## WELL SUMMARY

A/S NORSKE SHELL
WELL NO.: $31 / 2-10$

## WELL SUMMARY

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WELL NO.: 31/2-10

## GENERAL SUMMARY

OPERATOR A/S NORSKE SHELL
WELL NO. ..... 31/2-10
OPERATOR'S REPRESENTATIVES
Mr. Frans van Kampen, Mr. Chris Weston
CONTRACTOR Dolphin Services
RIG Borgny Dolphin
CONTRACTOR'S REPRESENTATIVESMr. John Butchart, Mr. Harald Frigstad
ANCHOR ENGINEERS

Mr. C. Blanchard, Mr. C. Atkinson

WATER DEPTH ..... 332 m
SEABED to RKB ..... 357 ..... m
36" HOLE DRILLED TO ..... 472 ..... m
30" CASING SET AT ..... 454 m
26" HOLE DRILLED TO ..... 810 m
20" CASING SET AT ..... 793 m
$171 / 2$ " HOLE DRILLED TO ..... 1530 ..... m
13 $3 /{ }^{\prime \prime}$ CASING SET AT ..... 1514 m
121/4" HOLE DRILLED TO ..... 1575 ..... m
95/8" CASING SET AT
81/2" HOLE DRILLED TO ..... 1833 ..... m
7" LINER SET AT
6" HOLE DRILLED TO

## DATE

01.10 .82

Ran anchors. Checked inventory.
Prepared to mix spud mud.

## DATEO 2.10.82

Mixed 1950 bbls of spud mud for viscous pills while drilling 36 " hole. Drilled from 357 to 414 m . Spotted 25 bbls hivis mud on connections. During first survey 50 bbls of mud were pumped around, and also a 200 bbl pill of hivis mud.

After drilling to casing point $472 \mathrm{~m}, 50 \mathrm{bbls}$ of mud were spotted and chasedd with seawater. Then 250 bbls of hivis mud were spotted on wiper trip.

No fill after running back in hole. Again 50 bbls were pumped around and 900 bbls were displaced to the hole.

DATE
03.10 .82

Mixed 200 barrels of cement water with 4750 kg sacks of $\mathrm{CaCl}_{2}$. Mixed 1500 bbls of spud mud for $26^{\prime \prime}$ hole.

Ran $30^{\prime \prime}$ casing and cemented same. Displaced cement with seawater and circulated well head clean. RIH and tagged cement at 444 m . Drilled cement from 444 m to 470 m .

Drilled $26^{\prime \prime}$ hole from 472 m to 474 m .

DATE
04.10 .82

Drilled $143 / 4^{\prime \prime}$ hole from 474 m to 475.5 m . Pumped 2 x 50 bbls pills and chased with seawater. POOH and ran marine riser. Made up new BHA. RIH and displaced hole with gel mud. Drilled $143 / 4^{\prime \prime}$ hole from 475.5 m to 540 m . Ran wiper trip and survey. Maximum overpull 20,000 lbs. Continued drilling to 704 m . Dropped survey.

DATEO5.10.82
POOH to $30^{\prime \prime}$ shoe and recovered survey. RIH and drilled to 810 m . Ran wiper trip and survey. Circulated hole clean and spotted 325 bbls hivis of 1.35 SG mud. POOH. Ran logs. Displaced to seawater at 445 m . Opened dump valve. RIH to 650 m and displaced to seawater. RIH to 810 m and displaced to seawater.

Checked for flow. Spotted 350 bbls of hivis mud in open hole. POOH . Mixed 600 bbls of 1.35 SG gel mud.

DATE
06.10 .82

Pulled riser. RIH to 455 m . Reamed hole from 455 m to 787 m ( $26^{\prime \prime}$ hole). Pumped 25 bbls viscous mud on each connection. Mixed 900 bbls total of 1.35 SG mud.

## DATE

07.10 .82

26" hole was drilled to 810 m and cleaned twice with 50 bbls slugs of hivis mud. The hole was then filled with 900 bbls of 1.35 SG gel mud after a wiper trip.

20" casing was then run and cemented.

DATE 08.10 .82
Jetted and cleaned well head to run BOP's. Mixed 500 bbls of new KCl mud, 1.26 SG.

