

Denne rapport  
tilhører



# L&U DOK. SENTER

L. NR. 12383050150

KODE Well 31/2-11 nr 21

Returneres etter bruk

## DRILLING PROGRAMME

LOCATION 31/2-M

(11)

Drilling Progr. 31/2-M (11)

January 1983

A/S NORSKE SHELL  
LICENCE 054

Drilling Progr. 3A/2-M (11)

DRILLING PROGRAMME

LOCATION 31/2-M

(11)

January 1983

A/S NORSKE SHELL  
LICENCE 054

NORSKE SHELL E.B.P. FORUS.

DRILLING PROGRAMME

CONFIDENTIAL

LOCATION: 31/2-H  
WELL: 31/2-11  
RIG: Borgny Dolphin




PRODUCTION LICENCE No.: 054  
ESTIMATED DAYS: 50 (incl. Prod. test)

CO-ORDINATES OF LOCATION  
60 deg 49' 28.3" N  
03 deg 25' 29.7" E

HOLE SIZE (IMS)	MOLE DEPTH / CASING DEPTH (metres)	CASING SIZE / WT / GRAD / CPLG	CEMENT		MUD		LOGGING	DERRICK FLOOR ELEVATION	M. ABOVE SEA BED	
			Type / Mj/water	Reqd on Board (Tons)	REMARKS	REMARKS				REMARKS
36"	465 / 455	30" / 1" WT / 310 / X-52 ATD-RB Squinch	Class "G" S'water	150	See Enclosure 2A	1.03 (445)	Seawater + Viscous P111s (+/- 100 MF)	None	FORMATION TOP	360 M ABOVE SEA BED
26" See note 3	810 / 800	20" / 129 / X-52 Vetco LS - LH	Class "G" S'water	220	See Enclosure 2B	1.03 (445)	Gelled seawater + viscous p111s	(In 14-3/4" pilot hole) ISF/SONIC/SP/GR LDT/CNL/CAL/GR	Seabed (Quaternary/Pliocene/Miocene) Oligocene Eocene Baldor Formation Paleocene Selle Formation Lista Formation Upper Cretaceous Maureen Formation	360 +/- 3 785 +/- 5 1160 +/- 5 1360 +/- 5 1400 +/- 5 1420 +/- 5 1540 +/- 5
17 1/2"	1530 / 1520	13-3/8" / 72 / N80 / BTC	Class "G" F'water	150	See Enclosure 2C	1.26 (545) to 1.35 (585)	KCL/Polymer system KCL: +/- 35 ppb MF: 50-60 secs PV/YP 20-25/15-20 WL: Less than 10 ccs	ISF/SONIC/SP/GR LDT/CNL/CAL/GR	Upper Jurassic Sandstone * Top reservoir Sogn Formation Zone 1 Middle Heather fm. Zone 2 Fens Formation Zone 3 TD	1550 +/- 5 1550 +/- 5 1605 +/- 10 1685 +/- 10 1735
12-1/4" See note 8	1735 / 1725	9-5/8" / 43.5 / N-80 / BTC.	Class "G" F'water	100	See Enclosure 2D	1.14 (494)	KCL/Polymer system from 17 1/2" section. Addition of KCL will be stopped. MF: 50 - 60 PV/YP: 20-25/15-20 WL: Less than 5 ccs	ISF/SONIC/SP/NGT LTD/CNL/CAL/GR MSFL/DLL/CAL/SP/GR MDT RFT's (as required) Velocity Survey SMS (as required) CBL (on 13-3/8" and 9-5/8" casing).	* Primary Target	

NOTES:

- All mud weights are to be adjusted in the light of hole problems (i.e. sloughing shales, high mud gas readings etc.).
- Formation leak off tests are required below 20" and 13-3/8" casing shoes.
- 14-3/4" pilot hole is to be drilled to 20" casing depth and logged for shallow gas prior to pulling the MR and opening the hole to 26".
- Cutting Collection: Every 10 m below the 30" casing shoe. Every 3 m below 1325 m BDF.
- Estimate pore pressure is +/- 2290 psi at 1550 m BDF.
- Coring is to commence from top of the reservoir in the Upper Jurassic sandstone, and is to continue through the complete hydrocarbon bearing sequence until just below top of zone 2 in the U.S. Approximate interval to be cored is 1550 - 1615 m BDF.
- Testing is subject to confirmation upon receipt of logs.
- 9-5/8" casing will be set only if testing is required.

SIGNED:   
PRODUCTION MANAGER  
OPERATIONS SUPERINTENDENT HEAD OF DRILLING  
CHIEF PETROLEUM ENGINEER   
DATE: 

# DRILLING PROGRESS CURVE 31/2-M

## TIME BREAKDOWN (DAYS)

RIG MOVE/ANCHORING : 3

DRILL, LOG, CASE TO TD. : 28

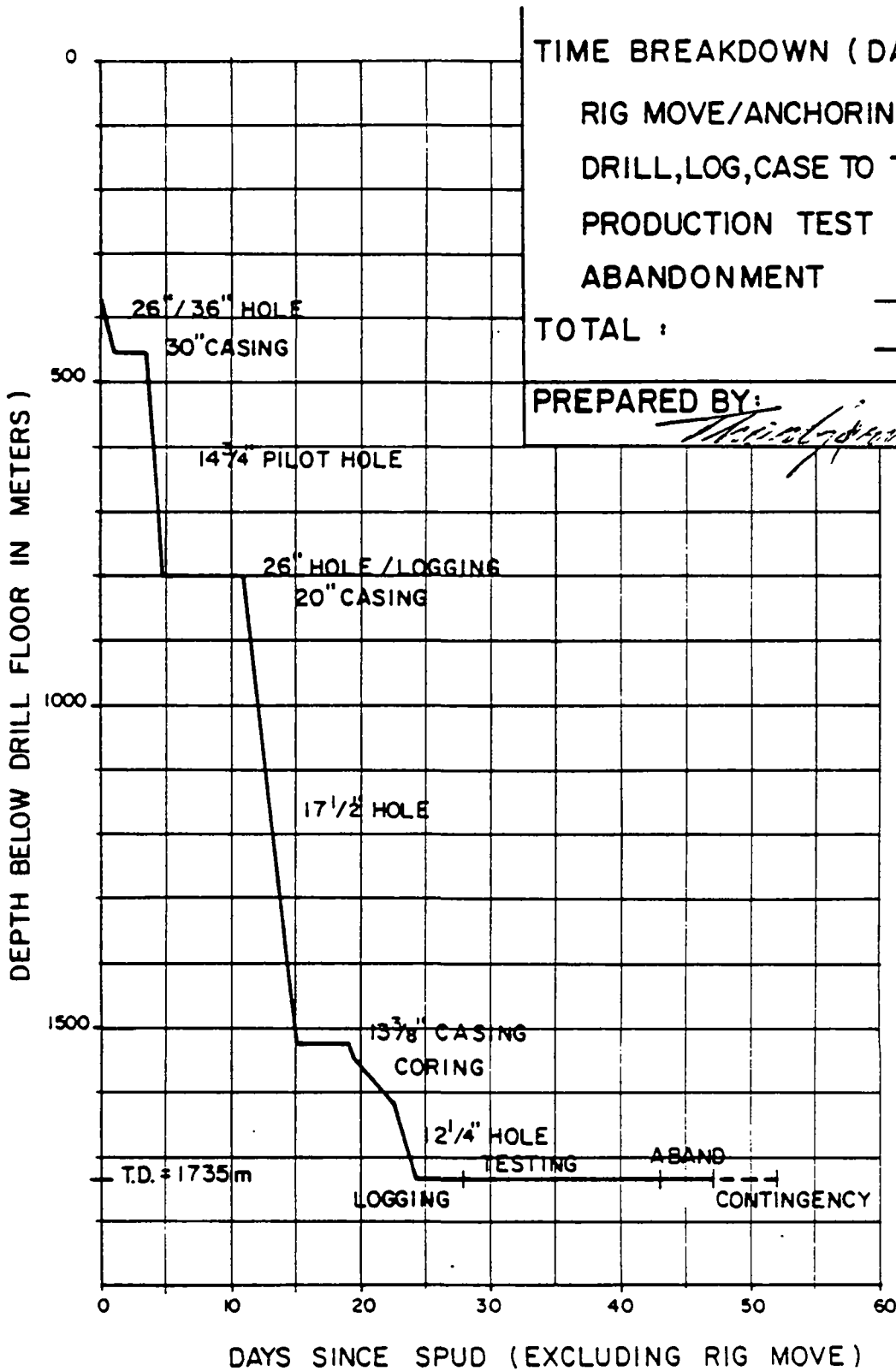
PRODUCTION TEST : 15

ABANDONMENT : 4

TOTAL : 50

PREPARED BY:

*W. J. ...*



CONTENTS:

PAGE

A. GENERAL

1

1.	Location	1
2.	Base	1
3.	Depth References	1
4.	Type of well	1
5.	Total Depth	2
6.	Drilling Installation	2
7.	Objectives	2
8.	Prognosis	3
9.	Pressure Regime	5
10.	Mud Resume	5
11.	Well Control	6
12.	Deviation Control	6
13.	Casing Summary	7
14.	Wellhead Equipment	7
15.	Formation Leak-off Tests	7
16.	Casing Accessories	7
17.	Cement Calculations	8
18.	Contingency Plans - Stand-by vessel	8

B. SUMMARY OF OPERATION

9

1.	Pre-Spud Phase	9
2.	Rig Positioning	10
3.	Spudding in, 36" hole/30" casing	10
4.	26" hole/20" casing	12
5.	17-1/2" hole/13-3/8" casing	18
6.	12-1/4" hole/9-5/8" casing	19
7.	Abandonment	20

C. BLOWOUT PREVENTION EQUIPMENT TESTING

21

D. <u>EVALUATION REQUIREMENTS</u>	24
1. Cutting sampling	24
2. Coring	24
3. Logging Programme	25
4. Testing Programme	25
E. <u>CASING DESIGN</u>	26
F. <u>GLOSSARY OF ABBREVIATIONS</u>	27

ENCLOSURES

1. Casing designs
2. Cement calculations
3. Estimated Pore pressure curve/Fracture gradient curve
4. Velocity - Time function
5. Velocity - Depth function
6. Prognosis Appraisal well 31/2-M

FIGURE

1. Drilling Progress Curve 31/2-M

A/S NORSKE SHELL

DRILLING PROGRAMME - LOCATION 31/2-M

A. GENERAL

1. Location

- a) A/S Norske Shell - Block 31/2 - Production Licence 054
- b) Preliminary surface co-ordinates (centre of location) corresponding to SP 778 on seismic line 79-406 and SP 334.5 on seismic line 82-432.

