Denne rapport tilhører

STATOIL

nr. 2

L&U DOK. SENTER

L. NR. 20088370022

KODE Well 31/2-9

Returneres etter bruk

RESERVOIR FLUID STUDY

for

A/S Norske Shell Exploration & Production

Well: 31/2-9

North Sea, Norway.

CORE LABORATORIES UK LTD. Petroleum Reservoir Engineering ABERDEEN, SCOTLAND

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Petroleum Reservoir Engineering ABERDEEN, SCOTLAND

1st February 1983

A/S Norske Shell Exploration & Production Gamle Forusvei 43 P.O. Box 10 N-4033 Forus NORWAY

Subject: Reservoir Fluid Study

Well: 31/2-9
Field: Troll

North Sea, Norway.

Our File: RFLA 820292

Attention: Mr. J. C. Jolly.

Gentlemen.

On the 6th June 1982, samples of separator gas and liquid were collected from the subject well. These samples were submitted to our Aberdeen laboratory for use in a reservoir fluid study, the results of which are presented in the following report.

On arrival in the laboratory the hydrocarbon compositions of the gas samples were determined by gas chromatography, and the gas in cylinder number A4796 was found to be contaminated. The composition of the gas from cylinder number A3908 is presented on page two of this report. Stock tank liquid from the RFT provided and gas were recombined to produce a saturation pressure of 2280 psig at 154°F as requested, and the resulting fluid was used for the entire study.

The hydrocarbon composition of the fluid to heptanes plus was determined by low temperature fractional distillation. This composition in terms of both mol and weight percent may be found on page three of this report. The hydrocarbon composition to eicosanes plus will be reported shortly in a supplementary report.

A portion of the reservoir fluid was placed in a high pressure visual cell and thermally expanded to the reservoir temperature of 154°F. During a constant composition expansion at this temperature, a saturation pressure of 2280 psig was observed. The results of the pressure-volume relations may be found on page five, with the associated volumetric data for the undersaturated fluid presented on page four.

A large volume of reservoir fluid was then subjected to a differential vaporisation at 154°F, resulting in the liberation of a total of 291 standard cubic feet of gas per barrel of residual oil, with an associated relative volume of 1.146 barrels of saturated fluid per barrel of residual oil. At several pressure levels below the observed saturation pressure, oil density, gas gravity and gas compressibility factor were monitored. These data are tabulated on page six, and graphically represented on pages eleven and twelve.

The viscosity of the liquid phase was measured in a rolling ball viscosimeter at the reservoir temperature of 154°F. These measurements were made over a wide range of pressures, from above saturation pressure to atmospheric pressure, and showed a minimum viscosity of 1.704 centipoise at saturation pressure, and a maximum of 3.666 centipoise at atmospheric pressure. This data, together with the calculated gas viscosity is presented on page seven, and graphically represented on page thirteen.

Continued Over/.....

At conditions specified by A/S Norske Shell Exploration & Production, a series of flash separation tests were performed in the laboratory. The factors and data derived from these tests may be found on page eight.

On the first separator test at both primary and secondary stages, the gas evolved was collected and analysed for hydrocarbon composition to undecanes plus by gas chromatography. These compositions are presented on page nine of this report.

It was requested that we analyse the residual liquid from the 450 psig flash separation test to determine pour point, cloud point, wax content and melting point of the wax. These results may be found on page ten.

It has been a pleasure to be of service to A/S Norske Shell Exploration & Production. Should any questions arise concerning data presented in this report, or if we may be of assistance in any metter, please do not hesitate to contact us.

