	A.A. without mica
511	1461	1018	968	39.3				2.65	A.A
400	1350	1160	1110	39.4				2.72	A.A.with mica trace
046	996	812	772	38.5	28.9	22.0	41.1	2.66	A.A without mica
00	860	753	713	37.8				2.67	A.A
66	726	623	593	37.5				2.68	A.A. w/mica trace
18	878	720	680	37.1	27.6	21.6	40.1	2.69	<b>A.A</b>
.073	1023	1073	1023	38.6				2.66	A.A
.169	1119	1022	972	38.5				2.66	A.A
.462	1412	1187	1137	39.9	37.3	26.2	40.2	2.68	A.A
.241	1191	1120	1070	37.2				2.67	A.A
.079	1029	873	833	38.3				2.72	A.A
J.H.P	.P	1146	1096		30.1	23.8	37.8		
								2.66	A.A
	18 073 169 462 241 079	18     878       073     1023       169     1119       462     1412       241     1191       079     1029       .H.P.P	18       878       720         073       1023       1073         169       1119       1022         462       1412       1187         241       1191       1120         079       1029       873         .н.Р.Р       1146	18       878       720       680         073       1023       1073       1023         169       1119       1022       972         462       1412       1187       1137         241       1191       1120       1070         079       1029       873       833         .H.P.P       1146       1096	18       878       720       680       37.1         073       1023       1073       1023       38.6         169       1119       1022       972       38.5         462       1412       1187       1137       39.9         241       1191       1120       1070       37.2         079       1029       873       833       38.3         .H.P.P       1146       1096	18       878       720       680       37.1       27.6         073       1023       1073       1023       38.6          169       1119       1022       972       38.5          462       1412       1187       1137       39.9       37.3         241       1191       1120       1070       37.2         079       1029       873       833       38.3	18       878       720       680       37.1       27.6       21.6         073       1023       1073       1023       38.6	18       878       720       680       37.1       27.6       21.6       40.1         073       1023       1073       1023       38.6	18       878       720       680       37.1       27.6       21.6       40.1       2.69         073       1023       1073       1023       38.6       2.66         169       1119       1022       972       38.5       2.66         462       1412       1187       1137       39.9       37.3       26.2       40.2       2.68         241       1191       1120       1070       37.2       2.67       2.67         079       1029       873       833       38.3       2.72         .H.P.P.       1146       1096       30.1       23.8       37.8

ļ

1



#### **FINAL REPORT**

Company	Statoil	Date	October 1979
Well	34/10-4	Core	No. 3
Field		State	Norway

	DEPTH	Í PERMI	ONTAL EBILITY DARCY   KL	PERME	TICAL ABILITY DARCY KL	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORE-SAT PORESA SO	URATION TORAT STW.	GRAIN DENS.	FORMATION DESCRIPTION
18	72.98-					/0	70				s
	73.06	770	730	244	224	35.9	-			2.72	s.st.Gy Med/Fine gr. w/poor cemented w/mica trace calcitic
- - (	*				e.,						
-											
											·
			· · ·		i						
	L										
lunu I											
		· .									
1										-	
L								•			
	. <del></del>		<u> </u>								
1:	·				-						
		. <u>.</u>	1								

1



#### **FINAL REPORT**

	Company	Statoil	. Date .	October 1979
j.	Well	. 34/10-4	. Core	No. 3
	Field		. State	.Norway