GEOGRAPHICAL

UTM (ZONE 31)

60 deg. 49' 28.3" N

NORTHING 6743478 M

03 deg. 25' 29.7" E

EASTING 523110 M

Tolerance: 25 meter radius from proposed location.

2. Base

Tananger Shore Base to Location 267 kms

Bergen Shore Base to Location 118 kms

3. Depth References

- a) All depths are given with respect to the rotary table (derrick floor) of the drilling vessel at the specified drilling draught.
- b) The drilling draught will be ca. 21.0 m.
- c) Expected water depth at location is +/- 335 m (MSL-seabed)
- d) Distance from rotary table to MSL is taken as +/- 25 m for this programme but will be measured on site. Distance from rotary table to seabed is taken as +/- 360 m for this programme but will be measured on site.

4. Type of well

Appraisal well.

5. Total Depth

TD in Upper Jurassic Sandstones is anticipated to be +/- 1735 m BDF (+/- 1710 m SS).

6. Drilling Installation

"Borgny Dolphin" - Aker H-3 semi-submersible.

7. Objectives

1. To establish the reservoir quality in the southern extension of the 31/2-7 accumulation and to assist in the mapping of permeability distribution in the oil province.
2. To provide an additional data point for the correlation and mapping of the depositional units.
3. To investigate the southerly extension of the 28 m oil column.
4. To obtain additional oil production test data for input to the development studies.
5. To investigate whether the high induced skin can be reduced by improved gravel pack techniques.



8. Prognosis

<u>Formation Tops</u>	<u>Lithology</u>	<u>Depth</u> <u>TVBDF (m)</u> <u>(Thickness m)</u>	<u>Seismic</u> <u>Tolerance (m)</u>
<u>Seabed</u> (Quaternary- Pliocene-Miocene)	Clay, Claystones, Occasionally sandy.	360 (425)	+/- 3
<u>Oligocene</u>	Claystones.	785 (375)	+/- 5
<u>Eocene</u>	Claystones.	1160 (200)	+/- 5
Balder formation	Claystones, Tuffa- ceous claystone.	1360 (40)	+/- 5
<u>Paleocene</u>			
Sele formation	Claystones, silty claystones.	1400 (20)	+/- 5
Lista formation	Claystones, silty. Marls.	1420 (120)	+/- 5
<u>Upper Cretaceous</u>			
Maureen formation	Mudstone, silty mudstone. Limestones.	1540 (10)	+/- 5
<u>Upper Jurassic Sandstones</u>			
Top reservoir		1550	+/- 5
Sogn formation Zone 1	Fine to coarse unconsolidated sandstone. Fine micaceous sandstone. Occasional car- bonate cemented bands.	1550 (55)	+/- 5
GOC	Expected in Zone 1	1566	+/- ?

OWC	Expected in Zone 1	1594	+/- ?
Middle Heather Fm. Zone 2	Fine - silty, consolidated, micaceous sand- stones.	1605 (80)	+/- 10
Fens formation Zone 3	Fine to medium, consolidated, micaceous sand- stones.	1685	+/- 10

TD +/- 1735 m BDF

9. Pressure Regime

Data gained from drilling, electric logging, RFT pressure measurements and production tests show that the wells drilled to-date in block 31/2 are hydrostatically pressured. (See enclosure 3)

The proposed location 31/2-M is some 3.9 km SSW of 31/2-7 and 5.95 km NNW of well 31/2-5 and is considered to be in the same hydrostatically pressured regime.

10. Mud Resumé

36" Hole

The 36" hole section is to be drilled with a seawater and viscous pill combination. Some 350 bbls of viscous mud will be used to drill the first 10 - 20 m into seabed.

26" Hole

The 14-3/4" pilot hole for the 26" hole section is to be drilled with an unweighted gelled-seawater mud combined with the frequent spotting of viscous pills. The 14-3/4" pilot hole will be opened up to 26" using seawater and viscous pills, with the riser removed and returns to seabed. (See section B4).

Note:

Prior to pulling out of the 14-3/4" pilot hole and 26" hole for logging and the running of 20" casing respectively, mud of 1.35 SG is to be spotted in the open hole section, to ensure hole stability.

17½" Hole

The 17½" hole section will be drilled with a KCL/Polymer mud system with a mud weight of 1.26 - 1.35 SG (.545 - .585 psi/ft)

Note:

From experience gained on other wells drilled in the block a mud weight of 1.35 SG was required to stabilize this hole section.

### 12-1/4" Hole

For the 12-1/4" hole section the addition of KCL will be stopped in the KCL/Polymer mud. A mud weight of 1.14 SG (.494 psi/ft) will be used in this section. The fluid loss is to be brought down to the lowest practical value but certainly below 5cc.

#### Note:

- 1) Mud weights mentioned are a guide only and are liable to change if hole conditions dictate.
- 2) The mud weight used in the 12-1/4" hole will exert +/- 130 psi overbalance on top of the reservoir in the event of the riser being disconnected.

### 11. Well Control

A diverter will be hooked up to the riser during the drilling of the 14-3/4" pilot hole for 20" casing. In addition, 1.4 SG mud (.606 psi/ft) should be available during this diverter drilling in case flows are encountered. Cement will also be available on the rig for use in an emergency. Pressure control will be maintained from the 20" casing point to TD in accordance with the well control policy manual EP 40806.

### 12. Deviation Control

Totcos are to be taken while drilling the 36" and 26" hole sections. Magnetic single shot (MSS) surveys will be taken just below the 20" casing point and thereafter every 90 meters, to coincide with bit trips where possible. The well path is to be calculated using the "Minimum Radius of Curvature" method.

13. Casing Summary

<u>Size</u>	<u>Grade</u>	<u>Weight</u>	<u>Coupling</u>	<u>Interval BDF</u>	<u>Casing requirements</u>
30"	X-52, 1"WT	310 lbs/ft	ATD-RB squnch	Seabed - 455 m	(95 m)
20"	X-52	129 lbs/ft	Vetco LS-LH	Seabed - 800 m	(440 m)
13-3/8"	N-80	72 lbs/ft	BTC	Seabed - 1520 m	(1160 m)
9-5/8"	N-80	43.5 lbs/ft	BTC	Seabed - 1725 m	(1365 m)

Note:

- 1) The 9-5/8" casing will only be set if the well is to be tested.
- 2) The 13-3/8", N-80, 72 lbs/ft, BTC casing has been specially drifted at the mill (during manufacturing) and will again be drifted on the pipe rack of the rig (before running) to ensure a 12-1/4" bit will pass.

14. Wellhead Equipment

Vetco SG-5 18-3/4", 10,000 psi wellhead equipment.

15. Formation Leak-off Tests

Leak-off tests will be made after drilling 5 metres of new hole below 20" and 13-3/8" casing shoes.

16. Casing Accessories

- 30" Float shoe.
- 20" Guide shoe (B & W Trico) and baffle collar one joint above shoe. Two spring centralizers on the shoejoint and 3 on the next 6 joints (one per two joints). Two spring centralizers equally spaced inside 30" conductor.
- 13-3/8" Float shoe + float collar one joint above shoe. 10 spring centralizers - 2 on shoe joint, 6 on the next 12 joints (one every second joint) and 2 inside 20" shoe, spaced 1 joint apart.

9-5/8" Float shoe + float collar 2 joints above the shoe. Two spring centralizers on the shoe track, 1 centralizer per joint up to the base of the OWC, no centralizers across the oil zone, 1 centralizer per joint up to the 13-3/8" shoe and 1 centralizer per 3 joints over the first 100 m of 9-5/8" inside the 13-3/8" casing.

Casing test pressures will be as follows:

20"	1000 psi for 15 mins
13-3/8"	2500 psi for 15 mins
9-5/8"	3000 psi for 15 mins

Pressure tests on the 20", 13-3/8" and 9-5/8" casings to be carried out immediately after bumping the top plug. The casing may be retested using an RTTS packer set below the top of cement around the particular casing if there is concern over the casing being worn.

17. Cement Calculations: See enclosure 2.
18. Contingency Plans - Stand-by vessel

The current A/S Norske Shell Exploration & Production Emergency Contingency Plan dated 4th of January 1982, and updated 23 July 1982, is valid for this drilling operation.

The name of the stand-by vessel which will be used is M/V "Nautik".

## B. SUMMARY OF OPERATION

### 1. Pre-Spud Phase

#### Site Survey

##### a) Objectives

A/S Geoteam was commissioned by A/S Norske Shell Exploration and Production to perform a site survey in block 31/2 to cover an area of approximately 4 x 4 km centered on the proposed well location 31/2-M. The field work took place in the period between 3 December and 15 December 1982.