Very truly yours

Core Laboratories UK Limited Reservoir Fluid Analysis

LKS/TGB/stb 10cc/Addressee Les. K. Sebborn Manager - RFL Aberdeen

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		File_	ŘFL	A 82029	2	
Company A/S Norske Shell Expl. & Prod. I	Date Sampi	led <u>6th</u>	June 1	982		
Well 31/2-9	County	Nort	h Sea			
Field Troll S	State	Norv	ay			
FORMATION CHA	ARACTERIS	rics				
Formation Name	-					
Date First Well Completed	-				19	
Original Reservoir Pressure	_	F	SIG @_			М.
Original Produced Gas-Liquid Ratio	-				SCF/	
Production Rate	-			. <u> </u>	Bbls/	
Separator Pressure and Temperature	-	<u>-</u>	SIG			°F.
Liquid Gravity at 60°F.	-					API
Datum	A CTURED T COULT	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~			. Sub	sea
WELL CHAR	ACTERISTI	R.K.B.				
Total Depth		K•K•D•				М.
Producing Interval	-	1584-1590	5*			_M.
Tubing Size and Depth	=	3"VAM & 4				-м.
Open Flow Potential	-	J VA1 & 4	2 1110 6		MSCF/	
Last Reservoir Pressure	•		PSIG @		- 1.501 /	M.
Date		6th June			1982	
Reservoir Temperature	•	154	°F. 6	1576.8		M.
Status of Well	•		_ ` `			_
Pressure Gauge	•	····	· · · · · · · · · · · · · · · · · · ·			
SAMPLING	CONDITION	S				
Wellhead Tubing Pressure		223			F	SIG
Flowing Bottom Hole Pressure	•	_			F	SIG
Primary Separator Pressure		92			F	SIG
Primary Separator Temperature		71				°F.
Secondary Separator Pressure					F	SIG
Secondary Separator Temperature			·			°F.
Field Stock Tank Liquid Gravity					c @ 60	
Primary Separator Gas Production Rate		·		N	MSCF/	'Day
Pressure Base 14.73						
Temperature Base 60	°F.					
Compressibility Factor (Fpv) 1.009						
Gas Gravity (Laboratory) 0.640						
Gas Gravity Factor (F_0) 1.250					Dhla	/Da
Primary Sep Liquid Production Rate @ 71°					_Bbls/	_
	Ratio			ıd	SCF/ ols/M	
	r	Flopetrol		BI) T () (, II,	- DCL
Sampled by		TOPECTOI				

REMARKS: *Milled Out Section.

These analyses, opinions or interpretations are based on observations and material supplied by the client to whom, and for whose exclusive and confidential use, this report is made. The interpretations or opinions expressed represent the best judgement of Core Laboratories, Inc. (all errors and omissions excepted): but Core Laboratories, Inc. and its officers and employees, assume no responsibility and make no warranty or representations as to the productivity, proper operation, or profitableness of any oil, gas or other mineral well or sand in connection with which such report is used or relied upon.

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				Page	2	_of	13
				File	RFL	8202	292
Company	A/S Nors	ske Shell Expl. & Prod.	_ Formation		,		· · · · · · · · · · · · · · · · · · ·
Well	31/2-9		_ County	North	Sea		
Field_	Troll		_ State	Norway	, 		
		HYDROCARBON ANALYSIS OF S	EPARATOR GA	S SAMPLE*			
COMPONE	NT	MOL PER	CENT		C	GPM	
Hydroge	en Sulfide	e NIL	ı				
Carbon	Dioxide	1.22					
Nitroge		0.80					
Methane	<u>:</u>	88.06					
Ethane		7.40			_		
Propane		1.23				338	
iso-But		0.72				236	
n-Butar		0.13				041	
iso-Per		0.12 0.02				.044	
n-Penta		0.15				.061	
Hexanes Heptane		0.15				.068	
neprane	sa bras	100.00				795	

Calculated gas gravity (air = 1.000) = 0.640

Calculated gross heating value = 1103 BTU per cubic foot of dry gas at 14.73 psia and 60°F.

Collected at 92 psig and 71°F.

* Cylinder Number: A3908.