DEPTH	Horizo Perme Millie Ka	BILITY	PERME	TICAL ABILITY DARCY KL	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORE-SAT PORESA SO		GRAIN DENS.	FORMATION DESCRIPTION
1865.30-38	1923	1863	1931	1871	40.6				2.71	s.st.Gy.Med/Fine gr. poor cemented trace of mica/calcitic
1865.68-77	865	825	149	134	36.7	39.3	28.1	29.8	2.73	A.A
3.00-07	702	662	599	569	37.0				2.72	s.st.Gy.Med/Fine gr, w/poor cemented w/mica calcitic
1866.32-41	1666	1616	1506	1456	39.1				2.67	s.st.Gy Med/Fine gr. poor cemented w/mica trace calcitic
1966.72-80	2126	2066	1603	1553	39.6	34.8	25.8	32.7	2.67	A.A
1867.22-32	2320	2240	1784	1724	40.3				2.67	A.A
1867.77-87	1601	1551	1215	1165	39.7				2.67	A.A
1868.07-18	758	718 '	643	613	37.1	39.0	29.3	33.0	2.71	A.A
1868.44-52	1472	1422	603	573	38.9				2.69	A.A
1868.80-86	1235	1185	947	907	38.4				2.69	A.A
, 18 <sup>(9</sup> .22-35	1210	1160	901	861	36.9	34.8	33.3	32.7	2.70	A.A
1869.74-82	1061	1011	889	849	38.3				2.69	A.A
1870.22-30	1195	1145	964	924	38.6				2.67	A.A
1870.49-63	1529	1479	978	938	39.3	34.3	24.5	39.0	2.66	A.A
1870.77-85	1271	1221	936	896	38.2				2.68	A.A
1871.17-25	1327	1277	603	573	38.7				2.68	A.A
1871.48-57	1050	1000	555	525	37.7	32.2	27.3	32.5	2.67	A.A
-1871.88-96	N.M.P	P	142	- 128	38.2				2.68	A.A
1872.19-29	422	392	106	94	34.0				2.75	A.A. w/poor cemented
1872.60-74	1073	1023	876	836	36.7	30.8	26.6	32.2	2.70	A.A

1

.

**FINAL REPORT** 



Company	Statoil	Date October 1979	
• •		No. 3	

i i

l

Į.

Ľ	DEPTH	Horizo Perme Millid Ka	BILITY	VERT PERME/ MILLIE KA	ABILITY	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORE-SAT PORESA SO		GRAIN DENS.	FORMATION DESCRIPTION
1857	7.00-14	N.M.P.		1484	1434		39.6	27.6	36.9	2.68	s.st.Gy.Med/Fine gr. poor cemented trace of mica/calcitic
1857	7.38-47	2251	2191	1523	1473	39.9				2.67	A.A
	7.66-74	1753	1693	1382	1332	38.3				2.68	A.A
1858	8.06-18	1388	1338	976	936	38.2	32.3	21.5	31.9	2.70	A.A
1858	8.46-54	934	894	595	565	37.2				2.70	A.A
1858	8.80-88	1570	1520	1384	1334	39.6				2.67	A.A
185	9.12-22	2066	2006	1694	1644	39.9	32.8	17.9	31.1	2.67	A.A
1859	9.65-73	1781	1721	1876	1816	39.3				2.68	A.A
L_186	0.34-42	1722	1662	1565	1515	39.1				2.68	A.A
186	0.71-83	1860	1800	1560	1510	39.4	36.5	33.2	29.2	2.69	A.A
<b>e</b> a <sup>11</sup>	1.10-22	1843	1783	1508	1458	39.2				2.68	A.A .
<sup>1</sup> /186	1.51-62	1881	1821	1641	1591	38.8				2.69	A.A
186	2.00-08	N.H.P	.P	1977	1917		36.9	25.3	33.8		·
186	2.48-56	N.H.P	•P	1640	1590						
186	3.30-39	1456	1406	1266	1216	38.2				2.69	A.A
186	53.50-64	0.56	0.37	2.3	1.7	11.9	18.8	23.6	26.4	2.71	s.st.Gy Fine gr. v.w.cemented calcitic
	53.92- 54.00	1322	1272	939	899	37.2				2.68	s.st.Gy Med/Fine gr.poor cemented trace of mice/
	54.25-33		1112	996	956	36.9				2.68	calcitic A.A
186	54.59-72	993	953	198	178	36.7	36.0	30.8	35.0	2.69	A.A
	54.98 <b>-</b> 55.04	1410	1360	1236	1180	38.8				2.72	A.A