The survey was a combined seafloor investigation, bathymetric survey and a high resolution seismic survey. In order to map the sea floor topography and locate any debris or wrecks that might cause problems to drilling operations, profiles were run with an echo-sounder and side scan sonar. For observation of the uppermost zone of soft sediments, profiles were run with a deep towed boomer.

##### b) Conclusion

The Side Scan Sonar data shows the seabed in the area to be mostly flat and featureless with the exception of frequent depressions (pockmarks). These pockmarks vary in diameter from 15 to 50 meters and are in general between 1 and 3 meter in depth. Except for these pockmarks, no debris or obstructions which might cause problems for drilling operations or anchoring were evident. The seabed consists of soft silty clay with a water depth of 336 m at the proposed location.

Unit I 361 - 396 m BDF (35m thick) soft, silty clays.

Unit II 396 - 425 m BDF (29m thick) Overconsolidated clays.

Unit III 425 - 430 m BDF (5m thick) Probably consisting of glacial till with boulders interbedded.

Unit IV 430 - 470 m BDF (40m thick) Hard clay with isolated sandpockets.

Unit V 470 - 505 m BDF (35m thick) Consists of a series of erosion surfaces at the base of the Quaternary sediments. The sediments in this zone are thought to be sand and gravel.

No indication of shallow gas is observed in these units

The Tertiary bedrock below 505 m BDF is mainly composed of claystone with sandlayers.

A/S Geoteam states in their report that: "at 760 m BDF (735 m SS) a strong reflector is seen. 250 - 800 meters south of the planned well location at this level there is an anomalous reflection that might indicate gas. In Norske Shell's opinion and experience in the 31/2-area, the possibility of encountering gas at this level (top Oligocene) in the proposed location is unlikely. It should be noted that A/S Geoteam has been using too low interval velocities in their time-depth conversion thus indicating top of Oligocene at +/- 760 m BDF.

According to the well prognosis and well correlation top Oligocene is expected to be encountered at 785m +/-5m BDF.

2. Rig Positioning

The rig will be brought on to location utilizing Decca Pulse-8 with HP minicomputer. All anchors will be run out plus/minus 1400 m. The rig will be positioned with a heading of 290 deg True North. After anchors have been set, each anchor will be tested to plus/minus 400,000 lbs for 1 hour. After a satisfactory mooring test, approximately 250,000 lbs tension will be maintained on all anchor chains.

Satellite Navigation will be used to determine the final coordinates of the location, a minimum of 40 satellite passes are required.

3. Spudding in, drilling 36" hole and running 30" Casing

1. Check the seabed condition by lowering underwater TV on the guide lines prior to setting the TGB on seabed.

2. Set TGB (with 5 m skirt). A Regan slope indicator is to be run on the TGB running tool to give an indication of the TGB angle. The TGB guide lines are to be marked at the spider deck level so that any subsequent sinking or tilting will be detected.

Note:

Calculate the DF - seabed distance and Mean Sea Level (MSL) after landing the TGB, taking into account the drilling draught and tidal variation.



3. Make up a 36" hole opener and 26" pilot bit assembly. Drill down to 30" casing setting depth, taking a survey (Totco) after the first kelly down. Additional surveys will be carried out as necessary, depending on hole angle. If hole angle is greater than  $1\frac{1}{2}$  degree then contact Base.

Before POH to run 30" casing circulate high viscosity mud (60 MF) in the hole, using 100% excess.

4. Run 30" casing plus PGB equipped with a Regan slope indicator (to be installed in the middle of a side beam, as close to the beam as possible). Install a second Regan slope indicator on the 30" running tool. Ensure that the slope indicators are properly level and zeroed and will be visible on the subsea TV.
5. When the 30" casing is landed observe the angle with the subsea TV camera. If the angle is 1 degree or less, cement the casing using 150% excess cement. (For cement calculations see enclosure 2A.)
6. WOC. RIH with jetting sub and wash in and around the wellhead housing. Divers to check around the guide bases with an observation dive, if thought necessary.
7. If excessive cratering is observed, re-cementing around the guide base or seabed may be considered prior to drilling out of the 30" casing. Or if this problem is anticipated, consider using 300% excess cement instead of 150%.

Note:

- a) For the single stack system the angle of the PGB and the BOP stack, and the base being level, are of utmost importance and good support is required to carry the heavy load of the stack.
- b) Observe operations such as placing of the TGB and PGB, spudding in, stabbing in, drilling with returns to seabed, cementing of the 30" and 20" casings, with the rig's underwater TV camera.

- c) Adjust anchor tension to facilitate stabbing, running and cementing of the 30" casing.
- d) Ensure that the tension of the guide lines is optimum so that the TGB will not be lifted on one side or be tilted by excessive uneven guide line tension.
- e) In previous wells, the guide bases have sunk into the soft sea bed when landing the 30" casing/PGB. In the case that this phenomena is observed, the 30" casin should be kept in tension whilst cementing and W.O.C.

4. Drilling 26" hole and running 20" casing

1. Drill out cement in 30" casing and 36" pocket with 26" hole opener and 14-3/4" pilot bit with a stabilizer at 20 m and start 14-3/4" pilot hole. POH and lay down 26" hole opener and stabilizer.
2. Run 30" hydraulic latch and dump valve complete with ball joint on 21" riser. Fill up riser with seawater and observe fluid level.
3. Make up 14-3/4" pilot hole drilling assembly. Use a float sub, with the float installed, and run in hole.
4. Close diverter around drill pipe, and circulate through both diverter lines to check the diverter equipment, gradually building up to maximum circulating rate. Open diverter packing.
5. Drill 14-3/4" pilot hole to the 20" casing setting depth, allowing for a 10 m pocket and taking Totco surveys as required.

Note:

This section is to be drilled using an unweighted gelled mud and the weight of annular returns is to be continuously monitored. If the weight of annular returns causes losses or exceeds 1.15 SG (.498 psi/ft) stop drilling and circulate the hole clean. ROP must be controlled whilst drilling this section.

6. Perform a check trip to the 30" shoe and back to bottom, clean out any fill and spot viscous mud of 1.35 SG (.585 psi/ft) in the open hole section prior to pulling out of hole for logging.

7. Rig up Schlumberger and log as programmed.

Note:

Inspect the logs for indications of shallow gas prior to continuing with the programme. If any indications of shallow gas are observed then call Base and a revised programme will be issued.

8. Rig down Schlumberger and run in hole to 30" shoe and displace the casing and riser to seawater. Continue to RIH to TD. Circulate the hole volume to seawater and open the dump valve (close kelly cock). Observe well static for  $\frac{1}{2}$  hour and then spot viscous mud in the open hole section. If flow occurs, the 14-3/4" pilot hole will be under-reamed as described under "Notes on Diverter Drilling" item d page 15.

Note:

The 1.35 SG mud spotted prior to logging, should be circulated out in steps and dumped via the dump valve to prevent losses to the formation due to the heavy mud entering the marine riser.

9. Pull out of hole and retrieve the 30" hydraulic latch on riser.

10. Make up the 18-3/4" housing with running tool, B.J. stinger and top plug and stand back in derrick.

11. Pick up a 14-3/4" pilot bit and 26" hole opener with a 26" stabilizer at 20 m above the bit. Open the hole up to 26" using seawater and viscous pills as required.

12. Perform a check trip to the 30" shoe and back to bottom, clean out any fill and spot viscous mud of 1.35 SG (.585 psi/ft) in the open hole section prior to pulling out of hole for running casing.
13. Run and cement 20" casing as per programme.  
Note:
  - a) Guide shoe and baffle collar with special profile will be used. The baffle collar will be installed between the first and second casing joints and 1 subsea plug (top plug) will be used for cement displacement and will subsequently latch into the baffle collar.
  - b) If gas has been encountered in the pilot hole a regular float shoe will be used instead of the guide shoe.
14. Unlatch the running tool and POH.
15. RIH with a jetting sub and wash in and around the 18-3/4" wellhead housing. POH and lay down the jetting sub.
16. Install the 18-3/4" BOP stack and 21" Marine Riser. Test BOP stack, complete with casing. For stack test procedure see "Blowout Prevention Equipment Testing" item C. Make up drill pipe hang off assembly and circulating head assembly. Install seat protector.

Notes on Diverter Drilling/ Shallow gas drilling

- a) A diverter system is fitted on the "Borgny Dolphin" to provide a means of controlling the flow should shallow pressures be encountered whilst drilling for the first casing string (20" surface casing).
- b) The diverter system is not a blowout preventer. It is not designed to hold pressure, but instead, to direct the flow overboard. The controls of the flowline valves are manifolded in such a way that it is impossible to hold any pressure in the diverter. The downwind blow-off line must always be open.

c) Severe Losses

If severe losses are encountered while drilling with returns to surface, pull out and drill a 8½" pilot hole instead of 14-3/4" and restrict penetration rates to obtain the lightest possible annular returns. If severe losses continue, open the dump valve and drill a 8½" pilot hole with returns to seabed.

If gas is encountered whilst drilling 8½" pilot hole with seawater and returns to seabed, spot heavy mud and inform Base.

d) Gas Flow (No Losses)

If there are any signs of gas having been encountered whilst drilling the 14-3/4" pilot hole, carry out the following programme: -

- i) Drill to 20" casing setting depth with the mud weight required.