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			File	RFLA	82029	2	
Company	A/S Norske Shell Expl. & Prod.	Formation_	· · · · · · · · · · · · · · · · · · ·				
Well	31/2-9	County	North	Sea			
Field	Troll	State	Norway	Y			

HYDROCARBON ANALYSIS OF RESERVOIR FLUID SAMPLE

COMPONENT	MOL PERCENT	WEIGHT PERCENT	DENSITY	API	MOL WEIGHT
Hydrogen Sulfide	NIL	NIL			
Carbon Dioxide	0.48	0.13			
Nitrogen	0.79	0.14			
Methane	30.21	3.04			
Ethane	3.51	0.66			
Propane	0.79	0.22			
iso-Butane	0.91	0.33			
n-Butane	0.22	0.08			
iso-Pentane	0.38	0.17			
n-Pentane	0.11	0.05			
Hexanes	0.43	0.23			
Heptanes plus	62.17	94.95	0.8833	28.5	244
	100.00	100.00			

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2280 PSIG @ 154 °F.

Well

VOLUMETRIC DATA OF RESERVOIR FLUID SAMPLE

2. Specific volume at saturation pressure: ft 3 /lb 0.01979 @ 154 °F.

3. Thermal expansion of saturated oil @ 5000 PSIG = 0.01979 @ 0.01979 @ 0.01979 @ 0.01979 PSIG = 0.01979 @ 0.01979 PSIG = 0.01979 PSI

4. Compressibility of saturated oil @ reservoir temperature: Vol/Vol/PSI:

Saturation pressure (bubble-point pressure)

From 5000 PSIG to 4000 PSIG = $5.66 \times 10-6$ From 4000 PSIG to 3000 PSIG = $6.23 \times 10-6$ From 3000 PSIG to 2280 PSIG = $6.81 \times 10-6$

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PRESSURE-VOLUME RELATIONS AT 154°F.

Pressure	Relative	Y
PSIG	Volume(1)	Function(2)
5000	0.9833	
4000	0.9889	
3000	0.9951	
2700	0.9971	
2600	0.9978	
2500	0.9985	•
2400	0.9992	
2300	0.9999	
2280 Saturation	1.0000	
Pressure		
2256	1.0020	5.322
2239	1.0034	5.303
2222	1.0049	5.295
2206	1.0063	5.280
2160	1.0106	5.228
2061	1.0206	5.132
1985	1.0292	5.059
1829	1.0499	4.903
1651	1.0799	4.726
1463	1.1217	4.541
1263	1.1832	4.343
1118	1.2442	4.200
- 970	1.3278	4.057
860	1.4115	3.944
735	1.5387	3.824
620	1.7062	3.702
52 0	1.9125	3.605
395	2.3211	3.480
285	2.9692	3.377
185	4.1936	3.280

(2) Y Function = (Psat-P) (Pabs) (V/Vsat-1)

⁽¹⁾ Relative Volume: V/Vsat is barrels at indicated pressure per barrel at saturation pressure.

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DIFFERENTIAL VAPORISATION AT 154°F.

al													
Incremental Gas	Gravity		0.767	0.717	9.676	0.644	0.627	0.630	0.653	0.671	669*0	0.940	
Gas Formation Volume	Factor(4)		0.00672	0.00813	06600.0	0.01261	0.01718	0.02636	0.05323	0.07887	0.14928		
Deviation Factor	2		0.836	0.848	0.862	0.881	0.904	0.932	0.964	0.975	0.987		
Oil Density	gm/cc	0.8097	0.8112	0.8159	0.8200	0.8241	0.8287	0.8338	0.8396	0.8418	0.8443	0.8489	
Relative Total	Volume(3)	1.146	1,159	1.206	1.271	1,380	1,575	2.003	3,329	4.640	8.257		
Relative Oil	Volume(2)	1.146	1,141	1.128	1,116	1,104	1,091	1.078	1.063	1.058	1.052	1.041	000
Solution Gas/Oil	Ratio(1)	291	276	237	203	168	133	94	52	36	20	0	
Pressure	PSIG	2280	2150	1800	1500	1200	006	009	300	200	100		

• }

Gravity of Residual Oil = 28.5° API at 60°F.

Cubic feet of gas at 14.73 psia and 60°F. per barrel of residual oil at 60°F. £36£

Barrels of oil at indicated pressure and temperature per barrel of residual oil at 60°F. Barrels of oil plus liberated gas at indicated pressure and temperature per barrel of residual oil at 60°F.