ļ



### **FINAL REPORT**

Company	Statoil	Date	October 1979
Well		Core	No. 2
Field		State	Norway

DEPTH	HORIZO PERME MILLID KA	BILITY	PERME	FICAL ABILITY DARCY KL	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORE-SAT PORESA SO		grain Dens.	FORMATION DESCRIPTION
1845.20-30		1128	988	948	37.1	32.0	27.0	38.2	2.74	s.st.Gy.Med/Fine gr. w/poor cemented calcitic
1845.65-75	1146	1096	947	907	37.0				2.74	A.A
15.95-										
46.00	1425	1375	1035	985	37.8				2.72	A.A
1846.30-35	961	921	845	805	35.7	38.2	25.1	34.3	2.78	A.A
L1846.60-67	1257	1207	940	900	36.9				2.74	A.A
1846.90-95	1758	1698	692	662	38.6	26.7	31.4	40.3	2.70	A.A
1847.25-30	N.M.P	P,	1281	1231	38.6				2.69	A.A
1847.60-65	1492	1442	1479	1429	39.1	39.4	33.2	36.9	2.69	A.A
1847.95- 48.95-	1486	1436	1173	1123	38.2				2.70	A.A
	1211	1161	571	541	37.0		,		2.74	A.A
1848.80-85	1439	1389	1278	1228	38.1	37.0	33.7	35.9	2.70	A.A
18 <u>49.15-25</u>	1919	1859	1532	1482	38.9	33.6	30.6	38.2	2.67	A.A
1849.55-60	1550	1500	1283	1233	37.9				2.70	A.A
1849.85-90	1781	1721	1448	1398	38.2	37.1	29.9	36.1	2.70	A.A
1850.20-25	2156	2096	1628	1578	39.2				2.68	A.A
1850.58-63	1729	1669	1346	1296	37.6				2.69	A.A
1850.95-	1121	1171	966	- 926	36.6	36.8	31.2	34.1	2.71	A.A
1851.85- 52.00	0.058		0.01	0.01	6.9		·		2.71	s.st.Gy.Fine gr. v.w.cemented calcitic
1852.00- 52.10	0.166	0.10	0.03	5 0.02	10.6	30.2	38.4	39.4	2.71	A.A

. ÷ 🛲

÷....

4

l



#### **FINAL REPORT**

	Company	Statoil	Date .	
<b>a</b> r	Well	.34/10-4	Core .	
	Field		State	Norway

DEPTH	PERME	ONTAL BILITY DARCY   KL	PERME	FICAL ABILITY DARCY KL	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORE-SAT PORESA SO	URATION TORAT STW.	GRAIN DENS.	FORMATION DESCRIPTION
1841.96-										
42.06	1176	1126	747	707	36.6				2.76	s.st.Gy.Med.gr.w/poor cemented w/mica calciti
12.50-59	0.57	0.37	0.45	0.29	14.6				2.73	s.st.Gy Med/Fine gr. v.w.cemented calcitic
1842.88-										
43.00	0.012	0.01	0.03	0.02	2.6	10.4	0.0	1.4	2.73	A.A
18 <u>43.45-55</u>	0.012	0.01	0.021	0.01	2.4				2.73	A.A
1843.86-										
44.00	0.93	0.63	0.36	0.23	13.3	21.2	36.1	33.7	2.72	A.A
· · · · ·										
•										
• 										
							. •			
• . 										
· · · · · · · · · · · · · · · · · · ·				-						
ξ										