DATE
09.10 .82

Ran BOP's and riser. Tested BOP's. Made up new BHA.

# ANCHOR DRILLING FLUIDS AS 

OSLO - STAVANGER

OPERATOR<br>A/S NORSKE SHELL

ENGINEERS C. BLANCHARD
${ }^{\text {DATE }} 10.10 .82$
RIH to top of cement at 780 m . Drilled to 815 m . Pulled into $20 "$ shoe for leak off test. Leak off equivalent to 1.51 SG. Circulated hole clean. Drilled $17 \frac{1}{2} "$ hole to 1253 m. Ran survey and wiper trip. Tight hole at 1047 m . 130,000 lbs overpull.

DATE 1. 10.82
POOH to $20^{\prime \prime}$ shoe. Worked tight spot from 1047 m to 906 m . RIH and worked tight spots. Washed to bottom 1253 m with 3 m fill. Drilled to 1348 m . Circulated hole clean. Ran survey.

POOH to shoe. 60,000 lbs overpull. Drilled to 1434 m . Dropped survey and pulled out to the shoe. Tight hole from 1332 m to 1358 m . RIH to 1429 m with 5 m of fill. Drilled from 1434 m to 1530 m .
${ }^{\text {DATE }} 12.10 .82$
Circulated and cleaned hole. Ran survey. Tight hole on wiper trip from 1418 m to 1304 m . RIH to 1380 m . Worked tight spots. RIH to 1530 m with 2 m fill.

Circulated and cleaned hole. POOH to shoe. Maximum overpull 40,000 lbs. RIH to 1519 m . Washed and reamed to 1530 m . Circulated hole clean. POOH. No drag. Ran logs.

## DATE

13.10 .82

RIH and tagged bottom at 1530 m . Circulated and cleaned hole. POOH. Ran 13 3/8" casing. Prior to cement casing 300 bbls of 1. 20 SG mud were pumped. Bumped plug at 4660 strokes. Lost 85 bbls of mud on displacement of cement. Began to water back mud for next section of hole. Changed all shaker screens.

DATE 4.10 .82
Changed over mud system to 1.18 SG . Tagged cement at 1500 m . Drilled to 1535 m . Ran leaks off test.

Equivalent mud weight of 1.59 SG. Pipe stuck at 1490 m . Circulted and worked free. Drilled to 1575 m . Circulated bottoms up. POOH .

DATE
15.10 .82

Made up 30 ft core barrel. RIH. Cut core from 1575 m to 1585 m . POOH. Recovered core no. 1 ( 62 \%). Made up 60 ft barrel.

RIH. Washed and reamed to bottom. Cut core from 1585 m to 1588 m .
Maintained system properties as per specification with maximum mud weight at 1.18 SG .

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OPERATOR
    A/S NORSKE SHELL
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ENGINEERS C. ATKINSON / C. BLANCHARD
${ }^{\text {DATE }} 16.10 .82$
Cut core from 1588 m to 1599 m (very low ROP $\frac{1}{2}-1 \mathrm{~m} / \mathrm{hr}$ ). POOH.
Recovered core no. 2 ( $52 \%$ ). RIH. 1 m fill. Washed and reamed
to T.D. Cut core from 1599 m to 1613 m .
Maintained rheology with Drispac Regular.
DATE17.10.82

Cut core from 1613 m to 1617.5 m . POOH. Recovered cores no. 3 ( 97 \%). Changed BHA. RIH. No fill. Cut core from 1617.5 m to $1673 \mathrm{~m} . \mathrm{POOH}$. Recovered core no. 4 (91 \%).

DATE 18.10 .82
Started RIH. Repaired compensator. Continued RIH. Washed and reamed to T.D. ( 1 m fill). Cut core from 1637 m to 1655.5 m POOH. Recovered core no. 5 ( $99 \%$ ). RIH. Hung off inside casing.

Waited on weather.