Cubic feet of gas at indicated pressure and temperature per cubic foot at 14.73 psia and 60°F.

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VISCOSITY DATA AT 154°F.

Pressure	Oil Viscosity	Calculated Gas Viscosity	Oil/Gas Viscosity
	-		
PSIG	<u>Centipoise</u>	Centipoise	Ratio
5000	2.182		
4000	2.008		
3500	1.920		
3000	1.831		
2500	1.745		
	ration 1.704		
	sure		
	1.713	0.0178	96.4
2150		•	
1800	1.804	0.0161	111.8
150 0	1.944	0.0151	128.6
1200	2.143	0.0144	149.2
900	2.407	0.0138	174.4
600	2.747	0.0132	207.8
300	3.183	0.0127	250.7
200	3.343	0.0125	267.7
100	3.507	0.0122	286.3
		0.0122	200.5
0	3.666		

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Well___31/2-9

SEPARATOR TESTS OF RESERVOIR FLUID SAMPLE

Separator Pressure PSI Gauge	Separator Temperature °F.		Gas/Oil Ratio (2)	Stock Tank Gravity °API @ 60°F.	Formation Volume Factor(3)	Separator Substitution Substitution Substitution Substitution (4) Figure 1. Separator (4) Figure 1. Se	ravity of
450 to	58	190	197			1.037	0.598*
0	58	89	89	28.8	1.142	0.999	0.719*
250 to	58	230	235			1.021	0.620
0	58	51	51	28.8	1.142	0.999	0.749
150 to	58	253	256			1.012	0.634
0	58	31	31	28.8	1.142	0.999	0.764
50 to	58	276	277			1.004	0.661
0	58	11	11	28.8	1.142	0.999	0.756

- * Gas collected and analysed for extended hydrocarbon composition.
- (1) Gas/Oil Ratio in cubic feet of gas at 14.73 psia and 60°F. per barrel of oil at indicated pressure and temperature.
- (2) Gas/Oil Ratio in cubic feet of gas at 14.73 psia and 60°F. per barrel of stock tank oil at 60°F.
- (3) Formation Volume Factor is barrels of saturated oil at 2280 psig and 154°F. per barrel of stock tank oil at 60°F.
- (4) Separator Volume Factor is barrels of oil at indicated pressure and temperature per barrel of stock tank oil at 60°F.

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HYDROCARBON ANALYSES OF SEPARATOR GAS SAMPLES

Separator Conditions:	450 PSIG @ 58°F.	0 PSIG @ 58°F.
Component	Mol Percent GPM	Mol Percent GPM
Hydrogen Sulfide	NIL	NIL
Carbon Dioxide	0.81	1.89
Nitrogen	3.30	0.68
Methane	92.29	77.83
Ethane	3.04	14.20
Propane	0.27 0.074	2.43 0.669
iso-Butane	0.13 0.043	1.65 0.540
n-Butane	0.04 0.013	0.34 0.107
iso-Pentane	0.03 0.011	0.34 0.125
n-Pentane	0.01 0.004	0.17 0.062
Hexanes	0.03 0.012	0.14 0.057
Heptanes	0.03)	0.23)
Octanes	0.01) 0.023	0.07) 0.150
Nonanes plus	0.01)	0.03)
-	$\overline{100.00} \qquad \overline{0.180}$	$\overline{100.00} \qquad \overline{1.710}$

Calculated gas gravity(Air=1.000): 0.598 0.719

Calculated gross heating value (BTU per cubic foot of dry gas

at 14.73 psia and 60°F.): 1007 1212

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ANALYSIS OF RESIDUAL LIQUID FROM FLASH SEPARATION TEST* Pour Point L -50°C Cloud Point -20°C Wax Content 2.77 Drop melting point of wax (IP 133) 50.8°C