1

L

l

### **FINAL REPORT**



Company	Statoil	Date	October 1979
Well	34/10-4	Core	No. 1
Field		State .	Norway

DEPTH	Horizo Perme Millie Ka	BILITY	PERME	TICAL ABILITY DARCY	HELIUM PORO- SITY	SATURA- TION POROSITY	PORESA	TURATION	GRAIN DENS.	FORMATION DESCRIPTION
1833.69-80	2214	2154	1627	кL 1577	% 39.7	<u>%</u>			2.67	s.st.Gy.Med.gr.Poor cemented w/mica
L 18 <u>34.02-17</u>	2187	2127	1770	1710	39.2	38.5	33.2	33.2	2.68	AzA
4.56-65	1888	1828	1439	1389	38.5				2.72	A.A
1834.90-99	1200	1150	939	899	35.7		-		2.77	A.A.slight calcitic
1835.32-46	1875	1815	1266	1216	37: 9	27.4	19.5	35.2	2.73	A.A.without calcite
1835.68-75	1746	1686	1224	1174	37.9				2.73	A.A
1836.15-24	2413	2333	1695	1645	39.4				2.67	A.A
1836.74-88	2161	2101	1768	1708	39.8	38.5	28.2	31.4	2.68	A.A
_1837.16-29	2134	2074	1999	1939	40.9				2.67	A.A
1837.44-50	1708	1648	1023	973	39.6				2.69	A.A
-18°7.58-74	1515	1765	N.V.I	P.P.	40.3	30.2	25.7	29.8	2.69	A.A
1838.00-05	N.P.P									
1838.30-35	N.P.P									
1838.50-60	N.P.P					34.0	24.2	35.7		
_1838.90-95	N.P.P					-				
18 <u>39.25-</u> 33	1688	1638	1333	1283	38.1				2.71	A.A
 1839.49-63	1596	1546	1367	1317	38.8	36.7	32.7	29.9	2.70	A.A
1840.50-55	1910	1850	1440	- 1390	39.4				2.69	A.A
1841.00-08	1553	1503	1833	1773	39.5				2.70	A.A
1841.46-56	N.P.P					36.2	27.9	34.2		