- ii) Circulate the hole clean and make a wiper trip to the 30" shoe and back to bottom. Circulate bottoms-up and spot weighted viscous mud as required. POH.
- iii) Run logs as programmed.
- iv) RIH with 14-3/4" bit and displace hole to mud with required weight for under-reaming. Dump heavy mud via dump valve. POH.
- v) RIH with 26" hydraulic under-reamer with a 14-3/4" pilot bit and 17½" stabilizer.
- vi) Under-ream the 14-3/4" hole to 26". Check hole size with a BGT log.
- vii) RIH and circulate the hole clean.
- viii) Increase the weight of the mud in the interval TD - seabed, to give an overbalance to any potential gas zones and thus compensate for removing the riser.
- ix) POH to seabed. Circulate the drillpipe and marine riser to seawater and close kelly cock. Open the dump valve and observe the well static for 30 mins. Unlatch the 30" hydraulic latch and pull the marine riser.
- x) Make up the 18-3/4" housing with running tool, B.J. stinger and top plug and stand back in derrick.
- xi) Run a BGT to check hole size.
- xii) Rig up and run 20" casing.
  - Note:
  - Regular float shoe will be used together with the baffle collar.
  - Casing will be filled with mud, weight as in step viii above, whilst RIH.
  - If the casing has to be circulated down and when circulating prior to cementing, weighted mud (as used in step viii) above is to be used.

e) Gas Flow and Severe Losses

If any flow of gas is encountered whilst drilling the 14-3/4" pilot hole with returns to surface, and the required increased mud weight to counteract the gas flow causes severe losses, then inform Base and the various options will be considered.

Note:

There should be sufficient barytes and SAPP (1500) kg onboard the rig to allow for the setting of baryte plugs. Further programme will be advised in this case.

5. Drilling 17½" hole and running 13-3/8" casing

1. Drill out shoe track and shoe with a 17½" bit. Drill 5 m of new hole, and carry out a formation leak-off test.
2. Drill 17½" hole to programmed depth.

Note:

This hole section will be drilled with a KCL/Polymer mud starting off with a mud weight of 1.26 SG which will be increased to 1.35 SG before reaching casing setting depth.

3. Log as per programme. Make up 13-3/8" casing hanger with seal assembly and subsea cementing assembly (use two plugs) and stand back in derrick.
4. Make checktrip to casing setting depth and wash wellhead area on the way out. Pull wearbushing and run 13-3/8" casing to landing point, leaving 10 m pocket below the 13-3/8" shoe.
5. Cement 13-3/8" casing as per programme. Test casing to 2500 psi after bumping the plug. Energize the seal assembly and test to 4250 psi as per "Blowout Prevention Equipment Testing" Section C. Clean out the stack area prior to pulling out with the running string.
6. Carry out stack test as per "Blowout Prevention Equipment Testing" Item C. Install wearbushing. Make up drillpipe hang-off assembly and circulating head assembly. Carry out a kickdrill.



6. Drilling 12-1/4" hole and running 9-5/8" casing

1. Drill out float collar, cement and shoe. Drill 5 m of new hole, and carry out a formation leak-off test.
2. Drill 12-1/4" hole to programmed depth. Bit weight, RPM, bit selection and bottom hole assembly to be determined on site for optimum penetration rate.

Note:

Coring will commence, using fibreglass inner corebarrel and 8½" core head, from the top of the reservoir in the Upper Jurassic sandstone. Approximate interval to be cored is 1550 - 1615 m BDF. The cored interval will be opened up to 12-1/4" prior to logging.

3. Carry out logging programme, including wire line tests if necessary.

Note:

Dependent upon the results of the logs the well will either be abandoned or 9-5/8" casing will be run to allow for testing. If the well is to be tested, then proceed with step 4 below.

4. Make up 9-5/8" casing hanger with seal assembly and subsea cementing assembly (using two plugs) and stand back in derrick.
5. Make check trip and wash wellhead on the way out. Pull wearbushing and run 9-5/8" casing to landing point, leaving a 10 m pocket below the 9-5/8" shoe.
6. Cement the 9-5/8" casing as per programme. Whilst displacing, (in turbulent flow at 250 ft/min or higher), returns are to be monitored closely. If losses are observed adjust pump rates until full returns are obtained. Test casing to 3000 psi after bumping the plug. Energize the seal assembly and test to 4250 psi. Clean out the stack area prior to pulling out the running tool.

7. Carry out stack test as per "Blowout Prevention Equipment Testing" Item C. Install wearbushing. Carry out a kickdrill.

Note: At this point the testing phase will commence and a separate testing programme will be advised.

7. Abandonment

A specific abandonment/suspension programme will be prepared and issued when the well reaches total depth, but the general points below will apply:

1. If there is open hole below the last casing then all porous zones in the open hole interval will be isolated with cement plugs extending 50 m above and below each zone. In addition a cement plug, extending 50 m above and below the casing shoe, shall be set. The top of the cement plug shall be located and load tested. A mechanical bridge plug may be set in the lower part of the casing but not more than 50 m above the shoe. A 20 m cement plug must be placed on top of the bridge plug. The plugs at the last casing shoe shall be tested to 1000 psi (70 bar) differential pressure.
2. Perforations shall be isolated by means of a mechanical bridge plug and squeeze cemented, or a cement plug shall be placed across the perforations extending 50 metres above and below the perforated interval or down to a casing plug whichever is less.
3. Cement plugs of at least 50 metres shall be placed in the smallest casing string extending to seabed. These plugs shall be placed at the level of the 13-3/8" casing shoe and the 20" casing shoe.
4. A cement plug of at least 200 metres, with the top of the plug not more than 50 metres below the sea floor, shall be placed in the smallest string of casing extending to the sea floor.
5. Casing strings and other installations extending above the sea floor will be removed to a depth of at least 5 metres below the ocean floor.
6. The sea floor in the vicinity of the borehole will be inspected by underwater TV/observation dive to ensure that no obstructions remain on the sea bed which may cause danger or impediment to fishing or shipping.

C. BLOWOUT PREVENTION EQUIPMENT TESTING

The regular tests of the BOP stack in service have to be limited to the following pressures, unless differently advised by the base.

18-3/4", 10,000 psi BOP Stack

1. Pipe Rams : 4000 psi
  2. Variable pipe ram : See note d.
  3. Blind Rams : Casing test pressure, as specified in Item A-16
  4. Kill/choke lines and valves : 4000 psi
  5. Annular preventers : 2000 psi around 5" DP  
1500 psi around 3-1/2" DP
- a) Test 1, 2, 4 and 5 to be carried out with a test tool run on DP and landed in the wellhead unless tested immediately after energizing the seal assembly.
  - b) Test 3 to be carried out only when the cement of the last casing is not yet drilled out.
  - c) The 13-3/8" and 9-5/8" seal assemblies are to be tested to 4250 psi. Note that the collapse pressure of the 13-3/8" and 9-5/8" casings are 2670 psi and 3810 psi respectively, thus an accurate check of the volume required to pressure up is required to ensure that any leak is observed, and a collapse situation is not created.
  - d) Variable pipe ram to be tested to same pressures as annular preventers. The variable pipe ram will be tested to 4000 psi only before entering the objectives, ie. before drilling out the 13-3/8" casing.

Accumulator Tests

The accumulators must have sufficient capacity to be able to close, open and close all preventer with both air and electric charge pumps off, and then still have enough pressure left to provide working fluid for 25% of one closing function. Minimum recharge time from above condition with both air and electric pumps running should be in accordance with manufacturer's specifications. A note that this test has been carried out (and results) must be made in the Drilling Report and on weekly BOP test checklist. For frequency see item 10 of this section.

Notes on Testing

1. The BOP stack has to be tested on all functions and all rams tested to the full rated WP (10,000 psi) at surface prior to running the Stack. However, the blind/shear rams will be tested only on orders of Base, but at least once per month during a routine stack test. After the surface tests all Cameron clamp connections and all studded connections must be checked for tightness.
2. All pressure tests to be carried out with water, unless differently advised by Base.
3. All surface equipment has to be satisfactorily pressure tested prior to testing the BOP stack underwater.
4. When running the Marine Riser with integral kill and choke lines, the kill and choke lines can be tested while running in at various stages. This should be done at least twice, firstly as soon as the stack is below sea level, and secondly, just before landing the stack.
5. When testing the BOP stack underwater with a test tool in the wellhead, use the vented red-painted test single.
6. All pressure tests should be done in 500 psi stages up to the required test pressure.
7. The test pressure should be kept on for 15 minutes, and the acceptable pressure drop over this 15 minutes period is 10% of the initial test pressure, provided that the pressure remains constant for the next 5 to 10 minutes.
8. All pressure tests to be recorded on pressure recorder charts. A record is to be kept of the volumes required to obtain the test pressure, and of the volumes returned when bleeding off.

9. For all pressure tests either the Shell TP or WSPE will be present at the pumping unit to monitor volumes/pumped and pressures.
  
10. The opening/closing times and the volumes of hydraulic operating fluid required for the operation of the various underwater stack components (such as: rams, kill and choke valves, annular preventers, hydraulic connectors, etc.) should be recorded during testing of the stack underwater. These results should be compared with the normal opening/closing times and volumes required of the hydraulic system. Any major differences are an indication that the system is not operating "normally" and may require further investigation and/ or repairs.
  
11. The testing of 10,000 psi BOP stack will be done to 4000 psi only, at the weekly routine BOP test underwater. If higher test pressures are required then, depending on the well programme, the test pressure will be increased to the value required and carried out with test tool, e.g. subjecting the seals of the seal assembly to the same pressure as the BOP stack, or by means of a weight set tester, subjecting only the stack to the required test pressure. Run 2 stands drill collars below the weight set tester to assist in shearing the pins with set down weight.  
  
See item 1 on blind/shear rams.
  
12. Accumulator tests (as described previously) should be performed either on request of Base, or after repairs have been made to the accumulator system, i.e. bottles, bladders, pumps, etc.