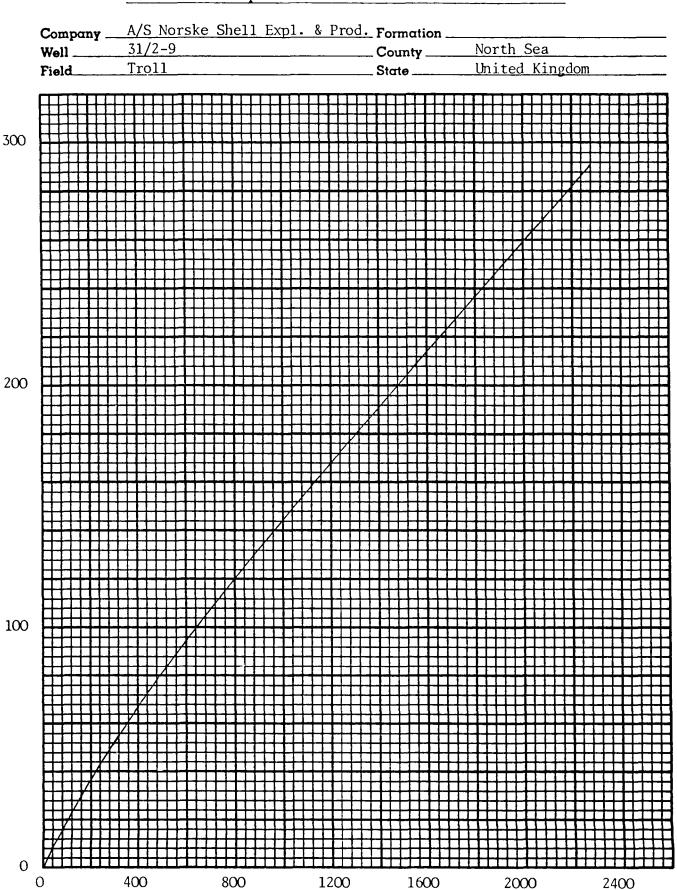
L = Less Than

^{* 450} psig @ 58°F to 0 psig @ 58°F.

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Differential Vaporisation of Reservoir Fluid at 154°F.

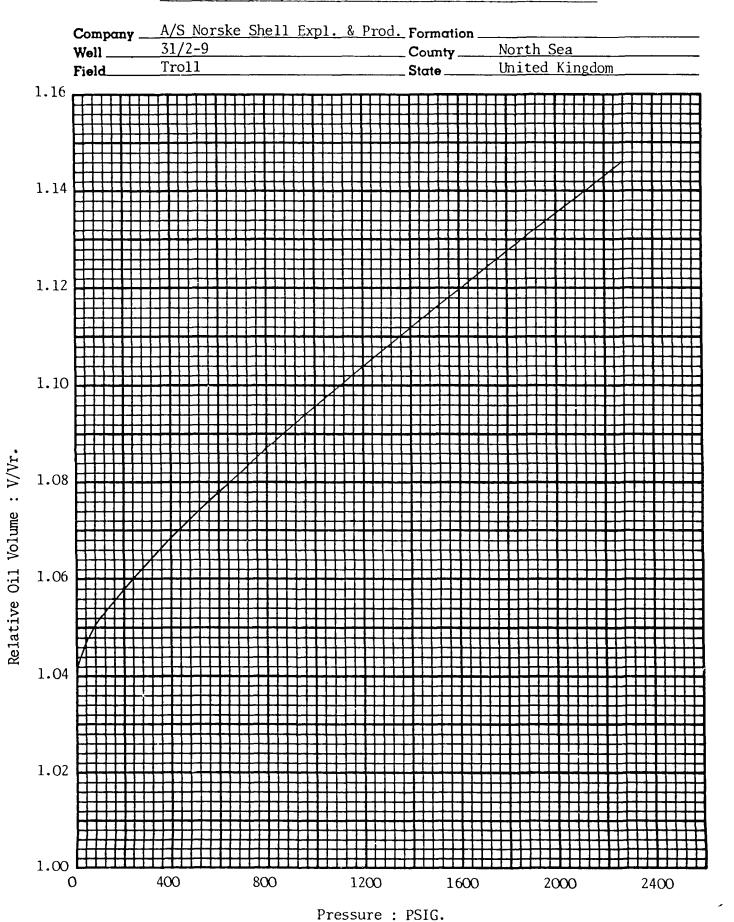


Pressure: PSIG.

