RESERVOIR FLUID STUDY 34/10-4.

REGIOTRERT

In order to obtain good information about the properties of the reservoir fluid in 34/10-4-Alfa, eight bottom hole samples were taken in the test of 34/10-4. Four samples in DST \neq 1 and four in DST \neq 2.

To check the quality of the samples it was decided to run a shortened PVT program which included determination of: Bubble point, compressability, GOR, Bo, reservoir fluid composition and the density of saturated reservoir fluid. All data were abailable before the two samples were selected for full PVT analysis.

Table no. 1 present the results, one each of seven samples. No. 8 was found to have a bubble point in the shipping container of approx. 340 Bar, of-course indicating that this would be unrepresentative. For the purpose of process simulation a composition among the seven was chosen to be given as representative of 34/10. This was sample bottle marked 73FA230-26. The value of bubble point, GOR and Bo lay nearest to the mean of all the samples. The variation in composition throughout are only slight and within the error limits of the analysis.

Reported in table 2 are the extended analysis of the reservoir fluid wnich is calculated on the basis of chromatography and TBP destillation of 34/10-1 crude.

The analysis show that sampling condition and handling has been very good. Variation in bubble point show up with higher GOR and Bo, but overall changes are only very slight and are random. The samples show a uniform reservoir hydrocarbon system over the depth of reservoir and the data derived from these should be good.

Statoil Production Laboratory,

Per Thomassen

Groupleader PVT/Chemistry

File: 050 050-P5

DEL 34/10-2 .17.04

BOTTOM HOLE

SAMPLES

STATOIL RESERVOIR WELL FLUID 34/10-4 STUDY

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DST # :	1	1	1	1	2	2	2	.2
BHS # :	1	2	3	4	1	2	3	4
Bottle No.:	22024-68	73FA230-26	22024-73	2657/30	22226-116	20475-62	20475-66	14068/66
Components:			RESERVO	OIR FLUID CO	MPOSITION, M	OLE %		
N ₂	0.52	0.50	0.50	0.54	0.52	0.49	0.49	δ
ω_2	0.94	0.93	0.92	0.92	0.98	1.00	1.00	SAMPLE
c_1^2	44.51	44.19	44.38	43.98	44.10	44.25	44.43	
C ₂	3.74	3.71	3.75	3.70	3.79	3.63	3.73	NOT
c ₃	1.32	1.29	1.33	1.31	1.35	1.25	1.33	
iC ₄	0.60	0.58	0.61	0.61	0.62	0.59	0.61	REPRESENTATIVE
nC_4	0.76	0.74	0.78	0.77	0.79	0.75	0.79	SEN
ic ₅	0.65	0.64	0.67	0.66	0.67	0.64	0.67	TAT
nC ₅ ·	0.38	0.38	0.39	0.40	0.40	0.37	0.40	IVE
c ₆	1.00	1.00	0.98	1.01	0.97	0.94	1.00	
C ₇ +	45.57	46.05	45.69	46.10	45.81	46.08	45.56	
,	100.00	100.00	100.00	100.00	100.00	100.00	100.00	
C7+ mol. weight	238	238	238	238	238	238	238	
C ₇ + density	0.8859	0.8863	0.8869	0.8866	0.8863	0.8863	0.8863	
Density of res.fl.	0.761	0.766	0.763	0.769	0.766	0.769	0.761	
Bubble pt., Bar	244.3	243.0	243.7	241.0	243.4	241.5	242.0	
Co, vol/vol/bar l	0^{-5} 11.2	11.2	11.0	11.0	11.6	11.3	11.6	
$GOR SM^3/M^3$	101.2	99.7	100.8	99.3	100.6	98.7	100.9	
Density of oil g/o	cc 0.8820	0.8827	0.8828	0.8828	0.8824	0.8821	0.8820	
Gravity gas*	0.7034	0.7040	0.7043	0.7091	0.7098	0.6945	0.7049	1
Bo, $M^{3}/M^{3}**$	1.274	1.265	1.271	1.261	1.266	1.257	1.273	,
Form. temp.	72.2°C	72.2 ⁰ C	72.2°C	72.2°C	71.70 _C	71.7°C	71.7°C	

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* γg , GOR, Bo from sigleflash of oil from reservoir condition to 1 atm., $15^{\circ} C$.

** Bo is M³ of reservoir fluid pr. M³ of stock tank fluid at l atm., 15°C.

*** Average compressability to oil above saturation pressure.

Error limits on reported values:

GOR : $\pm 0.3 \text{ sm}^3/\text{m}^3$, 1.7 SCF/BBL

BO : $\pm 3 \times 10^{-3} \text{ M}^3/\text{M}^3$

 ρ res. fluid: $\pm 2 \times 10^{-3}$ g/cc

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Table 2: Extended Reservoir Fluid Analysis based on Chromatography and TBP distillation.

	Components	Mole %	Mole weights	Spes. grav.g/cc	at SC
	N ₂	0.50			
**	co ₂	0.93			
•	c_1^{-}	44.19			
•	c_2^-	3.71	•		
	c_3	1.29			
	iC ₄	0.58			
	nC ₄	0.74			.
	iC ₅	0.64		•	:
Groups	nC ₅	0.38			
CUTI	c ₆	1.00	84	0.700	•
CUT2	C ₇	2.91	96	0.743	:
CUT3	c ₈	3.34	107	0.766	·
CUT4	c ₉	3.14	121	0.787	-
CUT5	c ₁₀	2.78	134	0.803	
CUT6	c_{11}	2.65	147	0.813	-
CUT7	c ₁₂	2.53	161	0.831	
CUT8	c ₁₃	2.14	175	0.843	
CUT9	c ₁₄	1.91	190	0.854	
CUT10	C _{15,16,17}	5.30	221	0.871	
CUT11	^C 18,19,20		263	0.880	
CUT12	C _{21,22,23}		303	0.900	
CUT13	C ₂₄ +	12.78	393	0.946	
		100.00			