D. EVALUATION REQUIREMENTS

1. Cutting Samples

Ditch cuttings to be collected every 10 m below 30" casing down to 1325 m BDF, and every 3 m thereafter. The following samples will be required for partners/ government bodies:

- a) 5 x full large bags (2 kg each) of wet cuttings.
- b) 1 x medium large bag (1 kg) of wet cuttings for biostratigraphy.

1 x 2 kilogram large bag of wet samples from each interval should be kept on board until the well has reached TD when the complete set should be sent in. 4 x 2 kilogram samples should be sent ashore ASAP by boat, marked for attention of EPXV/1, Tananger. Biostratigraphy samples should be in cardboard boxes and sent in by the first available helicopter.

2. Coring

Coring is to commence from top of the reservoir in the Upper Jurassic sandstone, and is to continue through the complete hydrocarbon-bearing sequence until just below top of zone 2 in the Upper Jurassic sandstone. Approximate interval to be cored is 1550 - 1615 m BDF, (i.e. 65 m section).

8-1/2" core-head and fiberglass innerbarrels are to be used.

Note: A 150 gram sand sample will be taken from each 90 cm length of core, taken across the oil bearing sand and properly labelled. This sample will be used in sieve analysis to optimize sand size for a possible gravelpack completion.

3. Logging Programme

At 20" casing depth	ISF/SONIC/SP/GR (GR to seabed) LDT/CNL/CAL/GR
At 13-3/8" casing depth	ISF/SONIC/SP/GR LDT/CNL/CAL/GR
At 9-5/8" casing depth (TD logging)	ISF/SONIC/SP/NGT LDT/CNL/CAL/GR MSFL/DLL/CAL/SP/GR HDT RFT's (as required) Velocity Survey SWS (as required) CBL (on 13-3/8" casing and 9-5/8" casing).

4. Testing Programme

Testing of the well is subject to confirmation upon receipt of logs.

The intention is to production test the oil zone if sufficient thickness of oil column is found to be present. The completion technique to be applied, will be internal gravel pack (IGP).

E. CASING DESIGN

Casing designs are presented for the 20", 13-3/8" and 9-5/8" casings (See Encl. 1.0.)

The following assumptions apply:

1. For tension, a design safety factor of 1.6 is used, neglecting buoyancy in the drilling fluid.
2. Bi-axial effects have been neglected except in the case of the lowering of collapse resistance caused by tension. No allowance is given for the increase of burst resistance caused by tension.
3. For burst, a design safety factor of 1.1 is employed. The pressure distribution for the burst loading assumes a 40% evacuation of mud from the well by a kick. (This is equivalent to a kick volume in excess of 100 bbls).

In the production test design for casing burst, a tubing leak is assumed putting full THP on the tubing/casing annulus, filled with 1.15 S.G. completion fluid.

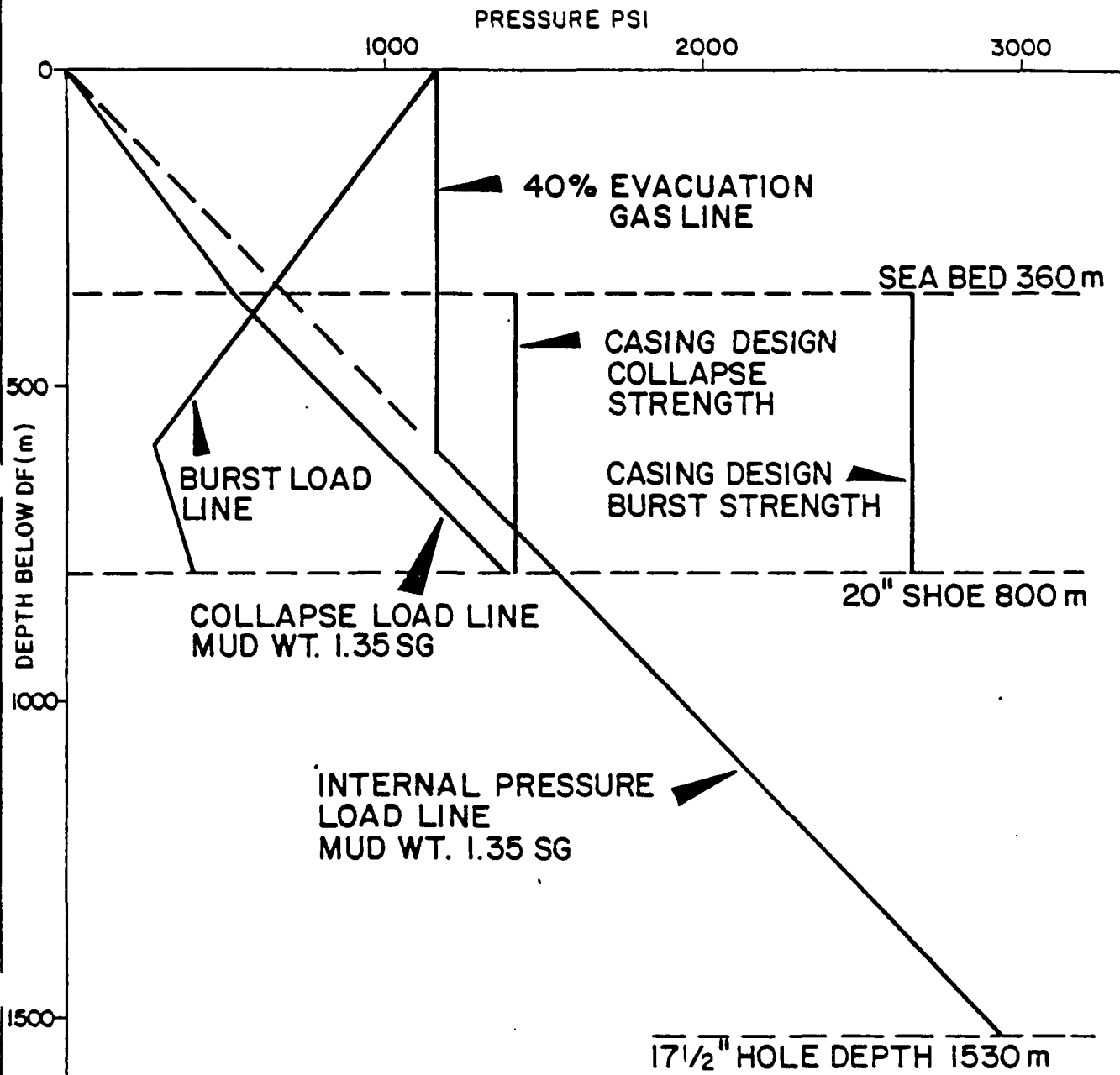
4. For collapse, a design safety factor of 1.0 is employed. For the 20" and 9-5/8" casings total evacuation has been assumed for the design. For the 13-3/8" casing, evacuation of 85 % has been assumed for the design.



F. GLOSSARY OF ABBREVIATIONS

BDF	:	below derrick floor
BGT	:	borehole geometry tool
BOP	:	blow out preventer
DF	:	Derrick Floor
FS	:	fail safe (as in FS valve)
GOC	:	gas oil contact
ID	:	internal diameter
MF	:	Marsh funnel (mud viscosity)
MR	:	Marine riser
MSL	:	mean sea level
MSS	:	magnetic single shot
OD	:	outside diameter
OWC	:	oil water contact
PGB	:	permanent guide base
PPG	:	pounds per US gallon
PV	:	plastic viscosity
ROP	:	rate of penetration
SS	:	sub sea
TD	:	total depth
TGB	:	temporary guide base
THP	:	tubing head pressure
TMCM	:	Transverse Mercator Central Meridian
UGF	:	universal guide frame
YP	:	yield point
WHP	:	wellhead pressure
WP	:	working pressure
WOC	:	wait on cement
UTM	:	Universal Transverse Mercator