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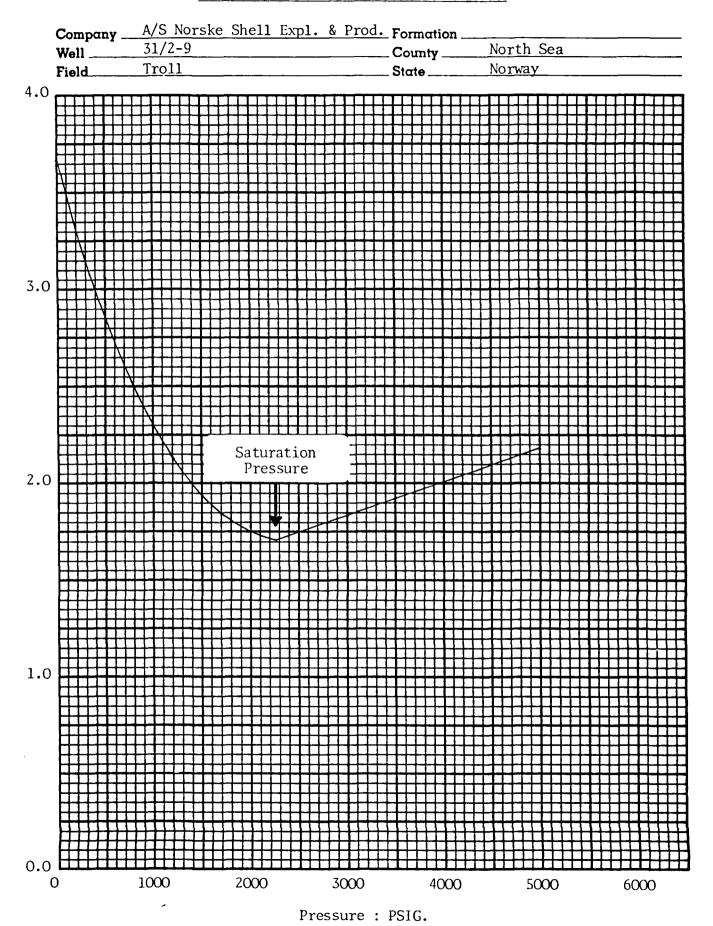
<u>Differential Vaporisation of Reservoir Fluid at</u> 154°F.



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Viscosity of Reservoir Fluid at 154°F.



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A/S NORSKE SHELL EXPLORATION & PRODUCTION Well: 31/2-9

RFLA 820292

Core Laboratories UK Limited Reservoir Fluid Analysis

Les. K. Sebborn

Manager - RFL Aberdeen

31/2-9 RFT SAMPLES

The first two paragraphs of Corelab's covering letter to this report require clarification. The following account explains the procedures employed in the recovery and analysis of RFT samples from well 31/2-9.

An unsegregated and a segregated RFT sample were taken in the 31/2-9 oil zone. The unsegregated sample was drained into steel cans on the rig and the RFT chamber containing the segregated sample was sent to shore for transfer. During the transfer it became evident that the chamber contained only a small amount of oil (later found to be 35 cc). It was evident that this was insufficient for a complete PVT analysis. Therefore Corelab were asked to recombine crude oil from the unsegregated sample with associated gas from the 31/2-7 oil zone test (bottle No. A3908). A complete analysis was performed on this sample and is reported in this document (RFLA 820292).

The 35 cc sample (bottle 9024-48) sufficed only for the pressure volume relationship and compositional analysis. This is reported in the Partial Fluid Study (RFLA 830015). The data obtained are very similar to those from the recombined crude sample and thus tend to confirm the validity of the full PVT analysis as reported in this report.

B. Reinholdtsen Reservoir Engineer A/S Norske Shell