L

1

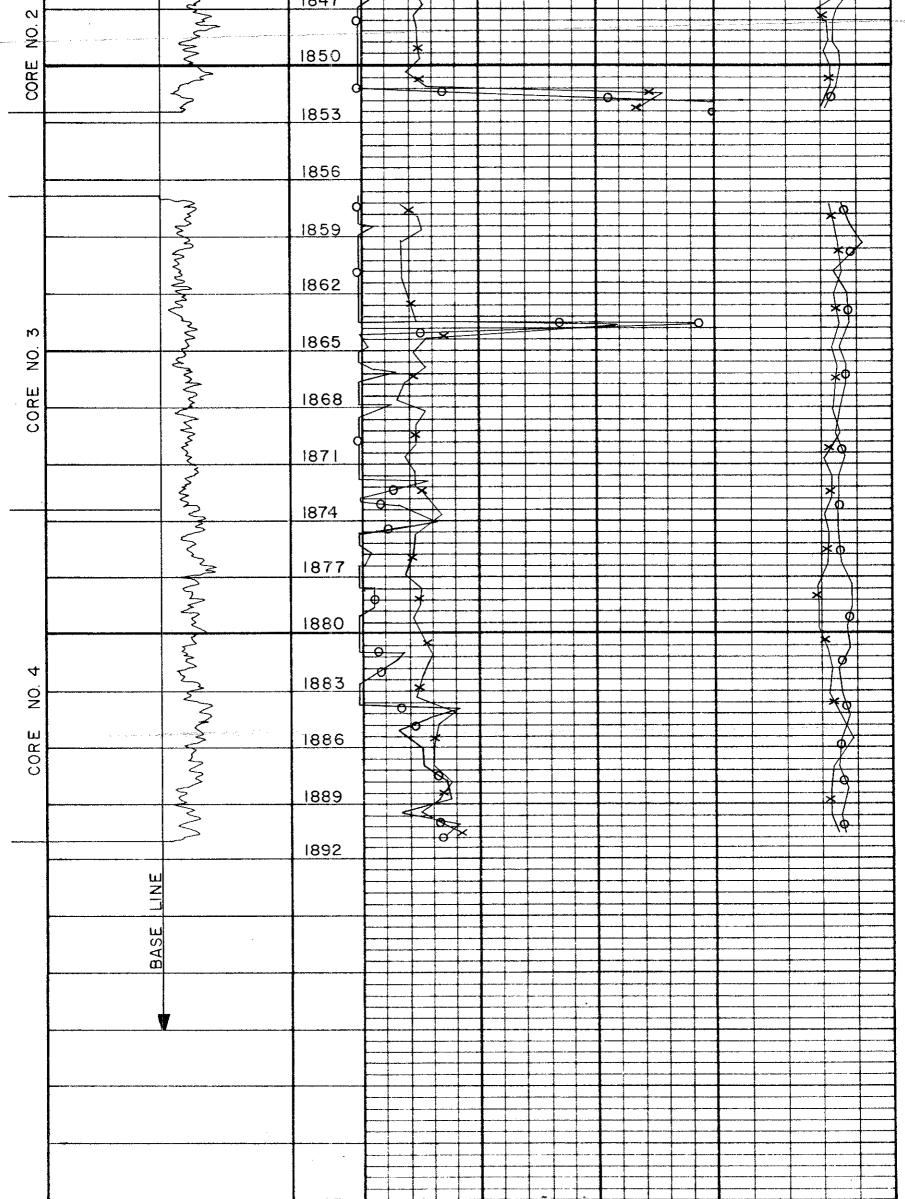
#### **FINAL REPORT**



Company	Statoil	Date	October 1979
• •			No. 1
Field		State	Norway

-	DEPTH	PERME	ONTAL BILITY DARCY KL	PERME	FICAL ABILITY DARCY KL	HELIUM PORO- SITY %	SATURA- TION POROSITY %	PORE-SAT PORESA SO		GRAIN DENS.	FORMATION DESCRIPTION
18	326.45-55		873	490	460	34.7	34.8	22.9	39.9	2.69	ssst.Gy Med.gr.w/poor cemented calcitic w/mica
L - 18	326.80,86	1171	1121	952	912	34.4				2.94	A.A sideritic
	27.04-12	1101	1051	912	872	33.4				2.92	A.A
1 18	327.26-36	1105	1055	941	901	32.9	29.0	31.9	34.5	2.94	A.A
18	327.70-77	1396	1346	996	956	35.2				2.84	s.st.Gy.Med.gr. poor cemented w/mica
	828.05-12	1748	1688	1371	1321	36.9		-		2.74	A.A.
182	28.41-50	N.H.P	Р.	948	908		34.8	23.3	36.8		
182	28.72-80	1176	1126	958	918	35.6				2.81	A.A
	29.05-16	1206	1156	893	853	35.5				2.77	A.A
182	29.32-49	1875	1815	1140	1090	37.9	33.1	28.3	32.8	2.73	A.A
1 3.0'	^9.72-80	1289	1239	978	938	36.7				2.71	A.A
L <sub>18:</sub>		1782	1722	.1407	1357	37.9				2.70	A.A
18	30.54-63	1534	1484	N.V.I	P.P.	37.4	39.5	30.9	35.0	2.73	A.A
18	30.91-98	1751	1691	1234	1184	38.5				2.72	A.A
L_18	31.26-34	1527	1477	1162	1112	38.1				2.74	A.A
18	31.58-72	1661	1611	1123	1073	37.8	36.2	30.2	33.7	2.71	A.A
18	32.00-08	1445	1395	1080	1030	37.4				2.71	A.A
-18	32.38-45	2025	1965	1517	- 1467	38.9				2.70	A.A
18	32.84-95	2109	2048	1411	1361	39.7	33.2	24.5	32.5	2.68	A.A
18	33.26-36	2207	2147	1564	1514	35.9				2.68	A.A