# 20" CASING DESIGN 31/2-M



FOR 20", 129.3 LB/FT, X-52, VETCO LS-LH CASING

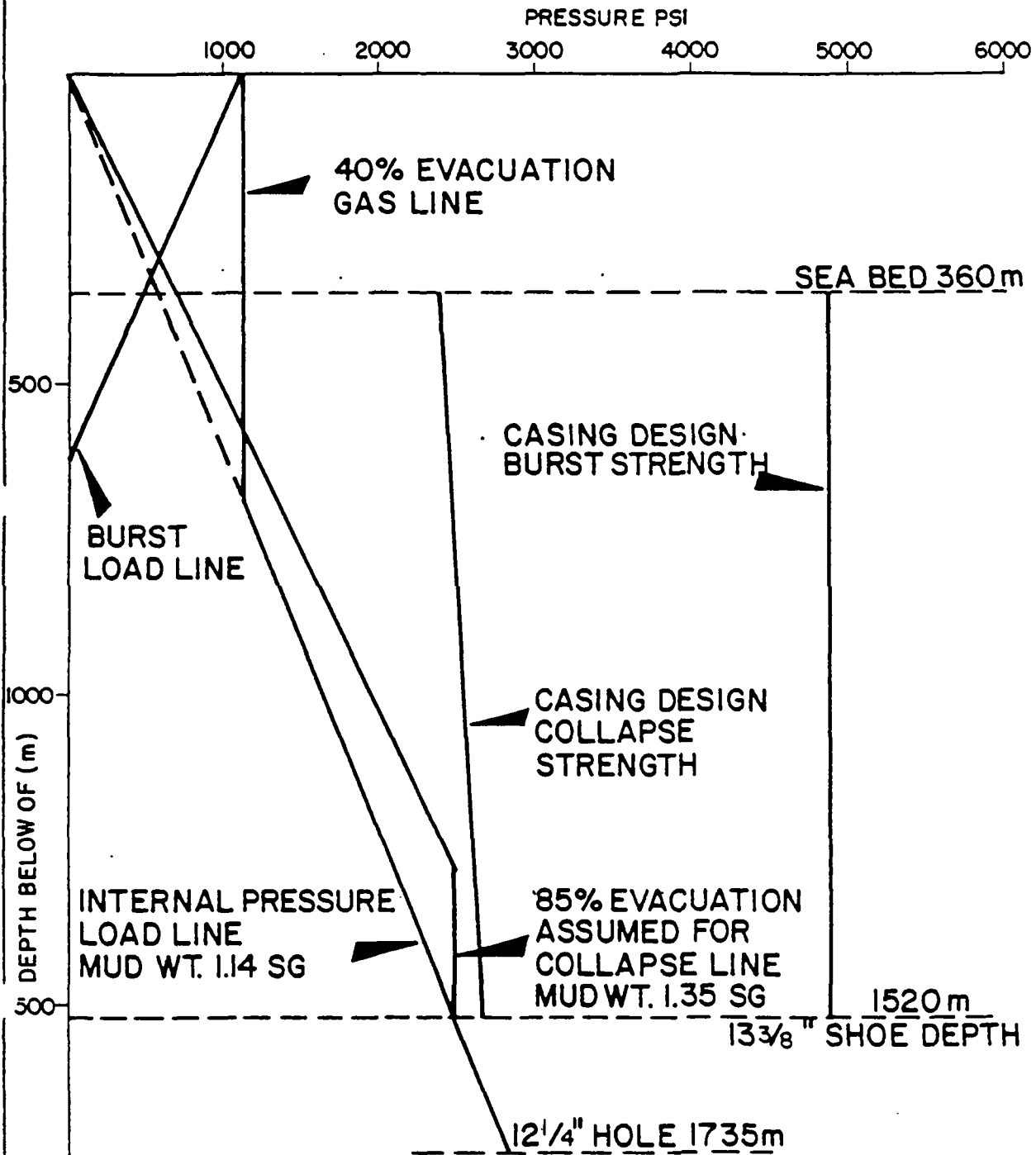
	<u>COLLAPSE</u>	<u>BURST</u>	<u>TENSION</u>
API RATING	.1410	2930	1.978.000
SAFETY FACTOR	1.0	1.1	1.6
DESIGN FACTOR	1410	2663	1.236.250

MAXIMUM TENSILE LOAD =  $129.3 \times 3.281 \times (800 - 360) = 186.663 \text{ LBS}$

20" 129.3 LB/FT, X-52 CASING IS THEREFORE SATISFACTORY IN BURST, COLLAPSE AND TENSION FOR THIS WELL.

a.s Norske Shell  
EXPLORATION & PRODUCTION (NORWAY) AS   
20" CASING DESIGN 31/2-M

# 13 3/8" CASING DESIGN 31/2-M



FOR 13 3/8", 72 LB/FT, N 80 BTC CASING

	<u>COLLAPSE</u>	<u>BURST</u>	<u>TENSION</u>
API RATING	2670	5380	1661000
SAFETY FACTOR	1.0	1.1	1.6
DESIGN STRENGTH	2670	4891	1038125

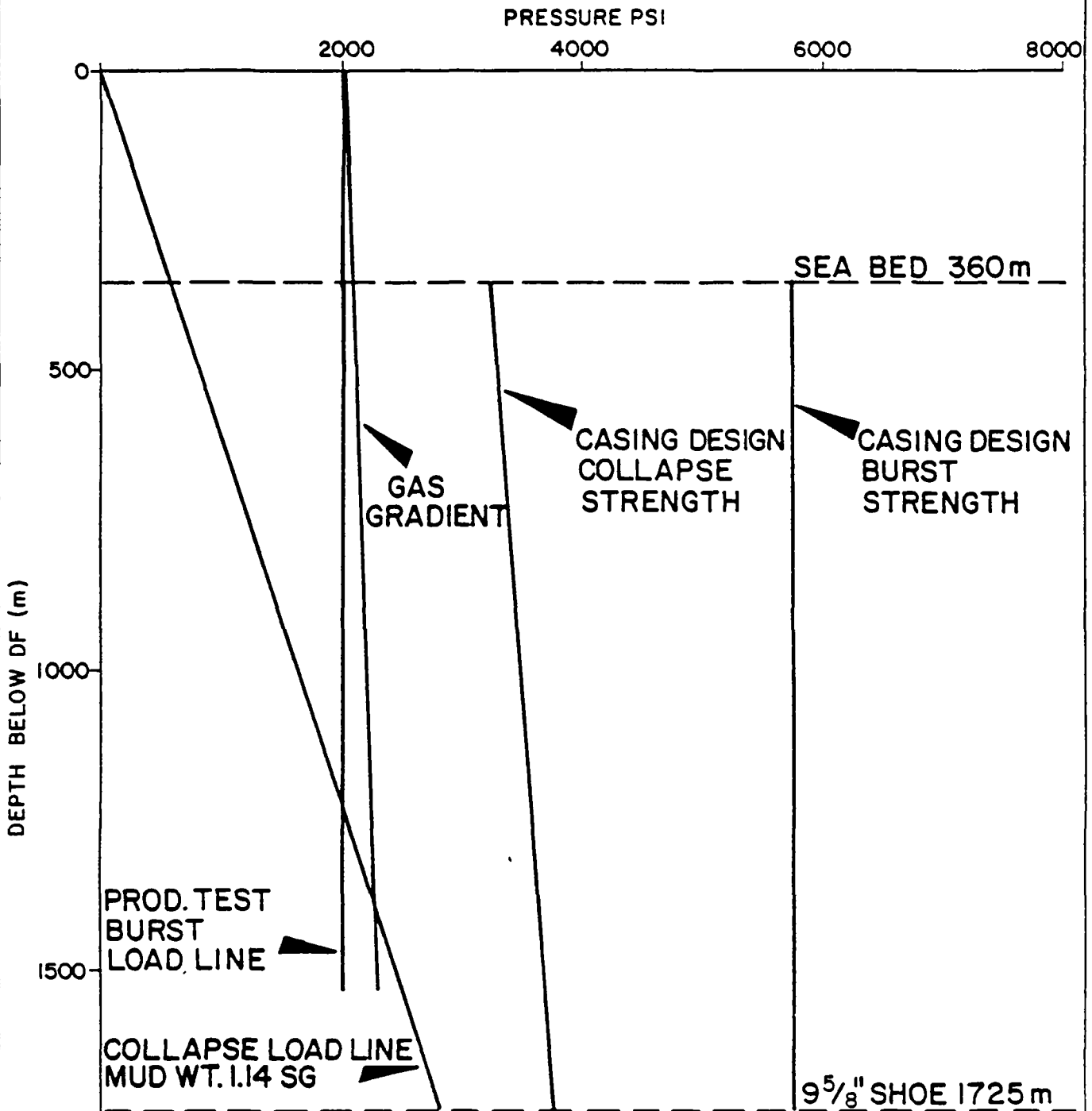
MAXIMUM TENSILE LOAD = 72 x 3.281 (1520-360)  
 = 274.029 LBS

13 3/8", 72 LB/FT, N80, BTC CASING IS THEREFORE SATISFACTORY IN BURST, COLLAPSE AND TENSION FOR THIS WELL.

a-s Norske Shell  
 EXPLORATION & PRODUCTION SERVICES   
 13 3/8" CASING DESIGN 31/2-M

EPPP/11 18 DEC 82  
 G1301/3

# 9 5/8" CASING DESIGN 31/2-M



**FOR 9 5/8", 43.5 LB/FT, N 80, BTC CASING**

	<u>COLLAPSE</u>	<u>BURST</u>	<u>TENSION</u>
API RATING	3810	6330	1005000
SAFETY FACTOR	1.0	1.1	1.6
DESIGN STRENGTH	3810	5754	628125

MAXIMUM TENSILE LOAD = 43.5 x 3.281 x (1725 - 360) = 194,818 LBS

9 5/8", 43.5 LB/FT, N 80 BTC CASING IS THEREFORE SATISFACTORY IN BURST, COLLAPSE AND TENSION FOR THIS WELL.

THE DESIGN SHOWS THAT THE CASING CAN WITHSTAND A PRODUCTION TEST ON THE MAIN GAS RESERVOIR.

a-s Norske Shell  
EXPLORATION & PRODUCTION SERVICES   
**9 5/8" CASING DESIGN 31/2-M**

EPPP/11      DEC. 82  
IC      JAN 83 G1301/4

CEMENT CALCULATIONS30" Cementation

Extended Norcem Class "G" cement of lead slurry weight 13.2 ppg(1.58 SG) and 10 m of 15.8 ppg(1.90 SG) tail slurry above the shoe are to be used. The casing is to be cemented back to seabed, and an excess of 150 % is to be used over open hole intervals. Cement displaced to 10 m above shoe.

Data: Casing 30" 1" WT/VETCO "ATD-RB"  
 Seabed 360 m BDF  
 30" shoe 455 m BDF  
 36" hole 465 m BDF

13.2 ppg Lead Slurry Volumes

i) 36" x 30" annulus =  $(445-360) \times 3.281 \times 2.1598 \times 2.5$  = 1505.8 cu.ft.  
 Cement required =  $1505.8 / 1.89$  = 796.7 sxs  
 = 34.0 m/t  
 Seawater required =  $796.7 \times 10/42$  = 189.7 bbls  
 Econolite required =  $796.7 \times 0.36$  = 286.8 gals.