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DATE 19.10.82
Waited on weather．Retrieved hang off tool．RIH．Washed and reamed to T．D． 8 m fill．
Cut core from 1655.5 m to 1663.5 m ．
DATE20．10．82
Cut core from 1663.5 m to 1674 m ．POOH．Recovered core no． 6 （100 \％）．RIH．Washed and reamed to bottom．
Cut core from 1674 m to 1686 m ．
DATE
21.10 .82
Cut core from 1686 m to 1622.5 m ．POOH．Recovered core no． 7
（67 \％）．RIH．Washed and reamed to T．D．
Cut core from 1692.5 m to 1704.5 m ． POOH due to high angle on riser（more than 50）．
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WELL NAME 31/2-10

OPERATOR<br>A/S NORSKE SHELL

## ENGINEERS C. ATKINSON/ C. BLAANCHARD

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DATE
22.10.82
    Recovered core no. 8 (99 %). Waited on weather. Rig off location.
    Displaced riser to seawater (dumped }\pm200\textrm{bbls}\mathrm{ mud. Surface
    pits full). Moved rig back over loca\overline{tion. Displaced riser to}
    mud. RIH. Cut core from 1704 m to 1706.5 m.
    Mixed new volume in pit no. 2 at l.l8 SG (60 bbls water to give
    265 bbls total).
    Reserve pit no. 3 at 1.24 SG.
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${ }^{\text {DATE }} 23.10 .82$

Cut core from 1706.5 m to 1723 m . POOH. Recovered core no. 9 (100 \%). RIH. Cut core from 1723 m to 1741.5 m . POOH.

## DATE

24.10 .82

Recovered core no. 10 (100 \%). Laid down core barrel. Made up rock bit and BHA. RIH. Drilled $8 \frac{1}{2}$ " hole from 1741.5 m to 1805 m . Circulated $1 / 4$ hour. Surveyed ( $1^{\circ}$ ). Wiper trip to shoe. RIH. Drilled from 1805 m to 1833 m . Circulated to clean hole.

POOH . No drag. Rigged up and ran Schlumberger logs.
Ran 2nd mud pump down choke line to give extra cleaning capacity in riser.

ENGINEERS C. ATKINSON
${ }^{\text {DATE }} 25.10 .82$
Ran logs.
Cleaned out gumbo box, header box and shaker ditch.
Changed shaker screens to $\frac{S 20}{S 40} \times \frac{B 60}{B 100} \times \frac{B 60}{S 50}$.
Serviced Thule unit. (Ordered spare set of hydraulic hoses).
Carried out chemical inventory.

DATE26.10.82
Continued logging.
Rigged down and waited on weather.
Started to make up $27 / 8^{\prime \prime}$ tubing.

## DATE 27.10 .82

RIH and set cement plugs. No. 1 at 1790 m to $1590 \mathrm{~m} . \mathrm{POOH}$. Reversed circulation at 1570 m . Dumped water. Plug no. 2 set at 1570 m to 1420 m . POOH. Reversed circulation at 1370 m . No contamination. POOH. Laid down drill pipe. Made up $121 / 4^{\prime \prime}$ bit and RIH. Tagged cement. Pressure test plug to 1500 psi . POOH. Laid down drill pipe.

Picked up casing cutters. RIH to cut $133 / 8^{\prime \prime}$ casing at 757 m .

DATE
28.10 .82

Finished pulling $133 / 8^{\prime \prime}$ casing. RIH with $27 / 8^{\prime \prime}$ tubing on drill pipe. Pumped 50 m hivis pill at 860 m . POOH to 810 m

Set cement plug no. 3. POOH to 630 m . Reversed circulation. No contamination.

DATE

DATE

## SUMMARY OF EVENTS

OPERATOR:
A/S NORSKE SHELL

WELL NO.
31/2-10
36"
HOLE/ $30^{\prime \prime}$

The $36^{\prime \prime}$ hole was drilled with seawater and viscous prehydrated Bentonite slugs. While spudding in, approximately 300 bbls of viscous mud was used to begin the well. 25 bbls hivis pills were pumped on connections.