			, , ,																	
	ECO			- j		R			)C											
COMPANY <u>STATOIL</u> WELL <u>34/10 - 4</u>																				n-
																				-
							,				-									
		0		DE	ſ											×				
		Ŀ	0	nE	U		1A		Π											
to whom, a	lyses, opinions o and for whose exi	clusive	and co	ntidenti	aluse,	this I	report	is ma	ade. T	he in	terpre	tation	soro	e clie opinio	nt ns					
expressed	represent the be	st judg	iment o	f Geco	labor	atorie	s and	its o	fficers	and	empl	oyees		r.						
			VER	TICAL	SCA	LE	1:	200	·								÷			
	1	T	-																	
CORE - GAMMA SURFACE - LOG (PATENT APPLIED FOR) GAMMA RAY		PC PE			%	mD	HOR VER	- X NZON TICAL	ITAL -		- 0		×			FLU	ЛD	SATU	RATI	0
RADIATION INCREASE 985 V	DEPTH METER	i i	1 39	1	,	F 1	: 1	ļ	1		5 12	9	6	3	%	отні		01L 0-		- >
INTEGRATING TIME 11 SEC. COUNTS PER MINUTE 10 K		100(	DmD 6	4	2 100	)mD			<b>├</b> ╋	10r	nD		+	+	0	8	0 	60		20
					-								+							
																		+		+
X	1826																			+
Zm			0		5														* €	<b>)</b> 
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	1829	0		×															$ \rangle$	
$\sim$	1070	E														···· , · · · · · · · ·			16	-+
2	1832													i					*	
- Mary	1835			$\frac{1}{2}$															R	
$\langle \rangle$			<b>,</b>	4															+	<b>Ž</b>
	1838		$\left  \right\rangle$																- ]\$	
			$\left  \right\rangle$					 											X	+
	1841					<u> </u>													Å	
33	1844	F							<b>×</b>				×		۶ç					7
				*															×1 0×	+
	1847	$\checkmark$		$\left\{ + \right\}$	+	1		<b></b>	<b> </b>								<b></b>	-	139	1





		GECO			ratory	
						SEPT. 79
					ELEV	
		to whom, and for whose e	or interpretations are ba xclusive and confidential best ludgment of Geco I	GRAPH sed on observations and materi- use, this report is made. The is aboratories and its officers and	terpretations or opinions	
	CORE - GAMMA SURFAC (PATENT APPLIED FOR GAMMA RAY RADIATION INCREASE		PERMEABILIT	X	- 0	FLUID SATURATION
	VOLTAGE INTEGRATING TIME COUNTS PER MINUTE	METER	/0	100mD <sub>80</sub> 60 40 20 10		<u> </u>
	· · · · · · · · · · · · · · · · · · ·	1891				
	- WWW	1894				
		1897				
	No.	1900				
	Maria					
		1903				
┝		3 1906		00		
	-	> 1909	<b>}</b> ++++	X	A	0