15.8 ppg Tail Slurry Volume

i) 36" x 30" annulus =  $(455-445) \times 3.281 \times 2.1598 \times 2.5$  = 177.2 cu.ft.  
 ii) 36" pocket =  $(465-455) \times 3.281 \times 7.0686 \times 2.5$  = 579.8 cu.ft.  
 iii) 30" casing fill =  $10 \times 3.281 \times 4.2761$  = 140.3 cu.ft  
 Total slurry = 897.3 cu.ft.  
 Cement required =  $897.3 / 1.17$  = 766.9 sxs  
 = 32.7 m/t  
 Seawater required =  $766.9 \times 5.15/42$  = 94.0 bbls  
 CaCl<sub>2</sub> required 3%(BWOC) =  $766.9 \times 94 \times 0.03/2205$  = 1.00 m/t

20" Cementation

Extended Norcem Class "G" cement of lead slurry weight 13.2 ppg(1.58 SG), and 60 m of tail slurry above the shoe, of weight 15.8 ppg(1.90 SG) are to be used. The casing is to be cemented back to seabed and an excess of 100% is to be used over open hole intervals. Cement to be displaced to the baffle collar approximately 12 m above the guide shoe using 1 subsea cement plug.

Data: Casing 20"/129 lbs/ft/X-52/Vetco LS-LH  
 30" shoe at 455 m BDF  
 36" hole at 465 m BDF  
 20" shoe at 800 m BDF  
 26" hole at 810 m BDF

13.2 ppg Lead Slurry Volumes

i)	30" x 20" annulus	= (455-360)x3.281x2.0944	=	652.8 cu.ft.
ii)	36" x 20" annulus	= (465-455)x3.281x4.8869x2	=	320.7 cu.ft.
iii)	26" x 20" annulus	= (740-465)x3.281x1.5053x2	=	<u>2716.4 cu.ft.</u>
	Total slurry volume		=	3689.9 cu.ft.

Cement required	= 3689.9/1.89	=	1952.3 sxs
		=	83.3 mt
Seawater required	= 1952.3 x 10/42	=	464.8 bbls
Econolite required	= 1952.3 x 0.36	=	702.8 gals

15.8 ppg Tail Slurry Volumes

i)	26" x 20" annulus	= (800-760)x3.281x1.5053x2	=	592.7 cu.ft.
ii)	26" pocket	= 10 x 3.281 x 3.6870 x 2	=	241.9 cu.ft.
iii)	20" casing fill	= 12 x 3.281 x 1.9133	=	<u>75.3 cu.ft.</u>
	Total slurry volume		=	909.9 cu.ft.

Cement required	= 909.9/1.17	=	777.7 sxs
		=	33.2 mt
Seawater required	= 777.7 x 5.15/42	=	95.4 bbls
CaCl <sub>2</sub> required 2% (BWOC)	= 777.7 x 94 x 0.02/2205	=	0.66 mt

13-3/8" Cementation

Extended Norcem Class "G" cement of lead slurry weight 13.2 ppg(1.58 SG), and 100 m of tail slurry above the shoe, of weight 15.8 ppg(1.90 SG) to be used. The casing is to be cemented back to 150 m inside the 20" casing using 20 % excess on open hole volumes. If caliper is available, use 10 % excess over and above the estimated caliper volume. Cement will be displaced to a float collar c. 13 m above the shoe.

Data: Casing 13-3/8"/72 lb/ft/N80/BTC  
 20" shoe at 800 m BDF  
 26" hole at 810 m BDF  
 13-3/8" shoe at 1520 m BDF  
 17-1/2" hole at 1530 m BDF

13.2 ppg Lead Slurry Volumes

i) 20" x 13-3/8" annulus	= (800-650)x3.281x0.9377	=	461.5 cu.ft
ii) 26" x 13-3/8" annulus	= (810-800)x3.281x2.7113x1.2=		106.7 cu.ft
iii) 17½"x 13-3/8" annulus	=(1420-810)x3.281x0.6946x1.2=		<u>1668.2 cu.ft</u>
	Total slurry volume	=	2236.4 cu.ft

Cement required	= 2236.4/1.79	=	1249.4 sxs
		=	53.3 mt
Mixwater required	= 1249.4 x 9.47/42	=	281.7 bbls

Additives to be advised.

15.8 ppg Tail Slurry Volumes

i) 17½"x 13-3/8" annulus	=(1520-1420)x3.281x0.6946x1.2=		273.5 cu.ft.
ii) 17½" pocket	= 10 x 3.281 x 1.6703 x 1.2 =		65.7 cu.ft.
iii) 13-3/8" shoe track	= 13 x 3.281 x .8314	=	<u>35.5 cu.ft.</u>
	Total slurry volume	=	374.7 cu.ft

Cement required	= 374.7/1.15	=	325.8 sxs
		=	13.9 mt
Mixwater required	= 325.8 x 5.07/42	=	39.3 bbls

Additives to be advised.

9 5/8" Cementation

Norcem Class "G" cement at 15.4 ppg(1.85 SG) slurry weight will be used as the main slurry up to 1345 m BDF. 50 bbls (262 m) of 13.5 ppg(1.62 SG) scavenger slurry (Class "G") is to be pumped ahead of the main 15.4 ppg slurry. A 10% excess is to be used over and above estimated caliper volume over open hole intervals, and cement is to be displaced to a float collar c.24 m above the shoe.

Data: Casing 9-5/8"/43.5 lb/ft/N80/BTC  
 13-3/8" shoe at 1520m BDF  
 17-1/2" hole at 1530m BDF  
 9-5/8" shoe at 1725m BDF  
 12-1/4" hole at 1735m BDF

15.4 ppg Slurry Volume

i) 13-3/8"x9-5/8" annulus (1520-1345)3.281x.3262	=	187.3 cu.ft.
ii) 17-1/2"x9-5/8" annulus (1530-1520)3.281x1.1651x1.1	=	42.1 cu.ft.
iii) 12-1/4"x9-5/8" annulus (1725-1530)3.281x.3132x1.1	=	220.4 cu.ft.
iv) 12-1/4" pocket 10x3.281x0.8185x1.2	=	32.2 cu.ft.
v) 9-5/8" shoe track 24 x 3.281 x 0.4180	=	<u>32.1 cu.ft.</u>
Total slurry volume	=	514.1 cu.ft.

Cement required	= 514.1/1.24	=	414.6 sxs
		=	17.7 mt

Mixwater required	= 414.6 x 5.67/42	=	56.0 bbls
-------------------	-------------------	---	-----------

Additives to be advised.

13.5 ppg Scavenger Slurry Volumes

i) 13-3/8" x 9-5/8" annulus (1345-1083)3.281x.3262	=	280.4 cu.ft.
--	---	--------------

Cement required	= 280.4/1.71	=	164.0 sxs
		=	7.0 mt

Mixwater required	= 164.0 x 9.27/42	=	36.2 bbls
-------------------	-------------------	---	-----------

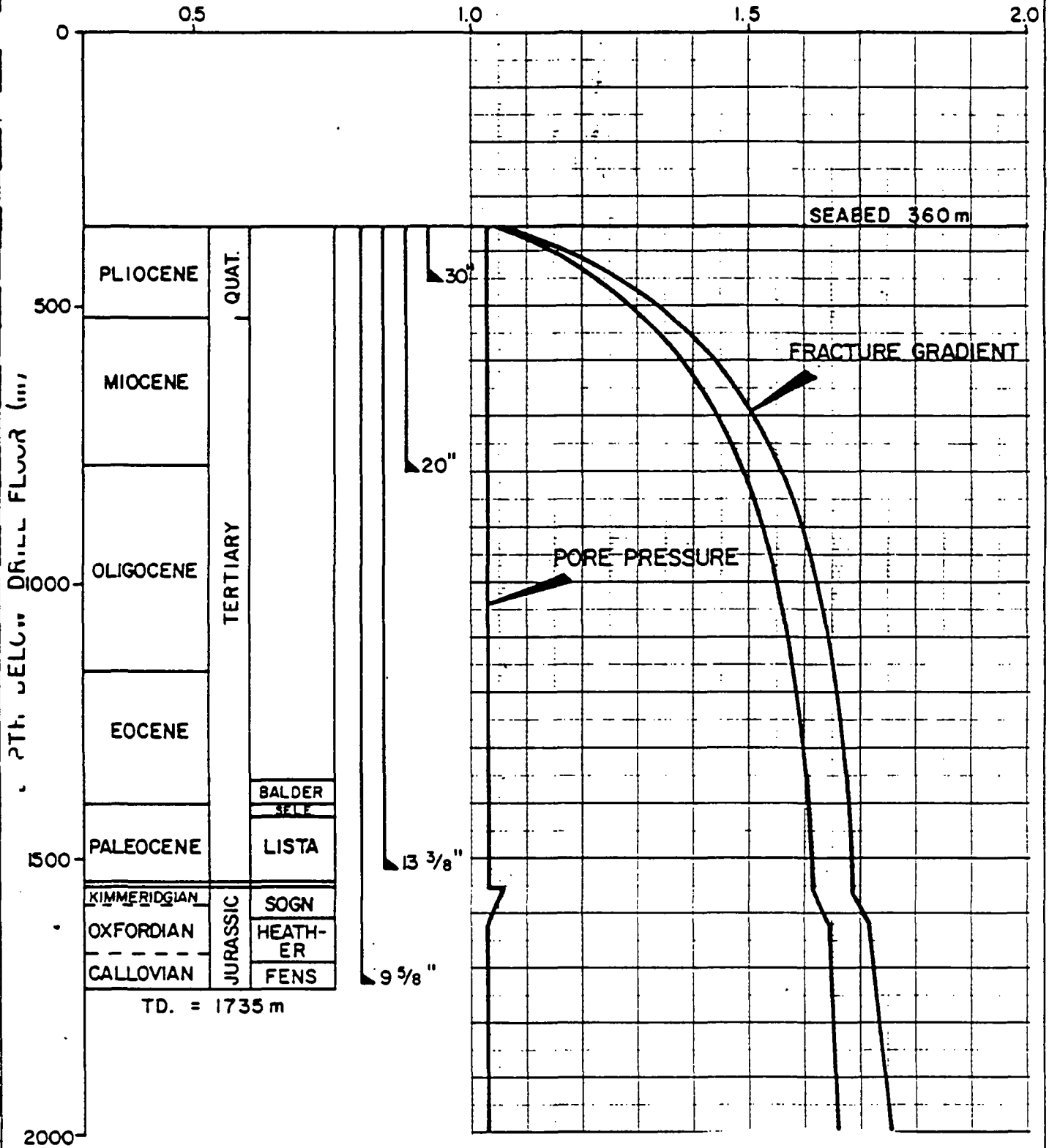
Additives to be advised.