During surveys, 50 bbls of hivis mud was pumped and circulated with seawater, and then 200 bbls hivis mud was pumped after drilling to T.D. 472 m . Again 50 bbls of hivis mud were spotted and circulated with seawater and then hole was displaced with 250 bbls hivis mud during the wiper trip with no fill. Before setting casing another 50 bbls of hivis mud were spotted and circulated, and the hole was displaced with 900 bbls of viscous mud. 200 bbls of $\mathrm{CaCl}_{2}$ water was mixed for the cement job and $30^{\prime \prime}$ casing was set at 454 m .

## SUMMARY OF EVENTS

OPERATOR: A/S NORSKE SHELL

WELL NO.
31/2-10
14 3/4" PILOT HOLE
26" HOLE/ $\qquad$ CASING INTERVAL

This section was drilled with pre-hydrated Bentonite/ seawater mud, using slugs of mud as necessary to clean the hole. 1500 bbls were initially mixed up for drilling this seciton and cement was tagged at 444 m with $26^{\prime \prime}$ hole being drilled to 474 m .
$143 / 4 "$ hole was then drilled from 474 m to 475 m and 50 bbls of hivis mud was spotted and circulated with seawater after which the marine riser and BHA were made up. The hole was then displaced to gel mud.
$143 / 4$ " hole was drilled to 590 m and survey with 20,000 lbs overpull when running to shoe. Drilling was then continued to 704 m and a survey was run. 310 bbls of 1.35 SG of kill mud was also mixed while drilling. After running in hole this section was drilled to 810 m and survey and wiper trip were done with no fill. 325 bbls of 1.35 SG mud was then spotted in the hole and logs were run. The hole was then displaced to seawater in stages at 445 m .650 m and at 810 m .

The hole was then checked for flow and 350 bbls of hivis mud was spotted in the hole. The riser was then pulled and the hole was reamed from 455 m to 810 m with $26^{\prime \prime}$ bit. 25 bbls viscous slugs were pumped on each connection while reaming.

The hole was then cleaned twice with 50 bbls of hivis slugs and circulated with seawater. The hole then was displaced with 900 bbls 1.35 SG mud after a wiper trip and $20^{\prime \prime}$ casing was run and cemented.

## SUMMARY OF EVENTS

OPERATOR:<br>A/S NORSKE SHELL

31/2-10

## WELL NO.

17夝" $\qquad$
HOLE/ _ CASING INTERVAL

The $17 \frac{1}{2}$ " hole was drilled with a KCl/Polymer mud. While running BOP's 1500 bbls of 1.26 SG mud was built and 650 bbls of KCl 90 lbs/bbl brine was received prior to mixing.

Cement was tagged at 780 m in the $20^{\prime \prime}$ casing and new hole was drilled to 815 m and the leak off test done ( 290 psi equivalent to 1.51 SG$)$. Drilling continued to 1005 m and a wiper trip and survey was run with $20-30,000 \mathrm{lbs}$ of drag while pulling to the shoe. The next survey was run at 1253 m and during the wiper trip tight hole was encountered at 1047 m with 130,000 lbs overpull. When running back in hole the tight spot from 946 m to 1047 m was reamed and 3 m of fill were encountered while starting to drill at 1253 m .

Drilling continued to 1348 m and during wiper trip 60,000 lbs of overpull occured. At 1434 m another wiper trip was done to the shoe and tight hole found from 1332 m to 1358 m . When running in the hole 5 m of fill were encountered and the hole was drilled to casing point from 1434 m to 1530 m . The hole was then circulated clean and a survey was run with tight hole from 1418 m to 1304 m . Tight spots were worked and the hole circulated clean again with 2 m of fill. Another wiper trip was run with 40,000 lbs overpull. While running in, the hole was washed and reamed from 1519 m to 1530 m and then circulated clean. When pulling out for logs there was no drag. After running logs the hole was circulated clean and $133 / 8^{\prime \prime}$ casing was run and cemented with 85 bbls lost to the formation during cement displacement.

## SUMMARY OF EVENTS

OPERATOR: A/S NORSKE SHELL
WELL NO. 31/2-10
12 1/4" - $8 \frac{1_{2}^{\prime \prime}}{}$ HOLE/ $\qquad$ CASING INTERVAL

Before drilling out cement at $13 \mathrm{3} / 8^{\prime \prime}$ shoe the mud system was diluted and treated for mud weight at 1.18 SG. A leak off test was taken at 1535 m , giving an equivalent formation break down of 1.59 SG.