																						• • •	
				<b>I</b>									$\vdash$										
				<u>}</u>	<u> </u>																		
		a parameter a dispersion and a second se													·· — · · ·	•••							
				<u> </u>									h						······································				··
		· ·····	2350										L										
		23		┣──													X	ļ,	<u> </u>		<u> </u>	-	C
9		5		<u> </u>														<u> </u>	2			×	
		5	2353			C				-										×			(
NO.		<u> </u>	2333	ļ		0			X			<b>0</b>	<u> </u>							<u> </u>			
~		5									X	0		a					L	<u>├</u> \	i		- Ø
CORE		~~~~																					
ЦС		5	2356																				
ö		3	2000																				
										_													
								<u> </u>								<b> </b>							
			2359																· · .				
													+				<u> </u>						
				<u>t</u>																			
		<b> </b>		<u> </u>					ļ												<u> </u>		
				<u> </u>	╞───┤			· · · ·														ł	
											·											1	
				<b>}</b>														ļ	ļ				
·													t		•••								
																						[	
				<u> </u>									+										
															[								
				L	[																		
										ļ				·				<u> </u>		ļ			···-
·-					L								<u> </u>										
ia.				_			<u> </u>						<u> </u>	<b> </b>		<b> </b>		ļ				ļ	
				· · · · · ·									<u> </u>							ļ		<u> </u>	
													ļ			[							
				<b></b>													i						
										·													
				[	ļ		<b> </b>							ļ		L					ļ		
														·					·····	·····		<u> </u>	
		· · · · · · · · · · · · · · · · · · ·	·																				
				┣—	<u> </u>								+					i				<u></u>	
												r	1									[	
						<b> </b>							+			<u> </u>		┟──┤				*	
	······································	· · · · · · · · · · · · · · · · · · ·	<u> </u>		1																	1	
					[																	Į	
					+	<u> </u>									ļ		·	<b></b>		<u>}</u>		<u> </u>	
																						t	
				Į	<b></b>	<u> </u>								<b> </b>	ļ	<b> </b>		ļ				ļ	
				├		<b> </b>	<u>.</u>						<u> </u>	<u> </u>	<u> </u>	<u> </u>				h		+	
	ngan se sengersegaenen in som	the second s											1									1	
	· · · · · · · · · · · · · · · · · · ·		······································	<b></b>	÷				┣──				+	──	<u> </u>	<b> </b>		+		<u> </u>	<u> </u>	<u> </u>	
					1													<b></b>				1	
				L	<u> </u>	ļ	<b> -</b>		ļ				<b>_</b>				<u> </u>		L	L			
				<u> </u>	<u>†</u>	-							1	1	<u>t                                    </u>	1		<u> </u>			<u> </u>	<u>†</u>	
					<b>F</b>					<u> </u>			ļ		ļ						ļ		
					<u> </u>		-						1	<u> </u>			<b></b> -				<u> </u>	<u>+</u>	
				F	<u> </u>	<b>—</b>	<u> </u>			F				<u> </u>		<b>—</b>		<b>—</b>			ļ	<u> </u>	
	·····			t		1						<u> </u>				1				1			
				[	ļ	ļ									<b>_</b>	Į							
				<u> </u>	<u>+</u>		<u> </u>	+	<b> </b>	<del> </del>			<u> </u>	<b> </b>	•	<u> </u>		<u> </u>		<b> </b>		<b></b>	
					İ										1						<u> </u>	1	
					ļ	ļ	ļ	ļ	L	ļ					ļ			<u> </u>		ļ	[	<b>İ</b>	
				<u> </u>	<b>+</b>	<del> </del>	<u> </u>	<u> </u>	<b>[</b>				+		–	<b> </b>	<b> </b>	<del> </del>	<b> </b>		<b>+</b>	+	<b> </b>
					1	<u> </u>	1											1				1	
				<b> </b>		Į	ļ	ļ	ļ	ļ		ļ		<b> </b>	ļ			ļ		ļ	ļ		L
				<b> </b>	+	<u> </u>	<del> </del>	<b> </b>	ł—	<u> </u>			+		<b>.</b>	<u>+</u>	<b> </b>	<b>∤</b>		<b>+</b>	<b> </b>		
					1										<b></b>	1							
				<b> </b>	ļ	ļ			I			]			1	ļ		<b></b>		+		4	
		······································	· · · · · · · · · · · · · · · · · · ·	t	<u>†</u>	<b>†</b>	<u>+</u>		<b>†</b>	<u> </u>		<u> </u>			<u>†</u>	<u>t</u>	<u> </u>	<u>†</u>	<b> </b>	<u>+</u>	<u>+</u>	<u> </u>	<b> </b>
					ļ		[			<u> </u>						<b></b>	[			ļ			
i				<u> </u>	<b>+</b>	<b> </b>	<u> </u>	<b> </b>	<b> </b>	<u>+</u>		<u>+</u>	+	<b> </b>	<del> </del>	<u> </u>	<u> </u>			<u> </u>	+	. <b>.</b>	
					1	<u> </u>	<u> </u>	<u> </u>		<u>†                                    </u>		<u> </u>	1			1	1			<u>t</u>	1	1	
		· · · · · -		┣		ļ	<u> </u>	ļ	<b> </b>	<u>+</u>	ļ	<u> </u>	+	<b> </b>	ļ			<u>                                     </u>		<u> </u>	ļ	ļ	
					ţ		<u>†</u>			1		<b></b>	1		1				<b></b>	<u></u>	<u></u>	<u> </u>	<u> </u>
				ļ	ļ	Į	<u> </u>	ļ	<b> </b>						ļ		·		Į	ļ	ļ	<u>+</u>	Į
				4	1	F.	1			1	1	1	1	1	1	1	E	1	4		1	1	f

	A	I I I		يبعد بالاحتيار فيترجد الم				· ·
--	---	-------	--	---------------------------	--	--	--	-----