# WELL 31/2 - M

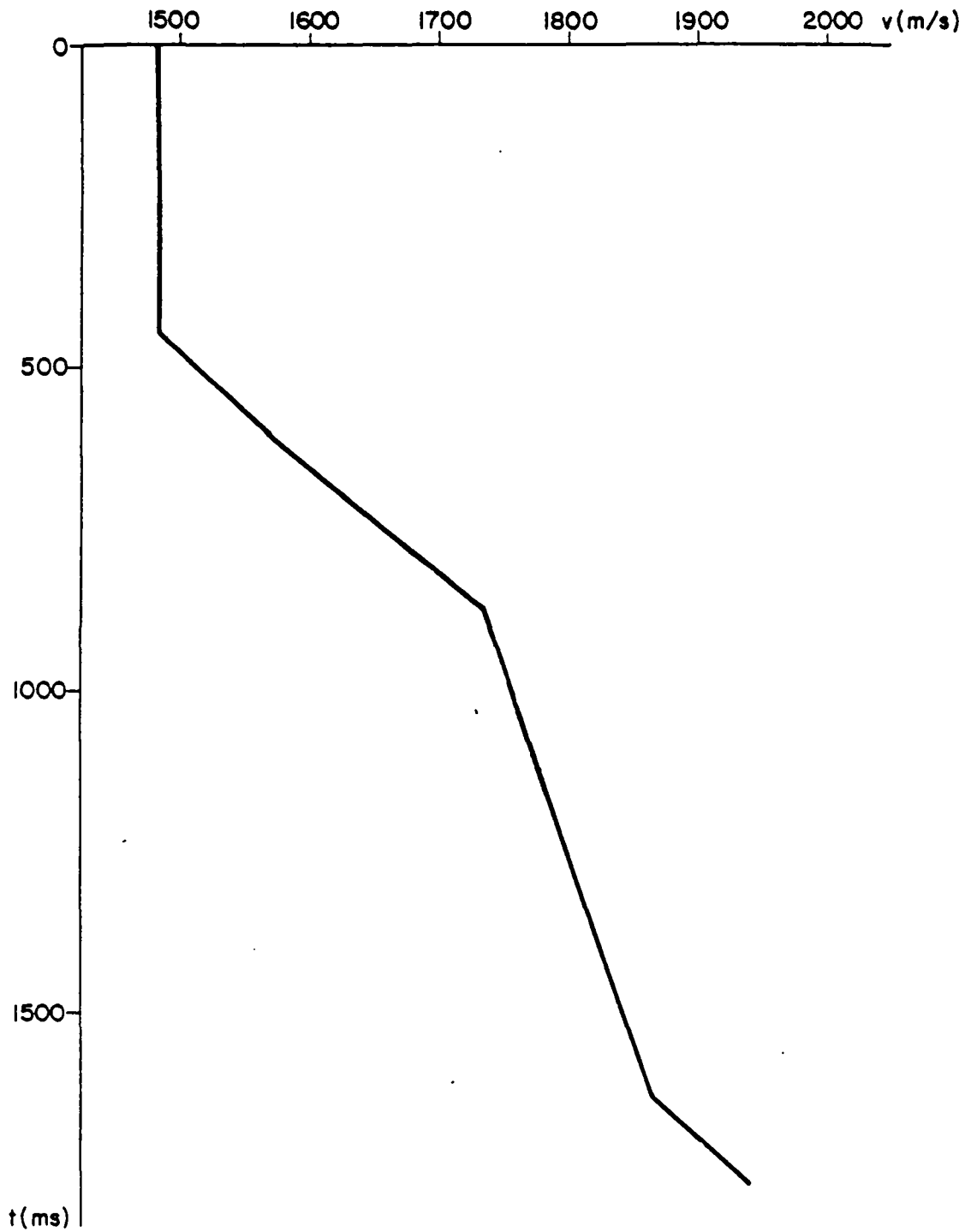
## ESTIMATED PORE PRESSURE AND FRACTURE GRADIENTS


MUD WEIGHT SG.



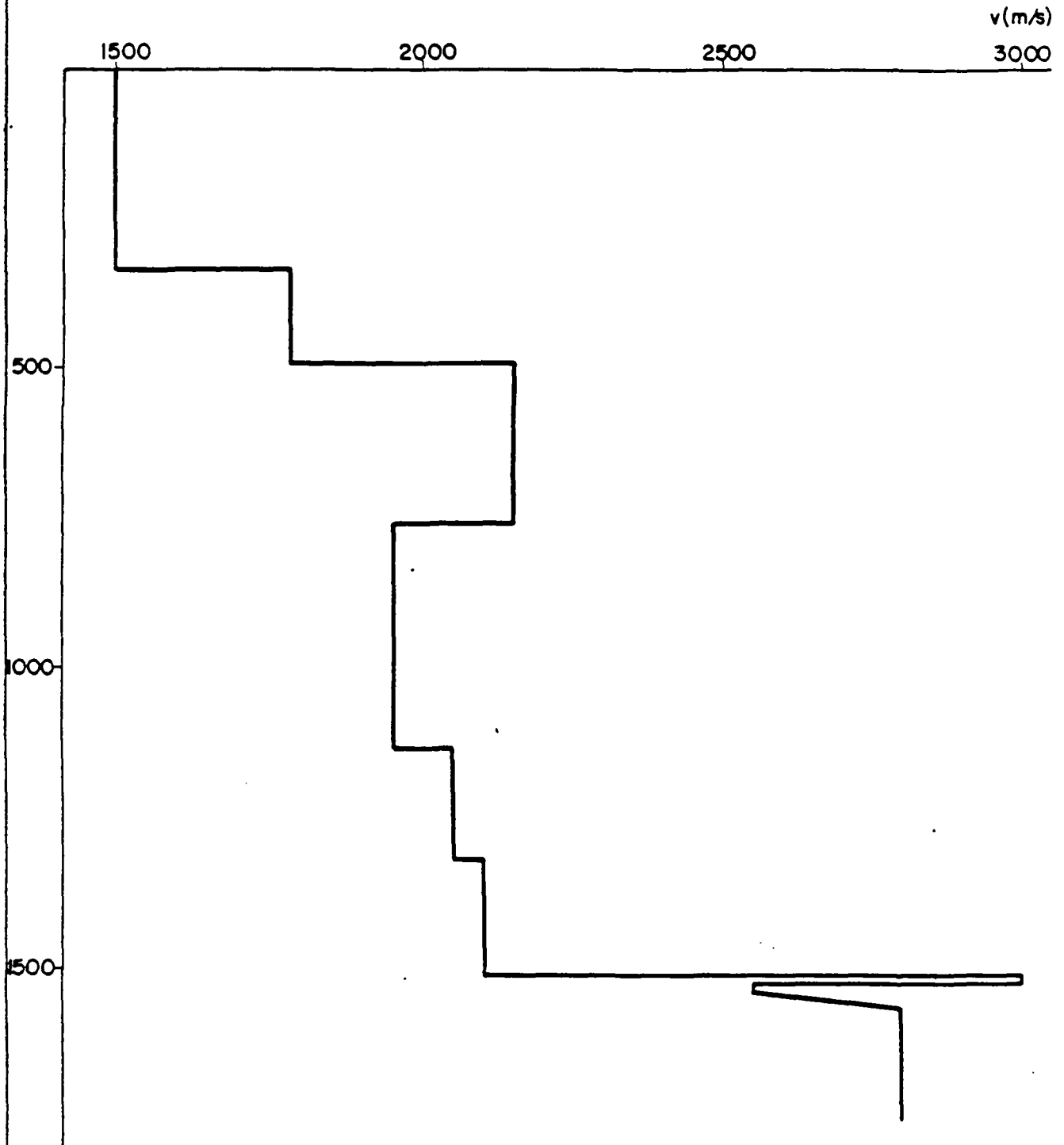
a-s Norske Shell		
EXPLORATION & PRODUCTION NORUS		
WELL 31/2 - M		
ESTIMATED PORE PRESSURE AND FRACTURE GRADIENTS SHOWING THE DEGREE OF UNCERTAINTY		
AUTHOR	ENCL	DATE
EPPP/11	3	DEC. '82
REPORT NO	DRAW NO G 1301/5	

# AVERAGE VELOCITY VS SEISMIC TIME



a.s Norske Shell		
EXPLORATION & PRODUCTION FORUS		
DRILLING PROGRAMME		
LOCATION 31/2-M		
AUTHOR EPPP/35	INC. 4	DATE DEC '82
REPORT NO		DRAW NO

# INTERVAL VELOCITY VS DEPTH



a-s Norske Shell  
EXPLORATION & PRODUCTION MANAGER

DRILLING PROGRAMME  
LOCATION 31/2-M

AUTHOR: EPPP/33  
REPORT NO: 5

DATE: DEC. 82