The drilling of $121 / 4^{\prime \prime}$ hole then continued as far as 1575 m when it was decided to start coring with an $8 \frac{1}{2}{ }^{\prime \prime}$ core bit. A total of 10 cores were taken between depths 1575 m and 1741.5 m . This taking 9 days altogether due greatly to a slower than normal ROP in this section.

The mud system was basically a seawater/Drispac system with little treatment required, only occasional additions for rheology and fluid loss control (specifications were YP 15 - 20 and fluid loss less then 5 cc$)$. The KCl/Polymer system used in $17 \frac{1}{2}$ " section was allowed to naturally deplete in the 12 1/4" section since no reactive clays were encountered.

After coring it was decided to just continue drilling ahead with an $8 \frac{1}{2}$ " bit to T.D. Rather than open the hole to $121 / 4^{\prime \prime}$ and drill a $12 \mathrm{l} / 4^{\prime \prime}$ hole, since the cores had resulted in the probable decision not to test the well.

A T.D. of 1833 m was reached and a logging programme commenced.
Cement plugs were then set prior to abandoning location.

## RECOMMENDATIONS

## CONCLUSION

Although this section was drilled rapidly there were no serious hole problems. It is, however, pertinent that some tight spots were in evidence and some fill was experienced after trips.

If sufficient data is not already available on the formation at the tight spots $1047 \mathrm{~m}, 1332 \mathrm{~m}, 1358 \mathrm{~m}$ and 1418 m it would be advisable to determine what this formation is and what can be done to aleviate the problem. It is also possible that a small increase in mud weight may assist in controlling this situation. The leak off test established a 290 psi equivalent to l.5l SG the actual mud weights used were 1.26 to 1.36 maximum. The mud weight could be increased to 1.36 SG - 1.46 SG over this hole section, and if the hydraulics and rheology are controlled the resulting increase in E.C.D. can be maintained below l.51 SG.

After trips samples of the fill should be analyzed by Shell on location and Anchor Drillings laboratory in Tananger. This would enable an accurate assesment to be made as to the reason for this fill. However, until this can be done it is recommended that sufficient time be allowed to enable a full circulation of the hole to be made before a trip, consideration should also be given to the slip velocity of the cuttings when carrying out this operation. Additional hole cleaning can be achieved by making a 40 bbl sweep of 'mud' with a yield point of $25 \mathrm{lbs} / 100 \mathrm{sq} . \mathrm{ft}$. This should be pumped slightly slower than normal circulation rate so at to give a flatter flow profile resulting in greater carrying capacity and lower E.C.D.

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OPERATOR A/S NORSKE SHELL
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WELL NO. 31/2-10
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## MATERIAL CONSUMPTION \& COST ANALYSIS

| $36^{\prime \prime}$ | HOLE DRILLED TO | 472 | Meters <br> FEXX | $30^{\prime \prime}$ | CASING SET AT 454 | Meters KXX |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ACTUA | MOUNT OF HOLE DR | LLED | 113 | Meters <br> Fegx | DAYS ON INTERVAL | 1 |
| DRILLIN | FLUID SYSTEM | SPUD MUD |  |  |  |  |


| MATERIAL | UNIT SIZE | PROG. | USED | VARIANCE $\pm$ | COST |
| :--- | :---: | :---: | :---: | :---: | :---: |
| BENTONITE | MT | 20 | 20 | - | $6.560,-$ |
| CAUSTIC SODA | 25 kg | 20 | 14 | -6 | $266,-$ |
| SODA ASH | 50 kg | 3 | 14 | +11 | $259,-$ |
| CaCl $_{2}$ | 50 kg |  | 0 | 58 | - |
|  |  |  |  |  | $1.334,-$ |
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| COST/DAY | US $\$ 8.419,-$ | TOTAL COST FOR INTERVAL | US $\$ 8.419,-$ |
| :--- | :--- | :--- | :--- |
| COST/MI. OXXK | US $\$ 74,50$ | PROG. COST FOR INTERVAL | US $\$ 7.025,-$ |
| ENGR. COST |  |  |  |

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OPERATOR A/S NORSE SHELL
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WELL NO. 31/2-10
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## MATERIAL CONSUMPTION \& COST ANALYSIS

## 14 3/4" Pilot

 dRILLING FLUID SYSTEM GEL/SEAWATER


COST/DAY

COST/Mt.xorxex

ENGR. COST

US $\$ 5.314,13$ TOTAL COST FOR INTERVAL US $\$ 21.256,50$
$\square$

PROG. COST FOR INTERVAL US\$ 17.970,COST VARIANCE FOR INTERVAL

## MATERIAL CONSUMPTION \& COST ANALYSIS

| $17 \frac{1}{2}$ | HOLE DRILLED TO | 1530 | Meters | $33 / 8{ }^{\prime}$ | CASING SET AT | 1514 | $\begin{aligned} & \text { Meters } \\ & \text { Keek } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | ACTUAL ARIOUNT OF HOLE DRILLED

DRILLING FLUID SYSTEM

| MATERIAL | UNIT SIZE | PROG. | USED | VARIANCE $\pm$ | COST |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BARITE | MT | 205 | 168 | - 137 | $22.512,-$ |
| DRISPAC REGULAR | 50 lbs | 90 | 82 | - 8 | 13.882,60 |
| CAUSTIC SODA | 25 kg | 115 | 61 | - 54 | 1.159,- |
| SODA ASH | 50 kg | 30 | 45 | + 15 | 832,50 |
| CMC LOVIS | 25 kg | 81 | 58 | - 23 | 3.422, - |
| LF-5 | 25 kg | 180 | 117 | - 63 | 5.616,- |
| ANCOPOL | 551 bs | 85 | 68 | - 17 | 10.064, - |
| KCl sacks | 50 kg | 954 | 73 | -881 | 1.306,70 |
| KCl brine | bbls | 0 | 1408 | +1408 | $30.835,20$ |
| DRILLING DETERGENT | 2001 lr. | 15 | 0 | - 15 | - |
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COST/DAY

COST/MI. OFix $\square$ US\$14.938.33 TOTAL COST FOR INTERVAL
PROG. COST FOR INTERVAL
US\$ 89.630, -
US\$ 92.412,60

OPERATOR A/S NORSKE SHELL

WELL NO. 31/2-10

## MATERIAL CONSUMPTION \& COST ANALYSIS



| MATERIAL | UNIT SIIE | PROG | USED | VARIANCE $\pm$ | COST |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BARITE | MT | 100 | 36 | - 64 | 4.824, - |
| BENTONITE | MT | 0 | 0 | 0 | - |
| BENTONITE | 50 kg | 220 | 0 | - 220 | - |
| CAUSTIC SODA | 25 kg | 70 | 36 | - 34 | 684,- |
| SODA ASH | 50 kg | 4 | 18 | + 14 | 333, |
| LF-5 | 25 kg | 50 | 74 | + 24 | 3.552,- |
| CMC LOVIS | 25 kg | 25 | 55 | + 30 | 3.245,- |
| DRISPAC REGULAR | 50 lbs | 60 | 51 | - 9 | 8.634,30 |
| LIGNO | 25 kg | 175 | 0 | - 175 | - |
| XC-POLYMER | 50 lbs | 15 | 0 | - 15 | - |
| DRILLING DETERGENT | 2001. | 10 | 0 | - 10 | - |
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| COST/DAY | US\$ 1.519,45 | TOTAL COST FOR INTERVAL | US\$ $21.272,30$ |
| :---: | :---: | :---: | :---: |
|  | US\$ 70.21 | PROG. COST FOR INTERVAL | US\$ 44.221,- |
| ENGR. COST |  | COST VARIANCE FOR INTERVAL | US\$-22.948,70 |

## TOTAL CONSUMPTION \& COST ANALYSIS

TOTAL DEPTH

TOTAL DAYS
27


COST/DAY

COST/Mt

ENGR. COST

US\$ 5.206.58 TOTAL COST FOR • WELL PROG. COST FOR • WELL COST VARIANCE FOR WELL

US\$ 140.577,80

US\$ $161.629,10$






